ITEM 1

Town of Kittery Planning Board Meeting May 10, 2018

459 U.S. Route One - Mixed-use development - Site and Subdivision Preliminary Plan Review

<u>Hold a public hearing, approve or deny application.</u> Owner, DSS Land Holdings, LLC, and applicant, Michael Brigham of Landmark Hill, LLC, requests consideration of a mixed-use development consisting of 26 elderly housing units , two buildings with retail/commercial units and 16 apartments and one additional commercial/clubhouse building. All are located at 459 U.S. Route 1 (Tax Map 60 Lot 24) in the Mixed Use (MU), Rural-Residential (R-RL) and Shoreland Overlay Zone. (OZ-SL) Agent is Ken Wood, Attar Engineering.

INCIDECT	INACKING	-	
REQ'D	ACTION	COMMENTS	STATUS
YES	Sketch Plan	Scheduled for September 14, 2017, approved on October 12, 2017	APPROVED
NO	Site Visit	Held April 3, 2018 at 11:00 am	HELD
YES	Preliminary Plan Review Completeness/Acceptance	February 8, 2018	APPROVED
YES	Public Hearing	Held on April 12, 2018	HELD
YES	Preliminary Plan Approval	Possible for May 10, 2018	PENDING
YES	Final Plan Review and Decision	TBD	TBD
Applicant: variances THE MA 16.4.4.13	Prior to the signing of the a (by the BOA) must be placed P AND LOT NUMBER IN 1 - Grading/Construction Final F	pproved Plan any Conditions of Approval related to the Findings of Fact along I on the Final Plan and, when applicable, recorded at the York County Registry /4" HIGH LETTERS AT LOWER RIGHT BORDER OF ALL PLAN SHEET lan Required Grading or construction of roads, grading of land or lots, or construct	with waivers and of Deeds. PLACE S. <u>As per Section</u> ction of buildings is
prohibited applicable	until the original copy of th	e approved final plan endorsed has been duly recorded in the York County register	stry of deeds when

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Background

This is a preliminary plan review for a proposed mixed-use development located at 459 State Route 1 in the Mixed Use (MU) Zone, previously approved as the Sowerby mixed use in 2008. Since then the six residential lots have been conveyed and developed with single-family homes. As part of this development, a sewer force main has been installed connecting the lots to public sewer in Route 1 via an easement that burdens this property. There are also wetlands on the property.

The applicant is proposing 26 elderly single-family housing units, two buildings with first-floor office/retail and 16 second-floor apartment residential uses and one building split between commercial use and a club house. Office and/or retail on first floors and residential uses on the upper floors of a mixed-use building, the proposed elderly housing as well as single retail uses of less than 50,000 square feet are all permitted in the Mixed Use (MU) Zone. The elderly housing is a Special Exception Use.

The Board approved the sketch plan on October 12, 2017 and reviewed the preliminary plan for completeness on January 11, 2018. The Board found the application complete on February 8, 2018. On March 22, 2018 the Board set a date for a site walk (an earlier site walk had to be postponed) and the public hearing. A site walk was held on April 3, 2018 and the public hearing was held on April 12th. The Board discussed the application further on April 12th and made a motion to allow the applicant 90 days to address the additional comments and the CMA peer review.

Staff comments on the revised preliminary plan and submission are below.

Staff Review

<u>February 8, 2018 meeting:</u> the Applicant included narrative describing how the elderly single-family housing special exception use meets the requirements of 16.3.2.13.G as requested by the Board. At this meeting the Board discussed moving two of the stormwater ponds out of the 100-foot setback and wanted to see the net residential calculations include travel ways and parking areas. The Board found the application complete at this meeting.

<u>March 22, 2018 meeting</u>: the Applicant's agent briefed the Board on the plan revisions the Board could expect to see on the plans submitted for this meeting. These revisions are primarily the result of the net residential acreage calculations including travel ways and parking areas being applied.

April 12, 2018 meeting: the Applicant's agent walked the Board through the plan revisions. The stormwater ponds near the wetlands of special significance have been removed from the wetland setbacks. The Board discussed a parking waiver request which would allow the Applicant to remove parking spaces from the wetland setback near the building labeled C1 on the plans. The Board pointed out several changes that needed to be made on the plans (incorrect labels, map and lot etc.). The Board moved to allow the Applicant 90 days to complete plan revisions and address CMA's comments.

<u>Special Considerations</u>: The applicant is requesting that the Board consider granting a 50-foot extension of the MU Zone which would allow the entire parcel to be considered under the MU Zone. The applicant addressed the 7 conditions found in 16.7.2.5 that the Board must consider in order to grant this request in the original submission letter. The Board also has the option of requesting additional information or a study from the applicant when considering this request.

Staff recommends that the Board request a no-cut buffer around the wetlands of special significance at the 100-foot wetland setback line. The revised plans have Note 14 that seems to describe this but the buffer should be shown on all applicable plan sheets and it should be made clear in Note 14 that no cutting of trees is permitted beyond the wetland setback line.

CMA Review: CMA's latest review is included in the packet.

Review Considerations

- 1. The proposed development consists of two primary types of buildings: two mixed-use buildings with first floor commercial space and parking and 16 dwelling unit apartments on the upper floors and the 26 single-family elderly housing units along a new street. Maintenance of the stormwater management systems must be assignable to an entity or an owner. It appears that two associations will be created: a condominium association and a development association.
- 2. The net residential calculations shown in General Note 6 on Sheet 1 now subtract the amount of travel way and parking proposed and the sewer easement per 16.7.8.2.
 - a. Plan Sheet 1.1's final net residential density statement still appears incorrect. Assuming the net residential area is correct after subtracting the wetlands, hydric soils, travel ways, sewer easement and parking, the Net Residential Density statement should read:

 $428,974.5 - ((26 \times 10,000) - (16 \times 10,000) = 420,000) = 8,947.5$ left as the 26 elderly single-family homes each require 10,000 sf of land area when parking is encompassed within the building as in this case where each unit has a double car garage (see Note 3 under 16.3.2.13.D). Each of the 16 apartments also require 10,000 sf of land area too <u>unless</u> the apartments have garages in which case it would be 7,500 sf. The submission letter seems to say they do.

3. From previous staff notes: the preliminary plan design should, as it continues to integrate the elderly housing within the mixed-use development, provide for opportunities for common space to congregate and enjoy some outdoor space adjacent to some staple facilities that may cater to the over 55 community as well as to the other residents on site.

In this preliminary plan submission, the applicant has provided a building with a first-floor club house, while the second floor will be commercial. There are trails shown in the open space and a passive recreation area which includes part of the sewer easement. See Plan Sheet 1.2.

a. One part of the trail is shown moving off the subject property to the north onto another parcel. Is this an existing trail?

The Applicant submitted a narrative for the February 11, 2018 meeting as requested by the Board to demonstrate how the proposed elderly single-family housing meets 16.3.2.13.G.

- 4. Wetlands on-site to the north and east are associated with an existing natural pond to the north which qualifies them per Article 16.9.3.1.B as being wetlands of special significance (WoSS). The site is also within the MS-4 area. Kittery's wetland regulations are stricter than the State's. The stormwater ponds associated with the WoSS have been moved outside the 100-foot buffer for the most part (see a. below). The remaining stormwater ponds are located at least 25 feet from the wetlands to the west which are not WoSS. Their locations have been reviewed by DEP although a permit may not have been issued yet. Staff has spoken with the DEP staff person who is doing the permitting for this project and is satisfied with the stormwater ponds' location.
 - a. Some grading of stormwater pond #40 and #10 will be within the 100-foot setback for the WoSS. Is the long "tail" of pond #40 only grading? Similarly pond #20 has a long narrow "tail". Update: the "tails" have been removed they represented grading.
 - b. A portion of the parking area for the commercial/clubhouse building labeled C1 is within the 100-foot setback for the WoSS. Can this parking area be redesigned to stay within the setbacks or could one of the other parking areas add one or two spaces so that this parking area could be downsized to stay within the WoSS setbacks? See Note 10 also. Update: parking has been removed from the WoSS setback.
- 5. As proposed, the elderly single-family units are 3 BR 2,800 sf. The apartments are 2 BR with a single 3 BR unit on the top floor of each building. There is 4,000 sf of commercial space in each of the two buildings labeled A1 and A2. The C1 building has 2,000 sf of commercial space on the second floor with a 2,000 sf clubhouse on the first floor.
- 6. The example rendering of the proposed mixed-use buildings seem to show residential-only buildings.
- 7. All buildings will be sprinkled.
- 8. From previous plan notes: A minimum of one street tree must be planted for each 25 feet of street frontage and 10 shrubs or flowering perennials per 40 feet of street frontage. Staff estimates the parcel has over 1,500 feet of frontage, therefore 60 street trees and 375 shrubs/flowering perennials are required.

A landscaping plan was submitted – the required 30 foot planter strip along Route 1 includes 476 plants: 66 sugar maple, larch and red oak trees and 410 shrubs, the species of which are not named. Note 10 on Plan Sheet 1.1 gives spacing details which meet requirements. There are also red oaks and a few green ash trees scattered throughout the development, including along parking area edges and red cedars along the wetland edges. The planter strip will also serve to screen the parking lot. The large parking area has 6 London plane trees in a landscaped strip that divides the parking lot and three more trees along the western side. The other parking lots have trees

scattered along the edges. Section 16.8.9.4.G requires 1 tree per eight parking spaces – all parking areas meet the requirements. Notes 10-12 on Sheet 6.2 address the requirements.

- 9. A traffic impact report was submitted for the February 8th meeting. The traffic impact analysis submitted gave additional information including average daily traffic for the various uses. Traffic patterns are indicated on the plans and show two-way traffic through the property. Plan Sheet 1.4 shows that the ingress/egress shared with the medical office next door whose existing driveway will be abandoned will have a left turning lane for exiting onto Route 1. The updated traffic impact analysis also cited the south-bound left turn lane added to Route 1 for turning onto Lewis Road. No north-bound left turn lane was added although it was a part of the former Sowerby project's permitting in 2008 by ME DOT. Route 1 north-bound appears to have space for a left turn lane that is currently yellow striped (probably because the 2008 project was never built). The Sowerby project as approved included a hotel, convenience store, restaurants and commercial space.
 - a. Lewis Road is directly opposite the proposed main entrance to the Homestead development. Will this affect traffic flow?
 - b. Has the ME DOT entrance permitting process begun? If so, what comments has DOT made so far? What is the process to create that the north-bound left turn lane? Update: the applicant will working with the ME DOT permit previously issued for the Sowerby project and the north-bound left turn lane creation process will be included.
 - c. Update: CMA has provided a traffic peer review.
- 10. As shown on the plans, there are 148 parking spaces with 152 required. Parking requirements are broken down as follows on Plan Sheet 1.1:

Elderly housing = 2 spaces/unit for 26 units = 52 (garages and driveways provide this)

Apartments = 2 spaces/unit for 16 units = 32

Retail (A1/A2) = 8,000 sf divided by 175 sf/parking space = 46

Retail (C1) = 2,000 sf divided by 175 sf/space = 12

Office (C1) = 2,000 sf divided by 250 sf/unit = 10 (8 based on sf + 2 required for the office)

- a. The elderly single-family housing as proposed appear to be larger than 2 bedrooms (at 2,800 sf and 3 BR) which would require 2 parking spaces per dwelling unit. Staff (including the CEO) believes that the elderly housing single-family residential units may count a single-car garage and a driveway of sufficient length to accommodate a parked car without blocking sidewalks or extending beyond the curb where no sidewalks exist for the two parking spaces. Update: no parking will be allowed on the street per Note 13 on Sheet 1.1.
- b. The clubhouse is shown with the 8 parking spaces required per *Offices, professional and public buildings*, but two more spaces are also required because 16.8.9.4.D Off-Street Parking Standards states that "*two parking spaces for each office unit plus 1 space for each 250 feet of gross floor area*". Update: the parking area in front of the clubhouse has three spaces and is outside the 100 foot wetland setback.
- c. Removing the 52 spaces being provided by garages and driveways, the total number of required parking spaces in parking areas total 100. The number of proposed parking spaces in the six parking areas is 96 and a parking waiver has been submitted.

- 11. Snow storage is shown all four proposed locations are located at an acceptable distance from stormwater ponds and wetlands. One snow dump was relocated from the passive recreation area to the other side of the street.
- 12. Open space requirements appear to be met per 16.3.2.13.D as is the 10% minimum use requirement per 16.3.2.13.D.4.
- 13. The plan sheets show the Map and Lot as Map 24, Lot 60 when it is Map 60 Lot 24. Also Sheet 1.1 shows a discrepancy in the scale in the title block and the scale on the plan itself. Update: these have been addressed.
- 14. On Plan Sheet 2.1 and perhaps others, an arrow labeled "retaining wall" does not seem to point to anything. Is there a wall proposed? Update: arrow and label have been removed.
- 15. The Applicant states in Note 13 that the road will remain private but the note should be modified to read as follows: – All roads shall be and must remain private roads, with the property owners, HOA or other such entities bearing all responsibility for maintenance including but not limited to, snowplowing, paving and stormwater system operation and repair.
- 16. Because the roads will remain private, the Applicant requests a waiver from road standards (ROW and shoulders in particular) found in Table 1 in Chapter 16.8.
- 17. Sidewalks will need to be installed along Route 1 per the Public Works Commissioner. Sidewalks within the development will be 5 feet in width.
- 18. It came to Staff's attention that a conservation area was created for protection of wetlands and the pond when the original 2008 Sowerby application was approved. This conservation area is noted in deeds for the Lots 2, 3 and 6 (abutting parcels to the northeast which were part of that original approval). Similarly, there should be a conservation area created 100 feet from the pond on the Homestead parcel. The conservation area will need to be shown on the plans, noted in the homeowner's association document and marked appropriately on the ground after final approval. This area is not proposed for development by the Applicant so is mostly a matter of documentation. Update: the conservation area is shown on the plans.
- 19. 16.8.4.2 Layout states that only one entrance per 1,000 feet of frontage is allowed onto arterial and secondary arterial roadways. CMA's last review mentioned that the Applicant has two entrances less than 1,000 feet from each other. The frontage towards the northeast has wetlands. The Applicant has requested a waiver.
- 20. The Applicant should be prepared to address the Planning Board question concerning whether or not an easement for the old power lines exists and if so, the process to extinguish it.
- 21. The Applicant will need to prepare HOA documents to be included with submission of the final plan. The HOA document will be reviewed by the Town's attorney at the Applicant's expense.

Recommendation

The Board held a public hearing on April 12th and voted to give the Applicant 90 days to address CMA comments, Board comments and parking issues. This step of preliminary plan review provides the Board an opportunity to discuss plan revisions, submission materials, staff comments and CMA's review.

- 1. Based on Title 16 and as shown in the review notes, the plan as submitted meets the necessary requirements with the inclusion of two waivers as noted below:
 - a. Parking requires 100 parking spaces in parking areas where 96 are shown for which a waiver has been requested.

b. Entrances to arterial/secondary arterial roads must be 1,000 feet apart for which a waiver has been requested.

If the Board is generally satisfied with the plans, the Board may vote to approve the preliminary plan, likely with conditions based on CMA's review and staff recommendations. If the Board decides additional time on the preliminary plan is needed, the Board need take no action as the 90 days the Board granted the Applicant on April 12th will not end until July. The motions to approve moving the Mixed-Use zone 50 feet, waive the parking requirements from 152 spaces to 148 spaces, waive the 1,000 foot spacing for the two entrances, waive the road standards and approve the preliminary plan are below.

Staff recommends that Board approve the preliminary plan with the conditions as shown in the motion. If during discussion, additional conditions are needed, they may be added.

Move to approve the 50-foot extension of the MU Zone which would allow the entire parcel located at 459 U.S. Route 1 (Tax Map 60 Lot 24) to be considered under the MU Zone as requested by applicant, Michael Brigham of Landmark Hill, LLC.

Move to approve the parking waiver request by applicant, Michael Brigham of Landmark Hill, LLC to allow 148 parking spaces rather than 152 at 459 U.S. Route 1 (Tax Map 60 Lot 24) for the preliminary site and subdivision plan application dated April 18th 2018.

Move to approve the 1,000 foot entrance location waiver request by applicant, Michael Brigham of Landmark Hill, LLC to allow two entrances closer than 1,000 feet apart at 459 U.S. Route 1 (Tax Map 60 Lot 24) for the preliminary site and subdivision plan application dated April 18th 2018.

Move to approve the street standards waiver request by applicant, Michael Brigham of Landmark Hill, LLC to allow private roads to be 20 and 22-feet wide, no ROW and 3-foot shoulders at 459 U.S. Route 1 (Tax Map 60 Lot 24) for the preliminary site and subdivision plan application dated April 18th 2018.

Move to approve the preliminary site and subdivision plan application dated April 18th 2018 from applicant, Michael Brigham of Landmark Hill, LLC, for 459 U.S. Route 1 (Tax Map 60 Lot 24) in the Mixed Use Zone with these conditions

- a. All CMA comments must be addressed prior to submission of the final plan.
- b. The no-cut buffer along the 100-foot setback must be shown on the plans prior to final plan submission.
- c. Plan Note 13 must be revised per Staff Note #15 prior to final plan submission.
- d. Sidewalks along Route 1 must be shown on the plans prior to final plan submission.
- e. [state any additional conditions].





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May 3, 2018

Kathy Connor, Town Planner Town of Kittery P.O. Box 808 Kittery, Maine 03904

RE: Town of Kittery, Planning Board Services Preliminary Plan Review -The Homestead 459 U.S. Route 1 (Tax Map 60, Lot 24) CMA #591.115

Dear Ms. Connor:

CMA Engineers received the following information for Assignment #115, review of the site plan application for property at 459 U.S. Route 1:

- 1) "The Homestead Subdivision, U.S. Route 1 Kittery, Maine", prepared for Landmark Hill, LLC, 79 Congress Street Portsmouth, NH by Attar Engineering, Inc., 1284 State Road, Eliot, Berwick, ME 03903 dated January18, 2018 and revised April 19, 2018.
- 2) "459 U.S. Route 1-Kittery, Revisions" by Attar Engineering, Inc., 1284 State Road, Eliot, Berwick, ME 03903 dated April 18, 2018.
- 3) "Addendum to Traffic Assessment Report, The Homestead-459 U.S. Route 1, Kittery, Maine", by Attar Engineering, Inc., 1284 State Road, Eliot, Berwick, ME 03903 dated January 16, 2018.
- 4) "Landmark Hill Update of Peak Hour Trip Generation for Sowerby Parcel Kittery, Maine," Prepared by Eaton Traffic Engineering, dated December 13, 2017.
- 5) "Addendum to Traffic Assessment Report, The Homestead 459 U.S. Route 1, Kittery, Maine," Prepared by Attar Engineering, Inc., dated January 16, 2018.

We have reviewed the information submitted for conformance with the Kittery Land Use and Development Code Zoning Ordinance and general engineering practices and offer the comments below that correspond directly to the Town's Ordinances. The project is in the Mixed Use, Residential-Rural and Shoreland Overlay Zone districts.

There are numerous comments from our previous review that have not been addressed. These comments are included with new comments below.

16.8 Design and Performance Standards-Built Environment

Article IV. Streets and Pedestrian Ways/Sidewalks Site Design Standards

16.8.4.3. The streets within the development have been designed mostly to Minor Street standards. Deviations from these standards include shoulder widths, shoulder materials and gravel subbase thickness. We note that the narrowed shoulders are justifiable by the use as a private, residential roadway. The applicant should apply for a waiver from the deviations from the street design standards.

Article VI.: Water Supply

16.8.6.1 The applicant should show the existing water main location in U.S. Route 1 and provide information on existing water main material and size.
Proposed water service locations and curb stops should be shown on the plans.
Show how the existing relocated hydrant will tie in to the existing or proposed water main.

Article VII.: Sewage Disposal

16.8.7.1 Proposed sewer service and cleanout locations should be shown on the plan. All sewer pipe lengths and slopes should be included on the roadway profile.

Article VIII. Surface Drainage

The stormwater analysis has changed since our previous review. Several post development flows have increased from their existing condition flows. We note that the increases are for the 2-year storm at two analysis points and are small. The Ordinance requires that peak discharge be limited to pre-development flows for 2 and 25-year storms. The applicant should review/modify or apply for a waiver of this standard.

We have the following comment on Sheet 5.3:

- The detail for Underdrained Soil Filter Pond 20P shows an incorrect emergency spillway elevation.
- 16.8.8.2.D. The O&M manual should conform with the provisions of the post construction stormwater management plan.

Article IX: Parking. Loading and Traffic

- 16.8.9.4.D.I.1 The applicant should show width of the aisle adjacent to the accessible parking spaces on the plans.
- 16.8.9.4.G. Note 11 on Sheet 6.2 should be changed to indicate number of trees required in parking.

Article X. Signs

The Applicant should submit details of proposed signs for CEO approval.

Article XXIV. Exterior Lighting

The Applicant should provide lighting details (i.e. indicate which lights are proposed in the Spec/Ordering information).

The uniformity ratio exceeds that allowed by the Ordinance. Applicant should adjust the lighting or apply for a waiver (an adjustment is recommended).

Traffic Assessment Report

The number of estimated vehicle trips generated by the newly proposed land use appears reasonable and is significantly less than the approved Sowerby mixed-use development, approved in 2007. The improvements designed and constructed (turn lanes on Route 1) will be more than adequate to accommodate the proposed number of peak hour trips generated by the new mixed development. When the development is constructed, Route 1 should be restriped to provide these turn lanes.

General Comments

- 1. The applicant should provide an existing conditions plan that includes existing utilities.
- 2. Applicant should include notes, a plan and details of the demolition of the existing building, driveway and utilities.
- 3. Where is the location of the timber guardrail?
- 4. The two leaders "Residential (2800SF) First Level Garage" and "Elderly Housing Units (TYP) 2800SF" appear to refer to the same houses. If these are different, please clarify. If these are the same thing, remove one leader.
- 5. The applicant has met the required number of streetside and parking area trees and indicates that planting should be at 25'CL spacing. It is not clear on the landscape plan (Sheet 6.2) that this spacing is feasible. Please clarify.
- 6. The cover sheet and notes plan attached to the on-site parking waiver is not the correct plan. It has since been updated.

Should you have any questions, please do not hesitate to call.

Very truly yours, CMA ENGINEERS, INC.

Jodie Branktrickland

Jodie Bray Strickland, P.E. Project Engineer





Kathy Connor Contract Planner Town of Kittery P.O. Box 808 Kittery, Maine 03904 April 18, 2018 Project No.: C052-18

Re: 459 US Route 1 - Kittery Revisions

Dear Ms. Connor:

On behalf of Michael Brigham, President of Landmark Hill, LLC, I have enclosed a revised Plan set for your review and consideration. The site is located on 459 US Route 1 in the Mixed Use District and is described by the Town of Kittery Assessor's Map 60 as Lot 24. The parcel contains 20 +/- acres and is located in the Mixed-Use (MU) District.

The revisions address comments received during the Board meeting and also from Staff review and CMA Engineers. Please note the following;

Staff and Planning Board meeting (April 12, 2018) comments

- Net Residential Calculation (Apartments) The calculation addresses both the apartment units that have interior parking (7,500 SF/unit) and also the apartments that have only exterior parking (10,000 SF/Unit).
- 2) The trail shown provides for an off-site connection.
- 3) Stormwater Ponds discussed at the April 12, 2018 meeting.
- Parking A waiver from Kittery's parking standards (attached) has been submitted requesting a deduction of 4 spaces to resolve the Public Building parking spaces which were located within 100' of the Wetland of Special Significance (WOSS).
- 5) Landscaping A revised Landscaping Plan is attached addressing plant materials discussed at the April 12 meeting.
- 6) MDOT Permit The project currently has a MDOT Entrance Permit for the former Sowerby Mixed-Use Development. Both proposed entrances are in the same location that the Sowerby project had proposed. Traffic counts expected from the Homestead are substantially less than the Sowerby development, as evidenced by the submitted Traffic Report. We will contact MDOT for their review of this project in relation to the Entrance permit.
- 7) Parking Parking requirements were discussed at the April 12 meeting.
- 8) Snow Storage Snow storage near the recreation area has been relocated.
- 9) Map/Lot Map and Lot numbers and other leaders have been revised.
- 10) Deed Restriction A deed restriction for the area adjacent to the pond is

1284 State Road, Eliot, ME 03903 🚸 tel (207) 439-6023 🚸 fax (207) 439-2128

attached.

11) Pole Easement – Former deeds note an undescribed pole easement benefiting the Kittery Light Co. and New England Telephone. We will contact the predecessors of bot utilities to determine if the easement should be updated to reflect the UG power location.

CMA Engineer Comments

- 1) Net Residential Acreage See Item 1 above.
- 2) Street Design The submitted Traffic Assessment report noted that Elderly Detached (Class. 251) units generate Average Daily Traffic (ADT) of 3.71 trips. The 26 proposed units, which will utilize the Homestead Lane road yield 96.42 trips. Minor streets (Figure 1, Section 16.32) have an ADT capacity of 35 to 200. This results in a surplus ADT of 103 trips/day which are available to the other uses within the development, although it is doubtful that these will use the road network due to their close proximity to Route 1. Homestead Lane, which provides access to the elderly units has 1 20' pavement width. The plans reflect a wider pavement section of 22' minimum for both entrances and the access road (Market St) serving the two retail and apartment use buildings. All roads specify a 3" total depth of pavement which meets the secondary road standards (ADT 201 800).
- 3) R.O.W. As discussed in previous meeting a dedicated R.O.W., is not proposed for the development.
- 4) Water Supply The water line in Route 1 is shown on the plan; additional hydrants are also shown.
- 5) Sewer Service Sewer Line is Route 1 is shown; some sewer manholes are located just off of the paved road surface. The system will remain private and all pipe lengths are less than 300' between manholes. The location of manholes was discussed with the Kittery Sewer Superintendent. The sewer service detail is also provided.
- 6) Soil Filter Pond UDSF Pond 40P invert has been revised.
- 7) Parking Lot Design Additional dimensions, an accessible route and landscaping trees have been added and/or revised.
- 8) Signage Signage has been added.
- Lighting Details Are as noted on the Photometrics Plan and the Lighting Schedule.
- General The HISS/Existing Conditions Plan provides the existing conditions (Site, topography, soils, etc.) Other details have been clarified. The dumpster is for residents use, only.

Hopefully, this addresses all comments. We look forward to the next Board meeting and approving the Preliminary Plan.

Please contact me for any additional information or clarifications required.

Sincerely,

Kennt Olen

Kenneth A. Wood, P.E. President

cc: Landmark Hill, LLC

C052-18 Kittery Site App Cover & Summary.doc



CIVIL + STRUCTURAL + MARINE

Kathy Connor **Contract Planner** Town of Kittery P.O. Box 808 Kittery, Maine 03904 April 9, 2018 Project No.: C052-18

Re: 459 US Route 1 - Kittery Revisions

Dear Ms. Connor:

On behalf of Michael Brigham, President of Landmark Hill, LLC, I am submitting a waiver request for on-site parking in accordance with Section 16, Article IV "Waivers" (16.7.4.1).

Requirement: Section 16.8.9.4 specifies off-street parking requirements. Staff review has noted that a portion of the small parking area adjacent to Unit C1 (office/clubhouse) has 2 spaces located within 100' of a Wetland of Special Significance (WOSS). Also, 2 additional spaces are required for the Office/Clubhouse building (2 per unit plus 1/250 SF).

Rationale: A Waiver is requested to reduce the required number of parking spaces by 4: resulting available parking spaces is still sufficient to support the uses shown on the plan. A majority, if not all of the residents, using the Clubhouse will walk from their dwelling units.

If granted the site plan and Note 5 (attached) will be revised accordingly. Thank you for your consideration. Please contact me for any additional information or clarifications required.

Sincerely,

Kennt Olen

Kenneth A. Wood, P.E. President

cc: Landmark Hill, LLC

C052-18 Kittery Waiver.doc

1284 State Road, Eliot, ME 03903 🔹 tel (207) 439-6023 🔹 fax (207) 439-2128

Forms H1=3. SUGGESTED TEMPLATES FOR STORMWATER BUFFER DEED RESTRICTIONS. With some minor revisions the H=1. (Forested buffer, no:disturbance) template may be used to protect undisturbed stream buffers.

Forested buffer, No disturbance FORM H-1 04/06

DECLARATION OF RESTRICTIONS

(Forested Buffer, No Disturbance)

THIS DECLARATION OF RESTRICTIONS is made this ______ day of ______, 20___, by Landmark Hill, 79 Congress St, Portsmouth, NH 03801; Rockingham County, NH, (herein referred to as the "Declarant", pursuant to development approvals received from the Maine Department of Environmental protection and the Town of Kittery, Maine under the Site Location of Development Act, to preserve a buffer area on a parcel of land near Route 1 (west side near Adams Road in the Town of Kittery, Maine.

WHEREAS, the Declarant holds title to certain real property situated in Kittery, Maine described in a deed from David M. and Suzanne Sowerby to DSS Land Holdings Limited Liability Company, dated March 28, 1996 and recorded in Book 7784, Page 66 at the York County Registry of Deeds and a deed from DSS Land Holdings, LLC to Landmark Hill, LLC recorded in Book XXXX, Page XXXX, herein referred to as the "property"; and

WHEREAS, Declarant desires to place certain restrictions, under the terms and conditions herein, over a portion of said real property (hereinafter referred to as the "Restricted Buffer") described as follows: shown on a plan titled "Site and Subdivision Plan, The Homestead, 495 US Route 1, Kittery, Maine", prepared by Attar Engineering, Inc., 1284 State Road, Eliot, Maine 03903, dated February 8, 2018.

WHEREAS, pursuant to the Site Location of Development Act, 38 M.R.S.A. §§ 481-490, and Department Rules for stormwater management, Chapter 500, promulgated by the Maine Board of Environmental Protection, Declarant has agreed to impose certain restrictions on the Restricted Buffer Area as more particularly set forth herein and has agreed that these restrictions may be enforced by the Maine Department of Environmental Protection or any successor (hereinafter the "MDEP"),

NOW, THEREFORE, the Declarant hereby declares that the Restricted Buffer Area is and shall forever be held, transferred, sold, conveyed, occupied and maintained subject to the conditions and restrictions set forth herein. The Restrictions shall run with the Restricted Buffer Area and shall be binding on all parties having any right, title or interest in and to the Restricted Buffer Area, or any portion thereof, and their heirs, personal representatives, successors, and assigns. Any present or future owner or occupant of the Restricted Buffer Area or any portion thereof, by the acceptance of a deed of conveyance of all or part of the Covenant Area or an instrument conveying any interest therein, whether or not the deed or instrument shall so express, shall be deemed to have accepted the Restricted Buffer Area subject to the Restrictions and shall agree to be bound by, to comply with and to be subject to each and every one of the Restrictions hereinafter set forth.

1. Restrictions on Restricted Buffer Area. Unless the owner of the Restricted Buffer Area, or any successors or assigns, obtains the prior written approval of the MDEP, the Restricted Buffer Area must remain undeveloped in perpetuity. To maintain the ability of the Restricted Buffer Area to filter and absorb stormwater, and to maintain compliance with the Site Location of Development Act and the

permit issued thereunder to the Declarant, the use of the Restricted Buffer Area is hereinafter limited as follows.

a. No soil, loam, peat, sand, gravel, concrete, rock or other mineral substance, refuse, trash, vehicle bodies or parts, rubbish, debris, junk waste, pollutants or other fill material will be placed, stored or dumped on the Restricted Buffer Area, nor shall the topography of the area be altered or manipulated in any way;

b. No trees may be cut or sprayed with biocides except for the normal maintenance of dead, windblown or damaged trees and for pruning of tree branches below a height of 12 feet provided two thirds of the tree's canopy is maintained;

c. No undergrowth, ground cover vegetation, leaf litter, organic duff layer or mineral soil may be disturbed except that one winding path, that is no wider than six feet and that does not provide a downhill channel for runoff, is allowed through the area;

d. No building or other temporary or permanent structure may be constructed, placed or permitted to remain on the Restricted Buffer Area, except for a sign, utility pole or fence;

e. No trucks, cars, dirt bikes, ATVs, bulldozers, backhoes, or other motorized vehicles or mechanical equipment may be permitted on the Restricted Buffer Area;

f. Any level lip spreader directing flow to the Restricted Buffer Area must be regularly inspected and adequately maintained to preserve the function of the level spreader.

Any activity on or use of the Restricted Buffer Area inconsistent with the purpose of these Restrictions is prohibited. Any future alterations or changes in use of the Restricted Buffer Area must receive prior approval in writing from the MDEP. The MDEP may approve such alterations and changes in use if such alterations and uses do not impede the stormwater control and treatment capability of the Restricted Buffer Area or if adequate and appropriate alternative means of stormwater control and treatment are provided.

2. Enforcement. The MDEP may enforce any of the Restrictions set forth in Section 1 above.

3. Binding Effect. The restrictions set forth herein shall be binding on any present or future owner of the Restricted Buffer Area. If the Restricted Buffer Area is at any time owned by more than one owner, each owner shall be bound by the foregoing restrictions to the extent that any of the Restricted Buffer Area is included within such owner's property.

4. Amendment. Any provision contained in this Declaration may be amended or revoked only by the recording of a written instrument or instruments specifying the amendment or the revocation signed by the owner or owners of the Restricted Buffer Area and by the MDEP.

5. Effective Provisions of Declaration. Each provision of this Declaration, and any agreement, promise, covenant and undertaking to comply with each provision of this Declaration, shall be deemed a land use restriction running with the land as a burden and upon the title to the Restricted Buffer Area.

6. Severability. Invalidity or unenforceability of any provision of this Declaration in whole or in part shall not affect the validity or enforceability of any other provision or any valid and enforceable part of a provision of this Declaration.

7. Governing Law. This Declaration shall be governed by and interpreted in accordance with the laws of the State of Maine.

(NAME)

STATE OF MAINE, _____County, dated _____, 20_.

Personally appeared before me the above named ______, who swore to the truth of the foregoing to the best of (his/her) knowledge, information and belief and acknowledged the foregoing instrument to be (his/her) free act and deed.

Notary Public







GENERAL NOTES

1. SEWER MAINS TO BE 8" SDR 35 PVC. ALL OTHER APPURTENANCES SHALL MEET KITTERY SEWER DISTRICT STANDARDS.

2. ALL PIPES, VALVES, FITTINGS, AND CONNECTIONS SHALL MEET CURRENT KITTERY WATER DISTRICT STANDARDS.

3. ALL STORM DRAINS TO BE ADS N-12 (PE) OR APPROVED EQUAL.

4. A MINIMUM OF 5.0' OF COVER SHALL BE MAINTAINED OVER ALL WATER LINES. 5. CENTRAL MAINE POWER COMPANY WILL PREPARE THE ELECTRICAL PLAN FOR CONSTRUCTION. ALL ELECTRICAL, TELEPHONE, AND CABLE SERVICES WILL BE UNDERGROUND.

6. NEW WATER AND SEWER LINES SHALL BE TESTED IN ACCORDANCE WITH RESPECTIVE DISTRICT REQUIREMENTS.

7. EACH E & S CELL REPRESENTS A LIMITED AREA TO BE CONSTRUCTED WITH ALL EROSION & SEDIMENT CONTROL MEASURES IN PLACE. ALL "CELLS" SHALL BE PROTECTED BY EROSION & SEDIMENT CONTROL BEST MANAGEMENT PRACTICES AS REQUIRED BY THE E & S PLAN. EROSION & SEDIMENT CONTROL SHALL BE MAINTAINED FOR EACH CELL THROUGH-OUT THE COMPLETION OF THE ENTIRE PROJECT. THE CELLS SHALL BE ESTABLISHED IN THERE NUMERICAL ORDER.

240	320 (FEET)				
GISTRY OF DEEDS					
ND RECORDED IN AGE REGISTER		1.2	SITE A 459 US	ND SUBDIVISION THE HOMESTEAD ROUTE 1 KITTER	PLAN Y, MAINE
			FOR: LA POR	ANDMARK HILL, LLC 79 CONGRESS ST RTSMOUTH, NH 0380	D1
AN REVISION REVISION AN REVISION	4/19/2018 4/16/2018 03/27/2018		ATTA CIN 1284 ST PHONE: (20	RENGINEERING ML ← STRUCTURAL ← MAR ATE ROAD – ELIOT, MAINI 07)439-6023 FAX: (207	5, INC . INE E 03903)439–2128
JUSTMENT	02/08/2018		SCALE: 1" = 80'	APPROVED BY:	DRAWN BY: BRN
AN REVISION	1/18/2018		DATE: (the all	REVISION : DATE
DNS	DATE		JOB NO: C052-18	4/18/0018 FILE: THE HOMESTEAD BASE	SHEET 1.2

TAX MAP 60, LOT 24

GENERAL NOTES

1. SEWER MAINS TO BE 8" SDR 35 PVC. ALL OTHER APPURTENANCES SHALL MEET KITTERY SEWER DISTRICT STANDARDS.

2. ALL PIPES, VALVES, FITTINGS, AND CONNECTIONS SHALL MEET CURRENT KITTERY WATER DISTRICT STANDARDS.

3. ALL WATER SERVICES TO BE EQUIPPED WITH CURB STOPS.

4. ALL STORM DRAINS TO BE ADS N-12 (PE) OR APPROVED EQUAL.

5. A MINIMUM OF 5.0' OF COVER SHALL BE MAINTAINED OVER ALL WATER LINES. 6. CENTRAL MAINE POWER COMPANY WILL PREPARE THE ELECTRICAL PLAN FOR CONSTRUCTION. ALL ELECTRICAL, TELEPHONE, AND CABLE SERVICES WILL BE UNDERGROUND.

7. NEW WATER AND SEWER LINES SHALL BE TESTED IN ACCORDANCE WITH RESPECTIVE DISTRICT REQUIREMENTS.

8. EACH E & S CELL REPRESENTS A LIMITED AREA TO BE CONSTRUCTED WITH ALL EROSION & SEDIMENT CONTROL MEASURES IN PLACE. ALL "CELLS" SHALL BE PROTECTED BY EROSION & SEDIMENT CONTROL BEST MANAGEMENT PRACTICES AS REQUIRED BY THE E & S PLAN. EROSION & SEDIMENT CONTROL SHALL BE MAINTAINED FOR EACH CELL THROUGH-OUT THE COMPLETION OF THE ENTIRE PROJECT. THE CELLS SHALL BE ESTABLISHED IN THERE NUMERICAL ORDER.

DRAINAGE	STRUCTURE	SCHEDULE	

DESC	RIM ELEV	INV IN	INV OUT	PIPE SIZE(IN.)
CB 1	57.8	55.4, 55.4	55.3	15
CB 2	60.8	56.4	56.2	12
CB 3	60.6	.–	56.6	12
CB 4	62.7	56.4	56.3	12
CB 5	60.4	57.0	56.9	12
_	-		—	12
CB 7	61.3	57.4	57.3	12
CB 8	62.6	58.5	58.4	12
_	-	_	_ ·	12
_		_	-	12
CB 11	64.5	-	58.0	12
CB 12	57.9	54.9	54.8	12
CB 13	58.6		55.4	12

02/08/2018

DATE

4/18/2018

JOB NO: C052-18 | FILE: THE HOMESTEAD BASE |

F:04/19/2018

SHEET 2.1 TAX MAP 60, LOT 24

F	PRELIMINARY PLAN REVISION
E	SW PLAN REVISION
D	PRELIMINARY PLAN REVISION
С	SW POND ADJUSTMENT
В	SW POND ADJUSTMENT
A	PRELIMINARY PLAN REVISION
NO.	DESCRIPTION
	REVISIONS

SYMBOL	SOIL SERIES
Bm	BIDDEFORD MUCKY PEAT*
BS	BIDDEFORD-SCANTIC COMPLEX, FILLED AND DITCHED*
DANI	DEVELOPED AREA NOT INVESTIGATED
Dx	DIXFIELD FINE SANDY LOAM
Em	ELMWOOD VERY FINE SANDY LOAM
LT	LYMAN-TUNBRIDGE COMPLEX
Sc	SCANTIC SILT LOAM*
Sw	SWANTON VERY FINE SANDY LOAM
Ws	WESTBURY FINE SANDY LOAM
	* WETLAND SOILS
SOIL BOUI	

SOIL/WET	LAND
SOIL BORI	NG C
TEST PIT	
SLOPE LE	GEND
(NONE)	0 - 3%
В	3 - 8%
С	8 - 15%
D	15 - 25%
	·

GENERAL NOTES

1. PROPERTY LINES, WETLANDS, EXISTING CONDITIONS AND TOPOGRAPHY ARE FROM REFERENCE 1. WETLANDS WERE IDENTIFIED IN THE FIELD BY KENNETH A. WOOD, CWS IN DECEMBER, 1999 AND MICHAEL R. CUOMO, CWS, CSS IN MARCH, 2000. WETLANDS WERE LOCATED WITH SURVEY INSTRUMENT BY ATTAR ENGINEERING, INC. FROM DECEMBER, 1999 THROUGH APRIL, 2000. WETLAND DELINEATION WAS VERIFIED IN 2017 BY KENNETH A. WOOD, CWS. NO CHANGES WERE NOTED FROM THE PREVIOUS DELINEATION.

2. SOIL TYPES SHOWN ON THIS PLAN WERE IDENTIFIED BY MICHAEL CUOMO (MAINE CERTIFIED SOIL SCIENTIST #211) IN APRIL, 2000.

10JANZ018 D MICHAEL CUOMO, MAINE CERTIFIED SOIL SCIENTIST #211

THIS MAP COMPLIES WITH THE STANDARDS FOR CLASS "B" HIGH INTENSITY SOIL SURVEY. SEE REPORT DATED 14 APRIL 2000 FOR DESCRIPTION METHODS OF SOIL.

		· · · · · · · · · · · · · · · · · · ·				
			1.1	HIGH II 459 US	NTENSITY SOIL S THE HOMESTEAD ROUTE 1 KITTER	SURVEY XY, MAINE
				FOR: LA POR	NDMARK HILL, LLC 79 CONGRESS ST TSMOUTH, NH 0380	D1
·····				ATTA CIV 1284 ST PHONE: (20	RENGINEERING /IL ◆ STRUCTURAL ◆ MAR ATE ROAD – ELIOT, MAIN 07)439-6023 FAX: (207	6, INC. INE E 03903)439–2128
	DATE			SCALE: 1'' = 100' DATE: 12/20/2017	APPROVED BY: AUCUL	DRAWN BY: BRN REVISION : DATE -:-
				JOB NO: C052-17	CAD FILE: MBRIGHAM LBASE	SHEET 4.1

EROSION & SEDIMENTATION CONTROL NOTES

- SILTATION FENCE OR HAY BALE BARRIERS WILL BE INSTALLED DOWNSLOPE OF ALL STRIPPING OR CONSTRUCTION OPERATIONS. A DOUBLE SILT FENCE BARRIER SHALL BE INSTALLED DOWNSLOPE OF ANY SOIL MATERIAL STOCKPILES. SILT FENCES SHALL BE INSPECTED AFTER EACH RAIN EVENT AND DAILY DURING PROLONGED RAIN. SILT AND SOIL PARTICLES ACCUMULATING BEHIND THE FENCE SHALL BE REMOVED AFTER EACH SIGNIFICANT RAIN EVENT AND IN NO INSTANCE SHOULD ACCUMULATION EXCEED 1/2 THE HEIGHT OF THE FENCE. TORN OR DAMAGED AREAS SHALL BE REPAIRED.
- TEMPORARY AND PERMANENT VEGETATION AND MULCHING IS AN INTEGRAL COMPONENT OF THE EROSION AND SEDIMENTATION CONTROL PLAN. ALL AREAS SHALL BE INSPECTED AND MAINTAINED UNTIL THE DESIRED VEGETATIVE COVER IS ESTABLISHED. THESE CONTROL MEASURES ARE ESSENTIAL TO EROSION PREVENTION AND ALSO REDUCE COSTLY REWORK OF GRADED AND SHAPED AREAS.
- SEEDING, FERTILIZER AND LIME RATES AND TIME OF APPLICATION WILL BE DEPENDENT ON SOIL REQUIREMENTS. TEMPORARY VEGETATION SHALL BE MAINTAINED IN THESE AREAS UNTIL PERMANENT SEEDING IS APPLIED. ADDITIONALLY, EROSION AND SEDIMENTATION MEASURES SHALL BE MAINTAINED UNTIL PERMANENT VEGETATION IS ESTABLISHED.
- ALL LAWN AREA, OUTER POND SIDE SLOPES AND SWALES SHALL BE PERMANENTLY SEEDED WITH THE FOLLOWING MIXTURE: 20 LB/ACRE CREEPING RED FESCUE, 2 LB/ACRE REDTOP AND 20 LB/ACRE TALL FESCUE FOR A TOTAL OF 42 LB/ACRE. FERTILIZER AND LIME RATES SHALL BE DEPENDENT ON SOIL TESTING. IN THE ABSENCE OF SOIL TESTS, FERTILIZE WITH 10-20-20 (N-P205-K201) AT 800 LB/ACRE AND LIME AT 3 TONS/ACRE. MULCH WITH HAY AT 70-90 LB/1000 S.F. 4" OF LOAM SHALL BE APPLIED PRIOR TO SEEDING.
- POND BOTTOMS AND INNER POND SIDESLOPES SHALL BE PERMANENTLY SEEDED WITH THE FOLLOWING MIXTURE: 20 LB/ACRE CREEPING RED FESCUE, 8 LB/ACRE BIRDSFOOT TREFOIL AND 20 LB/ACRE TALL FESCUE FOR A TOTAL OF 48 LB/ACRE. SEE THE ABOVE NOTE FOR FERTILIZER, LIME AND MULCHING RATES.
- TEMPORARY VEGETATION OF ALL DISTURBED AREAS, MATERIAL STOCKPILES AND OTHER SUCH AREAS SHALL BE ESTABLISHED BY SEEDING WITH EITHER WINTER RYE AT A RATE OF 112 LB/ACRE OR ANNUAL RYEGRASS AT A RATE OF 40 LB/ACRE. WINTER RYE SHALL BE USED FOR FALL SEEDING AND ANNUAL RYEGRASS FOR SHORT DURATION SEEDING. SEEDING SHALL BE ACCOMPLISHED BEFORE OCTOBER 1
- TEMPORARY SEEDING OF DISTURBED AREAS SHALL BE ACCOMPLISHED BEFORE OCTOBER 1. PERMANENT SEEDING SHALL BE ACCOMPLISHED BEFORE SEPTEMBER 15.
- B. ALL SEEDED AREAS SHALL BE MULCHED WITH HAY AT A RATE OF 2 BALES (70-90 LB) PER 1000 S.F. OF SEEDED AREA.
- SLOPES 2:1 OR STEEPER SHALL BE TREATED WITH POLYJUTE OPEN WEAVE GEOTEXTILE (OR EQUIVALENT) AFTER SEEDING. JUTE MATS SHALL BE ANCHORED PER MANUFACTURER'S SPECIFICATIONS.
- 10. EXCESSIVE DUST CAUSED BY CONSTRUCTION OPERATIONS SHALL BE CONTROLLED BY APPLICATION OF WATER OR CALCIUM CHLORIDE.
- 11. THE CONTRACTOR MAY OPT TO USE EROSION CONTROL MIX BERM AS A SEDIMENT BARRIER IN LIEU OF SILTATION FENCE OR HAY BALE BARRIERS WITH APPROVAL FROM THE INSPECTING ENGINEER.
- 12. MINIMIZE DISTURBED AREAS AND PROTECT NATURAL DOWNGRADIENT BUFFER AREAS TO THE EXTENT PRACTICABLE. CONTROL STORMWATER VOLUME AND VELOCITY WITHIN THE SITE TO MINIMIZE SOIL EROSION. MINIMIZE THE DISTURBANCE OF STEEP SLOPES. CONTROL STORMWATER DISCHARGES, INCLUDING BOTH PEAK FLOW RATES AND VOLUME, TO MINIMIZE EROSION AT OUTLETS. THE DISCHARGE MAY NOT RESULT IN EROSION OF ANY OPEN DRAINAGE CHANNELS, SWALES, STREAM CHANNELS OR STREAM BANKS, UPLAND, OR COASTAL OR FRESHWATER WETLANDS OFF THE PROJECT SITE.

EROSION & SED. CONTROL NOTES (CONT.)

- 13. WHENEVER PRACTICABLE, NO DISTURBANCE ACTIVITIES SHOULD TAKE PLACE WITHIN 50 FEET OF ANY PROTECTED NATURAL RESOURCE. IF DISTURBANCE ACTIVITIES TAKE PLACE BETWEEN 30 FEET AND 50 FEET OF ANY PROTECTED NATURAL RESOURCE, AND STORMWATER DISCHARGES THROUGH THE DISTURBED AREAS TOWARD THE PROTECTED NATURAL RESOURCE, PERIMETER EROSION CONTROLS MUST BE DOUBLED. IF DISTURBANCE ACTIVITIES TAKE PLACE LESS THAN 30 FEET FROM ANY PROTECTED NATURAL RESOURCE, AND STORMWATER DISCHARGES THROUGH THE DISTURBED AREAS TOWARD THE PROTECTED NATURAL RESOURCE, PERIMETER EROSION CONTROLS MUST BE DOUBLED AND DISTURBED AREAS MUST BE TEMPORARILY OR PERMANENTLY STABILIZED WITHIN 7 DAYS.
- 14. PRIOR TO CONSTRUCTION, PROPERLY INSTALL SEDIMENT BARRIERS AT THE DOWNGRADIENT EDGE OF ANY AREA TO BE DISTURBED AND ADJACENT TO ANY DRAINAGE CHANNELS WITHIN THE DISTURBED AREA. SEDIMENT BARRIERS SHOULD BE INSTALLED DOWNGRADIENT OF SOIL OR SEDIMENT STOCKPILES AND STORMWATER PREVENTED FROM RUNNING ONTO THE STOCKPILE. MAINTAIN THE SEDIMENT BARRIERS BY REMOVING ACCUMULATED SEDIMENT. OR REMOVING AND REPLACING THE BARRIER. UNTIL THE DISTURBED AREA IS PERMANENTLY STABILIZED. WHERE A DISCHARGE TO A STORM DRAIN INLET OCCURS, IF THE STORM DRAIN CARRIES WATER DIRECTLY TO A SURFACE WATER AND YOU HAVE AUTHORITY TO ACCESS THE STORM DRAIN INLET, YOU MUST INSTALL AND MAINTAIN PROTECTION MEASURES THAT REMOVE SEDIMENT FROM THE DISCHARGE.
- 15. PRIOR TO CONSTRUCTION, PROPERLY INSTALL A STABILIZED CONSTRUCTION ENTRANCE (SCE) AT ALL POINTS OF EGRESS FROM THE SITE. THE SCE IS A STABILIZED PAD OF AGGREGATE, UNDERLAIN BY A GEOTEXTILE FILTER FABRIC, USED TO PREVENT TRAFFIC FROM TRACKING MATERIAL AWAY FROM THE SITE ONTO PUBLIC ROW'S. MAINTAIN THE SCE UNTIL ALL DISTURBED AREAS ARE STABILIZED.
- 16. WITHIN 7 DAYS OF THE CESSATION OF CONSTRUCTION ACTIVITIES IN AN AREA THAT WILL NOT BE WORKED FOR MORE THAN 7 DAYS. STABILIZE ANY EXPOSED SOIL WITH MULCH, OR OTHER NON-ERODIBLE COVER. STABILIZE AREAS WITHIN 75 FEET OF A WETLAND OR WATERBODY WITHIN 48 HOURS OF THE INITIAL DISTURBANCE OF THE SOIL OR PRIOR TO ANY STORM EVENT, WHICHEVER COMES FIRST
- 17. REMOVE ANY TEMPORARY CONTROL MEASURES, SUCH AS SILTATION FENCE, WITHIN 30 DAYS AFTER PERMANENT STABILIZATION IS ATTAINED. REMOVE ANY ACCUMULATED SEDIMENTS AND STABILIZE.
- 18. IF THE AREA WILL NOT BE WORKED FOR MORE THAN ONE YEAR OR HAS BEEN BROUGHT TO FINAL GRADE, THEN PERMANENTLY STABILIZE THE AREA WITHIN 7 DAYS BY PLANTING VEGETATION, SEEDING, SOD, OR THROUGH THE USE OF PERMANENT MULCH, OR RIPRAP, OR ROAD SUB-BASE. IF USING VEGETATION FOR STABILIZATION SELECT THE PROPER VEGETATION FOR THE LIGHT, MOISTURE, AND SOIL CONDITIONS; AMEND AREAS OF DISTURBED SUBSOILS WITH TOPSOIL, COMPOST, OR FERTILIZERS; PROTECT SEEDED AREAS WITH MULCH OR, IF NECESSARY, EROSION CONTROL BLANKETS; AND SCHEDULE SODDING, PLANTING, AND SEEDING SO TO AVOID DIE-OFF FROM SUMMER DROUGHT AND FALL FROSTS. NEWLY SEEDED OR SODDED AREAS MUST BE PROTECTED FROM VEHICLE TRAFFIC, EXCESSIVE PEDESTRIAN TRAFFIC, AND CONCENTRATED RUNOFF UNTIL THE VEGETATION IS WELL-ESTABLISHED WITH 90% COVER BY HEALTHY VEGETATION. IF NECESSARY, AREAS MUST BE REWORKED AND RESTABILIZED IF GERMINATION IS SPARSE, PLANT COVERAGE IS SPOTTY, OR TOPSOIL EROSION IS EVIDENT. ONE OR MORE OF THE FOLLOWING MAY APPLY TO A PARTICULAR SITE.
- 19. FOR SEEDED AREAS, PERMANENT STABILIZATION MEANS A 90% COVER OF THE DISTURBED AREA WITH MATURE, HEALTHY PLANTS WITH NO EVIDENCE OF WASHING OR RILLING OF THE TOPSOIL.
- 20. FOR SODDED AREAS, PERMANENT STABILIZATION MEANS THE COMPLETE BINDING OF THE SOD ROOTS INTO THE UNDERLYING SOIL WITH NO SLUMPING OF THE SOD OR DIE-OFF.
- 21. FOR MULCHED AREAS, PERMANENT MULCHING MEANS TOTAL COVERAGE OF THE EXPOSED AREA WITH AN APPROVED MULCH MATERIAL. EROSION CONTROL MIX MAY BE USED AS MULCH FOR PERMANENT STABILIZATION ACCORDING TO THE APPROVED APPLICATION RATES AND LIMITATIONS.
- 22. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ADEQUATE HOUSEKEEPING PRACTICES DURING THE CONSTRUCTION OF THE PROJECT. THESE STANDARDS CAN BE FOUND IN THE FOLLOWING DOCUMENT: MDEP CHAPTER 500 (STORMWATER MANAGEMENT), APPENDIX C. HOUSEKEEPING. HOUSEKEEPING PRACTICES INCLUDE, BUT ARE NOT LIMITED TO. SPILL PREVENTION, GROUNDWATER PROTECTION, FUGITIVE SEDIMENT AND DUST, DEBRIS AND OTHER MATERIALS, EXCAVATION DEWATERING, AUTHORIZED NON-STORMWATER DISCHARGES AND UNAUTHORIZED NON-STORMWATER DISCHARGES.

WINTER CONSTRUCTION NOTES

NOVEMBER 1 - APRIL 15 1. AN AREA SHALL BE CONSIDERED STABILIZED WHEN EXPOSED SURFACES HAVE BEEN EITHER MULCHED WITH HAY AT A RATE OF 100 LB/1000 S.F. OR DORMANT SEEDED, MULCHED AND ADEQUATELY ANCHORED BY AN APPROVED ANCHORING TECHNIQUE. IN ALL CASES, MULCH SHALL BE APPLIED SO THAT THE SOIL SURFACE IS NOT VISIBLE THROUGH THE MULCH.

2. FROM OCTOBER 15 TO APRIL 1, LOAM AND SEED WILL NOT BE REQUIRED. DURING PERIODS OF TEMPERATURES ABOVE FREEZING, DISTURBED AREAS SHALL BE FINE GRADED AND PROTECTED WITH MULCH OR TEMPORARILY SEEDED AND MULCHED UNTIL PERMANENT SEEDING CAN BE APPLIED. AFTER NOVEMBER 1, DISTURBED AREAS MAY BE LOAMED, FINE GRADED AND DORMANT SEEDED AT A RATE 200-300% HIGHER THAN THE SPECIFIED PERMANENT SEEDING RATE. IF CONSTRUCTION CONTINUES DURING FREEZING WEATHER DISTURBED AREAS SHALL BE GRADED BEFORE FREEZING AND TEMPORARILY STABILIZED WITH MULCH. DISTURBED AREAS SHALL NOT BE LEFT OVER THE WINTER OR FOR ANY OTHER EXTENDED PERIOD OF TIME UNLESS STABILIZED WITH MULCH.

3. FROM NOVEMBER 1 TO APRIL 15 ALL MULCH SHALL BE ANCHORED BY EITHER PEG LINE. MULCH NETTING, ASPHALT EMULSION CHEMICAL, TRACK OR WOOD CELLULOSE FIBER. MULCH NETTING SHALL BE USED TO ANCHOR MULCH IN ALL DRAINAGE WAYS WITH SLOPES GREATER THAN 3%, SLOPES EXPOSED TO DIRECT WINDS AND FOR SLOPES GREATER THAN 8%. MULCH NETTING SHALL BE USED TO ANCHOR MULCH IN ALL AREAS WITH SLOPES GREATER THAN 15%. AFTER OCTOBER 1, THE SAME APPLIES TO ALL SLOPES GREATER THAN 8%.

4. SNOW SHALL BE REMOVED FROM AREAS OF SEEDING AND MULCHING PRIOR TO PLACEMENT.

5. FOR WINTER STABILIZATION, HAY MULCH SHALL BE APPLIED AT TWICE THE STANDARD TEMPORARY STABILIZATION RATE. AT THE END OF EACH CONSTRUCTION DAY, AREAS THAT HAVE BEEN BROUGHT TO FINAL GRADE SHALL BE STABILIZED. MULCH SHALL NOT BE SPREAD ON TOP OF SNOW.

6. ALL AREAS WITHIN 75 FEET OF A PROTECTED NATURAL RESOURCE SHALL BE PROTECTED WITH A DOUBLE ROW OF SEDIMENT BARRIERS.

7. ALL VEGETATED DITCH LINES THAT HAVE NOT BEEN STABILIZED BY NOVEMBER 1. OR WILL BE WORKED DURING THE WINTER CONSTRUCTION PERIOD. SHALL BE STABILIZED WITH AN APPROPRIATE STONE LINING BACKED BY AN APPROPRIATE GRAVEL BED OR GEOTEXTILE UNLESS SPECIFICALLY RELEASED FROM THIS STANDARD BY THE MDEP.

8. MULCH NETTING SHALL BE USED TO ANCHOR MULCH ON ALL SLOPES GREATER THAN 8% UNLESS EROSION CONTROL BLANKETS OR EROSION CONTROL MIX IS BEING USED ON SUCH SLOPES.

E&S INSPECTION/MAINTENANCE DURING CONSTRUCTION

A. INSPECTION AND CORRECTIVE ACTION. INSPECT DISTURBED AND IMPERVIOUS AREAS, EROSION CONTROL MEASURES, MATERIALS STORAGE AREAS THAT ARE EXPOSED TO PRECIPITATION. AND LOCATIONS WHERE VEHICLES ENTER OR EXIT THE SITE. INSPECT THESE AREAS AT LEAST ONCE A WEEK AS WELL AS BEFORE AND WITHIN 24 HOURS AFTER A STORM EVENT (RAINFALL), AND PRIOR TO COMPLETING PERMANENT STABILIZATION MEASURES. A PERSON WITH KNOWLEDGE OF EROSION AND STORMWATER CONTROL, INCLUDING THE STANDARDS AND CONDITIONS IN THE PERMIT. SHALL CONDUCT THE INSPECTIONS.

- MAINTENANCE. IF BEST MANAGEMENT PRACTICES (BMPS) NEED TO BE REPAIRED. THE REPAIR WORK SHOULD BE INITIATED UPON DISCOVERY OF THE PROBLEM BUT NO LATER THAN THE END OF THE NEXT WORKDAY. IF ADDITIONAL BMPS OR SIGNIFICANT REPAIR OF BMPS ARE NECESSARY, IMPLEMENTATION MUST BE COMPLETED WITHIN 7 CALENDAR DAYS AND PRIOR TO ANY STORM EVENT (RAINFALL). ALL MEASURES MUST BE MAINTAINED IN EFFECTIVE OPERATING CONDITION UNTIL AREAS ARE PERMANENTLY STABILIZED.
- C. DOCUMENTATION. KEEP A LOG (REPORT) SUMMARIZING THE INSPECTIONS AND ANY CORRECTIVE ACTION TAKEN. THE LOG MUST INCLUDE THE NAME(S) AND QUALIFICATIONS OF THE PERSON MAKING THE INSPECTIONS, THE DATE(S) OF THE INSPECTIONS, AND MAJOR OBSERVATIONS ABOUT THE OPERATION AND MAINTENANCE OF EROSION AND SEDIMENTATION CONTROLS. MATERIALS STORAGE AREAS, AND VEHICLES ACCESS POINTS TO THE PARCEL, MAJOR OBSERVATIONS MUST INCLUDE BMPS THAT NEED MAINTENANCE, BMPS THAT FAILED TO OPERATE AS DESIGNED OR PROVED INADEQUATE FOR A PARTICULAR LOCATION. AND LOCATION(S) WHERE ADDITIONAL BMPS ARE NEEDED. FOR EACH BMP REQUIRING MAINTENANCE. BMP NEEDING REPLACEMENT, AND LOCATION NEEDING ADDITIONAL BMPS, NOTE IN THE LOG THE CORRECTIVE ACTION TAKEN AND WHEN IT WAS TAKEN. THE LOG MUST BE MADE ACCESSIBLE TO DEPARTMENT STAFF AND A COPY MUST BE PROVIDED UPON REQUEST. THE PERMITTEE SHALL RETAIN A COPY OF THE LOG FOR A PERIOD OF AT LEAST THREE YEARS FROM THE

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NO.		;	DESC
	•		RFV

VICINITY MAP

1	BEARING TABLE	
LINE	BEARING	DIST
L1	S 01'57'16" E	44.39
L2	S 28'20'00" E	19.58
L3	S 28°07'30" E	77.88
L4	S 8112'20" W	3.43
L5	N 08'34'48" E	46.62
L6	N 05°11'57" W	63.24
L7	N 00°21'24" W	68.54
L8	N 08'05'53" E	68.69
L9	S 77'06'20" E	54.19
L10	S 13'46'22" W	50.12
L11	S 88"11'01" E	44.40
L12	N 11'00'33" E	42.51
L13	S 82'23'52" E	24.39
L14	N 82°23'52" W	43.83
L15	N 78°21'23" W	52.97
L16	N 77'06'20" W	59.39
L17	N 77°06'20" W	16.40
L18	N 55*38'01" W	21.06
L19	S 12'14'31" W	45.25
L20	N 79'30'24" W	36.02
L21	N 12"14'31" E	54.72

REFERENCE DEEDS:

1. David M. Sowerby and Suzanne Sowerby to DSS Land Holdings, LLC; dated March 28, 1996. Recorded at the Y.C.R.D. in Book 7784, page 66.

2. Arnold F. & Jean S. Dickinson to Sentry Commons, LLC; dated July 28, 2000. Recorded at the Y.C.R.D. in Book 10147, page 184.

3. Marion D. Lucas to the State of Maine; dated April 24, 1952. Recorded at the Y.C.R.D. in Book 1205, page 527.

4. Rose E. Adams to the State of Maine; dated March 13, 1952. Recorded at the Y.C.R.D. in Book 1204, page 324.

U.S. ROUTE ONE & ADAMS ROAD KITTERY, MAINE Suite 401 Cottage Place 433 II U.S. Route One York, Maine 03909 OWNER: DSS Land Holdings, LLC P.O. Box 242 York, ME 03909

MAP 60 LOT 24

6.1

C101 + 44

Sheet 1 of 1

LANDSCAPING NOTES

- THE CONTRACTOR SHAL FOLLOW BEST MANAGEMENT PRACTICES DURING CONSTRUCTION AND SHALL TAKE ALL MEANS NECESSARY TO STABILIZE AND PROTECT THE SITE FROM EROSION.
- 2) EROSION CONTROL SHALL BE IN PLACE PRIOR TO CONSTRUCTION.
- 3) EROSION CONTROL TO CONSIST OF HAY BALES AND EROSION CONTROL FABRIC SHALL BE STAKED IN PLACE BETWEEN THE WORK AND WATER BODIES, WETLANDS AND/OR DRAINAGE WAYS PRIOR TO ANY CONSTRUCTION.
- 4) THE CONTRACTOR SHALL VERIFY LAYOUT AND GRADES AND INFORM THE LANDSCAPE ARCHITECT OR CLIENT'S REPRESENTATIVE OF ANY DISCREPANCIES OR CHANGES IN LAYOUT AND/OR GRADE RELATIONSHIPS PRIOR TO CONSTRUCTION.
- 5) THE CONTRACTOR SHALL VERIFY EXACT LOCATION AND ELEVATION OF ALL UTILITIES WITH RESPECTIVE UTILITY OWNERS PRIOR TO CONSTRUCTION. CALL DIGSAFE AT 1-888-344-7233.
- 6) THE CONTRACTOR SHALL GUARANTEE ALL PLANTS FOR NOT LESS THAN TWO YEARS FROM THE TIME OF ACCEPTANCE.
- 7) ALL LANDSCAPING SHALL BE PROVIDED WITH EITHER OF THE FOLLOWING:
- 7)1) AN UNDERGROUND SPRINKLER SYSTEM7)2) AN OUTSIDE HOSE ATTACHMENT WITHIN 150 FEET
- 8) TREES, GROUND COVER, AND SHRUB BEDS SHALL BE MULCHED TO A DEPTH OF 2" WITH ONE-YEAR-OLD, WELL-COMPOSTED, SHREDDED NATIVE BARK NOT LONGER THAN 4" IN LENGTH AND 1/2" IN WIDTH, FREE OF WOODCHIPS AND SAW DUST. MULCH FOR FERNS AND HERBACEOUS PERENNIALS SHALL BE NO LONGER THAN 1" IN LENGTH. TREES IN LAWN AREAS SHALL BE MULCHED IN A 5' DIAMETER MIN. SAUCER.
- 9) ALL DISTURBED AREAS WILL BE DRESSED WITH 4" OF TOPSOIL AND PLANTED AS NOTED ON THE PLANS OR SEEDED EXCEPT PLANT BEDS. PLANT BEDS SHALL BE PREPARED TO A DEPTH OF 12" WITH 75% LOAM AND 25% COMPOST.

10) NUMBER OF TREES AND PLANTS REQUIRED AT FRONTAGE:

REQUIRED PROPOSED	TREES 60 66	PLANTS 375 410	
11) NUMBER OF	TREES AND	PLANTS REQUIRED	AT FRONTAGE:

PROPOSED 38

TREES REQUIRED 1 PER 8 SPACES (13)

12)LANDSCAPED BUFFER TREES TO BE PLANTED AT 25' CL SPACING.

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TAX MAP 60, LOT 24

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` 240 320 (FEET) STORMWATER: EXISTING CONDITIONS 7.1 THE HOMESTEAD 459 US ROUTE 1 KITTERY, MAINE FOR: LANDMARK HILL, LLC 79 CONGRESS ST PORTSMOUTH, NH 03801 INTE OF MANN ATTAR ENGINEERING, INC. KENNETH A REVISION 4/19/2018 CIVIL ◆ STRUCTURAL ◆ MARINE 1284 STATE ROAD - ELIOT, MAINE 03903 PHONE: (207)439-6023 FAX: (207)439-2128 COOW ISION 4/16/2018 No. 5992 REVISION 03/27/2018 SCALE: 02/08/2018 APPROVED BY: DRAWN BY: CENSE BRN 1" = 80' 02/06/2018 1.SSSIONAL SW POND ADJUSTMENT DATE: **REVISION : DATE** 1/18/2018 PRELIMINARY PLAN REVISION \bigcirc X19/2018 F:04/19/2018 aul 02/08/2018 DATE DESCRIPTION JOB NO: C052-18 FILE: THE HOMESTEAD BASE SHEET 7.1 REVISIONS TAX MAP 60, LOT 24

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TAX MAP 60, LOT 24

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459 US Rt. 1 3-story mixed use apartment/commercial building concept look

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Kathy Connor Contract Planner Town of Kittery P.O. Box 808 Kittery, Maine 03904 May 3, 2018 Project No.: C052-18

Re: 459 US Route 1 - Kittery Revisions

Dear Ms. Connor:

On behalf of Michael Brigham, President of Landmark Hill, LLC, I am submitting a waiver request for entrance separation distance in accordance with Section 16, Article IV "Waivers" (16.7.4.1).

Requirement: Section 16.32 specifies street design standards; this section also specifies road geometry and design criteria for Minor Streets and Secondary Collectors.

Rationale: A Waiver is requested to allow for the streets to be constructed as shown on the Site/Subdivision and Grading Plans – widths vary from 22' to 20' with 5' sidewalks and 3' shoulders. Because the road network is part of the development no ROW is proposed. All roads will remain private in perpetuity.

Thank you for your consideration. Please contact me for any additional information or clarifications required.

Sincerely,

Kennet Q all

Kenneth A. Wood, P.E. President

cc: Landmark Hill, LLC

C052-18 Kittery Waiver3.doc

1284 State Road, Eliot, ME 03903 • tel (207) 439-6023 • fax (207) 439-2128

April 9, 2018 Project No.: C052-18

Kathy Connor Contract Planner Town of Kittery P.O. Box 808 Kittery, Maine 03904

Re: 459 US Route 1 - Kittery Revisions

Dear Ms. Connor:

On behalf of Michael Brigham, President of Landmark Hill, LLC, I am submitting a waiver request for on-site parking in accordance with Section 16, Article IV "Waivers" (16.7.4.1).

Requirement: Section 16.8.9.4 specifies off-street parking requirements. Staff review has noted that a portion of the small parking area adjacent to Unit C1 (office/clubhouse) has 2 spaces located within 100' of a Wetland of Special Significance (WOSS). Also, 2 additional spaces are required for the Office/Clubhouse building (2 per unit plus 1/250 SF).

Rationale: A Waiver is requested to reduce the required number of parking spaces by 4; resulting available parking spaces is still sufficient to support the uses shown on the plan. A majority, if not all of the residents, using the Clubhouse will walk from their dwelling units.

If granted the site plan and Note 5 (attached) will be revised accordingly. Thank you for your consideration. Please contact me for any additional information or clarifications required.

Sincerely,

Kennet Q Cen

Kenneth A. Wood, P.E. President

cc: Landmark Hill, LLC

C052-18 Kittery Waiver.doc


Kathy Connor Contract Planner Town of Kittery P.O. Box 808 Kittery, Maine 03904 May 1, 2018 Project No.: C052-18

Re: 459 US Route 1 - Kittery Revisions

Dear Ms. Connor:

On behalf of Michael Brigham, President of Landmark Hill, LLC, I am submitting a waiver request for entrance separation distance in accordance with Section 16, Article IV "Waivers" (16.7.4.1).

Requirement: Section 16.8.4.2 specifies street layout requirements. Section 16.8.4.2.F states "Entrances onto existing or proposed arterial highways/secondary highways may not exceed a frequency of one per thousand (1,000) feet of street frontage." Section 16.8.4.2.C requires "Any development expected to generate average daily traffic of two hundred one (201) or more trips per day is to have at least two street connections with existing public streets."

Rationale: A Waiver is requested to reduce the separation distance from 1,000' to 440' as shown on the submitted site and subdivision plan. The development is required to have two street connections. Although adequate frontage exists on the site to achieve the 1,000', meeting this requirement would result in the second entrance being located an additional 560' easterly, on the opposite side of two large wetland complexes. This location is not preferred due to the extremely long distance the development's residents would need to travel to access Route 1. Additionally, in the event that this entrance is used by emergency response vehicles, the additional distance and travel time would be detrimental to life safety. This entrance would also result in a substantial increase in impervious area. It is also important to note that the current location of both entrances was approved by the Town for the former Sowerby Mixed-Use development, which had a much higher traffic generation and there is a current Maine DOT Entrance Permit approved for the current proposed locations of the entrances.

Thank you for your consideration. Please contact me for any additional information or clarifications required.

Sincerely,

Kennet Q all

Kenneth A. Wood, P.E. President

cc: Landmark Hill, LLC

C052-18 Kittery Waiver2.doc

1284 State Road, Eliot, ME 03903 🔹 tel (207) 439-6023 🔹 fax (207) 439-2128



AIIAR ENGINEERING, INC

CIVIL * STRUCTURAL * MARINE

Jennifer Harris Maine Department of Environmental Protection 312 Canco Road Portland, Maine 04103 April 23, 2018 Project No.: C052-18

RE: The Homestead Kittery, Maine Project Amendment

Dear Ms. Harris:

I have enclosed a revised set of revised plans for the referenced project; these revisions address Planning Board review comments.

Also, I have reviewed comments from Ben Viola, P.E. – plan revisions address the horizontal orifice/grate and Pond 10 outlet control elevations. I have also attached the HISS with boring logs. All ponds (Pond No's 10, 20, 30, 31 & 40) are specified with HDPE liners as required by Volume III, Section 7.1 of the Stormwater Technical Design Manual when there is less than 18" of separation distance from the bottom of the underdrain to the estimated seasonal high water table or bedrock. The following corresponds to the HISS Report and Grading and Details sheets of the plan-set.

Pond No.	TP/Bor	Exist EL	Bot. Pond EL	Bot. U/D EL	ESHWT/BRock
10	16	58	53.5	50.8	56.7
20P	20	47	41.5	38.8	45.3
30P	19/B1	46	42.5	39.8	44.7
31P	20*	48	48.5	45.8	46.3
40P	14/B5	64	58	55.8	62.3

I believe this responds to all comments received to date.

Thank you for your consideration. Please contact me for any additional information.

Sincerely;

Kenneth A. Wood, P.E. President

cc: Michael Brigham, Landmark Hill LLC

Ken Wood

From: Sent: To: Cc: Subject: Viola, Ben <Ben.Viola@maine.gov> Wednesday, April 18, 2018 1:34 PM Harris, Jennifer H Ken Wood The Homestead

Jen,

The following are my comments regarding the Homestead site location of development law application currently being reviewed by the Department.

HydroCAD Model

- The model pages in my application were mixed up, however I was able to review the model.
- The underdrained soil filters have outlet control structures with "Horiz. Orifice/Grate"s. The elevation of the "Horiz. Orifice/Grate"s should be called out on detail sheet 5.3 so they can be checked against the model inputs.
- The outlet control structure invert for pond 10 on sheet 2.1 (42.03) does not match invert in model (40.03). There is a problem with pond 40 also.
- <u>Plans</u> PE stamp needs to be signed and dated on all plans.
- The soils section was missing from my application booklet. Please provide the soil section of the application along with test pit information from each of the underdrained soil filters.

I will continue my review when I receive a response to the above issues. Please have the applicant explain how each issue is addressed in the cover letter accompanying the response.

If you, or Ken have any questions about my comments please contact me.

Ben Viola, PE

Environmental Engineer in the Bureau of Land Resources

Phone: 207-822-6365 (desk)

207-822-6300 (receptionist) 207-822-6303 (fax)

www.maine.gov/dep

SECTION 7.1 S.W. BMP VOL III

Impermeable Liner: An impermeable liner may be required if the basin is located over highly permeable soils or with less than 18 inches of separation between the bottom of the underdrain and the top of bedrock or the high seasonal water table, if the basin drains an impervious area that is greater than one acre or greater than 2 acres of developed area, and the impervious area is considered a hot spot (public road, fuel handling facility, high use parking and drive-through lanes, industrial facility, vehicle maintenance facility, etc.). The liner must seamlessly extend up the sides of the basin and be anchored into the subgrade.

Construction: Erosion and sedimentation from unstable construction areas is the most common reason for filter failure. The soil filter media should not be installed until the area that drains to it has been permanently stabilized or unless the runoff is diverted around the filter

- <u>Construction Components</u>: Underdrained filters consist of (from bottom up):
 - A geotextile fabric to separate the filter basin from the natural soils. An impermeable membrane
 may be required if groundwater impact or contamination is a concern, or if it may influence the
 effectiveness of the basin.
 - A 12-inch base of coarse clean stone or coarse gravel in which a 4-inch to 6- inch perforated underdrain pipe system is bedded.
 - o A gravel transition layer, if necessary.
 - o An 18-inch layer of uncompacted soil filter media.
 - o A surface cover of grass and mulch.
- <u>Basin Excavation</u>: The basin area may be excavated for underdrain installation and can be used as a sediment trap during construction. After excavation of the basin, the outlet structure and piping system may be installed if protected with a sediment barrier.
- <u>Sacrificial Mulch cover</u>: If the basin will be used as a sediment trap, the sides of the embankments
 must be stabilized and maintained to prevent erosion. The basin will need to be restored for its
 planned purpose after construction. Before final stabilization of the drainage area to the basin, a 2inch to 3-inch layer of sandy loam (with less than 2% clay content) may be spread on the surface of
 the soil filter media as a sacrificial protection layer. The sacrificial layer will need to be removed at the
 end of construction, and the soil filter media will need to be seeded and mulched.
- <u>Compaction of Soil Filter:</u> Filter soil media and underdrain bedding material should be applied to reach a bulk density of between 90% and 92% standard proctor. The soil filter media should be installed in at least two lifts of 9 inches to prevent pockets of loose media.
- <u>Remedial Loam Cover:</u> If vegetation is not established within the first year, the basin may be rototilled, reseeded and protected with a well-anchored erosion control blanket. Or, a 2-inch to 3-inch layer of fine sandy loam may be applied before seeding and mulching.
- <u>Construction Oversight</u>: Inspection of the filter basin must be provided for each phase of construction by the design engineer with required reporting to the DEP. All material intended for the filter basin must be approved by the design engineer after tests by a certified laboratory show that the material conforms to all DEP specifications. At a minimum, inspections will occur:
 - After the preliminary construction of the filter grades and once the underdrain pipes are installed (not backfilled);
 - o After the drainage layer is constructed and prior to the installation of the soil filter media;
 - o After the soil filter media has been installed, seeded and mulched; and
 - o After one year, to inspect vegetation and make corrections.

Testing and Submittals: The source of each component of the soil filter media needs to be identified prior to construction. All results of field and laboratory testing must be submitted to the DEP for approval.

- <u>Media Source</u>: Samples of each type of material should be blended for the mixed filter media and underdrain bedding material. Samples must be a composite of three different locations (grabs) from the stockpile or pit face. Sample size requirements will be determined by the testing laboratory.
- <u>Sieve Analysis</u>: A sieve analysis conforming to ASTM C136 should be performed on each type of the sample material.
- <u>Permeability Testing</u>: Testing the permeability of the soil filter media mixture is recommended with the
 mixture at a measured bulk dry density of 90-92% based on ASTM D698.

Michael Cuomo Soil Scientist

5 Mountain Road, Cape Neddick, Maine 03902 (207) 351-1943

Class "B" High Intensity Soil Survey

Kittery Retail Ventures, LLC US Route One, Adams Road, & Cutts Road Kittery, Maine

prepared for:

Attar Engineering, Inc.

prepared by:



Cerono Noho

14 April 2000

Michael Cuomo Soil Scientist 5 Mountain Road, Cape Neddick, Maine 03902 (207) 351-1943

This report is in reference to the 53.4 acre Kittery Retail Ventures LLC property, located between US Route One, Adams Road, and Cutts Road in Kittery, Maine. In April of this year I conducted a Class "B" High Intensity Soil Survey on this property. This report will discuss the methods and results of the soil survey. I previously marked the edge of the jurisdictional wetlands on most of this parcel with blue flagging. The remainder of the project site wetlands were delineated by Attar Engineering, Inc.

The soil survey is based on twenty backhoe test pits and additional soil information gathered from borings made with a hand auger. The frequency and location of soil observations were selected based on visual clues of a change in soils such as a change in the landform, surface appearance, or vegetation. Boundary delineations between different soils are also based on these visual clues and by interpolating between contrasting soil observations.

The soil series chosen were those which best fit the soils found on this site and which are commonly mapped in Maine. (A soil series is a detailed level of differentiation between contrasting soils.) Descriptions of the soil series and the range in characteristics are established by the USDA Natural Resource Conservation Service. Drainage class was assigned using the guidelines established by the Maine Association of Professional Soil Scientists. This work meets the standards for Class "B" Soil Surveys, as established by the Maine Association of Professional Soil Scientists, except for the developed areas which were not investigated (noted on the map as 'DANI') as discussed below.

The soil survey information is presented using the 1 inch = 100 feet topographic and boundary survey prepared by Attar

Soil Scientist 5 Mountain Road, Cape Neddick, Maine 03902 (207) 351-1943

Engineering, Inc. as a base map. Map units are named for the dominant soil series, but each map unit has "inclusions" of other soil series within it. Due to the natural complexity of soils, the small differences between some soil series, the frequency of soil observations, and the scale at which the map was prepared, it is not possible to detect or represent every subtle change in soil series. Soil survey standards allow for inclusions of up to 25% of other soil series or slopes within a soil map unit, as long as no dissimilar soil series which is limiting for the proposed land use exceeds one acre in size. This work by far exceeds this requirement.

Boundaries between map units are represented as a line on the soil map, but in some cases one soil series grades into the next in a diffuse transition zone.

Because of the regulatory importance of the wetlands, their boundary lines have been flagged in the field, survey located, and plotted on the topographic plan by Attar Engineering, Inc. with great accuracy. Wetland soil map units as small as 1/8th of an acre are shown, as is required by the Class "A" High Intensity Soil Survey Standards.

A commercial retail development served by municipal water and sewer services is proposed. The proposed use will necessitate considerable leveling and filling of the natural soils. Map unit design of this soil survey and soil interpretations in this report are in part influenced by the intended use of the site. Therefore, the information provided in this report may not be adequate or complete for other uses.

Six soil series and two soil complexes (made up of two soil series each) are mapped on the subject parcel. The descriptions and range

Michael Cuomo

Soil Scientist

5 Mountain Road, Cape Neddick, Maine 03902 (207) 351-1943

of characteristics given below are specific to this site. Also, four areas marked on the map as DANI were not investigated, and are therefore not soil map units, but are described briefly below.

Biddeford (Bm)

The Biddeford muck series forms in very poorly drained deposits of highly decomposed organic material over marine origin deposits. The thickness of the muck surface is less than 16 inches. Below the muck surface is silt loam textured soil. The substrate is typically silty clay loam, but on this site the substrate texture was highly variable. This series is typically deep to bedrock, and during this investigation no bedrock was found in these soils within five feet of the surface.

The Biddeford soil series forms in depressions which collect and trap surface and subsurface runoff. The four Biddeford soil map units on this parcel are level.

Inclusions noted in the Biddeford map units were small areas of the Ossipee soil series. The very poorly drained Ossipee series has a mucky layer at the surface more than 16 inches thick over fine textured mineral soils.

The Biddeford soil series is in hydrologic group "D." (The interpretation used for hydrologic group is an engineering designing erosion control estimating rainfall runoff and Biddeford is a wetland soil. There are considerable measures.) regulatory restrictions on activities within wetlands. The most important physical limitations to development of the Biddeford soil series are the prolonged presence of water at or above the soil surface and low bearing strength. The soil material responds manipulation by heavy equipment and becomes an poorly to unsuitable medium for plant growth.

Michael Cuomo Soil Scientist 5 Mountain Road, Cape Neddick, Maine 03902 (207) 351-1943

Biddeford-Scantic Complex, Filled and Ditched (BS)

This soil complex represents two soil series in such close association it was not possible to accurately separate them into different soil map units. The Biddeford soil series is described above. The Scantic soil series is described below.

This complex occurs in a landscape greatly manipulated by humans, which is the main reason the two soil series can't be mapped separately. This area has been ditched, with the ditch spoil both side cast into low berms and smoothed over nearby areas which were not ditched. Parts of this map unit have been partially filled with a thin layer of gravelly or stony fill, and other parts have been filled with trash.

Both Biddeford and Scantic are wetland soils. In one portion of the map unit, the fill over the wetland soils is deep enough that the area is no longer a jurisdictional wetland, provided that the legally. restriction to the The primary fill was placed development of Biddeford soils are the regulatory restrictions on dredge and fill activities within wetlands. The most important physical limitations to development of the Biddeford soil series are the prolonged presence of water at or above the soil surface and low bearing strength. The soil material responds poorly to manipulation by heavy equipment and becomes an unsuitable medium for plant growth.

The primary restriction to the development of Scantic soils are the regulatory restrictions on dredge and fill activities within wetlands. The most important physical limitation to the development of Scantic soils is the prolonged presence of ground water at or near the soil surface for much of the year. Other physical limitations are related to the texture of the soil, which makes it very difficult to work with heavy equipment when wet,

Michael Cuomo Soil Scientist 5 Mountain Road, Cape Neddick, Maine 03902 (207) 351-1943

which is the majority of the year. The soil also has very low infiltration capacity and high erosion rates once vegetation is removed. It is very difficult to establish vegetation on the exposed subsoil.

Disturbed Area, Not Mapped (DANI)

The areas marked on the soil survey as DANI were not soil mapped. This portion of the soil survey does not meet Maine Association of Professional Soil Scientists' standards for soil surveys. They are briefly described as follows:

<u>DANI (1)</u>: This area is the existing mobile home park which covers the western third of the subject property. This area was not investigated due to the safety hazard represented by the underground utilities and concerns about interrupting utility service to the park residents.

<u>DANI (2)</u>: This area is the existing nursing home and the landscaped area around it. This area was not investigated due to the safety hazard represented by the underground utilities and concerns about interrupting utility service to the residents.

DANI (3): This area contains the abandoned subsurface wastewater disposal systems which served the nursing home before municipal sewer service was extended to this use.

<u>DANI (4)</u>: This area along Adams Road contains an old house and barn foundations. Soil was obviously excavated and the area reshaped by humans. There are large amounts of debris and trash on the surface in this area.

Dixfield (Dx)

The Dixfield fine sandy loam series forms in moderately well drained deposits of unstratified basal till. The textures are sandy loam to fine sandy loam throughout the profile. Stones of various sizes are present. The Dixfield series has a compact 'hardpan' substrate, which impedes the internal drainage of water.

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This series is typically deep to bedrock, and in this investigation, no bedrock was found to a depth of at least five feet in these map units.

The Dixfield soil map units occupy some of the high ground and the side slopes of the subject property. The surface slopes of the Dixfield soils range from 3 to 15%. Test pits six, 14, 15, and 19 are examples of the Dixfield soil series.

There are inclusions of the well drained Marlow fine sandy loam soil series in the Dixfield map units. These inclusions are mostly on the steeper side slope landscape positions. Marlow is very similar to the Dixfield, but the Marlow soil series is better drained and deeper to the seasonal high water table. Test pit 13 is an example of a Marlow inclusion. There is also an area approximately 1/8th acre in size from which the topsoil has been removed from a Marlow soil map unit.

The Dixfield series is in Hydrologic Group C. Dixfield is not a wetland soil. The primary limitation to development is the presence of seasonal high water table 1.5 to 2 feet from the soil surface after storm events and during the winter and spring. This limitation can be overcome by drainage structures.

Elmwood (Em)

The Elmwood series forms in moderately well drained deposits of mixed geologic origin. The surface and subsoil are very fine sandy loam which probably forms from ancient wind-blown deposits. The substrate is glacial marine origin silt loam or silty clay loam. The percent of rock fragments is low. This series is typically deep to bedrock, and in this investigation, no bedrock was found to a depth of at least five feet in these map units.

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The Elmwood soil is found on side-slope landscape positions. The surface slopes of the Elmwood soil on this parcel range from 3 to 15%. Test pits 16 and 18 are examples of the Elmwood series.

There are inclusions of unnamed moderately well drained soils which have textures in the substrate which do not conform to the normal range of characteristics for the Elmwood soil series. Test pit ten is an example of this unnamed soil.

The Elmwood soil series is in hydrologic group "C." Elmwood is not a wetland soil. The primary limitation to the development of these soils is the seasonal presence of ground water within 1.5 to 2 feet of the soil surface. A secondary physical limitation is the fine texture of the soils, which make them difficult to work when wet and subject to significant erosion when the vegetation is removed. Once the substrate is exposed, reestablishing vegetation is very difficult.

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Lyman-Tunbridge Complex (LT)

The Lyman-Tunbridge complex represents two soil series which occur together on the landscape. The nature of their association is such that they are impossible to accurately separate into individual map units, so they are mapped as a complex.

The Lyman fine sandy loam and Tunbridge fine sandy loam series both form from unsorted glacial till. The Lyman is between 10 and 20 inches in total depth of soil above bedrock and is somewhat excessively drained. The Tunbridge is 20 to 40 inches deep to bedrock and is well drained. Both typically have fine sandy loam textures in the surface and subsoil. The texture in the substrate of the Tunbridge is usually fine sandy loam, but can range to loamy sand. Coarse fragments are a common feature.

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The Lyman series is represented by test pit three. The Tunbridge series is described in test pit nine. Test pits one, seven and eleven span both soil series, illustrating how difficult it would be to split them into separate soil map units. The Lyman-Tunbridge complex ranges in surface slope from 3 to 25% and occupies a variety of landscape positions.

Inclusions within the Lyman-Tunbridge complex map units include occasional bedrock exposures at the surface. The Abram fine sandy loam soil series, which has less than 10 inches of mineral soil over bedrock, is present as an inclusion. There are inclusions of the moderately well drained Waumbek fine sandy loam soil series, as described in test pit five, which occur in topographic swales. There are also unnamed soils which are moderately deep to bedrock and moderately well drained. Test pit four is an example of one such soil, which is similar to the Waumbek soil series but is moderately deep to bedrock. Test pit 20 is another unnamed moderately well drained soil, but it has a firm 'hardpan' layer above the bedrock. There are also inclusions of an unnamed somewhat poorly drained and moderately deep to bedrock soil.

The Lyman soil series is in hydrologic group C/D. The Tunbridge soil series is in hydrologic group C. Neither of these are wetland soils. The primary limitation to development is the presence of bedrock close to the soil surface. This limitation can be overcome by filling and blasting.

Scantic (Sc)

The Scantic series forms in poorly drained deposits of glacial marine origin silts and clays. The surface and subsoil textures are silt loam. The substrate texture is typically silty clay loam. The percent of rock fragments in all layers is very low. This

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series is typically deep to bedrock, and in this investigation, no bedrock was encountered within 60 inches of the surface.

The Scantic soil forms in low-lying flat or concave landscape positions which receive surface and subsurface runoff from better drained, higher, and/or more strongly sloping areas. The slopes of the Scantic soil on this parcel are 3% or less.

There are inclusions of an unnamed poorly drained soil along the edge of some of the Scantic soil map units where they adjoin glacial till origin soils. Test pits two and twelve show a substratum that is coarser than allowed in the normal range of characteristics for this soil series. One Scantic observation found an accumulation of sediment at the surface which had apparently eroded off an upslope field due to poor historic agricultural practices.

The Scantic soil series is in hydrologic group "D" and is a wetland soil. The primary restriction to the development of Scantic soils are the regulatory prohibitions on dredge and fill activities within wetlands. The primary physical limitation to the development of these soils is the prolonged presence of ground water at or near the soil surface for much of the year. Other physical limitations are related to the texture of the soil, which makes it very difficult to work with heavy equipment when wet, which is the majority of the year. The soil also has very low and suffers high infiltration capacity erosion rates once vegetation is removed. It is very difficult to establish vegetation on the exposed subsoil and substrate.

Swanton (Sw)

The Swanton very fine sandy loam soil series forms in poorly drained deposits of mixed geologic origin. The surface and subsoil

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are very fine sandy loam which probably derives from wind-blown deposits. The substrate is glacial marine origin silt loam or silty clay loam. The percent of rock fragments is low. This series is typically deep to bedrock, and in this investigation, no bedrock was found to a depth of at least five feet in this map unit. The Swanton soil series is similar in most respects to the Elmwood soil described above, but is wetter.

The Swanton soils occurs on this site at footslope landscape positions which receive surface and subsurface runoff from better drained, higher, and/or more strongly sloping areas. The slopes of the Swanton soil on this parcel range from 3 to 8%.

The Swanton series as described in the published literature spans two drainage classes, poorly drained and somewhat poorly drained. On this site the Swanton soil series was used only to represent somewhat poorly drained soils which are not wetlands. Poorly drained wetland soils on this site are mapped as Scantic.

Test pit 17 is an example of the Swanton soil series. No inclusions were noted in the Swanton soil map units.

The Swanton soil series is in hydrologic group "C/D." Swanton is not a wetland soil. The primary limitation to the development of these soils would be the prolonged presence of ground water within one foot of the soil surface for part of the year. Other physical limitations are related to the texture of the soil, which makes it very difficult to work with heavy equipment when wet. The soil has high erosion rates once vegetation is removed. It is very difficult to establish vegetation on the exposed substrate.

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Westbury (Ws)

The Westbury soil series forms in somewhat poorly drained deposits of unstratified basal till. The textures are typically sandy loam to fine sandy loam throughout the soil profile. Stones of various sizes are present within the profile. The Westbury series has a compact "hardpan" substrate, which impedes the internal drainage of water. Westbury is typically deep to bedrock, and no bedrock was encountered during this investigation to a depth of five feet. Westbury is similar to the Dixfield soil series in most respects but is wetter.

The Westbury occupies the bottom of a gentle swale. The slopes of the Westbury soil map unit are 8% or less. This swale receives runoff water from better drained soils which are higher in the landscape. The gentle slope, landscape position, and compact substrate combine to make these soils drain slowly.

The Westbury soil map unit includes sôme soils with textures of loamy fine sand in the substrate, as shown in test pit eight. This is outside the normal range of characteristics for this soil series.

The Westbury soil series is in Hydrologic Group "C" and is not a wetland soil. The most significant physical limitation to development is seasonal wetness within one foot of the surface.

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The following must appear on the plan which has the Soil Map.

Class "B" High Intensity Soil Survey Legend

Symbol	<u>Soil Series</u>
Bm	Biddeford mucky peat*
BS	Biddeford/Scantic complex, filled and ditched*
DANI	Developed area not investigated
Dx	Dixfield fine sandy loam
Em	Elmwood very fine sandy loam
\mathbf{LT}	Lyman/Tunbridge complex
SC	Scantic silt loam*
Sw	Swanton very fine sandy loam
Ws	Westbury fine sandy loam

These are wetland soils.

Slope Legend

(None)	0 to 3%
В	3 to 8%
C	8 to 15%
D	15 to 25%

Michael Cuomo, Maine Certified Soil Scientist #211

This map complies with the standards for High Intensity Soil Survey except as noted in report dated 14 April 2000.

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The following information for calculation purposes. This should not appear on the finished map.

Hydrologic Group Map Unit Drainage Class D Bm Very poorly drained D Very poorly drained and poorly drained вS UNKNOWN Drainage class not assigned DANI С Moderately well drained DX С Em Moderately well drained C/D Somewhat excessively drained and well drained \mathbf{LT} D Poorly drained SC C/D Somewhat poorly drained Sw С Somewhat poorly drained Ws

The following information for calculation purposes. This should not appear on the finished map.

Map Unit Drainage Class Hydrologic Group

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Bm	Very poorly drained	D
BS	Very poorly drained and poorly drained	D
DANI	Drainage class not assigned	UNKNOWN
Dx	Moderately well drained	C
Em	Moderately well drained	C
LT	Somewhat excessively drained and well drained	Ċ/D
SC .	Poorly drained	D
Sw	Somewhat poorly drained	C/D
Ws	Somewhat poorly drained	С



Ē	Town City Pleatetion								
	KITTERY	US ROUTE ONE	Street, Rood	Subdivision	KITTARY	Owner's Nome	VEND	0+4	



Town City Plantation				
KITTERY	US ROUTE ONE	Street, Road Subdivision AND ADAMS ROAD	Owner's Name KITTERY RETATI VENTU	0=4





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EXISTING CONDITION CALCULATIONS

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
4.177	HSG B	2S, 3S
18.006	HSG C	1S, 2S, 3S
7.060	HSG D	1S, 2S, 3S
2.920	Other	1S, 2S, 3S
32.163		TOTAL AREA

The Homestead EXT	Type III 24-hr 2 YEA	AR STORM Rainfall=3.30"
Prepared by Hewlett-Packard Comp	pany	Printed 4/20/2018
HydroCAD® 10.00 s/n 01988 © 2011 Hydro	droCAD Software Solutions LLC	Page 3
Time span= Runof Reach routing by Stor-In	=5.00-20.00 hrs, dt=0.05 hrs, 301 points ff by SCS TR-20 method, UH=SCS nd+Trans method - Pond routing by Sto	or-Ind method
Subcatchment1S:	Runoff Area=757,963 sf 11.63% Im Flow Length=1,580' Tc=36.4 min CN=	pervious Runoff Depth>1.05" 75 Runoff=11.72 cfs 1.522 af
Subcatchment 2S:	Runoff Area=418,478 sf 5.53% Im Flow Length=931' Tc=41.7 min CN=	pervious Runoff Depth>0.65" =67 Runoff=3.43 cfs 0.521 af
Subcatchment 3S:	Runoff Area=224,598 sf 7.08% Im	pervious Runoff Depth>0.85
	Flow Length=629' Tc=11.2 min CN:	=71 Runoff=4.33 cfs 0.365 af
Link 1L:		Inflow=11.72 cfs 1.522 af Primary=11.72 cfs 1.522 af
Link 2L:		Inflow=3.43 cfs 0.521 af
		Primary=3.43 cfs 0.521 af
Link 3L: 3L		Inflow=4.33 cfs 0.365 af Primary=4.33 cfs 0.365 af

Total Runoff Area = 32.163 ac	Runoff Volume = 2.408 af	Average Runoff Depth = 0.90"
90.	.92% Pervious = 29.244 ac	9.08% Impervious = 2.920 ac

The Homestead EXT	Type III 24-hr	10 YEAR STORM Rainfall=4.90"
Prepared by Hewlett-Packard Compa	ny	Printed 4/20/2018
HydroCAD® 10.00 s/n 01988 © 2011 Hydro	CAD Software Solutions LLC	Page 4
Time span=5 Runoff b Reach routing by Stor-Ind-	.00-20.00 hrs, dt=0.05 hrs, 30 by SCS TR-20 method, UH=S +Trans method - Pond routin	01 points CS ng by Stor-Ind method
Subcatchment1S:	Runoff Area=757,963 sf 1 ⁻ Flow Length=1,580' Tc=36.4 m	1.63% Impervious Runoff Depth>2.17" in CN=75 Runoff=24.79 cfs 3.149 af
Subcatchment 2S:	Runoff Area=418,478 sf Flow Length=931' Tc=41.7 r	5.53% Impervious Runoff Depth>1.56" min CN=67 Runoff=9.01 cfs 1.251 af
Subcatchment 3S:	Runoff Area=224,598 sf Flow Length=629' Tc=11.2 m	7.08% Impervious Runoff Depth>1.88" in CN=71 Runoff=10.13 cfs 0.807 af
Link 1L:		Inflow=24.79 cfs 3.149 af Primary=24.79 cfs 3.149 af
Link 2L:		Inflow=9.01 cfs 1.251 af Primary=9.01 cfs 1.251 af
Link 3L: 3L		Inflow=10.13 cfs 0.807 af Primary=10.13 cfs 0.807 af

Total Runoff Area = 32.163 ac	Runoff Volume = 5.206 af	Average Runoff Depth = 1.94"
90	.92% Pervious = 29.244 ac	9.08% Impervious = 2.920 ac

The Homestead EXT	Type III 24-hr 25 YEAR STORM Rainfall=6.20"
Prepared by Hewlett-Packard Compa	any Printed 4/20/2018
HydroCAD® 10.00 s/n 01988 © 2011 Hydro	OCAD Software Solutions LLC Page 5
Time span= Runoff Reach routing by Stor-Inc	5.00-20.00 hrs, dt=0.05 hrs, 301 points by SCS TR-20 method, UH=SCS I+Trans method - Pond routing by Stor-Ind method
Subcatchment1S:	Runoff Area=757,963 sf 11.63% Impervious Runoff Depth>3.19" Flow Length=1,580' Tc=36.4 min CN=75 Runoff=36.34 cfs 4.622 af
Subcatchment 2S:	Runoff Area=418,478 sf 5.53% Impervious Runoff Depth>2.44" Flow Length=931' Tc=41.7 min CN=67 Runoff=14.32 cfs 1.954 af
Subcatchment 3S:	Runoff Area=224,598 sf 7.08% Impervious Runoff Depth>2.84" Flow Length=629' Tc=11.2 min CN=71 Runoff=15.41 cfs 1.218 af
Link 1L:	Inflow=36.34 cfs 4.622 af Primary=36.34 cfs 4.622 af
Link 2L:	Inflow=14.32 cfs 1.954 af Primary=14.32 cfs 1.954 af
Link 3L: 3L	Inflow=15.41 cfs 1.218 af Primary=15.41 cfs 1.218 af

Total Runoff Area = 32.163 ac	Runoff Volume = 7.794 af	Average Runoff Depth = 2.91"
90	.92% Pervious = 29.244 ac	9.08% Impervious = 2.920 ac

Summary for Subcatchment 1S:

Runoff = 36.34 cfs @ 12.51 hrs, Volume= 4.622 af, Depth> 3.19"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

_	A	rea (sf)	CN	Description			
		88,161	98	Paved park	ing & roofs		
	4	63,315	70	Woods, Go	od, HSG C		
_	2	06,487	77	Woods, Go	od, HSG D		
	7	57,963	75	Weighted A	verage		
	6	69,802		88.37% Per	rvious Area		
		88,161		11.63% Imp	pervious Are	ea	
	Тс	Length	Slope	e Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	•	
	12.7	50	0.020	0.07		Sheet Flow,	
						Woods: Light underbrush n= 0.400 P2= 3.00"	
	4.7	257	0.0330	0.91		Shallow Concentrated Flow,	
						Woodland Kv= 5.0 fps	
	0.1	32	0.031) 3.92	2.74	Pipe Channel, Culvert	
						12.0" Round w/ 2.0" inside fill Area= 0.7 sf Perim= 3.0'	r= 0.23
	2.6	145	0.034	0.92		Shallow Concentrated Flow.	
			0.00	0.02		Woodland $Kv = 5.0 \text{ fps}$	
	0.1	18	0.031	3.92	2.74	Pipe Channel, Culvert	
						12.0" Round w/ 2.0" inside fill Area= 0.7 sf Perim= 3.0'	r= 0.23
						n= 0.025 Corrugated metal	
	15.9	1,038	0.015	0 1.09	119.37	Trap/Vee/Rect Channel Flow, Wetland	
						Bot.W=90.00' D=1.00' Z= 20.0 '/' Top.W=130.00'	
						n= 0.150	
	0.3	40	0.005	0 1.97	1.38	Pipe Channel,	
						12.0" Round w/ 2.0" inside fill Area= 0.7 sf Perim= 3.0'	r= 0.23
_						n= 0.020 Corrugated PE, corrugated interior	
	36.4	1,580	Total				

Summary for Subcatchment 2S:

Runoff = 14.32 cfs @ 12.60 hrs, Volume= 1.954 af, Depth> 2.44"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20" Type III 24-hr 25 YEAR STORM Rainfall=6.20" Printed 4/20/2018

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The Homestead EXT	Type III 24-h
Prepared by Hewlett-Packard Company	
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	Area (sf)	CN D	escription		
*	23,128 138,618 207,144 49,588	98 F 55 V 70 V 77 V	Paved park Voods, Goo Voods, Goo Voods, Goo	ing & roofs od, HSG B od, HSG C od, HSG D,	Wetlands
	418,478 395,350 23,128	67 V 9 5	Veighted A 4.47% Per .53% Impe	verage vious Area ervious Area	à
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
28.7	74	0.0230	0.04		Sheet Flow,
6.1	326	0.0320	0.89		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
6.9	531	0.0260	1.28	63.79	Trap/Vee/Rect Channel Flow, Wetland Bot.W=30.00' D=1.00' Z= 20.0 '/' Top.W=70.00' n= 0.150
41.7	931	Total			
			Su	mmary fo	r Subcatchment 3S:
Runoff	=	15.41 cf	s @ 12.1	6 hrs, Volu	me= 1.218 af, Depth> 2.84"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

	А	rea (sf)	CN	Description		
		15,896	98	Paved park	ing & roofs	
*		51,460	77	Woods, Go	od, HSG D,	, Wetland
	1	13,902	70	Woods, Go	od, HSG C	
_		43,340	55	Woods, Go	od, HSG B	
	2	24,598	71	Weighted A	verage	
	2	08,702	ļ	92.92% Pe	rvious Area	
		15,896	-	7.08% Impe	ervious Area	a
	Тс	Lenath	Slope	Velocitv	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
_	0.4	27	0.0200	1.03	. ,	Sheet Flow
	011		0.0200			Smooth surfaces $n=0.011$ P2= 3.00"
	22	153	0.0536	1 16		Shallow Concentrated Flow
	2.2	100	0.0000			Woodland K_{V} = 5.0 fps
	86	110	0.0110	0.87	56 45	Tran/Vee/Pect Channel Flow, Wetland
	0.0	3	0.0110	0.07	50.45	Bot $W_{-45} 00' D_{-1} 00' Z_{-20} 0 V' Top W_{-85} 00'$
						p = 0.150
_	44.0	000	Tatal			11-0.150
	11.2	629	i otal			

Summary for Link 1L:

 Inflow Area =
 17.400 ac, 11.63% Impervious, Inflow Depth > 3.19" for 25 YEAR STORM event

 Inflow =
 36.34 cfs @ 12.51 hrs, Volume=
 4.622 af

 Primary =
 36.34 cfs @ 12.51 hrs, Volume=
 4.622 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Link 2L:

Inflow /	Area =	9.607 ac,	5.53% Impervious, Inflow	Depth > 2.44"	for 25 YEAR STORM even	it
Inflow	=	14.32 cfs @	12.60 hrs, Volume=	1.954 af		
Primary	y =	14.32 cfs @	12.60 hrs, Volume=	1.954 af, Atte	en= 0%, Lag= 0.0 min	

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Link 3L: 3L

Inflow A	Area =	5.156 ac,	7.08% Impervious, Inflow	Depth > 2.84"	for 25 YEAR STORM event
Inflow	=	15.41 cfs @	12.16 hrs, Volume=	1.218 af	
Primary	/ =	15.41 cfs @	12.16 hrs, Volume=	1.218 af, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

DEVELOPED CONDITION CALCULATIONS

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Area Listing (all nodes)

Area	CN	Description		
(acres)		(subcatchment-numbers)		
2.029	55	Woods, Good, HSG B (4S, 19S)		
1.358	61	>75% Grass cover, Good, HSG B (4S, 14S, 15S, 19S, 24S)		
11.038	70	Woods, Good, HSG C (1S, 4S, 19S)		
5.585	74	>75% Grass cover, Good, HSG C (1S, 2S, 3S, 5S, 6S, 7S, 8S, 9S, 10S, 11S, 12S,		
		13S, 16S, 17S, 20S, 21S, 22S, 24S)		
5.922	77	Woods, Good, HSG D (1S, 19S)		
1.138	77	Woods, Good, HSG D, Wetlands (4S)		
0.060	86	Newly graded area, HSG B (25S)		
0.513	98	Existing Impervious (1S)		
0.573	98	Existing Road (19S, 24S)		
0.251	98	Houses AND Roads (11S)		
0.186	98	Houses and Roads (3S)		
0.264	98	Lot and Homes (21S)		
0.059	98	Paved parking & roofs (4S)		
0.180	98	Paved parking, HSG C (1S, 20S, 22S, 23S, 24S, 25S)		
0.029	98	Proposed Driveway, HSG C (19S)		
0.365	98	Roads and Homes (13S)		
0.406	98	Roads and Houses (2S)		
0.948	98	Roads and Parking Lot (14S, 15S, 16S, 17S)		
0.078	98	Roads, Driveway, Parking Lot (18S)		
0.108	98	Roads, Driveways (5S)		
0.296	98	Roads, Driveways, Houses (6S, 7S, 8S, 9S)		
0.167	98	Roads, Homes (12S)		
0.628	98	Roads, Houses (10S)		
32.182	75	TOTAL AREA		

Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
3.447	HSG B	4S, 14S, 15S, 19S, 24S, 25S
16.833	HSG C	1S, 2S, 3S, 4S, 5S, 6S, 7S, 8S, 9S, 10S, 11S, 12S, 13S, 16S, 17S, 19S, 20S,
		21S, 22S, 23S, 24S, 25S
7.060	HSG D	1S, 4S, 19S
4.843	Other	1S, 2S, 3S, 4S, 5S, 6S, 7S, 8S, 9S, 10S, 11S, 12S, 13S, 14S, 15S, 16S, 17S,
		18S, 19S, 21S, 24S
32.182		TOTAL AREA

The Horr Prepared HydroCAD®	by Hewlett-Pa 10.00 s/n 019) ackard Con 88 © 2011 F	Printed 4	/20/2018 Page 4					
Ground Covers (all nodes)									
HSG-A (acres	A HSG-B	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers		
0.000	0 1.358	5.585	0.000	0.000	6.943	>75% Grass cover, Good	1S, 2S, 3S, 4S, 5S, 6S, 7S, 8S, 9S, 10S, 11S, 12S, 13S, 14S, 15S, 16S, 17S, 19S, 20S, 21S,		
0.00	0.000	0.000	0.000	0.513	0.513	Existing Impervious	24S 1S		
0.000	0.000	0.000	0.000	0.573	0.573	Existing Road	19S, 24S		
0.00	0.000	0.000	0.000	0.251	0.251	Houses AND Roads	11S		
0.00	0.000	0.000	0.000	0.186	0.186	Houses and Roads	3S		
0.00	0.000	0.000	0.000	0.264	0.264	Lot and Homes	21S		
0.00	0.000	0.180	0.000	0.000	0.180	Paved parking	1S,		

							24S
0.000	0.000	0.000	0.000	0.251	0.251	Houses AND Roads	11S
0.000	0.000	0.000	0.000	0.186	0.186	Houses and Roads	3S
0.000	0.000	0.000	0.000	0.264	0.264	Lot and Homes	21S
0.000	0.000	0.180	0.000	0.000	0.180	Paved parking	1S,
							20S,
							22S,
							23S,
							24S,
							25S
0.000	0.000	0.029	0.000	0.000	0.029	Proposed Driveway	19S
0.000	0.000	0.000	0.000	0.365	0.365	Roads and Homes	13S
0.000	0.000	0.000	0.000	0.406	0.406	Roads and Houses	2S
0.000	0.000	0.000	0.000	0.059	0.059	Paved parking & roofs	4S
0.000	0.000	0.000	0.000	0.948	0.948	Roads and Parking Lot	14S,
							15S,
							165

16S, 17S

Ground Covers (all nodes) (continued)

HSG-A	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground	Subcatchment
(40100)			(40100)	(40:00)	(40100)		400
0.000	0.000	0.000	0.000	0.078	0.078	Roads, Driveway, Parking Lot	185
0.000	0.000	0.000	0.000	0.108	0.108	Roads, Driveways	5S
0.000	0.000	0.000	0.000	0.296	0.296	Roads, Driveways, Houses	6S,
							7S,
							8S,
							9S
0.000	0.000	0.000	0.000	0.167	0.167	Roads, Homes	12S
0.000	0.000	0.000	0.000	0.628	0.628	Roads, Houses	10S
0.000	0.060	0.000	0.000	0.000	0.060	Newly graded area	25S
0.000	2.029	11.038	7.060	0.000	20.127	Woods, Good	1S,
							4S,
							19S
0.000	3.447	16.833	7.060	4.843	32.182	TOTAL AREA	

The Homestead PRP	Type III 24-hr 25 YEAR STORM Rainfall=6.20"
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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: (new Subcat)	Runoff Area=410,732 sf 5.70% Impervious Runoff Depth>3.20" v Length=1,178' Tc=22.4 min CN=75 Runoff=24.50 cfs 2.517 af
Subcatchment 2S: (new Subcat)	Runoff Area=65,037 sf 27.21% Impervious Runoff Depth>3.82" Flow Length=188' Tc=5.6 min CN=81 Runoff=6.97 cfs 0.475 af
Subcatchment3S: (new Subcat)	Runoff Area=28,485 sf 28.49% Impervious Runoff Depth>3.82" Flow Length=195' Tc=4.7 min CN=81 Runoff=3.15 cfs 0.208 af
Subcatchment 4S:	Runoff Area=353,785 sf 0.72% Impervious Runoff Depth>2.44" ow Length=931' Tc=40.4 min CN=67 Runoff=12.31 cfs 1.653 af
Subcatchment5S: (new Subcat)	Runoff Area=9,321 sf 50.55% Impervious Runoff Depth>4.34" Flow Length=127' Tc=4.1 min CN=86 Runoff=1.18 cfs 0.077 af
Subcatchment 6S: (new Subcat) Flow Length=90	Runoff Area=8,073 sf 43.42% Impervious Runoff Depth>4.14" ' Slope=0.0667 '/' Tc=0.8 min CN=84 Runoff=1.05 cfs 0.064 af
Subcatchment7S: (new Subcat) Flow Length=102	Runoff Area=6,033 sf 37.33% Impervious Runoff Depth>4.03" ' Slope=0.0588 '/' Tc=1.0 min CN=83 Runoff=0.76 cfs 0.047 af
Subcatchment 8S: (new Subcat) Flow Length=99	Runoff Area=7,337 sf 35.23% Impervious Runoff Depth>3.93" ' Slope=0.0400 '/' Tc=1.2 min CN=82 Runoff=0.90 cfs 0.055 af
Subcatchment9S: (new Subcat) Flow Length=102	Runoff Area=11,435 sf 39.71% Impervious Runoff Depth>4.13" ' Slope=0.0588 '/' Tc=1.0 min CN=84 Runoff=1.48 cfs 0.090 af
Subcatchment10S: (new Subcat)	Runoff Area=60,852 sf 44.95% Impervious Runoff Depth>4.23" Flow Length=158' Tc=8.1 min CN=85 Runoff=6.62 cfs 0.493 af
Subcatchment11S: (new Subcat)	Runoff Area=28,681 sf 38.15% Impervious Runoff Depth>4.02" Flow Length=258' Tc=7.7 min CN=83 Runoff=3.04 cfs 0.221 af
Subcatchment12S: (new Subcat)	Runoff Area=29,337 sf 24.82% Impervious Runoff Depth>3.72" Flow Length=120' Tc=4.5 min CN=80 Runoff=3.20 cfs 0.209 af
Subcatchment13S:13S	Runoff Area=40,918 sf 38.90% Impervious Runoff Depth>4.02" Flow Length=300' Tc=6.1 min CN=83 Runoff=4.54 cfs 0.315 af
Subcatchment14S: (new Subcat)	Runoff Area=12,509 sf 87.37% Impervious Runoff Depth>5.08" Flow Length=190' Tc=1.1 min CN=93 Runoff=1.86 cfs 0.121 af
Subcatchment15S: (new Subcat)	Runoff Area=14,458 sf 85.80% Impervious Runoff Depth>5.08" Flow Length=120' Tc=0.8 min CN=93 Runoff=2.18 cfs 0.140 af
Subcatchment16S: (new Subcat)	Runoff Area=15,913 sf 68.89% Impervious Runoff Depth>4.87" Flow Length=86' Tc=0.4 min CN=91 Runoff=2.37 cfs 0.148 af

Type III 24-hr 25 YEAR STORM Rainfall=6.20"

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Subcatchment17S: (new Subcat)	Runoff Area=16,946 sf 41.19% Impervious Runoff Depth>4.13" Flow Length=376' Tc=6.1 min CN=84 Runoff=1.92 cfs 0.134 af
Subcatchment18S: (new Subcat) Flow Length=	Runoff Area=3,382 sf 100.00% Impervious Runoff Depth>5.51" 48' Slope=0.0050 '/' Tc=0.6 min CN=98 Runoff=0.53 cfs 0.036 af
Subcatchment19S: (new Subcat)	Runoff Area=197,865 sf 7.42% Impervious Runoff Depth>3.02" Flow Length=612' Tc=10.7 min CN=73 Runoff=14.68 cfs 1.145 af
Subcatchment 20S: (new Subcat) Flow Length=	Runoff Area=1,203 sf 52.04% Impervious Runoff Depth>4.35" 51' Slope=0.0290 '/' Tc=0.6 min CN=86 Runoff=0.16 cfs 0.010 af
Subcatchment 21S: (new Subcat)	Runoff Area=14,378 sf 80.05% Impervious Runoff Depth>5.08" Flow Length=114' Tc=0.5 min CN=93 Runoff=2.19 cfs 0.140 af
Subcatchment 22S: (new Subcat)	Runoff Area=3,701 sf 28.69% Impervious Runoff Depth>3.82" Flow Length=111' Tc=0.8 min CN=81 Runoff=0.45 cfs 0.027 af
Subcatchment 23S: (new Subcat) Flow Length=	Runoff Area=407 sf 100.00% Impervious Runoff Depth>5.51" 32' Slope=0.0170 '/' Tc=0.2 min CN=98 Runoff=0.06 cfs 0.004 af
Subcatchment 24S: (new Subcat)	Runoff Area=56,549 sf 25.34% Impervious Runoff Depth>3.02" Flow Length=361' Tc=12.8 min CN=73 Runoff=3.93 cfs 0.327 af
Subcatchment 25S: (new Subcat)	Runoff Area=4,529 sf 42.02% Impervious Runoff Depth>4.87" Flow Length=86' Tc=0.7 min CN=91 Runoff=0.67 cfs 0.042 af
Reach 1R: (new Reach) n=0.030 L	Avg. Flow Depth=0.02' Max Vel=1.82 fps Inflow=1.58 cfs 0.327 af =40.0' S=0.3000 '/' Capacity=483.59 cfs Outflow=1.58 cfs 0.327 af
Reach 2R: (new Reach) n=0.150 L=	Avg. Flow Depth=0.17' Max Vel=0.47 fps Inflow=9.32 cfs 1.499 af 700.0' S=0.0257 '/' Capacity=156.29 cfs Outflow=7.48 cfs 1.420 af
Reach 3R: (new Reach) n=0.150 L=	Avg. Flow Depth=0.07' Max Vel=0.24 fps Inflow=3.62 cfs 0.402 af 850.0' S=0.0212 '/' Capacity=141.83 cfs Outflow=1.45 cfs 0.346 af
Reach 4R: (new Reach) n=0.150 L=	Avg. Flow Depth=0.05' Max Vel=0.23 fps Inflow=1.60 cfs 0.337 af 531.0' S=0.0301 '/' Capacity=169.18 cfs Outflow=1.08 cfs 0.305 af
Reach 5R: (new Reach) n=0.030	Avg. Flow Depth=0.03' Max Vel=1.17 fps Inflow=0.62 cfs 0.037 af L=95.0' S=0.0558 '/' Capacity=63.43 cfs Outflow=0.56 cfs 0.037 af
Reach 6R: (new Reach) n=0.150 L=1,	Avg. Flow Depth=0.06' Max Vel=0.19 fps Inflow=3.93 cfs 0.327 af 128.0' S=0.0160 '/' Capacity=123.12 cfs Outflow=1.06 cfs 0.265 af
Pond 10P: (new Pond)	Peak Elev=54.26' Storage=2,656 cf Inflow=4.82 cfs 0.327 af Outflow=1.58 cfs 0.327 af
Pond 20P: (new Pond)	Peak Elev=43.78' Storage=11,106 cf Inflow=9.81 cfs 0.690 af Outflow=3.76 cfs 0.565 af
Pond 30P: (new Pond)	Peak Elev=45.36' Storage=18,017 cf Inflow=13.93 cfs 1.116 af Outflow=5.56 cfs 0.934 af

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Peak Elev=50.58'	Storage=7,263 cf	Inflow=6.49 cfs	0.492 af

Pond 31P: (new Pond)	Peak Elev=50.58' Storage=7,263 cf Inflow=6.49 cfs 0.492 af Outflow=3.62 cfs 0.402 af
Pond 40P: (new Pond)	Peak Elev=60.48' Storage=8,335 cf Inflow=5.44 cfs 0.432 af Outflow=1.60 cfs 0.337 af
Pond C1: (new Pond)	Peak Elev=57.18' Inflow=6.62 cfs 0.493 af 15.0" Round Culvert n=0.010 L=170.0' S=0.0753 '/' Outflow=6.62 cfs 0.493 af
Pond C10: (new Pond)	Peak Elev=59.69' Storage=296 cf Inflow=2.34 cfs 0.176 af 12.0" Round Culvert n=0.010 L=100.0' S=0.0030 '/' Outflow=2.15 cfs 0.176 af
Pond C11: (new Pond)	Peak Elev=58.89' Inflow=2.37 cfs 0.148 af 12.0" Round Culvert n=0.010 L=60.0' S=0.0100 '/' Outflow=2.37 cfs 0.148 af
Pond C12: (new Pond)	Peak Elev=55.20' Inflow=0.62 cfs 0.037 af 12.0" Round Culvert n=0.013 L=83.0' S=0.0096 '/' Outflow=0.62 cfs 0.037 af
Pond C13: (new Pond)	Peak Elev=55.63' Inflow=0.16 cfs 0.010 af 12.0" Round Culvert n=0.013 L=94.9' S=0.0053 '/' Outflow=0.16 cfs 0.010 af
Pond C14: (new Pond)	Peak Elev=59.71' Inflow=0.67 cfs 0.042 af 12.0" Round Culvert n=0.020 L=115.0' S=0.0017 '/' Outflow=0.67 cfs 0.042 af
Pond C2: (new Pond)	Peak Elev=57.04' Inflow=2.19 cfs 0.140 af 12.0" Round Culvert n=0.010 L=119.0' S=0.0647 '/' Outflow=2.19 cfs 0.140 af
Pond C3: (new Pond)	Peak Elev=57.60' Inflow=2.19 cfs 0.140 af 12.0" Round Culvert n=0.010 L=62.5' S=0.0032 '/' Outflow=2.19 cfs 0.140 af
Pond C30: (new Pond)	Peak Elev=55.87' Inflow=1.18 cfs 0.077 af 12.0" Round Culvert n=0.010 L=29.0' S=0.0103 '/' Outflow=1.18 cfs 0.077 af
Pond C31: (new Pond)	Peak Elev=55.93' Inflow=3.24 cfs 0.214 af 12.0" Round Culvert n=0.010 L=127.0' S=0.0921 '/' Outflow=3.24 cfs 0.214 af
Pond C32: (new Pond)	Peak Elev=58.87' Inflow=1.95 cfs 0.119 af 12.0" Round Culvert n=0.010 L=65.0' S=0.0708 '/' Outflow=1.95 cfs 0.119 af
Pond C33: (new Pond)	Peak Elev=55.85' Inflow=1.48 cfs 0.090 af 12.0" Round Culvert n=0.010 L=45.0' S=0.0089 '/' Outflow=1.48 cfs 0.090 af
Pond C34: (new Pond)	Peak Elev=59.01' Inflow=0.90 cfs 0.055 af 12.0" Round Culvert n=0.010 L=48.0' S=0.0062 '/' Outflow=0.90 cfs 0.055 af
Pond C4: (new Pond)	Peak Elev=59.73' Inflow=6.47 cfs 0.415 af 12.0" Round Culvert n=0.010 L=116.0' S=0.0121 '/' Outflow=6.47 cfs 0.415 af
Pond C5: (new Pond)	Peak Elev=60.84' Inflow=6.41 cfs 0.410 af 12.0" Round Culvert n=0.010 L=99.0' S=0.0051 '/' Outflow=6.41 cfs 0.410 af

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Pond C7: (new Pond)	Peak Elev=59.36' Inflow=4.55 cts 0.289 at
	12.0" Round Culvert n=0.010 L=60.0' S=0.0050 '/' Outflow=4.55 cfs 0.289 af
Pond C8: (new Pond)	Peak Elev=59.41' Inflow=2.41 cfs 0.212 af
	12.0" Round Culvert n=0.010 L=100.0' S=0.0040 '/' Outflow=2.41 cfs 0.212 af
l ink 1l ·	Inflow=25.15 cfs 4.547 af
	Primary=25.15 cfs 4.547 af
l ink 21 ·	Inflow-13.99 cfs. 2.284 af
	Primary=13.99 cfs 2.284 af
Link 2L, AD2	Inflow-14.69 of a 1.145 of
LIIIK JL. AFJ	Primary=14.68 cfs 1.145 af
	· · · · · · · · · · · · · · · · · · ·
Total Runoff A	ea = 32.182 ac Runoff Volume = 8.698 af Average Runoff Depth = 3.24" 84.30% Pervious = 27.130 ac 15.70% Impervious = 5.052 ac

Summary for Subcatchment 1S: (new Subcat)

Runoff = 24.50 cfs @ 12.31 hrs, Volume= 2.517 af, Depth> 3.20"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

	Area (sf)	CN D	Description				
	1,054	98 F	Paved parking, HSG C				
	21,035	74 >	75% Ġras	s cover, Go	ood, HSG C		
*	22,365	98 E	xisting Im	pervious			
	206,487	77 V	Voods, Go	od, HSG D			
	159,791	70 V	Voods, Go	od, HSG C			
	410,732	75 V	Veighted A	verage			
	387,313	9	4.30% Pei	vious Area			
	23,419	5	.70% Impe	ervious Are	a		
To	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
6.5	50	0.0380	0.13		Sheet Flow,		
					Grass: Dense n= 0.240 P2= 3.00"		
15.9	1,128	0.0150	1.19	110.23	Trap/Vee/Rect Channel Flow,		
					Bot.W=90.00' D=1.00' Z= 3.0 '/' Top.W=96.00'		
					n= 0.150		
22.4	1,178	Total					

Summary for Subcatchment 2S: (new Subcat)

Runoff = 6.97 cfs @ 12.09 hrs, Volume= 0.475 af, Depth> 3.82"

	A	rea (sf)	CN [Description		
		47,342	74 >	>75% Gras	s cover, Go	bod, HSG C
*		17,695	98 F	Roads and	Houses	
		65,037	81 \	Neighted A	verage	
		47,342	7	72.79% Pei	vious Area	
		17,695	2	27.21% Imp	pervious Ar	ea
					- ·	
	ŢĊ	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	4.3	75	0.0980	0.29		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.00"
	1.1	73	0.0270	1.15		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.2	40	0.0270	4.36	13.07	Trap/Vee/Rect Channel Flow,
						Bot.W=4.50' D=0.50' Z= 3.0 '/' Top.W=7.50'
						n= 0.030 Earth, grassed & winding
	5.6	188	Total			

Summary for Subcatchment 3S: (new Subcat)

Runoff 3.15 cfs @ 12.07 hrs, Volume= 0.208 af, Depth> 3.82" =

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

	A	rea (sf)	CN [Description		
*		8,115	98 H	louses and	dRoads	
_		20,370	74 >	<u>>75% Gras</u>	<u>s cover, Go</u>	bod, HSG C
28,485 81 Weighted Average						
		20,370	7	71.51% Pei	rvious Area	
		8,115	2	28.49% Imp	pervious Ar	ea
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.5	60	0.1000	0.28		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.00"
	0.8	48	0.0210	1.01		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.4	87	0.0230	3.64	17.30	Trap/Vee/Rect Channel Flow,
						Bot.W=8.00' D=0.50' Z= 3.0 '/' Top.W=11.00'
						n= 0.035
	4.7	195	Total			

195 Lotal

Summary for Subcatchment 4S:

12.31 cfs @ 12.58 hrs, Volume= 1.653 af, Depth> 2.44" Runoff =

	A	rea (sf)	CN I	Description								
		2,560	98	Paved park	ing & roofs							
		75,951	55	Noods, Go	od, HSG B							
	2	07,144	70	Noods, Go	od, HSG C							
*		49,588	77	Noods, Go	od, HSG D,	Wetlands						
		18,542	61 :	>75% Gras	5% Grass cover, Good, HSG B							
	3	53,785	67	Neighted A	verage							
	3	51,225	9	99.28% Pe	rvious Area							
		2,560	().72% Impe	ervious Area	а						
	Тс	Length	Slope	Velocity	Capacity	Description						
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	28.7	74	0.0230	0.04		Sheet Flow,						
						Woods: Dense underbrush n= 0.800 P2= 3.00"						
	4.8	326	0.0520	1.14		Shallow Concentrated Flow,						
						Woodland Kv= 5.0 fps						
	6.9	531	0.0260	1.28	63.79	Trap/Vee/Rect Channel Flow, Wetland						
						Bot.W=30.00' D=1.00' Z= 20.0 '/' Top.W=70.00'						
						n= 0.150						

40.4 931 Total

Summary for Subcatchment 5S: (new Subcat)

Runoff = 1.18 cfs @ 12.06 hrs, Volume= 0.077 af, Depth> 4.34"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

	A	rea (sf)	CN	Description								
		4,609	74	>75% Grass cover, Good, HSG C								
*		4,712	98	Roads, Driv	veways							
		9,321	86	Weighted A	Veighted Average							
		4,609		49.45% Pervious Area								
		4,712		50.55% Impervious Area								
	Тс	Length	Slope	e Velocity	Capacity	Description						
(1	min)	(feet)	(ft/ft) (ft/sec)	(cfs)							
	3.3	50	0.0800	0.25		Sheet Flow,						
						Grass: Short n= 0.150 P2= 3.00"						
	0.8	77	0.0519	9 1.59		Shallow Concentrated Flow,						
						Short Grass Pasture Kv= 7.0 fps						
	4.1	127	Total									

Summary for Subcatchment 6S: (new Subcat)

Runoff = 1.05 cfs @ 12.01 hrs, Volume= 0.064 af, Depth> 4.14"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

	A	rea (sf)	CN	Description						
*		3,505	98	Roads, Driv	veways, Ho	uses				
		4,568	74	>75% Gras	s cover, Go	ood, HSG C				
		8,073	84	Weighted A	hted Average % Pervious Area					
		4,568		56.58% Pe	5.58% Pervious Area					
		3,505		3.42% Impervious Area						
(r	Tc	Length	Slope	e Velocity	Capacity	Description				
(I	nin)	(leet)	(11/11) (II/Sec)	(CIS)					
	0.8	90	0.066	′ 1.81		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps				

Summary for Subcatchment 7S: (new Subcat)

Runoff = 0.76 cfs @ 12.01 hrs, Volume= 0.047 af, Depth> 4.03"

Type III 24-hr 25 YEAR STORM Rainfall=6.20" Printed 4/20/2018

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	Area (sf)	CN		Description						
*	2,252	98	F	Roads, Driv	eways, Ho	uses				
	3,781	74	- >	75% Gras	s cover, Go	ood, HSG C				
	6,033	83	۶ V	Veighted A	verage					
	3,781		6	2.67% Pervious Area						
	2,252		З	37.33% Impervious Area						
(mi	Tc Lengt in) (feet	h Sl t) (ope ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
1	.0 10	2 0.0	588	1.70		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps				

Summary for Subcatchment 8S: (new Subcat)

Runoff = 0.90 cfs @ 12.02 hrs, Volume= 0.055 af, Depth> 3.93"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

_	A	rea (sf)	CN	Description								
*		2,585	98	Roads, Driv	ads, Driveways, Houses							
		4,752	74	>75% Gras	s cover, Go	ood, HSG C						
		7,337	82	Weighted A	verage							
		4,752		64.77% Pei	.77% Pervious Area							
		2,585		35.23% Imp	5.23% Impervious Area							
	Тс	Length	Slope	e Velocity	Capacity	Description						
	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)							
	1.2	99	0.0400) 1.40		Shallow Concentrated Flow,						
						Short Grass Pasture Kv= 7.0 fps						

Summary for Subcatchment 9S: (new Subcat)

Runoff = 1.48 cfs @ 12.01 hrs, Volume= 0.090 af, Depth> 4.13"

	Area	(sf)	CN	Description							
*	4,	541	98	Roads, Driv	veways, Ho	uses					
	6,	894	74	>75% Gras	s cover, Go	bod, HSG C					
	11,	435	84	Weighted A	ghted Average						
	6,	894		60.29% Pe	0.29% Pervious Area						
	4,	541		39.71% lmp	pervious Ar	ea					
(m	Tc Le in) (ength (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description					
1	1.0	102	0.058	8 1.70		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps					

Summary for Subcatchment 10S: (new Subcat)

Runoff = 6.62 cfs @ 12.11 hrs, Volume= 0.493 af, Depth> 4.23"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

_	A	rea (sf)	CN I	Description		
*		27,350	98 I	Roads, Hou	ises	
_		33,502	74 >	>75% Gras	s cover, Go	bod, HSG C
60,852 85 Weighted Average						
		33,502	Ę	55.05% Pei	vious Area	l de la constante de
27,350 44.95% Impervious Are						ea
	_		-			
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.1	50	0.0120	0.12		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.00"
	1.0	108	0.0720	1.88		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps

8.1 158 Total

Summary for Subcatchment 11S: (new Subcat)

Runoff = 3.04 cfs @ 12.11 hrs, Volume= 0.221 af, Depth> 4.02"

	A	rea (sf)	CN	Description						
		17,738	74	>75% Grass cover, Good, HSG C						
*		10,943	98	Houses AN	D Roads					
		28,681	83	Weighted A	verage					
17.738 61.85% Pervious Area										
10,943 38.15% Impervious Are						ea				
	Тс	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	3.5	60	0.1000	0.28		Sheet Flow,				
						Grass: Short n= 0.150 P2= 3.00"				
	0.3	42	0.0950	2.16		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	3.9	156	0.0090	0.66		Shallow Concentrated Flow,				
_						Short Grass Pasture Kv= 7.0 fps				
	7.7	258	Total							

Summary for Subcatchment 12S: (new Subcat)

Runoff = 3.20 cfs @ 12.07 hrs, Volume= 0.209 af, Depth> 3.72"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

	A	rea (sf)	CN	Description		
		22,056	74	>75% Gras	s cover, Go	ood, HSG C
*		7,281	98	Roads, Hor	nes	
		29,337	80	Weighted A	verage	
		22,056		75.18% Pe	rvious Area	
		7,281		24.82% Imp	pervious Ar	ea
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	4.3	70	0.0850	0.27		Sheet Flow,
	0.2	50	0 3200	3.06		Grass: Short n= 0.150 P2= 3.00"
	0.2	50	0.3200	5.90		Short Grass Pasture Kv= 7.0 fps
	4.5	120	Total			

Summary for Subcatchment 13S: 13S

Runoff	=	4.54 cfs @	12.09 hrs.	Volume=	0.315 af.	Depth>	4.02"
1 COLLON	_		12.001110,	volumo-	0.010 01,	Dopuiz	1.02

	Area (sf)	CN	Description
	25,002	74	>75% Grass cover, Good, HSG C
*	15,916	98	Roads and Homes
	40,918	83	Weighted Average
	25,002		61.10% Pervious Area
	15,916		38.90% Impervious Area

Tc in)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	35	0.0200	0.13	(0.0)	Sheet Flow,
	45	0.004.0	4.00		Grass: Short $n=0.150$ P2= 3.00"
).6	45	0.0310	1.23		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
).5	64	0.0050	1.97	1.38	Pipe Channel,
					12.0" Round w/ 2.0" inside fill Area= 0.7 sf Perim= 3.0' $r= 0.23$
).2	110	0.0360	7.41	185.31	Trap/Vee/Rect Channel Flow,
					Bot.W=22.00' D=1.00' Z= 3.0 '/' Top.W=28.00'
ר ר	46	0 0050	1 07	1 28	n= 0.035 Pine Channel
J. 4	40	0.0000	1.97	1.50	12.0" Round w/ 2.0" inside fill Area= 0.7 sf Perim= 3.0' $r= 0.23$ n= 0.020 Corrugated PE, corrugated interior
	Tc in) 1.4).6).5).2	Tc Length (feet) i.1 35 i.2 45 i.2 110 i.4 46	Tc Length (feet) Slope (ft/ft) in) (feet) (ft/ft) i.4 35 0.0200 0.6 45 0.0310 0.5 64 0.0050 0.2 110 0.0360 0.4 46 0.0050	Tc Length (feet) Slope (ft/ft) (ft/sec) in) (feet) (ft/ft) (ft/sec) i.4 35 0.0200 0.13 0.6 45 0.0310 1.23 0.5 64 0.0050 1.97 0.2 110 0.0360 7.41 0.4 46 0.0050 1.97	Tc Length (feet) Slope (ft/ft) Velocity (ft/sec) Capacity (cfs) in) (feet) (ft/ft) (ft/sec) (cfs) i.4 35 0.0200 0.13 0.6 45 0.0310 1.23 0.5 64 0.0050 1.97 1.38 0.2 110 0.0360 7.41 185.31 0.4 46 0.0050 1.97 1.38

6.1 300 Total

Summary for Subcatchment 14S: (new Subcat)

Runoff = 1.86 cfs @ 12.01 hrs, Volume= 0.121 af, Depth> 5.08"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

	A	rea (sf)	CN	Description							
*		10,929	98	3 Roads and Parking Lot							
		1,580	61	>75% Gras	s cover, Go	ood, HSG B					
		12,509 1,580 10,929	93	Weighted A 12.63% Pe 87.37% Imp	verage rvious Area pervious Ar	ea					
	Tc (min)	Length (feet)	Slope (ft/ft)	e Velocity (ft/sec)	Capacity (cfs)	Description					
	0.6	91	0.0175	2.69		Shallow Concentrated Flow, Paved Kv= 20.3 fps					
	0.5	99	0.0050) 3.21	2.52	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013 Corrugated PE, smooth interior					
	1.1	190	Total								

Summary for Subcatchment 15S: (new Subcat)

Runoff = 2.18 cfs @ 12.01 hrs, Volume= 0.140 af, Depth> 5.08"

_	A	rea (sf)	CN I	Description			
*		12,405	98 I	Roads and	Parking Lo	t	
		2,053	61 :	>75% Gras	s cover, Go	ood, HSG B	
14,458 93 Weighted Average							
		2,053		14.20% Pei	vious Area		
		12,405	8	35.80% Imp	pervious Ar	ea	
	Тс	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	0.6	91	0.0175	2.69		Shallow Concentrated Flow,	
						Paved Kv= 20.3 fps	
	0.2	29	0.0050	3.21	2.52	Pipe Channel,	
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'	
_						n= 0.013 Corrugated PE, smooth interior	
	0.8	120	Total				

Summary for Subcatchment 16S: (new Subcat)

Runoff = 2.37 cfs @ 12.01 hrs, Volume= 0.148 af, Depth> 4.87"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

	A	rea (sf)	CN	Description									
*		10,963	98	Roads and	Parking Lo	t							
		4,950	74	>75% Gras	5% Grass cover, Good, HSG C								
		15,913	91	Weighted A									
4,950 31.11% Pervious Area													
		10,963		68.89% lmp	pervious Are	ea							
	_												
	Тс	Length	Slope	Velocity	Capacity	Description							
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)								
	0.2	49	0.0280	3.40		Shallow Concentrated Flow,							
						Paved Kv= 20.3 fps							
	0.2	37	0.0060	3.51	2.76	Pipe Channel,							
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'							
						n= 0.013 Corrugated PE, smooth interior							
	0.4	86	Total										

Summary for Subcatchment 17S: (new Subcat)

Runoff = 1.92 cfs @ 12.09 hrs, Volume= 0.134 af, Depth> 4.13"

	A	rea (sf)	CN I	Description		
*		6,980	98	Roads and	Parking Lo	t
		9,966	/4 :	>75% Gras	s cover, Go	
		16,946	84	Weighted A	verage	
		9,966	ļ	58.81% Pei	rvious Area	
		6,980	4	41.19% lmp	pervious Are	ea
(r	Tc min)	Length	Slope	Velocity	Capacity	Description
	<u>100</u>		0 0220	0.17	(013)	Shaat Flow
	4.0	50	0.0320	0.17		Sheet Flow,
	~ 4	00	0 0000	0.50		Glass. Short $T = 0.150$ P2= 3.00
	0.4	82	0.0300	3.52		Shallow Concentrated Flow,
	~ ~					Paved Kv= 20.3 fps
	0.2	46	0.0220	3.52	14.97	Trap/Vee/Rect Channel Flow,
						Bot.W=7.00' D=0.50' Z= 3.0 '/' Top.W=10.00'
						n= 0.035
	0.4	95	0.0210	4.04	2.82	Pipe Channel,
						12.0" Round w/ 2.0" inside fill Area= 0.7 sf Perim= 3.0' r= 0.23'
						n= 0.020 Corrugated PE, corrugated interior
	0.3	103	0.0390	5.50	3.85	Pipe Channel,
						12.0" Round w/ 2.0" inside fill Area= 0.7 sf Perim= 3.0' r= 0.23'

n= 0.020 Corrugated PE, corrugated interior

6.1 376 Total

Summary for Subcatchment 18S: (new Subcat)

Runoff = 0.53 cfs @ 12.01 hrs, Volume= 0.036 af, Depth> 5.51"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

	A	rea (sf)	CN	Description			_					
*		3,382	98	98 Roads, Driveway, Parking Lot								
		3,382		100.00% In	npervious A	rea						
	Тс	Length	Slope	Velocity	Capacity	Description						
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	0.6	48	0.0050	1.44		Shallow Concentrated Flow, Paved Kv= 20.3 fps						

Summary for Subcatchment 19S: (new Subcat)

Runoff	=	14.68 cfs @	12.15 hrs,	Volume=	1.145 af, Depth> 3	3.02"
--------	---	-------------	------------	---------	--------------------	-------

	A	rea (sf)	CN D	Description		
*		1,275	98 F	Proposed D	riveway, H	SG C
		5,391	61 >	75% Gras	s cover, Go	ood, HSG B
*		13,416	98 E	Existing Ro	ad	
		51,460	77 V	Voods, Go	od, HSG D	
	1	13,902	70 V	Voods, Go	od, HSG C	
		12,421	55 V	Voods, Go	od, HSG B	
	1	97,865	73 V	Veighted A	verage	
	1	83,174	9	2.58% Pei	vious Area	
	14,691		7.42% Impervious Area			а
	Та	Longth	Clana	Valaaitu	Consoitu	Description
	(min)	(foot)	Siope		Capacity (ofc)	Description
	0.5	(1661)			(015)	Shoot Flow
	0.5	30	0.0200	1.05		Sneet riow, Smooth surfaces $n = 0.011$ $P2 = 2.00"$
	10	100	0.0570	1 67		Shallow Concentrated Flow
	1.0	100	0.0370	1.07		Short Grass Pasture, Ky 7.0 fps
	92	482	0.0110	0.87	56 45	Tran/Vee/Rect Channel Flow
	0.2	702	0.0110	0.07	00.40	Bot W=45 00' D=1 00' Z= 20 0 '/' Top W=85 00'
						n= 0.150
	10.7	612	Total			

Summary for Subcatchment 20S: (new Subcat)

Runoff = 0.16 cfs @ 12.01 hrs, Volume= 0.010 af, Depth> 4.35"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

Summary for Subcatchment 21S: (new Subcat)

Runoff = 2.19 cfs @ 12.01 hrs, Volume= 0.140 af, Depth> 5.08"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR STORM Rainfall=6.20"

	A	rea (sf)	CN	Description					
*		11,509	98	Lot and Ho	mes				
2,869 74 >75% Grass cover, Good, HSG C									
		14,378	93	Weighted A	verage				
		11,509		80.05% Imp	pervious Ar	ea			
	_								
	Tc	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft	(ft/sec)	(cfs)				
	0.2	49	0.0280	3.40		Shallow Concentrated Flow,			
						Paved Kv= 20.3 fps			
	0.3	65	0.0050	4.17	3.28	Pipe Channel,			
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
						n= 0.010 PVC, smooth interior			
	0 5	444	Tatal						

0.5 114 Total

Summary for Subcatchment 22S: (new Subcat)

Runoff = 0.45 cfs @ 12.01 hrs, Volume= 0.027 af, Depth> 3.82"

Type III 24-hr 25 YEAR STORM Rainfall=6.20" Printed 4/20/2018

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A	rea (sf)	CN	Description					
	1,062	98	Paved park	ing, HSG C				
	2,639	74	>75% Grass cover, Good, HSG C					
	3,701	81	Weighted A	verage				
	2,639		71.31% Pe	rvious Area				
	1,062		28.69% Imp	pervious Ar	ea			
Тс	l enath	Slone	Velocity	Canacity	Description			
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	Description			
0.6	51	0.0290) 1.35	(0.0)	Sheet Flow.			
0.0	•	0.0200			Smooth surfaces $n= 0.011 P2= 3.00"$			
0.1	39	0.0500) 4.54		Shallow Concentrated Flow,			
					Paved Kv= 20.3 fps			
0.1	21	0.0060) 3.51	2.76	Pipe Channel,			
					12.0" Round Area= 0.8 st Perim= 3.1' r= 0.25'			
	111	Total			n= 0.013 Corrugated PE, smooth Interior			
0.8	111	Total						
		c	Summary	for Subc	atchment 23S: (new Subcat)			
			Jummary					
Runoff	=	0.06 c	cfs @ 12.0	0 hrs. Volu	me= 0.004 af Depth> 5.51"			
		0100		0 1110, 1010				
Runoff b	y SCS TF	R-20 me	thod, UH=S	SCS, Time S	Span= 5.00-20.00 hrs, dt= 0.05 hrs			
Type III 2	24-hr 25	YEAR S	STORM Rai	nfall=6.20"				
٨			Decemination					
A	rea (sr)		Description		<u></u>			
	407	98	Paved park	ing, HSG C	/			
	407		100.00% Iff	ipervious A	irea			
Тс	l enath	Slope	Velocity	Canacity	Description			
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)				
0.2	32	0.0170) 2.65		Shallow Concentrated Flow,			
					Paved Kv= 20.3 fps			
		S	Summary	for Subc	atchment 24S: (new Subcat)			
Runoff	=	3.93 c	ofs @ 12.1	8 hrs, Volu	Ime= 0.327 af, Depth> 3.02"			
Dun off h) <u>)</u> 0 m a			Shah E 00 20 00 hra dt. 0 05 hra			
	y 303 17 21-br 25		STORM Rai	nfall_6.20"	5par = 5.00-20.00 ms, u = 0.05 ms			
Type III 2	24-111 23			111411-0.20				
Α	rea (sf)	CN	Description					
	10,637	74	>75% Gras	s cover, Go	ood, HSG C			
	2,780	98	Paved park	ing, HSG C				
	31,580	61	>75% Gras	s cover, Go	bod, HSG B			

 31,580
 61
 >75% Grass cover, Good, HSC

 11,552
 98
 Existing Road

 56,549
 73
 Weighted Average

 42,217
 74.66% Pervious Area

 14,332
 25.34% Impervious Area

The Homestead PRP					Type III 24-hr 25 YEAR STORM Rainfall=6.20"		
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	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
8.5	50	0.0200	0.10	· · ·	Sheet Flow,		
4.3	311	0.0300	1.21		Grass: Dense n= 0.240 P2= 3.00" Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps		
12.8	361	Total					
Summary for Subcatchment 25S: (new Subcat)							
Runoff	=	0.67 cfs	s@ 12.0	1 hrs, Volu	me= 0.042 af, Depth> 4.87"		
Runoff b Type III 2	y SCS TF 24-hr 25	R-20 meth YEAR ST	nod, UH=S FORM Rai	SCS, Time S nfall=6.20"	Span= 5.00-20.00 hrs, dt= 0.05 hrs		
Α	rea (sf)	CN D	escription				
	1,903 2,626	98 P 86 N	aved park lewly grad	ing, HSG C <u>ed area, HS</u>	; SG B		
	4,529 2,626 1,903	91 V 5 4	Veighted A 7.98% Pei 2.02% Imp	verage vious Area pervious Are	ea		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
0.4	50	0.0200	2.12		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps		
0.3	36	0.0050	1.97	1.38	Pipe Channel, 12.0" Round w/ 2.0" inside fill Area= 0.7 sf Perim= 3.0' n= 0.020 Corrugated PE, corrugated interior	r= 0	
0.7	86	Total					

Summary for Reach 1R: (new Reach)

 Inflow Area =
 1.008 ac, 32.36% Impervious, Inflow Depth > 3.89" for 25 YEAR STORM event

 Inflow =
 1.58 cfs @ 12.35 hrs, Volume=
 0.327 af

 Outflow =
 1.58 cfs @ 12.36 hrs, Volume=
 0.327 af, Atten= 0%, Lag= 0.4 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Max. Velocity= 1.82 fps, Min. Travel Time= 0.4 min Avg. Velocity = 0.93 fps, Avg. Travel Time= 0.7 min

Peak Storage= 35 cf @ 12.36 hrs Average Depth at Peak Storage= 0.02' Bank-Full Depth= 0.50' Flow Area= 32.5 sf, Capacity= 483.59 cfs

 $50.00' \times 0.50'$ deep channel, n= 0.030 Short grass Side Slope Z-value= 30.0 '/' Top Width= 80.00'Length= 40.0' Slope= 0.3000 '/' Inlet Invert= 50.00', Outlet Invert= 38.00'







Type III 24-hr 25 YEAR STORM Rainfall=6.20" Printed 4/20/2018

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Elevation (feet)		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)						
53.50		3,157	0	0						
55.0	00	4,520	5,758	5,758						
57.0	00	6,971	11,491	17,249						
59.0	00	10,099	17,070	34,319						
Device	Routing	Invert	Outlet Devices	i						
#1	Primary	51.03'	12.0" Round	Culvert						
	-		L= 46.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= $51.03' / 50.00'$ S= $0.0224 '/'$ Cc= 0.900 n= 0.013 Corrugated PE smooth interior Flow Area= 0.79 sf							
#2	Device 1	51.23'	6.0" Round C	ulvert						
			L= 10.0' CMF	, square edge	headwall, Ke= 0.500					
			Inlet / Outlet Invert= 51.23' / 51.13' S= 0.0100 '/' Cc= 0.900							
			n= 0.013 Corr	ugated PE, sm	ooth interior, Flow Area= 0.20 sf					
#3	Device 2	53.50'	2.40 cfs Exfiltration at all elevations							
#4	Device 1	55.00'	8.0" Vert. Orifice/Grate C= 0.600							
#5	Device 1	58.00'	Limited to weir	12.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads						

Primary OutFlow Max=1.58 cfs @ 12.35 hrs HW=54.26' (Free Discharge)

-1=Culvert (Passes 1.58 cfs of 6.25 cfs potential flow)

-2=Culvert (Inlet Controls 1.58 cfs @ 8.03 fps) -3=Exfiltration (Passes 1.58 cfs of 2.40 cfs potential flow)

-4=Orifice/Grate (Controls 0.00 cfs)

-5=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond 20P: (new Pond)

Inflow Are	ea =	2.108 ac, 31.80% Impervious, In	flow Depth > 3.93" for 2	25 YEAR STORM event
Inflow	=	9.81 cfs @ 12.07 hrs, Volume=	0.690 af	
Outflow	=	3.76 cfs @ 12.33 hrs, Volume=	0.565 af, Atten= 62	2%, Lag= 15.7 min
Primary	=	3.76 cfs @ 12.33 hrs, Volume=	0.565 af	-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 43.78' @ 12.33 hrs Surf.Area= 6,851 sf Storage= 11,106 cf

Plug-Flow detention time= 102.0 min calculated for 0.565 af (82% of inflow) Center-of-Mass det. time= 52.2 min (825.9 - 773.7)

Volume	Invert Av	/ail.Storage	Storage	e Description	
#1	41.50'	25,716 cf	Custon	n Stage Data (Pris	smatic)Listed below (Recalc)
Elevation (feet)	Surf.Are (sq-fi	a Inc :) (cubi	:.Store c-feet)	Cum.Store (cubic-feet)	
41.50	3,01	4	0	0	
43.00	5,40	4	6,314	6,314	
44.00	7,25	4	6,329	12,643	
45.50	10,17	7 [·]	13,073	25,716	

Type III 24-hr 25 YEAR STORM Rainfall=6.20"

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Device	Routing	Invert	Outlet Devices
#1	Primary	39.03'	12.0" Round Culvert
	-		L= 91.0' CMP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 39.03' / 38.00' S= 0.0113 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#2	Device 1	39.23'	6.0" Round Culvert
			L= 10.0' CMP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 39.23' / 39.13' S= 0.0100 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.20 sf
#3	Device 2	41.50'	2.400 in/hr Exfiltration over Surface area
#4	Device 1	43.00'	8.0" Vert. Orifice/Grate X 3.00 C= 0.600
#5	Device 1	45.67'	12.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Primary OutFlow Max=3.75 cfs @ 12.33 hrs HW=43.78' (Free Discharge)

-1=Culvert (Passes 3.75 cfs of 7.71 cfs potential flow)

2=Culvert (Passes 0.38 cfs of 1.96 cfs potential flow) **3=Exfiltration** (Exfiltration Controls 0.38 cfs)

-4=Orifice/Grate (Orifice Controls 3.37 cfs @ 3.22 fps)

-5=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond 30P: (new Pond)

Inflow .	Area =	3.064 ac, 51.95% Impervious, Inflow Dep	oth > 4.37" for 25 YEAR STORM event
Inflow	=	13.93 cfs @ 12.06 hrs, Volume= 1	1.116 af
Outflow	v =	5.56 cfs @ 12.35 hrs, Volume= 0	0.934 af, Atten= 60%, Lag= 17.7 min
Primar	y =	5.56 cfs @ 12.35 hrs, Volume= 0).934 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 45.36' @ 12.35 hrs Surf.Area= 7,931 sf Storage= 18,017 cf

Plug-Flow detention time= 91.3 min calculated for 0.934 af (84% of inflow) Center-of-Mass det. time= 44.1 min (806.3 - 762.2)

Volume	Invo	ert Avail.Sto	rage Storage	Description			
#1	42.5	50' 32,38	B7 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)		
Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
42.5	50	4,718	0	0			
44.(00	6,330	8,286	8,286			
46.0	00	8,677	15,007	23,293			
47.0	00	9,510	9,094	32,387			
Device	Routing	Invert	Outlet Devices	8			
#1	#1 Primary 40.03'		12.0" Round Culvert L= $63.5'$ CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= $40.03' / 38.00'$ S= $0.0320' / Cc= 0.900$ n= 0.013 Corrugated PE smooth interior. Flow Area= 0.79 sf				
#2 Device 1 40.23' 6.0" Round Culvert L= 20.0' CMP, square edge hear Inlet / Outlet Invert= 40.23' / 40.13		headwall, Ke= 0.500 0.13' S= 0.0050 '/' Cc= 0.900					

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			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.20 sf
#3	Device 2	42.50'	2.400 in/hr Exfiltration over Surface area
#4	Device 1	44.00'	8.0" Vert. Orifice/Grate X 3.00 C= 0.600
#5	Device 1	45.67'	12.0" Horiz. Orifice/Grate C= 0.600

45.67 Limited to weir flow at low heads

Primary OutFlow Max=5.56 cfs @ 12.35 hrs HW=45.36' (Free Discharge)

1=Culvert (Passes 5.56 cfs of 8.31 cfs potential flow)

-2=Culvert (Passes 0.44 cfs of 1.95 cfs potential flow) -3=Exfiltration (Exfiltration Controls 0.44 cfs)

-4=Orifice/Grate (Orifice Controls 5.12 cfs @ 4.89 fps)

-5=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond 31P: (new Pond)

Inflow Are	ea =	1.382 ac, 48.36% Impervious, Int	flow Depth > 4.27" for 25 YEAR STORM ev	ent
Inflow	=	6.49 cfs @ 12.06 hrs, Volume=	0.492 af	
Outflow	=	3.62 cfs @ 12.22 hrs, Volume=	0.402 af, Atten= 44%, Lag= 9.4 min	
Primary	=	3.62 cfs @ 12.22 hrs, Volume=	0.402 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 50.58' @ 12.22 hrs Surf.Area= 4,438 sf Storage= 7,263 cf

Plug-Flow detention time= 100.8 min calculated for 0.402 af (82% of inflow) Center-of-Mass det. time= 50.2 min (814.8 - 764.6)

Volume	Invert	Avail.Sto	rage	Storage D	Description	
#1	48.50'	14,30	00 cf	Custom S	Stage Data (P	rismatic)Listed below (Recalc)
Elevatio (fee	on Su et)	urf.Area (sq-ft)	Inc. (cubic	.Store c-feet)	Cum.Store (cubic-feet)	
48.5 50.0 52.0	50 00 00	2,400 4,000 5,500		0 4,800 9,500	0 4,800 14,300	
Device	Routing	Invert	Outle	et Devices		
#1	Primary	46.03'	12.0 L= 59 Inlet n= 0.	' Round (9.5' CMP / Outlet In 013 Corru	Culvert , square edge vert= 46.03' / 4 ugated PE, sm	headwall, Ke= 0.500 3.50' S= 0.0425 '/' Cc= 0.900 ooth interior, Flow Area= 0.79 sf
#2	Device 1	46.23'	6.0" Round Culvert L= 20.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 46.23' / 46.13' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.20 sf			headwall, Ke= 0.500 6.13' S= 0.0050 '/' Cc= 0.900 ooth interior, Flow Area= 0.20 sf
#3 #4 #5	Device 2 Device 1 Device 1	48.50' 50.00' 51.67'	 2.400 in/hr Exfiltration over Surface area 8.0" Vert. Orifice/Grate X 4.00 C= 0.600 12.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads 			

Primary OutFlow Max=3.58 cfs @ 12.22 hrs HW=50.58' (Free Discharge)

1=Culvert (Passes 3.58 cfs of 7.61 cfs potential flow)

-2=Culvert (Passes 0.25 cfs of 1.78 cfs potential flow)

3=Exfiltration (Exfiltration Controls 0.25 cfs)

-4=Orifice/Grate (Orifice Controls 3.34 cfs @ 2.59 fps)

-5=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond 40P: (new Pond)

Inflow Are	ea =	1.229 ac, 43.35% Imperviou	s, Inflow Depth > 4	.22" for 25 YE	EAR STORM event
Inflow	=	5.44 cfs @ 12.11 hrs, Volur	ne= 0.432 a	:	
Outflow	=	1.60 cfs @ 12.48 hrs, Volur	ne= 0.337 a	, Atten= 71%, I	Lag= 22.5 min
Primary	=	1.60 cfs @ 12.48 hrs, Volur	ne= 0.337 a	-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 60.48' @ 12.48 hrs Surf.Area= 5,944 sf Storage= 8,335 cf

Plug-Flow detention time= 133.9 min calculated for 0.336 af (78% of inflow) Center-of-Mass det. time= 78.3 min (845.7 - 767.4)

Volume	Inve	ert Avail.Sto	orage Storag	ge Description	
#1	58.0	0' 19,3	35 cf Custo	om Stage Data (P	rismatic)Listed below (Recalc)
Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
58.0 59.5 60.0 62.0)0 50)0)0	2,028 2,873 5,124 8,536	0 3,676 1,999 13,660	0 3,676 5,675 19,335	
Device	Routing	Invert	Outlet Devi	ces	
#1	Primary	56.03'	12.0" Rou L= 81.0' C Inlet / Outle n= 0.013 C	nd Culvert MP, square edge t Invert= 56.03' / 5 Corrugated PE, sm	headwall, Ke= 0.500 5.00' S= 0.0127 '/' Cc= 0.900 ooth interior. Flow Area= 0.79 sf
#2	Device 1	56.23'	6.0" Roun L= 20.0' C Inlet / Outle n= 0.013 C	d Culvert MP, square edge et Invert= 56.23' / 5 Corrugated PE, sm	headwall, Ke= 0.500 6.13' S= 0.0050 '/' Cc= 0.900 ooth interior. Flow Area= 0.20 sf
#3 #4 #5	Device 2 Device 1 Device 1	58.00' 60.00' 61.00'	2.400 in/hr 8.0" Vert. (12.0" Horiz Limited to v	Exfiltration over Drifice/Grate X 2.0 2. Orifice/Grate (veir flow at low heat	Surface area 00 C= 0.600 C= 0.600 ads

Primary OutFlow Max=1.60 cfs @ 12.48 hrs HW=60.48 (Free Discharge)

-1=Culvert (Passes 1.60 cfs of 6.63 cfs potential flow)

-2=Culvert (Passes 0.33 cfs of 1.76 cfs potential flow) -3=Exfiltration (Exfiltration Controls 0.33 cfs)

-4=Orifice/Grate (Orifice Controls 1.27 cfs @ 2.36 fps)

-5=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond C1: (new Pond)

Inflow Area =1.397 ac, 44.95% Impervious, Inflow Depth > 4.23" for 25 YEAR STORM eventInflow =6.62 cfs @ 12.11 hrs, Volume=0.493 afOutflow =6.62 cfs @ 12.11 hrs, Volume=0.493 af, Atten= 0%, Lag= 0.0 minPrimary =6.62 cfs @ 12.11 hrs, Volume=0.493 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 57.18' @ 12.11 hrs Flood Elev= 58.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	55.30'	15.0" Round Culvert L= 170.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 55.30' / 42.50' S= 0.0753 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=6.46 cfs @ 12.11 hrs HW=57.12' (Free Discharge) 1=Culvert (Inlet Controls 6.46 cfs @ 5.27 fps)

Summary for Pond C10: (new Pond)

Inflow Area	a =	0.493 ac, 4	1.36% Impe	ervious,	Inflow Depth >	4.29"	for 25	YEAR STOR	A event
Inflow	=	2.34 cfs @	12.07 hrs,	Volume	= 0.176	af			
Outflow	=	2.15 cfs @	12.11 hrs,	Volume	= 0.176	af, Atte	en= 8%,	Lag= 2.6 min	
Primary	=	2.15 cfs @	12.11 hrs,	Volume	= 0.176	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 59.69' @ 12.11 hrs Surf.Area= 590 sf Storage= 296 cf Flood Elev= 60.00' Surf.Area= 735 sf Storage= 504 cf

Plug-Flow detention time= 1.0 min calculated for 0.175 af (100% of inflow) Center-of-Mass det. time= 1.0 min (766.3 - 765.4)

Volume	Inv	ert Avail.Sto	orage	Storage D	escription	
#1	59.	00' 5	604 cf	Custom S	itage Data (Pi	rismatic)Listed below (Recalc)
Elevatio	on et)	Surf.Area (sq-ft)	Inc. (cubic	Store -feet)	Cum.Store (cubic-feet)	
59.0 60.0)0)0	272 735		0 504	0 504	
Device	Routing	Invert	Outle	t Devices		
#1	Primary	58.70'	12.0 " L= 10 Inlet / n= 0.9	' Round C 00.0' CMF / Outlet Inv 010 PVC,	ulvert 9, square edge ert= 58.70' / 5 smooth interio	e headwall, Ke= 0.500 8.40' S= 0.0030 '/' Cc= 0.900 or, Flow Area= 0.79 sf

Primary OutFlow Max=2.12 cfs @ 12.11 hrs HW=59.68' (Free Discharge) -1=Culvert (Barrel Controls 2.12 cfs @ 3.44 fps)

Summary for Pond C11: (new Pond)

Inflow Area = 0.365 ac, 68.89% Impervious, Inflow Depth > 4.87" for 25 YEAR STORM event Inflow 2.37 cfs @ 12.01 hrs. Volume= 0.148 af = 2.37 cfs @ 12.01 hrs, Volume= Outflow 0.148 af, Atten= 0%, Lag= 0.0 min = 2.37 cfs @ 12.01 hrs, Volume= Primary = 0.148 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 58.89' @ 12.00 hrs Flood Elev= 61.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	58.00'	12.0" Round Culvert L= 60.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 58.00' / 57.40' S= 0.0100 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.32 cfs @ 12.01 hrs HW=58.88' (Free Discharge) **1=Culvert** (Inlet Controls 2.32 cfs @ 3.19 fps)

Summary for Pond C12: (new Pond)

Inflow Area = 0.113 ac, 34.42% Impervious, Inflow Depth > 3.95" for 25 YEAR STORM event Inflow 0.62 cfs @ 12.01 hrs, Volume= 0.037 af = Outflow 0.62 cfs @ 12.01 hrs, Volume= 0.037 af, Atten= 0%, Lag= 0.0 min = 0.62 cfs @ 12.01 hrs. Volume= Primarv = 0.037 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 55.20' @ 12.01 hrs Flood Elev= 57.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	54.80'	12.0" Round Culvert L= 83.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 54.80' / 54.00' S= 0.0096 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.59 cfs @ 12.01 hrs HW=55.19' (Free Discharge) **1=Culvert** (Barrel Controls 0.59 cfs @ 3.11 fps)

Summary for Pond C13: (new Pond)

Inflow /	Area =	0.028 ac, 52.04% Impervious, Inflow	Depth > 4.35" for 25 YEAR STORM event
Inflow	=	0.16 cfs @ 12.01 hrs, Volume=	0.010 af
Outflow	v =	0.16 cfs @ 12.01 hrs, Volume=	0.010 af, Atten= 0%, Lag= 0.0 min
Primary	y =	0.16 cfs @ 12.01 hrs, Volume=	0.010 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 55.63' @ 12.01 hrs Flood Elev= 58.00'

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Device	Routing	Invert	Outlet Devices
#1	Primary	55.40'	12.0" Round Culvert L= 94.9' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= $55.40' / 54.90'$ S= $0.0053 '/$ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.16 cfs @ 12.01 hrs HW=55.63' (Free Discharge) ☐ 1=Culvert (Barrel Controls 0.16 cfs @ 1.80 fps)

Summary for Pond C14: (new Pond)

Inflow A	Area =	0.104 ac, 42.02% Impervious, Inflov	w Depth > 4.87" for 25 YEAR STORM	event
Inflow	=	0.67 cfs @ 12.01 hrs, Volume=	0.042 af	
Outflow	/ =	0.67 cfs @ 12.01 hrs, Volume=	0.042 af, Atten= 0%, Lag= 0.0 min	
Primary	/ =	0.67 cfs @ 12.01 hrs, Volume=	0.042 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 59.71' @ 12.01 hrs Flood Elev= 60.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	59.00'	12.0" Round Culvert L= 115.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 59.00' / 58.80' S= 0.0017 '/' Cc= 0.900 n= 0.020 Corrugated PE, corrugated interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.65 cfs @ 12.01 hrs HW=59.69' (Free Discharge) -1=Culvert (Barrel Controls 0.65 cfs @ 1.57 fps)

Summary for Pond C2: (new Pond)

Inflow Ar	ea =	0.330 ac, 80.05% Impervious, Inflow	w Depth > 5.08" for 25 YEAR STORM even	nt
Inflow	=	2.19 cfs @ 12.01 hrs, Volume=	0.140 af	
Outflow	=	2.19 cfs @ 12.01 hrs, Volume=	0.140 af, Atten= 0%, Lag= 0.0 min	
Primary	=	2.19 cfs @ 12.01 hrs, Volume=	0.140 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 57.04' @ 12.01 hrs Flood Elev= 60.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	56.20'	12.0" Round Culvert L= 119.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= $56.20' / 48.50' S = 0.0647 '/' Cc= 0.900$ n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.14 cfs @ 12.01 hrs HW=57.02' (Free Discharge) **1=Culvert** (Inlet Controls 2.14 cfs @ 3.09 fps)

Summary for Pond C3: (new Pond)

 Inflow Area =
 0.330 ac, 80.05% Impervious, Inflow Depth > 5.08" for 25 YEAR STORM event

 Inflow =
 2.19 cfs @ 12.01 hrs, Volume=
 0.140 af

 Outflow =
 2.19 cfs @ 12.01 hrs, Volume=
 0.140 af, Atten= 0%, Lag= 0.0 min

 Primary =
 2.19 cfs @ 12.01 hrs, Volume=
 0.140 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 57.60' @ 12.01 hrs Flood Elev= 62.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	56.60'	12.0" Round 0.0070 L= 62.5' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 56.60' / 56.40' S= 0.0032 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.14 cfs @ 12.01 hrs HW=57.58' (Free Discharge) **1=0.0070** (Barrel Controls 2.14 cfs @ 3.45 fps)

Summary for Pond C30: (new Pond)

 Inflow Area =
 0.214 ac, 50.55% Impervious, Inflow Depth > 4.34" for 25 YEAR STORM event

 Inflow =
 1.18 cfs @ 12.06 hrs, Volume=
 0.077 af

 Outflow =
 1.18 cfs @ 12.06 hrs, Volume=
 0.077 af, Atten= 0%, Lag= 0.0 min

 Primary =
 1.18 cfs @ 12.06 hrs, Volume=
 0.077 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 55.87' @ 12.06 hrs Flood Elev= 57.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	55.30'	12.0" Round Culvert L= 29.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 55.30' / 55.00' S= 0.0103 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.14 cfs @ 12.06 hrs HW=55.86' (Free Discharge) ←1=Culvert (Barrel Controls 1.14 cfs @ 3.65 fps)

Summary for Pond C31: (new Pond)

Inflow Are	ea =	0.615 ac, 42.95% Impervious, Inflow Depth > 4.18" for 25 YEAR STORM even	ent
Inflow	=	3.24 cfs @ 12.03 hrs, Volume= 0.214 af	
Outflow	=	3.24 cfs @ 12.03 hrs, Volume= 0.214 af, Atten= 0%, Lag= 0.0 min	
Primary	=	3.24 cfs @ 12.03 hrs, Volume= 0.214 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 55.93' @ 12.03 hrs Flood Elev= 57.00'

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Device	Routing	Invert	Outlet Devices
#1	Primary	54.70'	12.0" Round Culvert L= 127.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 54.70' / 43.00' S= 0.0921 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=3.13 cfs @ 12.03 hrs HW=55.88' (Free Discharge) -1=Culvert (Inlet Controls 3.13 cfs @ 3.98 fps)

Summary for Pond C32: (new Pond)

Inflow .	Area =	0.354 ac, 39.52% Impervious, Inflo	ow Depth > 4.04"	for 25 YEAR STORM event
Inflow	=	1.95 cfs @ 12.01 hrs, Volume=	0.119 af	
Outflow	v =	1.95 cfs @ 12.01 hrs, Volume=	0.119 af, Atte	en= 0%, Lag= 0.0 min
Primar	y =	1.95 cfs @ 12.01 hrs, Volume=	0.119 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 58.87' @ 12.01 hrs Flood Elev= 59.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	58.10'	12.0" Round Culvert L= 65.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= $58.10' / 53.50'$ S= 0.0708 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.86 cfs @ 12.01 hrs HW=58.85' (Free Discharge) **1=Culvert** (Inlet Controls 1.86 cfs @ 2.95 fps)

Summary for Pond C33: (new Pond)

Inflow Area	a =	0.263 ac, 39.7	1% Impervious,	Inflow Depth >	4.13" for 25	5 YEAR STORM event
Inflow	=	1.48 cfs @ 12	01 hrs, Volume	e 0.090	af	
Outflow	=	1.48 cfs @ 12	01 hrs, Volume	e= 0.090	af, Atten= 0%	, Lag= 0.0 min
Primary	=	1.48 cfs @ 12	01 hrs, Volume	e= 0.090	af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 55.85' @ 12.01 hrs Flood Elev= 56.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	55.20'	12.0" Round Culvert L= 45.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= $55.20' / 54.80' = 0.0089 '/' Cc= 0.900$ n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.41 cfs @ 12.01 hrs HW=55.83' (Free Discharge) **1=Culvert** (Inlet Controls 1.41 cfs @ 2.70 fps)

Summary for Pond C34: (new Pond)

Inflow Area = 0.168 ac, 35.23% Impervious, Inflow Depth > 3.93" for 25 YEAR STORM event Inflow 0.90 cfs @ 12.02 hrs. Volume= 0.055 af = 0.90 cfs @ 12.02 hrs, Volume= Outflow 0.055 af, Atten= 0%, Lag= 0.0 min = 0.90 cfs @ 12.02 hrs, Volume= 0.055 af Primary =

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 59.01' @ 12.02 hrs Flood Elev= 60.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	58.50'	12.0" Round Culvert L= 48.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 58.50' / 58.20' S= 0.0062 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.86 cfs @ 12.02 hrs HW=59.00' (Free Discharge) 1=Culvert (Barrel Controls 0.86 cfs @ 3.20 fps)

Summary for Pond C4: (new Pond)

Inflow /	Area =	0.994 ac, 80.17% Impervious, In	flow Depth > 5.01" for 25 YE	AR STORM event
Inflow	=	6.47 cfs @ 12.01 hrs, Volume=	0.415 af	
Outflow	/ =	6.47 cfs @ 12.01 hrs, Volume=	0.415 af, Atten= 0%, La	g= 0.0 min
Primary	/ =	6.47 cfs @ 12.01 hrs, Volume=	0.415 af	-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 59.73' @ 12.01 hrs Flood Elev= 62.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	56.30'	12.0" Round Culvert L= 116.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 56.30' / 54.90' S= 0.0121 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=6.28 cfs @ 12.01 hrs HW=59.55' (Free Discharge) -1=Culvert (Inlet Controls 6.28 cfs @ 7.99 fps)

Summary for Pond C5: (new Pond)

Inflow A	rea =	0.984 ac, 79.98% Impervious, Infl	ow Depth > 5.00"	for 25 YEAR STORM event
Inflow	=	6.41 cfs @ 12.01 hrs, Volume=	0.410 af	
Outflow	=	6.41 cfs @ 12.01 hrs, Volume=	0.410 af, Atte	en= 0%, Lag= 0.0 min
Primary	=	6.41 cfs @ 12.01 hrs, Volume=	0.410 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 60.84' @ 12.01 hrs Flood Elev= 62.00'

Type III 24-hr 25 YEAR STORM Rainfall=6.20" Printed 4/20/2018

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Device	Routing	Invert	Outlet Devices
#1	Primary	56.90'	12.0" Round Culvert L= 99.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= $56.90' / 56.40'$ S= $0.0051'/$ Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=6.20 cfs @ 12.01 hrs HW=60.63' (Free Discharge) ☐ 1=Culvert (Barrel Controls 6.20 cfs @ 7.90 fps)

Summary for Pond C7: (new Pond)

Inflow /	Area =	0.697 ac, 76.94% Impervious	, Inflow Depth > 4.97	for 25 YEAR STORM event
Inflow	=	4.55 cfs @ 12.01 hrs, Volum	e= 0.289 af	
Outflow	/ =	4.55 cfs @ 12.01 hrs, Volum	e= 0.289 af, A	tten= 0%, Lag= 0.0 min
Primar	/ =	4.55 cfs @ 12.01 hrs, Volum	e= 0.289 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 59.36' @ 12.01 hrs Flood Elev= 61.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	57.30'	12.0" Round Culvert L= $60.0'$ CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= $57.30' / 57.00'$ S= $0.0050'/'$ Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=4.43 cfs @ 12.01 hrs HW=59.29' (Free Discharge) **1=Culvert** (Barrel Controls 4.43 cfs @ 5.64 fps)

Summary for Pond C8: (new Pond)

Inflow Area	a =	0.571 ac, 4	49.34% Impe	ervious,	Inflow Depth >	4.45"	for 25	YEAR STORM even	nt
Inflow	=	2.41 cfs @	12.09 hrs,	Volume	= 0.212	af			
Outflow	=	2.41 cfs @	12.09 hrs,	Volume	= 0.212	af, Atte	n= 0%,	Lag= 0.0 min	
Primary	=	2.41 cfs @	12.09 hrs,	Volume	= 0.212	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 59.41' @ 12.09 hrs Flood Elev= 62.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	58.40'	12.0" Round Culvert L= 100.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 58.40' / 58.00' S= 0.0040 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.40 cfs @ 12.09 hrs HW=59.41' (Free Discharge) ←1=Culvert (Barrel Controls 2.40 cfs @ 3.78 fps)

Summary for Link 1L:

 Inflow Area =
 17.282 ac, 21.97% Impervious, Inflow Depth > 3.16" for 25 YEAR STORM event

 Inflow =
 25.15 cfs @ 12.31 hrs, Volume=
 4.547 af

 Primary =
 25.15 cfs @ 12.31 hrs, Volume=
 4.547 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Link 2L:

Inflow A	Area =	10.359 ac,	8.86% Impervious, Inflow	Depth > 2.65"	for 25 YEAR STORM event
Inflow	=	13.99 cfs @	12.58 hrs, Volume=	2.284 af	
Primary	/ =	13.99 cfs @	12.58 hrs, Volume=	2.284 af, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Link 3L: AP3

Inflow /	Area =	4.542 ac,	7.42% Impervious, Inflow I	Depth > 3.02"	for 25 YEAR STORM event
Inflow	=	14.68 cfs @	12.15 hrs, Volume=	1.145 af	
Primary	y =	14.68 cfs @	12.15 hrs, Volume=	1.145 af, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

The Homestead PRP	Type III 24-hr 2 YEAR STORM Rainfall=3.30
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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1S: (new Subcat)	Runoff Area=410,732 sf 5.70% Impervious Runoff Depth>1.06" ow Length=1,178' Tc=22.4 min CN=75 Runoff=7.88 cfs 0.830 af
Subcatchment 2S: (new Subcat)	Runoff Area=65,037 sf 27.21% Impervious Runoff Depth>1.43" Flow Length=188' Tc=5.6 min CN=81 Runoff=2.67 cfs 0.178 af
Subcatchment3S: (new Subcat)	Runoff Area=28,485 sf 28.49% Impervious Runoff Depth>1.43" Flow Length=195' Tc=4.7 min CN=81 Runoff=1.20 cfs 0.078 af
Subcatchment 4S:	Runoff Area=353,785 sf 0.72% Impervious Runoff Depth>0.65" Flow Length=931' Tc=40.4 min CN=67 Runoff=2.95 cfs 0.441 af
Subcatchment5S: (new Subcat)	Runoff Area=9,321 sf 50.55% Impervious Runoff Depth>1.80" Flow Length=127' Tc=4.1 min CN=86 Runoff=0.50 cfs 0.032 af
Subcatchment 6S: (new Subcat) Flow Length=90	Runoff Area=8,073 sf 43.42% Impervious Runoff Depth>1.65" O' Slope=0.0667 '/' Tc=0.8 min CN=84 Runoff=0.43 cfs 0.025 af
Subcatchment 7S: (new Subcat) Flow Length=102	Runoff Area=6,033 sf 37.33% Impervious Runoff Depth>1.58" 2' Slope=0.0588 '/' Tc=1.0 min CN=83 Runoff=0.31 cfs 0.018 af
Subcatchment 8S: (new Subcat) Flow Length=99	Runoff Area=7,337 sf 35.23% Impervious Runoff Depth>1.50" 9' Slope=0.0400 '/' Tc=1.2 min CN=82 Runoff=0.35 cfs 0.021 af
Subcatchment 9S: (new Subcat) Flow Length=102	Runoff Area=11,435 sf 39.71% Impervious Runoff Depth>1.65" 2' Slope=0.0588 '/' Tc=1.0 min CN=84 Runoff=0.60 cfs 0.036 af
Subcatchment10S: (new Subcat)	Runoff Area=60,852 sf 44.95% Impervious Runoff Depth>1.72" Flow Length=158' Tc=8.1 min CN=85 Runoff=2.77 cfs 0.200 af
Subcatchment11S: (new Subcat)	Runoff Area=28,681 sf 38.15% Impervious Runoff Depth>1.57" Flow Length=258' Tc=7.7 min CN=83 Runoff=1.21 cfs 0.086 af
Subcatchment12S: (new Subcat)	Runoff Area=29,337 sf 24.82% Impervious Runoff Depth>1.37" Flow Length=120' Tc=4.5 min CN=80 Runoff=1.19 cfs 0.077 af
Subcatchment13S:13S	Runoff Area=40,918 sf 38.90% Impervious Runoff Depth>1.57" Flow Length=300' Tc=6.1 min CN=83 Runoff=1.82 cfs 0.123 af
Subcatchment14S: (new Subcat)	Runoff Area=12,509 sf 87.37% Impervious Runoff Depth>2.40" Flow Length=190' Tc=1.1 min CN=93 Runoff=0.92 cfs 0.058 af
Subcatchment15S: (new Subcat)	Runoff Area=14,458 sf 85.80% Impervious Runoff Depth>2.40" Flow Length=120' Tc=0.8 min CN=93 Runoff=1.07 cfs 0.067 af
Subcatchment16S: (new Subcat)	Runoff Area=15,913 sf 68.89% Impervious Runoff Depth>2.22" Flow Length=86' Tc=0.4 min CN=91 Runoff=1.13 cfs 0.068 af
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Type III 24-hr 2 YEAR STORM Rainfall=3.30" Printed 4/20/2018

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Subcatchment 17S: (new Subca	Runoff Area=16,946 sf 41.19% Impervious Runoff Depth>1.64" Flow Length=376' Tc=6.1 min CN=84 Runoff=0.79 cfs 0.053 af
Subcatchment 18S: (new Subca Flow	ht Runoff Area=3,382 sf 100.00% Impervious Runoff Depth>2.87" v Length=48' Slope=0.0050 '/' Tc=0.6 min CN=98 Runoff=0.28 cfs 0.019 af
Subcatchment 19S: (new Subca	t) Runoff Area=197,865 sf 7.42% Impervious Runoff Depth>0.95" Flow Length=612' Tc=10.7 min CN=73 Runoff=4.44 cfs 0.360 af
Subcatchment 20S: (new Subca Flow	Runoff Area=1,203 sf 52.04% Impervious Runoff Depth>1.80" Length=51' Slope=0.0290 '/' Tc=0.6 min CN=86 Runoff=0.07 cfs 0.004 af
Subcatchment 21S: (new Subca	t) Runoff Area=14,378 sf 80.05% Impervious Runoff Depth>2.40" Flow Length=114' Tc=0.5 min CN=93 Runoff=1.08 cfs 0.066 af
Subcatchment 22S: (new Subca	t) Runoff Area=3,701 sf 28.69% Impervious Runoff Depth>1.44" Flow Length=111' Tc=0.8 min CN=81 Runoff=0.17 cfs 0.010 af
Subcatchment 23S: (new Subca Flow	t) Runoff Area=407 sf 100.00% Impervious Runoff Depth>2.87" Length=32' Slope=0.0170 '/' Tc=0.2 min CN=98 Runoff=0.03 cfs 0.002 af
Subcatchment 24S: (new Subca	t) Runoff Area=56,549 sf 25.34% Impervious Runoff Depth>0.95" Flow Length=361' Tc=12.8 min CN=73 Runoff=1.19 cfs 0.103 af
Subcatchment 25S: (new Subca	t) Runoff Area=4,529 sf 42.02% Impervious Runoff Depth>2.22" Flow Length=86' Tc=0.7 min CN=91 Runoff=0.32 cfs 0.019 af
Reach 1R: (new Reach)	Avg. Flow Depth=0.02' Max Vel=1.72 fps Inflow=1.38 cfs 0.125 af 0.030 L=40.0' S=0.3000 '/' Capacity=483.59 cfs Outflow=1.38 cfs 0.125 af
Reach 2R: (new Reach) n=0	Avg. Flow Depth=0.05' Max Vel=0.21 fps Inflow=1.07 cfs 0.540 af .150 L=700.0' S=0.0257 '/' Capacity=156.29 cfs Outflow=0.91 cfs 0.442 af
Reach 3R: (new Reach) n=0	Avg. Flow Depth=0.02' Max Vel=0.11 fps Inflow=0.21 cfs 0.157 af .150 L=850.0' S=0.0212 '/' Capacity=141.83 cfs Outflow=0.20 cfs 0.088 af
Reach 4R: (new Reach) n=0	Avg. Flow Depth=0.02' Max Vel=0.12 fps Inflow=0.18 cfs 0.125 af .150 L=531.0' S=0.0301 '/' Capacity=169.18 cfs Outflow=0.17 cfs 0.093 af
Reach 5R: (new Reach)	Avg. Flow Depth=0.02' Max Vel=0.82 fps Inflow=0.24 cfs 0.014 af =0.030 L=95.0' S=0.0558 '/' Capacity=63.43 cfs Outflow=0.22 cfs 0.014 af
Reach 6R: (new Reach) n=0.1	Avg. Flow Depth=0.02' Max Vel=0.09 fps Inflow=1.19 cfs 0.103 af 50 L=1,128.0' S=0.0160 '/' Capacity=123.12 cfs Outflow=0.17 cfs 0.054 af
Pond 10P: (new Pond)	Peak Elev=53.60' Storage=307 cf Inflow=1.87 cfs 0.125 af Outflow=1.38 cfs 0.125 af
Pond 20P: (new Pond)	Peak Elev=42.88' Storage=5,663 cf Inflow=3.84 cfs 0.265 af Outflow=0.29 cfs 0.201 af
Pond 30P: (new Pond)	Peak Elev=44.20' Storage=9,606 cf Inflow=6.00 cfs 0.471 af Outflow=0.79 cfs 0.339 af

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Pond 31P: (new Pond)	Peak Elev=49.87' Storage=4,280 cf Inflow=2.72 cfs 0.204 af Outflow=0.21 cfs 0.157 af
Pond 40P: (new Pond)	Peak Elev=59.57' Storage=3,880 cf Inflow=2.28 cfs 0.177 af Outflow=0.18 cfs 0.125 af
Pond C1: (new Pond)	Peak Elev=56.15' Inflow=2.77 cfs 0.200 af 15.0" Round Culvert n=0.010 L=170.0' S=0.0753 '/' Outflow=2.77 cfs 0.200 af
Pond C10: (new Pond)	Peak Elev=59.28' Storage=95 cf Inflow=0.99 cfs 0.073 af 12.0" Round Culvert n=0.010 L=100.0' S=0.0030 '/' Outflow=0.93 cfs 0.073 af
Pond C11: (new Pond)	Peak Elev=58.55' Inflow=1.13 cfs 0.068 af 12.0" Round Culvert n=0.010 L=60.0' S=0.0100 '/' Outflow=1.13 cfs 0.068 af
Pond C12: (new Pond)	Peak Elev=55.04' Inflow=0.24 cfs 0.014 af 12.0" Round Culvert n=0.013 L=83.0' S=0.0096 '/' Outflow=0.24 cfs 0.014 af
Pond C13: (new Pond)	Peak Elev=55.55' Inflow=0.07 cfs 0.004 af 12.0" Round Culvert n=0.013 L=94.9' S=0.0053 '/' Outflow=0.07 cfs 0.004 af
Pond C14: (new Pond)	Peak Elev=59.48' Inflow=0.32 cfs 0.019 af 12.0" Round Culvert n=0.020 L=115.0' S=0.0017 '/' Outflow=0.32 cfs 0.019 af
Pond C2: (new Pond)	Peak Elev=56.74' Inflow=1.08 cfs 0.066 af 12.0" Round Culvert n=0.010 L=119.0' S=0.0647 '/' Outflow=1.08 cfs 0.066 af
Pond C3: (new Pond)	Peak Elev=57.24' Inflow=1.08 cfs 0.066 af 12.0" Round Culvert n=0.010 L=62.5' S=0.0032 '/' Outflow=1.08 cfs 0.066 af
Pond C30: (new Pond)	Peak Elev=55.65' Inflow=0.50 cfs 0.032 af 12.0" Round Culvert n=0.010 L=29.0' S=0.0103 '/' Outflow=0.50 cfs 0.032 af
Pond C31: (new Pond)	Peak Elev=55.31' Inflow=1.35 cfs 0.086 af 12.0" Round Culvert n=0.010 L=127.0' S=0.0921 '/' Outflow=1.35 cfs 0.086 af
Pond C32: (new Pond)	Peak Elev=58.55' Inflow=0.78 cfs 0.047 af 12.0" Round Culvert n=0.010 L=65.0' S=0.0708 '/' Outflow=0.78 cfs 0.047 af
Pond C33: (new Pond)	Peak Elev=55.59' Inflow=0.60 cfs 0.036 af 12.0" Round Culvert n=0.010 L=45.0' S=0.0089 '/' Outflow=0.60 cfs 0.036 af
Pond C34: (new Pond)	Peak Elev=58.80' Inflow=0.35 cfs 0.021 af 12.0" Round Culvert n=0.010 L=48.0' S=0.0062 '/' Outflow=0.35 cfs 0.021 af
Pond C4: (new Pond)	Peak Elev=57.49' Inflow=3.15 cfs 0.194 af 12.0" Round Culvert n=0.010 L=116.0' S=0.0121 '/' Outflow=3.15 cfs 0.194 af
Pond C5: (new Pond)	Peak Elev=58.10' Inflow=3.12 cfs 0.192 af 12.0" Round Culvert n=0.010 L=99.0' S=0.0051 '/' Outflow=3.12 cfs 0 192 af

The Homestead PRP	Type III 24-hr 2 YEAR STORM Rainfall=3.30"
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Pond C7: (new Pond)	Peak Elev=58.23' Inflow=2.20 cfs 0.134 af
	12.0" Round Culvert n=0.010 L=60.0' S=0.0050 '/' Outflow=2.20 cfs 0.134 af
Pond C8: (new Pond)	Peak Elev=59.00' Inflow=1.07 cfs 0.091 af
	12.0" Round Culvert n=0.010 L=100.0' S=0.0040 '/' Outflow=1.07 cfs 0.091 af
Link 11 ·	Inflow-8 15 cfs 1 414 af
	Primary=8.15 cfs 1.414 af
Link 2L:	Inflow=3.30 cfs 0.658 af
	Primary=3.30 cfs 0.658 af
Link 3L: AP3	Inflow=4.44 cfs 0.360 af
	Primary=4.44 cfs 0.360 af
Total Runoff A	rea = 32.182 ac Runoff Volume = 2.975 af Average Runoff Depth = 1.11" 84.30% Pervious = 27.130 ac 15.70% Impervious = 5.052 ac

The Homestead PRP	Type III 24-hr	10 YEAR STORM Rair	nfall=4.90"
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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: (new Subcat)	Runoff Area=410,732 sf 5.70% Impervious Runoff Depth>2.18" v Length=1,178' Tc=22.4 min CN=75 Runoff=16.71 cfs 1.715 af
Subcatchment2S: (new Subcat)	Runoff Area=65,037 sf 27.21% Impervious Runoff Depth>2.71" Flow Length=188' Tc=5.6 min CN=81 Runoff=5.01 cfs 0.337 af
Subcatchment3S: (new Subcat)	Runoff Area=28,485 sf 28.49% Impervious Runoff Depth>2.71" Flow Length=195' Tc=4.7 min CN=81 Runoff=2.26 cfs 0.148 af
Subcatchment 4S:	Runoff Area=353,785 sf 0.72% Impervious Runoff Depth>1.56" Flow Length=931' Tc=40.4 min CN=67 Runoff=7.75 cfs 1.058 af
Subcatchment5S: (new Subcat)	Runoff Area=9,321 sf 50.55% Impervious Runoff Depth>3.18" Flow Length=127' Tc=4.1 min CN=86 Runoff=0.87 cfs 0.057 af
Subcatchment 6S: (new Subcat) Flow Length=90	Runoff Area=8,073 sf 43.42% Impervious Runoff Depth>2.99" ' Slope=0.0667 '/' Tc=0.8 min CN=84 Runoff=0.77 cfs 0.046 af
Subcatchment 7S: (new Subcat) Flow Length=102	Runoff Area=6,033 sf 37.33% Impervious Runoff Depth>2.89" ' Slope=0.0588 '/' Tc=1.0 min CN=83 Runoff=0.56 cfs 0.033 af
Subcatchment 8S: (new Subcat) Flow Length=99	Runoff Area=7,337 sf 35.23% Impervious Runoff Depth>2.80" ' Slope=0.0400 '/' Tc=1.2 min CN=82 Runoff=0.65 cfs 0.039 af
Subcatchment9S: (new Subcat) Flow Length=102	Runoff Area=11,435 sf 39.71% Impervious Runoff Depth>2.99" ' Slope=0.0588 '/' Tc=1.0 min CN=84 Runoff=1.08 cfs 0.065 af
Subcatchment10S: (new Subcat)	Runoff Area=60,852 sf 44.95% Impervious Runoff Depth>3.08" Flow Length=158' Tc=8.1 min CN=85 Runoff=4.88 cfs 0.358 af
Subcatchment11S: (new Subcat)	Runoff Area=28,681 sf 38.15% Impervious Runoff Depth>2.89" Flow Length=258' Tc=7.7 min CN=83 Runoff=2.21 cfs 0.159 af
Subcatchment 12S: (new Subcat)	Runoff Area=29,337 sf 24.82% Impervious Runoff Depth>2.62" Flow Length=120' Tc=4.5 min CN=80 Runoff=2.28 cfs 0.147 af
Subcatchment 13S: 13S	Runoff Area=40,918 sf 38.90% Impervious Runoff Depth>2.89" Flow Length=300' Tc=6.1 min CN=83 Runoff=3.30 cfs 0.226 af
Subcatchment 14S: (new Subcat)	Runoff Area=12,509 sf 87.37% Impervious Runoff Depth>3.88" Flow Length=190' Tc=1.1 min CN=93 Runoff=1.44 cfs 0.093 af
Subcatchment15S: (new Subcat)	Runoff Area=14,458 sf 85.80% Impervious Runoff Depth>3.88" Flow Length=120' Tc=0.8 min CN=93 Runoff=1.69 cfs 0.107 af
Subcatchment16S: (new Subcat)	Runoff Area=15,913 sf 68.89% Impervious Runoff Depth>3.68" Flow Length=86' Tc=0.4 min CN=91 Runoff=1.82 cfs 0.112 af

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Type III 24-hr 10 YEAR STORM Rainfall=4.90"

Flow Length=111' Tc=0.8 min CN=81 Runoff=0.32 cfs 0.019 af

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Subcatchment17S: (new Subcat)	Runoff Area=16,946 sf 41.19% Impervious Runoff Depth>2.98" Flow Length=376' Tc=6.1 min CN=84 Runoff=1.41 cfs 0.097 af						
Subcatchment 18S: (new Subcat) Flow Length=48'	Runoff Area=3,382 sf 100.00% Impervious Runoff Depth>4.33" Slope=0.0050 '/' Tc=0.6 min CN=98 Runoff=0.42 cfs 0.028 af						
Subcatchment 19S: (new Subcat)	Runoff Area=197,865 sf 7.42% Impervious Runoff Depth>2.03" ow Length=612' Tc=10.7 min CN=73 Runoff=9.84 cfs 0.769 af						
Subcatchment 20S: (new Subcat) Flow Length=51'	Runoff Area=1,203 sf 52.04% Impervious Runoff Depth>3.18" Slope=0.0290 '/' Tc=0.6 min CN=86 Runoff=0.12 cfs 0.007 af						
Subcatchment21S: (new Subcat)	Runoff Area=14,378 sf 80.05% Impervious Runoff Depth>3.88"						

Flow Length=114'Tc=0.5 minCN=93Runoff=1.70 cfs0.107 afSubcatchment 22S: (new Subcat)Runoff Area=3,701 sf28.69% ImperviousRunoff Depth>2.71"

Subcatchment 23S: (new Subcat) Flow Length=32' Slope=0.0170 '/ Tc=0.2 min CN=98 Runoff=0.05 cfs 0.003 af

Subcatchment 24S: (new Subcat)Runoff Area=56,549 sf25.34% ImperviousRunoff Depth>2.03"Flow Length=361'Tc=12.8 minCN=73Runoff=2.63 cfs0.220 af

Subcatchment 25S: (new Subcat)Runoff Area=4,529 sf42.02% ImperviousRunoff Depth>3.68"Flow Length=86'Tc=0.7 minCN=91Runoff=0.51 cfs0.032 af

 Reach 1R: (new Reach)
 Avg. Flow Depth=0.02'
 Max Vel=1.77 fps
 Inflow=1.47 cfs
 0.233 af

 n=0.030
 L=40.0'
 S=0.3000 '/'
 Capacity=483.59 cfs
 Outflow=1.47 cfs
 0.233 af

 Reach 2R: (new Reach)
 Avg. Flow Depth=0.12'
 Max Vel=0.38 fps
 Inflow=5.84 cfs
 1.039 af

 n=0.150
 L=700.0'
 S=0.0257 '/'
 Capacity=156.29 cfs
 Outflow=4.19 cfs
 0.957 af

- Reach 3R: (new Reach)
 Avg. Flow Depth=0.04'
 Max Vel=0.17 fps
 Inflow=1.69 cfs
 0.282 af

 n=0.150
 L=850.0'
 S=0.0212 '/'
 Capacity=141.83 cfs
 Outflow=0.67 cfs
 0.220 af
- Reach 4R: (new Reach)
 Avg. Flow Depth=0.03'
 Max Vel=0.16 fps
 Inflow=0.56 cfs
 0.229 af

 n=0.150
 L=531.0'
 S=0.0301 '/'
 Capacity=169.18 cfs
 Outflow=0.44 cfs
 0.195 af

 Reach 5R: (new Reach)
 Avg. Flow Depth=0.03'
 Max Vel=1.04 fps
 Inflow=0.45 cfs
 0.027 af

 n=0.030
 L=95.0'
 S=0.0558 '/'
 Capacity=63.43 cfs
 Outflow=0.41 cfs
 0.026 af

 Reach 6R: (new Reach)
 Avg. Flow Depth=0.04'
 Max Vel=0.15 fps
 Inflow=2.63 cfs
 0.220 af

 n=0.150
 L=1,128.0'
 S=0.0160 '/'
 Capacity=123.12 cfs
 Outflow=0.58 cfs
 0.163 af

 Pond 10P: (new Pond)
 Peak Elev=53.91'
 Storage=1,367 cf
 Inflow=3.47 cfs
 0.233 af

 Outflow=1.47 cfs
 0.233 af

 Pond 20P: (new Pond)
 Peak Elev=43.44'
 Storage=8,875 cf
 Inflow=7.09 cfs
 0.492 af

 Outflow=2.01 cfs
 0.384 af

 Pond 30P: (new Pond)
 Peak Elev=44.80'
 Storage=13,742 cf
 Inflow=10.34 cfs
 0.820 af

 Outflow=3.86 cfs
 0.655 af

The Homestead PRP

oftware Solutions LLC		Page 7
		•
Dook Flow-FO 24' Storago-6 222 of	Inflow_4.79 of	0.250 of

Pond 31P: (new Pond)	Peak Elev=50.34' Storage=6,223 cf Inflow=4.78 cfs 0.359 af Outflow=1.69 cfs 0.282 af
Pond 40P: (new Pond)	Peak Elev=60.19' Storage=6,697 cf Inflow=4.02 cfs 0.315 af Outflow=0.56 cfs 0.229 af
Pond C1: (new Pond)	Peak Elev=56.60' Inflow=4.88 cfs 0.358 af 15.0" Round Culvert n=0.010 L=170.0' S=0.0753 '/' Outflow=4.88 cfs 0.358 af
Pond C10: (new Pond)	Peak Elev=59.51' Storage=200 cf Inflow=1.73 cfs 0.129 af 12.0" Round Culvert n=0.010 L=100.0' S=0.0030 '/' Outflow=1.62 cfs 0.129 af
Pond C11: (new Pond)	Peak Elev=58.74' Inflow=1.82 cfs 0.112 af 12.0" Round Culvert n=0.010 L=60.0' S=0.0100 '/' Outflow=1.82 cfs 0.112 af
Pond C12: (new Pond)	Peak Elev=55.13' Inflow=0.45 cfs 0.027 af 12.0" Round Culvert n=0.013 L=83.0' S=0.0096 '/' Outflow=0.45 cfs 0.027 af
Pond C13: (new Pond)	Peak Elev=55.60' Inflow=0.12 cfs 0.007 af 12.0" Round Culvert n=0.013 L=94.9' S=0.0053 '/' Outflow=0.12 cfs 0.007 af
Pond C14: (new Pond)	Peak Elev=59.61' Inflow=0.51 cfs 0.032 af 12.0" Round Culvert n=0.020 L=115.0' S=0.0017 '/' Outflow=0.51 cfs 0.032 af
Pond C2: (new Pond)	Peak Elev=56.91' Inflow=1.70 cfs 0.107 af 12.0" Round Culvert n=0.010 L=119.0' S=0.0647 '/' Outflow=1.70 cfs 0.107 af
Pond C3: (new Pond)	Peak Elev=57.44' Inflow=1.70 cfs 0.107 af 12.0" Round Culvert n=0.010 L=62.5' S=0.0032 '/' Outflow=1.70 cfs 0.107 af
Pond C30: (new Pond)	Peak Elev=55.78' Inflow=0.87 cfs 0.057 af 12.0" Round Culvert n=0.010 L=29.0' S=0.0103 '/' Outflow=0.87 cfs 0.057 af
Pond C31: (new Pond)	Peak Elev=55.59' Inflow=2.39 cfs 0.155 af 12.0" Round Culvert n=0.010 L=127.0' S=0.0921 '/' Outflow=2.39 cfs 0.155 af
Pond C32: (new Pond)	Peak Elev=58.73' Inflow=1.42 cfs 0.085 af 12.0" Round Culvert n=0.010 L=65.0' S=0.0708 '/' Outflow=1.42 cfs 0.085 af
Pond C33: (new Pond)	Peak Elev=55.74' Inflow=1.08 cfs 0.065 af 12.0" Round Culvert n=0.010 L=45.0' S=0.0089 '/' Outflow=1.08 cfs 0.065 af
Pond C34: (new Pond)	Peak Elev=58.93' Inflow=0.65 cfs 0.039 af 12.0" Round Culvert n=0.010 L=48.0' S=0.0062 '/' Outflow=0.65 cfs 0.039 af
Pond C4: (new Pond)	Peak Elev=58.53' Inflow=4.99 cfs 0.315 af 12.0" Round Culvert n=0.010 L=116.0' S=0.0121 '/' Outflow=4.99 cfs 0.315 af
Pond C5: (new Pond)	Peak Elev=59.44' Inflow=4.94 cfs 0.312 af 12.0" Round Culvert n=0.010 L=99.0' S=0.0051 '/' Outflow=4.94 cfs 0.312 af

The Homestead PRP	Type III 24-hr 10 YEAR STORM Rainfall=4.90"
Prepared by Hewlett-Pack	ard Company Printed 4/20/2018
HydroCAD® 10.00 s/n 01988	© 2011 HydroCAD Software Solutions LLC Page 8
Pond C7: (new Pond)	Peak Elev=58.80' Inflow=3.50 cfs 0.219 af
	12.0" Round Culvert n=0.010 L=60.0' S=0.0050 '/' Outflow=3.50 cfs 0.219 af
Pond C8: (new Pond)	Peak Elev=59.23' Inflow=1.83 cfs 0.157 af
	12.0" Round Culvert n=0.010 L=100.0' S=0.0040 '/' Outflow=1.83 cfs 0.157 af
l ink 1l ·	Inflow=17 23 cfs .3 056 af
	Primary=17.23 cfs 3.056 af
Link OL .	Inflow-0.28 of a 1.486 of
LINK ZL:	Drimony-0.29 of a 1.496 of
	F1111aly=9.20 CIS 1.400 al
Link 3L: AP3	Inflow=9.84 cfs 0.769 af
	Primary=9.84 cfs 0.769 af
Total Runoff	Area = 32.182 ac Runoff Volume = 5.983 af Average Runoff Depth = 2.23" 84.30% Pervious = 27.130 ac 15.70% Impervious = 5.052 ac

BMP CALCULATIONS

TABLE 1 - QUANT	TTY CALCULA	ATIONS	STORM EVENT			
		<u>2</u>	<u>10</u>	<u>25</u>		
EXISTING	AP 1	11.72	24.79	36.34		
	AP 2	3.43	9.01	14.32		
	AP 3	4.33	10.13	15.51		
DEVELOPED	AP 1	8.15	17.23	25.15		
	AP 2	3.30	9.28	13.99		
	AP 3	4.44	9.84	14.68		
CHANGE	AP 1	-3.57	-7.56	-11.19		
	AP 2	-0.13	0.27	-0.33		
	AP 3	0.11	-0.29	-0.83		
	TOTAL	-3.59	-7.58	-12.35		

TREATMENT CALCULATIONS

New Impervious Area to be Treated @95%	170,853	sf	3.92 Acres
New Developed Area to be Treated @80%	444,383	sf	10.20 Acres

AMENDED DEVELOPED CONDITIONS:

			IMP. (ft ²)				LA. (ft ²)			DEV. (ft ²)				
AREA	Ext.	Created Require to Treat	Total (Hydro CAD)	Treated	Not Treated	Ext. (HCAD)	Created Require to Treat	Total (Hydro CAD)	Treated	Not Treated	Ext.	Created Require to Treat	Total (Hydro CAD)	Treated	Not Treated
1S	37241	1,055		0	1,055		21,035		0	21,035	1,055	22,090	0	0	22,090
2S		17,695		17,695	0		47,342		47,342	0	17,695	65,037	0	65,037	0
3S		8,115		8,115	0		20,370		20,370	0	8,115	28,485	0	28,485	0
4S		2,560		0	2,560		18,452		0	18,452		21,012	0	0	21,012
5S		4,712		4,712	0		4,609		4,609	0		9,321	0	9,321	0
6S		3,505		3,505	0		4,568		4,568	0		8,073	0	8,073	0
7S		2,252		2,252	0		3,781		3,781	0		6,033	0	6,033	0
8S		2,585		2,585	0		4,752		4,752	0		7,337	0	7,337	0
9S		4,541		4,541	0		6,894		6,894	0		11,435		11,435	0
10S		27350		27350	0		33502		33502	0		60852		60852	0
11S		10943		10943	0		17738		17738	0		28681		28681	0
12S		7281		7281	0		22056		22056	0		29337		29337	0
13S		15916		15916	0		25002		25002	0		40918		40918	0
14S		10929		10929	0		1580		1580	0		12509		12509	0
15S		12405		12405	0		2053		2053	0		14458		14458	0
16S		10963		10963	0		4950		4950	0		15913		15913	0
17S		6980		6980	0		9966		9966	0		16946		16946	0
18S		3382		3382	0		0		0	0		3382		3382	0
19S	13416	1275		0	1275	50736	5391		0	5391		6666		0	6666
20S		626		626	0		577		577	0		1203		1203	0
21S		11509		11509	0		2869		2869	0		14378		14378	0
22S		1062		1062	0		2639		2639	0		3701		3701	0
23S		407		407	0		0		0	0		407		407	0
24S		2780		0	2780		10637		0	10637		13417		0	13417
25S		1903		1903	0		2626		2626	0		4529		4529	0
TOTAL	50,657	172,731	0	165,061	7,670	50,736	273,389	0	217,874	55,515	101,393	446,120	0	382,935	63,185

NEW

AREA	IMP. (ft ²)	DEV (ft ²)
Total Area	165061	382935
Total Acres	3.79	8.79
% Treated=	96.6%	86.2%

POND SIZING CALCULATIONS

AREA	IMP. (ft ²)	LA. (ft ²)	RA. (ft ²)	BMP	CPV (ft ³)	P. POOL (ft ³)	CHECK
Pond 10				Soil Filter			
3S	8,115	20.370			1.355	N/A	
6S	3,505	4.568			444		
8S	2,585	4,752			374		
Total	14,205	29,690			2,173	N/A	
			5% Impervious	+ 2% Landscaped Area =	1,304		
			5% Imperviou	s + 2% Remaining Area =	1,304		014
				Provided CPV =	5,758		OK
				Provided Area =	3157		ÜK
Pond 20				Soil Filter			
2S	17,695	47,342			3,053	N/A	
5S	4,712	4,609			546		
7S	2,252	3,781			314		
9S	4,541	6,894			608		
Total	29,200	62,626	0		4,521	N/A	0.00
			5% Impervious	+ 2% Landscaped Area =	2,713		
			5% Imperviou	s + 2% Remaining Area =	0.011		014
				Provided CPV =	6,314		OK
				Provided Area =	3,014		OK
Pond 30				Soil Filter			
10S	27,350	33,502			3,396		
12S	7,281	22,056			1,342		
14S	10,929	1,580			963		
15S	12,405	2,053			1,102		
16S	10,963	4,950			1,079		
23S	407	0			34		
Total	69,335	64,141			7,916	N/A	
			5% Impervious	+ 2% Landscaped Area =	4,750		
			5% Imperviou	s + 2% Remaining Area =			
				Provided CPV =	8,286		OK
				Provided Area =	4,756		OK
Pond 31				Soil Filter			
13S	15,916	25,002			2,160		
20S	626	577			71		
21S	11,509	2,869			1,055		
22S	1,062	2,639			176		
Total	29,113	31,087			3,462	N/A	0.00
			5% Impervious	+ 2% Landscaped Area =	2,077		
			5% Imperviou	s + 2% Remaining Area =	2,077		
				Provided CPV =	4,800		OK
				Provided Area =	2,434		OK
Pond 40				Soil Filter			
115	10 943	17 738			1,503	N/A	
17S	6,980	9.966			914		
18S	3.382	0			282		
25S	1903	2626			246		
Total	23,208	30,330	0		2,945	N/A	0.00
	-,	,	5% Impervious	+ 2% Landscaped Area =	1,767		
			5% Imperviou	s + 2% Remaining Area =	1,767		
			r	Provided CPV =	3,676		OK
				Provided Area =	2,028		OK

OPERATION AND MAINTENANCE PROGRAM

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AIIAN ENGINEERING, INC

THE HOMESTEAD - MIXED USE DEVELOPMENT 459 U.S. ROUTE 1 KITTERY, MAINE

OPERATION AND MAINTENANCE PROGRAM STORMWATER MANAGEMENT BMP's

This project contains specific Best Management Practices (BMP's) for the conveyance, storage, and treatment of stormwater and the prevention of erosion. These BMP's consist of swales, underdrained soil filter ponds, catchbasins and culverts. All components should be inspected quarterly, and after every significant rain event of 1" in any 24-hour period. Additional inspection intervals are specified for certain BMP's, specifically, underdrained soil filters.

The party responsible for implementing this Operation and Maintenance Program (O & M Program) shall be the property owner or condominium association.

Swales

All swales should be inspected for accumulation of debris, which could adversely affect the function of this BMP. These areas should also be maintained to have gradual slopes, which prevent channeling of stormwater and erosion of the bottom and sides of the swales.

Catch Basins

All catch basin grates, sumps, and inlets/outlets should be inspected for accumulation of debris, which could adversely affect the function of this BMP. Additionally, the basin inverts shall be inspected for clogging and material soundness. Sumps shall always be clear to a depth of 1' below the outlet invert. Inlet structures shall be inspected and cleaned of debris at least twice annually, once in the spring following snow melt and once in the autumn after leaf fall.

Culverts

Culvert inlets and outlets should be inspected for debris, which could clog the BMP. Additionally, the placement of rip-rap should be inspected to ensure that all areas remain smooth and no areas exhibit erosion in the form of rills or gullies.

Snow Removal

Snow shall be stockpiled only in the approved snow storage areas. Plowing of snow into wetland areas or detention ponds shall be avoided. Additionally, a mostly sand mix (reduced salt) shall be applied during winter months to prevent excessive salt from leaching into wetland areas. Excess sand shall be removed from the storage areas, all paved surfaces and adjacent areas each spring.

Underdrained Soil Filters

The underdrained soil filter area is a very effective BMP, however, long term maintenance is essential to its operation. The soil filter should be inspected after every major storm event during the first year to ensure proper function and at least twice-annually, thereafter. The inspection should ensure that the filter drains within 24 - 48 1284 State Road, Eliot, ME 03903 \diamond tel (207) 439-6023 \diamond fax (207) 439-2128

hours. The top several inches of the filter should be replaced with fresh filter material, when water ponds for longer than 72 hours. Debris and sediment that builds up should be removed from the pre-treatment structure at least annually. Outlet structures shall be inspected and cleaned of debris at least twice annually, once in the spring following snow melt and once in the autumn after leaf fall. The height of grass shall be maintained at a maximum of 12"; mowing shall be limited to no more than two times during the growing season.

Seeding, Fertilizing and Mulching

All exposed soil materials and stockpiles must be either temporarily or permanently seeded, fertilized and mulched in accordance with plan specifications. This is one of the most important features of the Erosion Control Plan, which will provide both temporary and permanent stabilization. Eroded or damaged lawn areas must be repaired until a 75% effective growth of vegetation is established and permanently maintained.

Record Keeping

Routine maintenance and inspections will be accomplished by the future property owner/developer [Michael Brigham, Landmark Hill, LLC; 79 Congress Street, Portsmouth, NH 03801, (603)-294-4000] until the condominium association had been formed and maintenance has been turned over to the association. At that time, routine maintenance and inspections will be the responsibility of the condominium association's maintenance staff or third party contracted by the property owner or condominium association. All inspections accomplished in accordance with this program shall be documented on the attached Inspection & Maintenance Log. Copies of the Log shall be kept by the property owner or condominium association, and be made available to the Department (Maine Department of Environmental Protection), upon request.



INSPECTION & MAINTENANCE LOG THE HOMESTEAD – MIXED USE DEVELOPMENT

Date	Purpose ¹	Maintenance Done ²	Ву
			····
	5-2		

- 1. Purpose is the reason for the inspection. For example; "quarterly' or "after a significant rain event."
- 2. Maintenance Done means any maintenance required as a result of the inspection, such as trash removal or re-seeding of areas.

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