Government Wharf Condition Assessment

Town of Kittery, ME

June 1, 2017



Submitted To:

Scott Alessi Harbormaster Town of Kittery 200 Rogers Road Kittery, ME 03904

Submitted By:

Barney Baker, PE Baker Design Consultants 7 Spruce Road Freeport, Maine 04032 b.baker@bakerdesignconsultants.com



BAKER DESIGN CONSULTANTS Civil, Marine, and Structural Engineering

7 Spruce Road, Freeport, Maine 04032

@ 2017 Baker Design Consultants

All Rights Reserved.

No part of this document may be photocopied, reproduced, stored in a retrieval system, or transmitted, in any form or by any means whether, electronic, mechanical for a purpose that does not relate to the project represented without the prior written permission of Baker Design Consultants. Baker Design Consultants reserves the right to change details in this publication without notice.

Baker Design Consultants 7 Spruce Road Freeport, Maine 04032 (207) 846-9724 B.Baker@bakerdesignconsultants.com



Table of Contents

Exe	cutive Summary	1
1.	Introduction/Overview	2
2.	Site Location and Exposure	3
3.	Pier Condition Review	5
4.	Condition Photographs	9
5.	Load Rating	24
6.	Conclusions & Recommendations	26
7.	Next Steps	27
APP	ENDIX A- Drawings	31

List of Tables

Table 1 – Project Elevations by Datum	3
Table 2 – Summary Condition Assessment of Government Wharf Pier	5
Table 3 – Results of Load Rating Analysis	25
Table 4 – Short-Term Repair Recommendation	26
Table 5 – Preliminary Opinion of Cost for Budgeting	26

List of Figures

Figure 1 – View of Topside of Pier	2
Figure 2 – View of East Side of Pier	2
Figure 3 – Section of Kittery Tax Map 4 (2016 Revision)	4
Figure 4 – Pier Location (Section of NOAA Chart 13283-Portsmouth Harbor)	4
Figure 5 – 2017 FEMA FIRM Section	4
Figure 6 – View of Pier from Town Landing Road	9
Figure 7 – Overview of Pier Topside	9
Figure 8 – East Side of Pier	10
Figure 9 – West side of pier	10
Figure 10 – View of bulkhead, pile supports, and bracing (Lines 4 & 5)	11
Figure 11 – Stone faced bulkhead. Note: water seepage beneath bulkhead	11
Figure 12 – Typical Condition of Decking	12

Government Wharf Condition Assessment

Town of Kittery, Maine

Figure 13 – Decking in poor condition near pavement interface
Figure 14 – Pier Stringers (Note: more algae growth and visible rot on older stringers)
Figure 15 – Pier Stringers (Note: more algae growth and visible rot on older stringers)
Figure 16 – Typical Condition of Stringers
Figure 17 – West end of bents 4 & 5. Note: significant deterioration of pile caps 4 & 5
Figure 18 – Significant deterioration of stringer near Line 5
Figure 19 – Failure of stringer at Line 5
Figure 20 – View of Bent 3 in very poor condition (believed to be abandoned) 16
Figure 21 – West end of Bent 4. Note: Split in pile cap, striations in end pile
Figure 22 – West end of Bent 5 Pile Cap. Note: Near complete failure of pile cap, significant rot in pile
Figure 23 – Typical Pile and Bracing
Figure 24 – End pile on Bent 4. Note: More severe deterioration
Figure 25 – End pile on Bent 4. Note: more severe deterioration
Figure 26 – Bent 5 pile cap supported on rock bulkhead
Figure 27 – Typical Railing and Curb on East side of pier
Figure 28 – Fender Pile at working face showing moderate rot
Figure 29 – Fender Pile at working face showing severe rot and connection failure
Figure 30 – Fender Pile Deterioration, view from water side
Figure 31 – View of Pier framing from water side, note: multiple generations of closely spaced stringers
Figure 32 – View of Pier framing on east edge. Note: outer stringer lifted due to hoist tension anchor
Figure 33 – Typical railing post connection with single timber bolt
Figure 34 – Hoist located at southeast corner of pier
Figure 35 – Underside of southeast corner of pier, note: hoist only fastened to decking
Figure 36 - AASHTO H-20 Truck

Executive Summary

In May 2017, Baker Design Consultants (BDC) was retained by the Town of Kittery to perform a condition assessment of Government Wharf on Town Landing Road in Kittery. The pier is used by commercial fisherman and was last inspected by Waterfront Engineers in 2007. At that time, the pier was estimated to have a remaining service life of 10 years. It has now been 10 years since the last inspection.

An inspection was performed by BDC to complete the following tasks.

- Document the current condition of the pier.
- Determine critical repair needs to keep the pier functioning.
- Provide an assessment of the remaining service life of the pier.
- Recommend a timeline for further inspection/repair or replacement of the structure.

Based on field observations and follow-up calculations to evaluate load capacity, there are several critical condition issues that make the pier unable to handle loading normally associated with commercial pier use. Until remedial action is taken to address these deficiencies, the pier must be 'posted' to reflect the reduced structural capacity of the structure.

The pier should be posted immediately with signage limiting uniform live load to 100 psf and maximum vehicle size to 3.5 tons. For reference, a 3.5-ton vehicle is roughly equivalent to a ½ ton pickup truck.

Critical deficiencies are noted below, described in more detail in the report and depicted in the appended plans.

- 1. Severe deterioration of pile caps in Lines 4 & 5
- 2. Missing shims between stringers/pile caps, and pile caps/piles in many locations that compromise member bearing conditions
- 3. (1) support pile in very poor condition
- 4. At least (6) fender piles in moderate to very poor condition
- 5. Poor anchorage for hoist to pier connection
- 6. Presence of "dead wood" beneath pier that will accelerate deterioration

In addition, several non-structural, code-compliance issues were observed that were not addressed after the 2007 inspection:

- 1. Existing ladder is not OSHA compliant and should be replaced.
- 2. Curbs on east and west sides are not OSHA compliant (7" curb height does not satisfy OSHA minimum height for vehicle curbs of 10")
- 3. Connection of railing posts to pier is questionable and may not satisfy OSHA loading requirements for handrails (50 plf uniform load or 200-lb point load)

Notwithstanding the critical issues and code noncompliance noted above, the pier structure condition is generally only in fair to serviceable condition due to the age of the structure. Even with the noted deficiencies corrected, the pier will only be serviceable for an estimated 5-10 years and will still need to be load rated.

Because of the short remaining service life of the pier, it is recommended that repairs also be short-term rather than long-term fixes. Notwithstanding this approach, it is likely that a repair program will cost in the range \$63,000 as noted in Table 5.

A replacement pier is estimated to cost in the range of \$300k to \$350k. Because of the timeframe needed for design, regulatory permitting, grant funding applications, and construction it is advised that this process begin as soon as possible.

1. Introduction/Overview

In May 2017, Baker Design Consultants (BDC) was retained by the Town of Kittery to perform a condition assessment of Government Wharf, an existing municipal fishing pier located on Town Landing Road in Kittery. The pier was previously inspected by Duncan Mellor of Waterfront Engineers in 2007¹. A list of recommended actions was provided in that report, and a remaining service life of 10 years was estimated. It has now been 10 years since the last inspection.

The inspection and analysis performed by BDC are intended to document the existing condition of the pier, determine any repair needs, assess the remaining service life, and establish a recommended timeline for further inspection/repair or replacement of the structure.

The existing pier is depicted in Figure 1 and Figure 2 below. The pier consists of a pile-supported timber structure approximately 32' wide x 36' long located directly seaward of a stone bulkhead abutment that makes up Town Landing Road. The timber pier is supported on a series of timber pile bents consisting of (6) or (7) piles and a timber pile cap. Four (4) pile bents currently exist, although one is an older bent that was abandoned in place. Piles are braced in both directions with timber diagonal bracing. Pier framing consists of 12x12 pile caps, 6x12 stringers, and 3x12 decking. Curbs and handrails are installed along the east and west faces of the pier. The working face of the pier (south) has a 12" vehicle curb, and no railings. There is a steel mast-and-spar style hoist mounted on the southeast corner of the pier which has a 1,000-lb capacity winch and a maximum reach of 17'.



Figure 1 – View of Topside of Pier

Figure 2 – View of East Side of Pier

The following sections review site location and exposure conditions, observations from the field inspection, and results of a load rating analysis for the pier. Finally, critical repair issues are identified and recommended remedial actions are described.

¹ Reference: "Inspections at Town Piers, Kittery & Kittery Point, Maine" by Waterfront Engineers, LLC, dated Jan. 21, 2008.

2. Site Location and Exposure

The existing pier is located at the end of Town Landing Road (presumably within the Town's Right-of-way), on the Kittery Shorefront. Refer to the section of Kittery Tax Map 4 provided as Figure 3, and the Nautical Chart section provided as Figure 4. The site is located across from Seavey Island and benefits from limited fetch and exposure due to its protected location. This is consistent with the FEMA mapping, base flood and zone designations for the site.

Site tidal elevations are listed in Table 1 below in Chart (MLLW = 0) and NAVD88 datum based on published data available from NOAA, Maine DEP, and FEMA. Based on the current (1986) FEMA map, the site is located in an A2 Zone with a 100-year flood elevation (BFE) = 9.8' (NAVD88). The 'preliminary' (2017) map which is pending approval, shows the site in an AE Zone with BFE = 10.0' (NAVD88). A section of the 2017 FEMA Map is provided in Figure 5.

The elevation of the existing pier has not been established by survey. Based on Maine GIS 2-ft contour data for Kittery, the pier deck elevation appears to be located at approximately 7' NAVD88, which is consistent with the location of high water staining on the support piles approximately 3' below the pier deck. This elevation is fairly low, and the pier can be expected to be overtopped during significant storm events, which is consistent with the limits of Special Flood Hazard Area identified by FEMA.

		CHART	NAVD88	Notos	
	VATION	(ft)	(ft)	Notes	
FEMA BFE		14.6	10.0	PRELIM (2017) ZONE AE (SITE IS ALSO MAPPED WITHIN REGULATORY FLOODWAY)	
FEN	1A BFE	14.4	9.8	EFFECTIVE (1986) ZONE A2	
	0.2% Annual Chance	14.4	9.8		
Stillwater Elevations	1% Annual Chance	13.8	9.2	PRELIM (2017) FEMA FIS	
	2% Annual Chance	13.4	8.8		
	10% Annual Chance	12.8	8.2		
Highest Annual Tide		10.5	5.9	2016 MEDEP Predictions	
MHHW		8.84	4.22		
MHW		8.43	3.81]	
NAVD88		4.62	0.00	BASED ON TIDAL BM	
MLW		0.32	-4.30		
MLL	W	0.00	-4.62		

Table 1 – Project Elevations by Datum



Figure 3 – Section of Kittery Tax Map 4 (2016 Revision)



Figure 4 – Pier Location (Section of NOAA Chart 13283-Portsmouth Harbor)



Figure 5 – 2017 FEMA FIRM Section

3. Pier Condition Review

An inspection of the pier was completed by Baker Design Consultants on May 18, 2017 from 0830 to 1230 at half- to low-tide (Low tide of +0.8 ft @ 1120). The inspection involved the following tasks:

- Visual inspection of the entire pier superstructure and substructure
- Measurement of pier dimensions, framing layout, pile locations, and section sizes for all primary structural members.
- Non-destructive physical evaluation of condition by probing/prodding of timber elements to assess location and depth of rot, and measurement to assess section loss in deteriorated areas
- The pier was thoroughly photographed to document overall condition configuration of all superstructure and substructure elements as well as any specific areas of concern.
- Underwater videos were taken around piles located beyond the low-water line to record the condition of the piles in the subtidal range.

The size, layout, and condition of the primary structural elements are described in Table 2 based on observations made during the May 2017 field inspection. Specific issues identified during the field survey are also identified in the table. Reference should also be made to Section 4 which provides photographs that demonstrate pier condition and configuration.

Element	Size, Material, Orientation, Spacing	May 2017 Condition
DECKING	3 X 12 Incised lumber Species, treatment level/ type and lumber grade unknown	General Condition Summary: The existing decking consists of incised 3x12 lumber sections. The decking is generally in worn but serviceable condition. A review of record inspection information (2008 inspection report by Waterfront Engineers) suggests that the decking in place today was installed sometime after that inspection, and is therefore 10 years or less old. Signs of wear observed during the inspection include discoloration, splitting, checking, and occasional loose nailed connections. More heavily worn sections were observed near the transition from the paved upland approach to the timber pier. Accelerated deterioration of these sections is believed to be caused by surface water runoff from the adjacent roadway. In general, the decking condition is consistent with its age, and can be considered serviceable. Issues Noted: The hoist that is located at the southeast corner of the pier is fastened to the decking by (4) through bolts. This connection does not appear to be suitable and strengthening is recommended.

Table 2 – Summary Condition Assessment of Government Wharf Pier

		General Condition Summary:			
		Two generations of stringers are present under the pier in many locations			
	6 X 12 FS Incised Species, treatment level/type and lumber grade unknown	Older stringers are in very poor condition and in some cases have failed or are deteriorated to the point no longer providing any load capacity to the structure. At the 2007 inspection it was recommended that dead wood (including old, un-utilized timber) be removed from beneath the pier to minimize the potential for additional rot due to water accumulation. This does not appear to have been completed, and is still recommended.			
STRINGERS		Newer stringers appear to be the same that were present at the 2007 inspection. The age of these members is not known. These stringers appear to be generally in fair condition. Most appear to be serviceable without the presence of significant rot or decay that would compromise their integrity. Probing of tops of strings with an awl revealed minimal depth of rot in most areas. Several localized issues were identified in that are described below.			
	Spacing varies:	Issues Noted:			
	31.5"+/- typ.	Stringers extending over Bent 5 show advanced rot at the interface with the filled area behind the pier. This is caused by the presence of freshwater that sits on the stringers from rain and stormwater runoff from the adjacent road.			
		In several areas, shims are missing beneath the stringers and poor bearing conditions exist. Stringers should be shimmed to provide full bearing.			
		At the connection of the hoist tension ties, the stringer appears to be lifting off of the pile cap. This suggests that the stringer is not adequately anchored to resist the necessary uplift force. An improved anchor should be incorporated into the design.			
		General Condition Summary:			
		General Condition Summary: There are multiple generations of pile caps present beneath the pier. It appears that Bent 3 is a remnant from earlier construction that was abandoned in place. There is significant variation in the condition of the pile caps. Condition of each element is summarized below:			
		 General Condition Summary: There are multiple generations of pile caps present beneath the pier. It appears that Bent 3 is a remnant from earlier construction that was abandoned in place. There is significant variation in the condition of the pile caps. Condition of each element is summarized below: Line 1 (furthest seaward) – Fair to good condition, no structural concerns. Note that a pile that was identified as missing at the 2007 survey has since been 			
PILE CAPS	12X12 FS Species, treatment level/type and lumber grade unknown	 General Condition Summary: There are multiple generations of pile caps present beneath the pier. It appears that Bent 3 is a remnant from earlier construction that was abandoned in place. There is significant variation in the condition of the pile caps. Condition of each element is summarized below: Line 1 (furthest seaward) – Fair to good condition, no structural concerns. Note that a pile that was identified as missing at the 2007 survey has since been replaced. Line 2 – Fair to good condition. Gap between pile and pile cap at west end results in no bearing and potential overstressing of pile cap. Line 3/3A – Very poor/failing condition. This bent is believed to have been abandoned in place and is not currently used. Removal is recommended. Line 4 – Very poor condition. Pile cap is split vertically down the center starting at the west end and extending a portion of its length. Repair or replacement is necessary. Missing shims between piles and pile cap. Line 5 (at bulkhead) – Very poor condition. Significant split is visible at west end extending through full depth of pile cap. Timber shows rot along its length at bulkhead connection. Potential for more deterioration in areas not able to be observed. Repair or replacement is necessary. 			
PILE CAPS	12X12 FS Species, treatment level/type and lumber grade unknown	 General Condition Summary: There are multiple generations of pile caps present beneath the pier. It appears that Bent 3 is a remnant from earlier construction that was abandoned in place. There is significant variation in the condition of the pile caps. Condition of each element is summarized below: Line 1 (furthest seaward) – Fair to good condition, no structural concerns. Note that a pile that was identified as missing at the 2007 survey has since been replaced. Line 2 – Fair to good condition. Gap between pile and pile cap at west end results in no bearing and potential overstressing of pile cap. Line 3/3A – Very poor/failing condition. This bent is believed to have been abandoned in place and is not currently used. Removal is recommended. Line 4 – Very poor condition. Pile cap is split vertically down the center starting at the west end and extending a portion of its length. Repair or replacement is necessary. Missing shims between piles and pile cap. Line 5 (at bulkhead) – Very poor condition. Significant split is visible at west end extending through full depth of pile cap. Timber shows rot along its length at bulkhead connection. Potential for more deterioration in areas not able to be observed. Repair or replacement is necessary. 			
PILE CAPS	12X12 FS Species, treatment level/type and lumber grade unknown	 General Condition Summary: There are multiple generations of pile caps present beneath the pier. It appears that Bent 3 is a remnant from earlier construction that was abandoned in place. There is significant variation in the condition of the pile caps. Condition of each element is summarized below: Line 1 (furthest seaward) – Fair to good condition, no structural concerns. Note that a pile that was identified as missing at the 2007 survey has since been replaced. Line 2 – Fair to good condition. Gap between pile and pile cap at west end results in no bearing and potential overstressing of pile cap. Line 3/3A – Very poor/failing condition. This bent is believed to have been abandoned in place and is not currently used. Removal is recommended. Line 4 – Very poor condition. Pile cap is split vertically down the center starting at the west end and extending a portion of its length. Repair or replacement is necessary. Missing shims between piles and pile cap. Line 5 (at bulkhead) – Very poor condition. Significant split is visible at west end extending through full depth of pile cap. Timber shows rot along its length at bulkhead connection. Potential for more deterioration in areas not able to be observed. Repair or replacement is necessary. Issues Noted: Line 4 and Line 5 pile caps are in a severe state of deterioration and should be repaired immediately to avoid potential failure. 			

		General Condition Summary:				
		Multiple generations of support piles exist beneath the pier. Quantities of piles in each bent line are listed below:				
		 Line 1 – 7 piles Line 2 – 7 piles Line 3/3A – 6 piles (line 3), 2 piles (line 3A) Line 4 – 6 piles Line 5 – Bulkhead, 1 pile 				
	12" NOMINAL	The oldest of the piles, which also represent those in the worst condition, are in Bent #3 and #3A. This bent is believed to have been abandoned in place and the piles are no longer used. It is recommended that any existing dead wood beneath the pier be removed.				
PIER SUPPORT PILES	Species and grade unknown, creosote treatment	The remaining piles are generally in fair to good serviceable condition, with the exception of issues noted below. There were no noted instances of significant necking/section loss at the mudline. There were several instances of marine borer damage within the tidal range that represented up to 3/4" of section loss. Remaining pile sections were generally solid and intact. Some amount of algae/marine growth is visible throughout all pile sections. No major settlement of substructure elements was observed that would be indicative of poor subsurface conditions or inadequate bearing capacity.				
		Issues Noted:				
		The westernmost pile in Bent 5 is in very poor condition, and has evidence of marine borer damage along its length. This pile also has notable rot at the top of the pile as it is exposed to freshwater from above. This pile should be replaced.				
		In several locations, piles do not have complete bearing on pile caps due to missing shims. Shims should be replaced where missing.				
		Pile capacity is not able to be evaluated due to lack of subsurface information.				
	3x8 and 3x12	General Condition Summary:				
PILE BRACING	Species, treatment level/type and lumber grade unknown	Bracing is in fair to good condition. Marine borer damage is visible commonly, but is limited in extent and does not appear to compromise the integrity of the bracing. Connections are generally solid and functional.				
		Issues Noted:				
		None noted.				
		General Condition Summary:				
FENDER PILES	12" NOMINAL Species, treatment, type and grade unknown	Along the south (berthing) face of the pier, there are 10 fender piles installed. These piles generally appear to be of newer construction than support piles. Fender piles show some wear along their outer faces which can be expected with use. Tops of piles show significant rot and splitting from freshwater exposure. Issues Noted: 6-7 piles show significant rot and splitting at the tops. In the worst cases, deterioration				
		is advanced to the point of compromising the pile to curb connection				

Town of Kittery, Maine

RAILINGS	4x4 posts 2x6 top rail 2x6 mid rail 42" high	General Condition Summary: Railings are 42" high and include a top rail, mid-height rail, and curb which appears to meet the general geometric criteria for OSHA compliance. Connection of the railing posts to the structure only use 1 bolt which may not adequately support the required 200 lb. top rail load per OSHA standards Issues Noted:
		Poor connections should be upgraded
	12x12 curb at working face	General Condition Summary: Curb materials are generally in good serviceable condition. It is believed that the curbs that exist today were installed sometime after the 2007 inspection was completed, and therefore are less than 10 years old. Condition is generally consistent with age with no major deterioration noted.
CURBS	4x12 on 4x12 blocks on side faces (7" total height)	Issues Noted: Based on OSHA requirements for marine facilities (Section 1917), vehicle curbs installed after October 3, 1983 are required to be at least 10" in height. (curbs installed prior to October 3, 1983 were only required to be 6"). It appears that the existing curbs were installed in the last 10 years, and as such should meet the 10" height requirement. Currently the south curb satisfies the OSHA height requirement, the east and west curbs do not.
stone Bulkhead	Stone varies in size and shape. Wall has been pointed, unsure if original Concrete cap	 General Condition Summary: The existing wall construction is largely unknown. The size of stones varies greatly from some very large (~2' + minimum dimension) to small (~6" minimum dimension). The wall cross section and bearing conditions are not known at this time and would be necessary in order to investigate the wall capacity. Sections of the bulkhead near the west corner are missing grout which suggests either this was never initially installed or has been lost at some point in the past. In general, the existing stone bulkhead appears to be relatively intact with no major signs of distress or failure observed that would indicate poor bearing conditions, instability, or overloading. The concrete cap at the top of the wall is in poor condition with significant cracking, damage, and section loss visible, particularly on the eastern side of the bulkhead Issues Noted: Water seepage was observed through wall at low tide, suggesting that water is being trapped behind the wall and an effective drainage medium likely does not exist. Concrete cap is failing and should be repaired.

4. Condition Photographs



Figure 6 – View of Pier from Town Landing Road



Figure 7 – Overview of Pier Topside



Figure 8 – East Side of Pier



Figure 9 – West side of pier



Figure 10 – View of bulkhead, pile supports, and bracing (Lines 4 & 5)



Figure 11 – Stone faced bulkhead. Note: water seepage beneath bulkhead



Figure 12 – Typical Condition of Decking



Figure 13 – Decking in poor condition near pavement interface



Figure 14 – Pier Stringers (Note: more algae growth and visible rot on older stringers)



Figure 15 – Pier Stringers (Note: more algae growth and visible rot on older stringers)



Figure 16 – Typical Condition of Stringers



Figure 17 – West end of bents 4 & 5. Note: significant deterioration of pile caps 4 & 5



Figure 18 – Significant deterioration of stringer near Line 5



Figure 19 – Failure of stringer at Line 5



Figure 20 – View of Bent 3 in very poor condition (believed to be abandoned)



Figure 21 – West end of Bent 4. Note: Split in pile cap, striations in end pile



Figure 22 – West end of Bent 5 Pile Cap. Note: Near complete failure of pile cap, significant rot in pile



Figure 23 – Typical Pile and Bracing



Figure 24 – End pile on Bent 4. Note: More severe deterioration



Figure 25 – End pile on Bent 4. Note: more severe deterioration



Figure 26 – Bent 5 pile cap supported on rock bulkhead



Figure 27 – Typical Railing and Curb on East side of pier



Figure 28 – Fender Pile at working face showing moderate rot



Figure 29 – Fender Pile at working face showing severe rot and connection failure



Figure 30 – Fender Pile Deterioration, view from water side



Figure 31 - View of Pier framing from water side, note: multiple generations of closely spaced stringers

Government Wharf Condition Assessment Town of Kittery, Maine



Figure 32 – View of Pier framing on east edge. Note: outer stringer lifted due to hoist tension anchor.



Figure 33 – Typical railing post connection with single timber bolt.

Government Wharf Condition Assessment Town of Kittery, Maine



Figure 34 – Hoist located at southeast corner of pier



Figure 35 - Underside of southeast corner of pier, note: hoist only fastened to decking

5. Load Rating

An analysis of the pier structure for vertical dead and live load was conducted using Woodworks software. For this analysis, the pier geometry, framing layout, and member sizes were as measured during the field inspection. The species of framing timber is unknown, but for the purpose of this analysis was assumed to be No. 2 Southern Pine. Reductions were made to member capacities to account for the observed level of deterioration as described in Table 3.

Live load cases considered on the pier included evaluation of effects of uniform load on the structure and the vehicle loading based on an AASHTO two axle truck. Three cases were considered for uniform loading

- 1. Uniform Live Load = 100 psf (pedestrian live loading for public spaces per IBC)
- 2. Uniform Live Load = 250 psf (uniform live load for areas subject to truck loading per IBC)
- 3. Maximum allowable live load based on element condition (if cases 1 and/or 2 not met)

Vehicle loading on the pier was considered based on a two-axle AASHTO truck based on an equivalent of the H-20 design vehicle. The AASHTO H-20 design truck (depicted in Figure 36) is a two-axle truck with a total weight of 20-tons (40 kip), with a 20/80 front to rear axle weight ratio. Individual wheel loads are applied over a rectangular area with dimensions 10"x20". If the pier is capable of safely carrying the H-20 vehicle, it can generally remain in service without a need for load posting. If the maximum safe vehicle load is less than an H-20, restrictions on truck loading are necessary to applied loading within safe operating conditions.



Figure 36 - AASHTO H-20 Truck

The results of the analysis for uniform and truck loading are presented in **Table 3**. In its current state, the pier capacity is considered to be very limited due to the severe condition of the pile caps in Bents 4 and 5. Due to this, it is recommended that live loading and vehicle loading on the pier be restricted to a maximum uniform live load of 60-psf or a maximum vehicle load of H-3.5 (7,000-lb GVWR) until repairs can be completed. This loading is representative of a ¹/₂-ton pickup truck.

If repairs are completed to the pile caps in Bents 4 and 5, the pier capacity will be controlled by the capacity of the stringers. In their current state of deterioration, the stringers can be considered to safely handle a maximum uniform live load of 125 psf, and a maximum vehicle weight of 14,000lb, or an H-7 vehicle. Because the live loading limits resulting from the analysis

are less than the values required by applicable codes, it is recommended that the pier be posted for limited safe loading, and use be monitored to minimize the possibility for excessive loading on the structure. With consideration for an additional factor of safety to account for the generally deteriorated and haphazard construction, **it is recommended that the pier load rating** of maximum uniform live load of 100 psf, or a maximum vehicle load of H-5 (10,000-lb GVWR) be posted after repairs are complete. For reference, a 5-ton vehicle is approximately equivalent to a 1-ton pickup truck.

If the recommended load limits are considered to be overly limiting to the use of the facility, selected upgrades could be designed to some or the entire pier to increase the safe live load capacity.

		Uniform Load Cases		Vehicle Load Cases		
Element	Notes/Assumptions	Case 1 100 psf LL	Case 2 250 psf LL	Maximum Allowable	H-20 Truck	Maximum Allowable
Deck Boards 3 X 12	 Assumed No. 2 Southern Pine Lumber 80% material capacity remaining 	ок	ок		ок	
Stringers 6 X12 @ 31.5"	 Assumed No. 2 Southern Pine Lumber 60% material capacity remaining 	ОК	No Good	125 PSF	No Good	H-7
Pile Caps Lines 1 & 2	 Assumed No. 2 Southern Pine 60% material capacity remaining 	ОК	No Good	225 psf	ОК	
Pile Caps Lines 4 & 5	 Assumed No. 2 Southern Pine 30% material capacity remaining 	No Good	No Good	60 psf	No Good	H-3.5
Piles	Assumed 75 % material capacity remaining	OK*	OK*		ОК*	

Table 3 – Results of Load Rating Analysis

*Piles were evaluated based on structural capacity only. Geotechnical capacity is unable to be evaluated at this time due to lack of subsurface information.

6. Conclusions & Recommendations

This report details the results of a field inspection and load rating analysis of the Government Wharf located on Town Landing Road in the Town of Kittery. Through this work, many issues have been identified that require short-term remediation in order for the pier to keep operating safely. These repair needs are listed in Table 4.

Table 4 – Short-Term Repair R	ecommendation
-------------------------------	---------------

Category	Recommendations				
Structural	 Install signage to post weight limits on pier of 100 psf uniform load or 5 ton truck load Install shims in locations where missing beneath stringers and pile caps Repair pile caps in lines 4 & 5 Replace westernmost pile in Bent 5 Replace deteriorated fender piles at pier face Remove dead wood (Grid Line 3 piles, caps, and stringers) beneath pier Strengthen hoist connection to decking Improve anchorage of hold downs for hoist tension ties 				
Code Compliance	 Replace ladder with OSHA Compliant version Upgrade curbs on east and west sides to be OSHA Compliant Upgrade connection of railing posts to pier and add new railing posts to ensure railings satisfy OSHA loading requirements 				

A preliminary opinion of cost for the short-term repair program is provided in Table 5 to support the Town's budgeting for the work. The estimated budget of \$63,000 includes a 25% contingency to account for the preliminary nature of the estimate. This budget can be further refined once the final scope of work for the repair program is determined.

ITEM				1			LINI	т		
					APPROA.					
NO.	ITEM				QUANTITY	UNIT	PRICE		AMOUNT	
1	MOBILIZATION				1	LS	\$	10,000	\$	10,000
2	INSTALL MISSING SHIMS				1	LS	\$	500	\$	500
3	BENTS #4 & 5 PILE CAP REPAIR	No.	Length							
	NEW TIMBER CAPS	2	40.0		80	LF	\$	25	\$	2,000.0
	BRACKETS AND HARDWARE				1	LS	\$	1,000	\$	1,000.0
	INSTALLATION				4	DAY	\$	2,000	\$	8,000.0
4	BENT #5 SUPPORT PILE REPLACEMENT				1	EA	\$	3,500	\$	3,500
5	FENDER PILE REPLACEMENT				7	EA	\$	2,500	\$	17,500
6	REMOVE DEAD WOOD BENEATH PIER				2	DAY	\$	2,000	\$	4,000
7/8	UPGRADE HOIST CONNECTIONS				1	LS	\$	2,000	\$	2,000.0
9	REPLACE TIMBER LADDER				1	LS	\$	500	\$	500.0
10/11	HANDRAIL AND CURB UPGRADES	No.	Length							
	ADD HANDRAIL POSTS	6	4.5		27	LF	\$	2.50	\$	67.5
	UPGRADE HARDWARE				14	EA	\$	50	\$	700.0
	UPGRADE CURBS (ADD 4X12)	2	36.0		72	LF	\$	7.00	\$	504.0
	INSTALLATION				1	LS	\$	500	\$	500.0
TOTAL CONSTRUCTION COST							Su	btotal	\$	50,772
CONTINGENCY								25%	\$	12,693
PRELIMINARY OPINION OF COST FOR BUDGETING							Т	OTAL	\$	63,000

7. Next Steps

It is recommended that the Town move ahead with the repairs described in Section 6 as soon as possible to allow the pier to remain in service and operate safely. BDC can assist in design and bid solicitation for the repair program by request.

While it is critical that the recommended repairs be completed, given the significant structural and regulatory compliance issues observed, any repairs or maintenance to the structure should be considered short term. The report outlines a series of repairs and upgrades that is intended to keep the pier operational for another 5-10 years. In the meantime it is recommended that the Town begin to plan and budget for replacing the pier within a 5-10 year timeframe.

It is recommended that the Town move toward a full replacement of the pier. A new pier design would consider structural loading requirements, resistance to wind and wave action, code compliance, and functional efficiency. Because the existing subsurface conditions at the pier are unknown, it is recommended that a geotechnical program be completed as part of this work to investigate subsurface conditions both within the existing filled bulkhead and within the area of the pile supported pier. A rough budgetary estimate for the cost of a total pier replacement is \$300,000-\$350,000 depending on the extent of repairs required to the stone bulkhead. An additional budget of approximately \$25,000 is recommended to cover fees for design and permitting of the replacement facility.

This work could be eligible for cost sharing under a State grant program such as the Maine DOT Small Harbor Improvement Program (SHIP), which will provide up to 50% state funding toward the design and construction of the facility. State funding is also available through the Maine Coastal Program Shore and Harbor Management Grant Program, which will provide up to 75% state funding toward planning and design activities related to harbor improvement projects such as the proposed pier replacement. BDC can assist the Town with grant funding applications, design, permitting, and bid solicitation for a replacement pier by request.

APPENDIX A- Drawings

- SK-1 General Plan
- SK-2 Pile and Framing Layout
- SK-3 Pier Condition Notes and Recommended Action





		N I-
		BAKER DESIGN CONSULTANT's Design of the point of th
		05.31.17 DJB DATE INT.
		INSPECTION REPORT SUBMISSION
	HARD BAR	OF MA NREY J. S737 CONTRACTOR S737 CONTRACTOR
	DESIGNED BY: DJB DRAWN BY: GTC	CHECKED BY: DJB & BJB SCALE: AS SHOWN
NOTES	HEET THE: PILE AND FRAMING LAYOUT	ROJECT: Kittery Port Authority GOVERNMENT WHARF INSPECTION Kittery, Maine
1. JOIST SPACING BASED ON AVERAGE MEASUREMENT SPACING OF INTACT, FUNCTIONAL JOISTS AND DOES NOT CONSIDER THE PRESENCE OF OLDER, SISTERED JOISTS, OR OBSOLETE "DEADWOOD". ACTUAL SPACING VARIES	DATE MAY CONTRAC 17 SHEET SK-	2017 2017 2017 2017 2017 2017 REV. 2017

