# CMA ENGINEERS, INC. CIVIL | ENVIRONMENTAL | STRUCTURAL

35 Bow Street Portsmouth, New Hampshire 03801-3819

> P: 603 | 431 | 6196 www.cmaengineers.com

ENGINEERS

September 2, 2021

Bart McDonough, Town Planner Town of Kittery 200 Rogers Road Kittery, Maine 03904

# RE: Town of Kittery, Planning Board Services 524 US Route 1, Good To-Go Site Plan and ROW Application Tax Map 67, Lot 1; MU Zone CMA #591.136

Dear Bart:

CMA Engineers has received the following information for Assignment #136, review of the Good To-Go facility site plan and Right of Way application, located at 525 US Route 1, Map 67 Lot 1 in the Mixed-Use Zone.

- 1) Letter of application, Application forms for Site Plan Review and Right-of-Way Plan Review; Letter outlining waiver requests, and related application materials for 524 US Route 1, Good To-Go Site Plan and ROW Application, prepared by Altus Engineering, Inc. of Portsmouth NH, dated July 22, 2021.
- 2) Drawings titled Good To-Go Specialty Food Facility (24 sheets), 524 U.S. Route 1, Kittery Maine Assessor's Parcel 67, Map 1, Plan Issue Date July 22, 2021, by Altus Engineering, Inc of Portsmouth, NH.
- 3) Traffic Impact Study, Proposed Manufacturing Facility, Kittery Maine, prepared by Sewall for Altus Engineering dated July 22, 2021.
- 4) Drainage Analysis, Site Development for Good To-Go, 524 U.S. Route 1 Tax Map 67, Lot 1, Prepared by Altus Engineering, Inc of Portsmouth, NH dated July 22, 2021.
- 5) Letters from Kittery Water District and Kittery Sewer Department, both dated July 12, 2021.

We have reviewed the information submitted for conformance with the Kittery Land Use and Development Code (LUDC) and general engineering practices and offer the comments below that correspond directly to the Town's Ordinances.

The proposed project includes establishing an approximately 900-foot public Right -of-Way (ROW) and site plan supporting a 20,000 square foot manufacturing building on an existing approximately 24-Acre lot. The facility would manufacture specialty foods for recreational and outdoor use. There is an existing residence on the lot, the driveway of which would be relocated from US Route 1 to the proposed ROW. The project is located in the Mixed-Use Zone (MU). A high intensity soils survey has been completed and identified wetlands that are outside the area of proposed disturbance, including no wetland buffer impacts. The development is proposed to be served by public water from the Kittery Water District, and connection via small diameter force main to the existing Kittery Sewer Department sewer on US Route 1. The application describes division of the property into two lots. Proposed Lot 2 contains the proposed manufacturing facility. Proposed Lot 1 is to the north and contains the residence and significant additional land. The proposed infrastructure would support more intensive development than is now proposed, in terms of estimates of traffic, water supply, etc. If a concept or description of potential development concepts for lot 1 is available, it would be useful in further understanding the proposal.

# 16.3 Zoning Regulations

# 16.3.2.13 Mixed Use (MU)

The proposed use is a permitted use, as a light industry, with size 20,000 sf or less.

The project conforms to all zoning standards for MU.

# 16.8 Design and Performance Standards-Built Environment

The applicant proposed to construct a roadway (secondary collector street) within a new public ROW. The ROW as proposed extends over 800 feet eastward from US Route 1. As a public ROW, it is proposed to meet Town standards for acceptance, with several waivers. The ROW would serve proposed Lots 1 and 2, including the existing residence. A short public easement extends between the ROW and Lot 2.

# Article IV. Streets and Pedestrian Ways

# 16.8.4.3 Street Classification

A Secondary Collector Street classification is proposed with a 60-ft width minimum. This standard is in the "Public" classifications on Table 1. This classification would accommodate up to 800 ADT. This level of use exceeds the traffic generation from the proposed facility and can accommodate additional traffic from other potential lots.

# 16.8.4.7 Dead End Streets

The ROW as proposed is a dead end, which is allowed for this street classification. The design does not include a cul-de-sac. The truck movements into the proposed facility apparently use the public ROW for turning into the private property. A cul-de-sac in the public ROW should be provided, or an explanation of why it is no required, with a waiver request.

## 16.8.4.8 Grades, Intersections and Sight Distances

Sight distances at Route 1 have been shown to be satisfactory.

The new driveway to the residence is appropriate and removes it from US Route 1. However, it is within about 75 feet of the intersection. An analysis that location, including any "stacking" of exiting vehicles including trucks, should be completed to determine if any conflicts would result.

The design of the intersection should be further developed indicating limits of paving, grades, striping, stop bars, and other details.

Applicant should determine ME DOT jurisdiction. Maine DOT should be consulted, and approval obtained if required. whether

Kittery Public works should be consulted for comments.

# 16.8.4.11 Street Construction Standards

The proposed street construction meets the requirements.

# 16.8.4.13 Sidewalks

The applicant has requested a waiver of sidewalk, because of the nature of the proposed development. The cross section of the ROW leaves space to accommodate a future sidewalk. Accordingly, the waiver at this time can be considered appropriate.

# Conformance with Table 1- Chapter 16.8 Article IV

The design of the roadway in the ROW meets the standard in Table 1, except

- Longitudinal Slope. Minor variation. Acceptable. (Waiver requested)
- Side Slope. Variation supported by expected conditions (ledge) and construction methods. (Waiver requested)
- Cul-de-sac. Requires resolution. No Waiver request yet.
- Sidewalk (waiver requested).
- Roadway Curve geometry. Appropriate requests given site conditions and travel speeds. (Waiver requested)

## Article VI Water Supply

The project proposes to use Kittery Water District water. An 8-inch water main extension is proposed within the new ROW off an existing 12-inch main in US Route 1. The Kittery water district has indicted via letter that capacity is available to provide the facility with required water.

Separate domestic and fire protection services are included to the facility in the preliminary design. A single fire hydrant is proposed in the ROW near the entrance to the manufacturing facility.

The water design details provided appear conventional and appropriate. The Kittery Water District should review and provide comment or concurrence with layout, design, and design details, including connection to the existing main, services at the facility, and number and location of hydrants.

It is assumed that the applicant desires the KWD to own and operate the proposed water main in the proposed public ROW after construction. This should be clarified.

The concepts for other potential uses of the lot(s) may need to be described to assess water design including location of hydrants.

## Article VII Sewage Disposal

The applicant proposes construction of a grease trap and duplex sewage pump station serving the facility. and a 2-inch low pressure force main that extends westerly in the proposed ROW, and then across portions of the lot, into the ME DOT ROW of US Route 1, and then discharges to an existing sanitary manhole in Route 1.



The provided sewer design details appear conventional and appropriate. We have the following questions/comments:

- Easement for KSD access for force main outside of proposed ROW should be provided.
- Prior to final approval, a basis of design report should be prepared for the pressure sewer system, providing documentation of sizing and design of the system, existing and future flows, nature of the sewage including grease/oil removal.
- The Kittery Sewer Department has indicated capacity to accept sewage from the facility. However, the KSD should review the specific design details associated with the facilities, particularly with respect to the connection to the KSD sewer in US Route 1.
- Does the proposed system accommodate the development of additional lots? Would sewage from future development be managed by the proposed pump station? Or separate pump station with shared force main? Other? Please clarify.
- Does ME DOT require review of the design and construction w/i the DOT ROW? If so, that should review should be incorporated.

## Article VIII. Surface Drainage

# 16.8.8.1 Stormwater Drainage

The project will require a ME DEP permitting construction of the roadway, site development. and stormwater management treatment devices. That applicant should provide a description of the specific ME DEP permitting process, and how it coordinates with local approval. The project, including the ROW and site development probably trigger Chapter 500 jurisdiction. Applicant should describe that process and provided to the town application documents when prepared.

The overall drainage and stormwater management system appears to be prudently conceived and reflected in the preliminary design. It was prepared using conventional methodology and the benefit of the HISS survey. A combination of best management practices is used to treat stormwater including separate grassed underdrained soil filters that receive all the stormwater generated from the proposed ROW and the site development.

The predicted performance meets Kittery's pre and post development standard.

The erosion and sediment control plan for during construction is similarly well conceived and protective.

We offer the following comments/questions:

- Is the proposed work in the ME DOT ROW reviewed/approved by DOT?
- Does the discharge from outlet structure #2 need to be spread out via level spreader or other means so as not to result in a concentrated discharge to the abutting property?

# 16.8.8.2 Post-Construction Stormwater Management

The Stormwater Management Facility O & M Manual is similarly well-conceived and presented. The following questions/comments are presented:



- Maintenance is left to Good To-Go c/o Cape House Management. Does that include both the ROW and the manufacturing facility? The ROW is proposed as public. Is maintenance of the pond flowing to Outlet Structure #1 included, as well as the pond flowing to outlet structure #2?
- The O&M plan should be reviewed and clarified specifically meet address the compliance requirements of the Post-Construction Stormwater Management section, including submitting a certification of inspection to the Town Code Enforcement Officer by July 31<sup>st</sup>. Please clarify.

# Article IX. Parking, Loading and Traffic

16.8.9.1

- The parking requirements are met for the manufacturing facility.
- The Traffic Impact Study demonstrates compliance of the intersection with US Route 1 general requirements, including peak traffic, ADT, and sight distances.
- The Town Public Works department should review and comment or concur with the intersection design.
- Does the ME DOT have jurisdiction/comment over the design issues of the intersection? Please clarify.
- For the trucks entering and leaving the facility:
  - Provide turning motions/templates demonstrating truck movements serving the facility.
  - Are backing motions required from the proposed public ROW? Or within the private site plan?

# Article XVI. Lots

As noted at the beginning of this review letter the ROW and site plan are proposed within a single lot. The applicant generally described future division of the lot, but no subdivision has been proposed. Lot configuration (and uses) are of general interest in the review of the current proposal.

# Article XVII. Utilities

The water and sewer utilities were addressed previously in this review.

Overhead electricity is proposed, which is appropriate for the long ROW and expected ledge.

The facility proposes using bottled propane with tanks on-site.

## Article XVIII. Landscaping

The site development is relatively remote from surrounding/abutting properties. (Other lots divided within the property have not been defined). A landscape plan has been prepared for the site development (Woodburn and Company, for Altus). The landscape plan is appropriate for the development.



#### Article XIXI. Sprinkler Systems

The proposed manufacturing building (20,000 sf) is proposed to have a separate fire service (6"). This will support a sprinkler system, subject to design by a fire protection specialist.

#### Article XXIV. Exterior Lighting

An exterior lighting plan has been prepared for the proposed site plan and building. Proposed fixtures comply with the standards in the LUDC, and the ground light levels are consistent with appropriate limitations.

## 16.8 Design and Performance Standards-Built Environment

#### Article 1 General

*16.9.1.3.* The applicant prepared an appropriate and effective erosion and sedimentation control plan.

*16.9.1.4.* The applicant has conducted a high intensity soil survey and designed the project appropriately with respect to that information.

#### Article II. Retention of Open Spaces and Natural or Historic Features

*16.9.2.5.A* The site contains a cemetery that is outside the proposed ROW and site plan development. Is it necessary or desirable to provide parking for visitors to the cemetery?

#### Article III. Conservation of Wetlands Including Vernal Pools

*16.9.3.1.* The soils survey on the property has identified wetlands, including a significant vernal pool. Site development and disturbance avoids the setbacks associated with the wetlands and verbal pool. No development is proposed in protected areas.

## Other

The site should be characterized with respect to protected species, including the New England Cottontail (NEC) habitat. Maine Department of Inland Fisheries and Wildlife (MIFW) should be consulted by applicant to determine the status of the property.

Should you have any questions, please do not hesitate to call.

Very truly yours,

CMA ENGINEERS, INC.

Jodue Brayttickland

Jodie Bray Strickland, P.E. Senior Project Engineer

WAS/JBS/kao

cc: Erik Saari, Altus Engineering Eric Weinrieb, P.E. Altus Engineering

Principal



Civil Site Planning Environmental Engineering

133 Court Street Portsmouth, NH 03801-4413

July 22, 2021

Kittery Planning Board 200 Rogers Road Kittery, Maine 03904

Re: Site Plan Review and Right of Way Applications Good To-Go 524 U.S. Route 1 Kittery, Maine

Dear Members of the Board,

On behalf of the applicant, C-Coast Properties and Good To-Go c/o Cape House Management, LLC, we respectfully submit Site Plan Review and Right of Way applications for property located at 524 U.S. Route 1. The property currently hosts a residential dwelling and is primarily wooded except for a few small sections of meadow around the existing house. The applications contemplate the construction of a public right of way to access a private site consisting of a 20,000 sf specialty food manufacturing facility. Good To-Go, a Kittery-based company currently located at 484 U.S. Route 1, makes dehydrated foods for hiking, camping and other outdoor activity. With this new facility, they anticipate being able to quadruple production to meet explosive demand for their award-winning creations.

If you have any questions or need additional information, please contact us. Thank you for your time and consideration.

Sincerely,

ALTUS ENGINEERING, INC.

Erik B. Saari Vice President

ebs/5116-00-CoverLetter-072221

Enclosures



# TOWN OF KITTERY, MAINE TOWN PLANNING AND DEVELOPMENT DEPARTMENT

200 Rogers Road, Kittery, Maine 03904 PHONE: (207) 475-1323 - FAX: (207) 439-6806 www.kittery.org

# **APPLICATION: SITE PLAN REVIEW**

		S300. 00 PLUS THE GREATER OF:		<b>□</b> \$5	60/USE C	OF UNIT; OR		\$5.00/100 SQ FT OF GROSS FLOOR AREA \$1,000			Application Fee Paid:		
FEE FO SITE PLA REVIEW	R AN /:			S0.50/LINEAR FOOT OF DOCK, SLIP & FLOAT; OR				S20.00/ UNIT INTENDED TO PROVIDE OVERNIGHT SLEEPING ACCOMODATIONS		IG	ASA Fee Paid:           (TITLE 3.3 TOWN CODE)           \$ Date:		
PROPERTY DESCRIPTION		Parcel ID	Мар	67	Lot	1		Zone: Base: Overlay: MS4:		MU  yes_X_no	Toto (Squ	al Land Area uare Feet)	1,040,714 sf (23.89 acres)
		Physical Address	524 L	J.S. Ro	ute 1								
		Name	C-Coa	oast Properties, LLC				0 Partis Parts					
PROPERTY OWNER'S		Phone	(207)	321-9569			Mailing		York, Maine 03911				
INFORMATION		Fax					Auc	11622					
		Email	kevinv	kevinwerikson@gmail.com			Namo of						
	-10	Name	Erik S	Erik Saari			Busi	iness	Altus Engineering, Inc.				
APPLICAN AGENT	r's	Phone	(603) 433-2335				Mailing						
INFORMAT	ION	Fax		ari@altus-eng.com			Address	dress					
		Email	esaari										
	Existing	Use: The	site cur	rently h	iosts a	single-far	nily r	residence	an	d some sections c	of fie	ld with the re	emainder
	of the site being wooded.												
z													
PTIO													
SCRI	Project	Name: G	iood To	-Go									
T DE	Propose	ed Use: S	pecialty	/ Food	Facility	/							
OJEC		2	0,000 s	f buildir	ng with	associate	ed pa	arking and	inf	rastructure			
РК													

# WAIVER REQUEST

	Ordinance Section	Describe why this request is being made.
DESCRIPTION	***EXAMPLE*** 16.32.560 (B)- OFFSTREET PARKING.	***EXAMPLE*** Requesting a waiver of this ordinance since the proposed professional offices have a written agreement with the abutting Church owned property to share parking.
		See attached Waiver Request Letter

# Related Kittery Land Use Code concerning waivers and modifications:

## 16.10.8.2.5 Conditions or Waivers.

Conditions required by the Planning Board at the final plan review phase must have been met before the final plan may be given final approval unless so specified in the condition or specifically waived, upon written request by the applicant, by formal Planning Board action wherein the character and extent of such waivers which may have been requested are such that they may be waived without jeopardy to the public health, safety and general welfare.

**16.7.4.1 Objectives Met.** In granting modifications or waivers, the Planning Board must require such conditions as will, in its judgment, substantially meet the objectives of the requirements so waived or modified.

I certify that, to the best of my knowledge, the information provided in this application is true and correct and will not deviate from							
the plans submitted without notifying the Kittery Planning Department of any changes.							
Applicant's	23: ()	Owner's	See attached LOA				
Signature: Date:	07/22/21	Signature: Date:	07/22/21				

#### COMPLETED BY OFFICE STAFF

ASA CHARGE		AMOUNT	ASA CHARGE		AMOUNT
REVIEW			SERVICES		
LEGAL FEES	(TBD)		Recorder		\$35
ENGINEERS REVIEW	(TBD)		FACT FINDING (7	TBD)	
ABUTTER NOTICES			3 <sup>RD</sup> PARTY INSPECTIONS	TBD)	
POSTAGE		\$20	OTHER PROFESSIONAL SERVICES		\$50
LEGAL NOTICES			PERSONNEL		
ADVERTISING		\$300	SALARY CHARGES IN EXCESS OF 20 HOU	RS	
SUPPLIES					
OFFICE		\$5			
SUI	B TOTAL		SUB T	OTAL	
			TOTAL ASA REVIEW F	EES	



# TOWN OF KITTERY MAINE TOWN PLANNING DEPARTMENT

200 Rogers Road, Kittery, Maine 03904 PHONE: (207) 475-1323 Fax: (207) 439-6806 www.kittery.org

# **APPLICATION: RIGHT-OF WAY PLAN REVIEW**

(APPLICABLE FOR A SINGLE LOT)

FEE FOR REVIEW		1	<b>□</b> \$3	00.00		Am	ount Paid:	\$	Date: _		
PROPERTY DESCRIPTION		Parcel ID	Мар	67	Lot	1	Zone(S): Base Overlay MS4	MU YES_XNO	Total Land Area	1,040,714 sf (23.86 acres)	
		Physical Address	524 L	524 U.S. Route 1							
		Name	C-Coa	ast Prop	erties	, LLC					
PROP	ERTY	Phone	(207) 321-9569				Mailing	8 Banks Rock	8 Banks Rock		
INFOF	RMATION	Fax					Address	York, Maine 03911	York, Maine 03911		
		Email	kevin	werikso	n@grr	nail.com					
		Name	Erik Saari			Name of Business	Altus Engineering, Inc	Altus Engineering, Inc.			
APPLICANT'S AGENT INFORMATION		Phone	(603) 433-2335					100 0			
		Fax					Address	Portsmouth NH 0380	71		
		Email	esaari@altus-eng.com			om					
	Existing Cond	i <b>tions</b> : The	e site cu	urrently	hosts	a single-fa	mily resider	nce and some sections of	field with	the remainder	
	of the site being wooded.										
z											
DITO											
SCRII	(Documents for	or dedicatio	<b>cal chang</b> n of the R	; <b>es:</b> {OW, mai	ntenan	ce agreemen	ts, riders to de	eds, grading, drainage and pave	ement, etc	)	
DE	The proposal adds a 60'-wide public right of way to access two private sites. One site is currently for sale while the										
	other is inc	luded in t	he acco	mpanyi	ing site	e plan revi	ew applicati	on. Said site will include a	a new 20	,000 sf	
	building wi	th associa	ated par	king an	d infra	structure.					
l certi	ify that, to the	e best of m	v knowl	edge, th	e infor	mation pro	ovided in this	application is true and corr	ect and v	vill not deviate from	
the P	lan submitted	without n	, otifying	the Kitt	ery To	wn Plannin	g Departmer	it of any changes.			
Appli	cant's ture:	23:	$\mathcal{L}$	$\sim$			Owner's Signature:	See attached LOA	See attached LOA		
Signature: Date:		07/22/21					Date:	07/22/21	07/22/21		

# **Minimum Submission Requirements**

	□ 15 COPIES OF THE RIGHT OF PLAN – 5 OF WHICH MUST BE 24"X 36"						
PRIOR PLANN INFOR DETEN 16.10.	TO COMMENCEMENT OF THE REVIEW PROCESS, THE NING BOARD WILL DECIDE WHETHER SUFFICIENT MATION HAS BEEN PROVIDED AND WILL VOTE TO RMINE COMPLETENESS/ACCEPTANCE. See Section 5.2	1) (I	Show the location and description of all structures, including: ☐ existing and proposed signage ☐ details of all structures and accesses located within one hundred (100) feet of the property line. The detail sheet must show:				
тн	E APPLICATN IS RESPONSIBLE TO <u>CLEARLY DESCRIBE THE</u> <u>PROJECT</u> .	,	<ul> <li>Structural pavement sections</li> <li>Brosion control detail</li> <li>Roadway cross sections</li> <li>Trenching details</li> <li>Sufficient detail(s) to clarify construction</li> </ul>				
A)	Paper size: No less than 11" X 17" (reduced) or greater than 24" X 36" (full).	K)	The completed application requires the following legal documents:				
B)	Scale size: □ Under 10 acres: no greater than 1″ = 30′ □ 10 + acres: 1″ = 50′		<ul> <li>A maintenance agreement for R.O.W. as a rider to the deed.</li> <li>Letters of approval from utility companies and town staff</li> </ul>				
C)	<ul> <li>Title block:</li> <li>Applicant's name and address</li> <li>Name of preparer of plans with professional information and professional seal</li> <li>Parcel's tax map identification (map – lot)</li> <li>Date of plan preparation</li> </ul>	L)	<ul> <li>The following supporting documentation:</li> <li>Copy of documents showing owner's legal interest</li> <li>Copy of any existing or proposed property encumbrances</li> <li>Erosion control plan and sedimentation endorsed by York</li> <li>County Soil and Water District</li> <li>A plan for stormwater management prepared by a registered professional engineer</li> </ul>				
D)	<ul> <li>Survey performed and sealed by licensed surveyor:</li> <li>Identify all existing property/R.O.W. markers</li> <li>Show all proposed boundary monuments (per ordinance)</li> </ul>		A copy of the soil survey (specific to this project area) for York County Where the soil survey shows soils with severe restrictions for development, a high intensity Class A soil survey must be submitted				
E)	Provide orientation: <ul> <li>Arrow showing true north and magnetic declination</li> <li>Graphic scale</li> <li>Signature block</li> </ul>	M)	An estimate of the amount and type of vehicular traffic on a daily basis and during peak hours. Where it is anticipated that four hundred (400) vehicle trips per day or more a traffic impact analysis must be conducted in				
F)	The right of way plans must include:      Size of the parcel minus the area in the R.O.W.     Length of lot frontage;		accordance with section 16.10.5.2.D.1.				
	<ul> <li>Zoning and zone boundaries  Front yard setbacks</li> <li>Deed docket and page numbers  Intersecting lot lines</li> <li>Existing topography  Horizontal alignment</li> <li>Vertical profile (existing ground and proposed grades)</li> <li>Sidewalks  Watercourses  forest cover</li> <li>Ledge outcroppings  Proposed areas of blasting</li> <li>Utilities (above and below ground)</li> <li>Above ground utilities (poles) that may be relocated</li> <li>Storm drainage systems and structures</li> <li>Parks  Open space  Conservation easements</li> <li>The location of all natural features or site elements to be preserved.</li> </ul>	N)	<ul> <li><u>Additional Requirements</u>. In its consideration of an application/plan, the Board may at any point in during the review, require the applicant to submit additional materials, studies, analyses, and agreement proposals as it may deem necessary for complete understanding of the application. Such materials may include those listed below.</li> <li>□ Fiscal Impact Analysis. An analysis of the relationship of the revenues to the town from the development and the costs of additional publicly funded resources;</li> <li>□ Traffic Impact Study (see Section 16.10.5.2.D.1)</li> </ul>				
G)	Show and locate on the plans the names and addresses of all owners of record of contiguous property, including those across the street. <u>WITH THE FIRST SUBMITTAL, PROVIDE 2 SETS OF</u> <u>MAILING LABLES</u> .	N T T	NOTE TO APPLICANT: THE PLANNING BOARD MAY CHOOSE TO CONDUCT A SITE WALK. PRIOR TO THE SITE WALK, TEMPORARY MARKERS MUST BE ADEQUATELY PLACED				
Н)	Provide sufficient information to identify and locate each interior lot line, right of way lines, and street alignments.	A	AND APPRAISE THE LAYOUT OF DEVELOPMENT.				
50	BIVITIALS THE TOWN PLANNER DEEMS SUFFICIENTLY LACKING IN CO	UNIEN	I WILL NOT BE SCHEDULED FOR PLANNING BOARD REVIEW.				



# TOWN OF KITTERY ~ MAINE PLANNING OFFICE

200 Rogers Road, Kittery, Maine 03904 PHONE: (207) 475-1323 Fax: (207) 439-6806 www.kittery.org

# APPLICATION: REQUEST FOR WAIVER

THIS REVIEW PROCESS REQUIRES APPROVAL FROM BOTH THE TOWN PLANNER AND THE CODE ENFORCEMENT OFFICER MU Zone 1,040,714 sf Parcel 67 1 **Total Land Area** Map Lot Base ID (23.89 ac.) PROPERTY Overlay DESCRIPTION Physical 524 U.S. Route 1 Address Name C-Coast Properties, LLC PROPERTY 8 Banks Rock Phone (207) 321-9569 Mailing **OWNER'S** Address York, Maine 03911 **INFORMATION** Fax kevinwerikson@gmail.com Email Name of Name Erik Saari Altus Engineering, Inc. **Business APPLICANT'S** Phone (603) 433-2335 133 Court Street AGENT Mailing Fax Portsmouth, NH 03801 **INFORMATION** Address Email esaari@altus-eng.com **Ordinance Section** Describe why this request is being made. \*\*\*EXAMPLE\*\*\* \*\*\*EXAMPLE\*\*\* 16.32.560 (B)- OFFSTREET Requesting a waiver of this ordinance since the proposed professional offices have a written agreement with the abutting Church PARKING. owned property to share parking. See attached Waiver Request Letter DESCRIPTION I certify that, to the best of my knowledge, the information provided in this application is true and correct and will not deviate from the plans submitted without notifying the Kittery Planning Department of any changes. **Applicant's Owner's** See attached Letter of Authorization Signature: Signature: 07/22/21 07/22/21 Date: Date:



Civil Site Planning Environmental Engineering

133 Court Street Portsmouth, NH 03801-4413

July 22, 2021

Kittery Planning Board 200 Rogers Road Kittery, Maine 03904

Re: Waiver Request Good To-Go 524 U.S. Route 1 Kittery, Maine

Dear Members of the Board,

On behalf of the applicant, we respectfully request that the following five provisions of Section 16.8, Attachment 1, Table 1 (Design and Construction Standards for Streets and Pedestrian Ways) for Secondary Collector streets be waived:

- Sidewalk (not proposed where required)
- Longitudinal Street Gradient (7.5% proposed where 7% required)
- Side Slope (2:1 in deep cuts and 1:2 in ledge proposed where 3:1 required)
- Tangent Between Reverse Curves (0', 50' & 54.42' proposed where 100' required)
- Min. Centerline Curve Radius (150', 200' & 200' proposed where 300' required)

The property has a number of unique characteristics that make a strict application of the standards impractical. Due to the need for the proposed roadway to be placed away from the abutting Landmark Hill driveway, the location of the existing house, the presence of a cemetery and the existing topography, adequate space for a roadway fully compliant with the standards is lacking.

The existing slope of the site requires a slightly steeper roadway than permitted. Even with relief from the street gradient requirement, the roadway will still require substantial cutting in some areas. By maintaining a 2:1 slope in these deep cut areas, the overall area of disturbance and tree clearing will be minimized. In addition, initial subsurface investigations indicate the presence of shallow ledge over the majority of the site. We expect that the deepest cut sections will require ledge removal which will leave a stable, near-vertical rock face that will have little potential for erosion. Were the exact letter of the standards applied, the design would result in significantly deeper cuts and longer side slopes that would require more extensive grading activities and ledge removal.

As for horizontal geometry, reduced tangents and centerline radii allow the road to navigate the existing obstacles while maintaining an adequate and safe public accessway. The knock-on effect of this is that the roadway design will promote slower vehicular speeds and will in essence become self-regulating in that respect. In addition, shorter tangents and radii will let the project maintain more of the existing buffer to the abutting property to the south by allowing the road to turn away from the property line more quickly once it passes below the cemetery.

Regarding the sidewalk, installing one at this location would not serve any purpose as the proposed use is not a retail establishment and will therefore not require pedestrian access. There is also no sidewalk network along this section of Route 1 for any new sidewalk to connect to. That said, we have designed the road to be able to easily accommodate a sidewalk in the future if additional development in the vicinity requires it.

We appreciate your time and consideration and hope that you will conclude that these waivers are justified given the nature of the project site. If you have any questions or need additional information, please contact us. We would be happy to address any concerns you may have.

Sincerely,

ALTUS ENGINEERING, INC.

21

Erik B. Saari Vice President

ebs/5116-WaiverRequest-072221

#### Letter of Authorization

I, Kevin W. Erikson of C-Coast Properties, LLC ("LLC"), hereby authorize Altus Engineering, Inc. of Portsmouth, NH to represent the LLC as the Owner in all matters concerning the engineering and related permitting of a site plan on Kittery Tax Map 67, Lot 1 located at 524 U.S Route 1 in Kittery Maine. This authorization shall include any signatures required for Federal, State and Municipal permit applications.

 
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## Letter of Authorization

We, Jennifer Scism and David Koorits of Good To-Go c/o Cape House Management, LLC hereby authorize Altus Engineering, Inc. of Portsmouth, NH to represent us as the Applicant in all matters concerning the engineering and related permitting of a site plan on Kittery Tax Map 67, Lot 1 located at 524 U.S Route 1 in Kittery Maine. This authorization shall include any signatures required for Federal, State and Municipal permit applications.

C Signature

FER SLEDM

David Kourts David Koorits

7/8/2 Date

Signature

franksuk Witness

Print Name

Garmente 7.8.21 Date

# WARRANTY DEED

Know all by these presents that TIDE RUN DEVELOPMENT, LLC, a Maine limited liability company, with a business mailing address of 70 Cider Hill Road, York, Maine 03909, for consideration paid, grants to C-COAST PROPERTIES LLC, a Maine limited liability company, with a business mailing address of P.O. Box 603, York Harbor, Maine 03911, with Warranty Covenants, the real property, situated partially in the Town of York and partially in the Town of Kittery, County of York and State of Maine, described as follows:

#### SEE EXHIBIT A ATTACHED HERETO

IN WITNESS WHEREOF, the said TIDE RUN DEVELOPMENT, LLC, has caused this instrument to be signed in its company name, under seal, by DEBORAH E. ERIKSON, its Manager, duly authorized, this  $24^{44}$  day of September 2018.

**TIDE RUN DEVELOPMENT, LLC** By:

Manacek

DEBORAH E. ERIKSON, MANAGER

STATE OF MAINE

York, ss.

September 24. 2018

Then personally appeared the above named Deborah E. Erikson and acknowledged the foregoing instrument to be her free act and deed in her said capacity and the free act and deed of said limited liability company.

Before me. Attornex at Law/N<del>otary</del>

J. Ballow Mame: mission Expires:

B a l l o u & B e d e l l 408 US Route One, 2<sup>nd</sup> Floor York Maine 03909 (207) 363-5300

# Ехнівіт А

# PARCEL 1

A certain lot or parcel of land together with the buildings thereon situate in said Kittery and in part in the Town of York. Both in the County of York and State of Maine bounded and described as follows:

BEGINNING on U.S. Highway No. 1 at land of Leo H. and Barbara L. Cain;

THENCE running South 27° East by land of said Cains to a marked tree in line of a stone wall;

THENCE continuing on a southeasterly course on the line of land formerly conveyed to said Leo and Barbara Cain to a stone wall on line of land now or formerly owned by Leon W. Main;

THENCE turning and running southwesterly as the wall runs by other land now or formerly of said Main to a corner in the wall;

THENCE turning and running southeasterly as the wall runs to land now or formerly of one Fuller, being the southeasterly boundary of the farm herein conveyed;

THENCE southwesterly by said Fuller land to land of William Crawford;

THENCE northwesterly land of said Crawford to land of Sheldon Doody;

THENCE northeasterly, four hundred (400) feet, by land of said Doody;

THENCE northwesterly, five hundred forty-four (544) feet, by land of said Doody to said U.S. Highway No. 1;

THENCE northeasterly by said Highway, seven hundred (700) feet, more or less, to the PLACE OF BEGINNING.

Containing forty acres, more or less.

Subject to a pole easement granted to New England Tel. & Tel. Co. by Wallace A. Main, by instrument dated September 3, 1925 and recorded at York County Registry of Deeds in Book 755, Page 21. Title reference is made to a deed recorded at York County Registry of Deeds in Book 1826, Page 490.

# PARCEL 2

A certain lot or parcel of land situate in the Town of York, County of York and State of Maine, being a woodlot lying adjacent to and north of the Kittery-York town line; being a portion of the

"Emerson Field", and delineated on Plan of Land of Kyra M. Kaplan by Moulton Engineering Co., dated 10/18/72, recorded in York County Registry of Deeds in Plan Book 59. Page 18, bounded and described as follows:

BEGINNING at a pipe in the ground beside an old set of bars at the southeasterly corner of said parcel, and running North eighty-five degrees forty-one minutes thirty seconds East (N 85° 41' 30" E) two hundred eighty-nine and thirty hundredths (289.30) feet to a pipe in the ground beside an old elm tree with spike in it;

THENCE running North twenty-two degrees thirty-eight minutes forty-five seconds West (N 22° 38' 45" W) six hundred ninety-nine and forty-six hundredths (699.46) feet to a pipe driven in a pile of stones;

THENCE running southwesterly by and along a stone wall four hundred forty-eight and fortynine hundredths (448.49) feet to a pipe in the corner of said stone wall;

THENCE running southeasterly by and along another stone wall four hundred sixty-seven and sixty-seven hundredths (467.67) feet to the POINT OF BEGINNING.

Together with the right of way, leading from said woodlot through land of heirs of Wallace A. Main to the highway known as U.S. Route 1.

Meaning and intending and hereby conveying the second parcel only described and conveyed in deed of Jack A. Drobish et ux. to Frank G. Leighton, Jr. et al., dated May 27, 1972, recorded at said Registry in Book 1950, Page 88. Title reference is made to a deed recorded at York County Registry of Deeds in Book 2010, Page 193.

# PARCEL 3

A certain lot or parcel of land situated in said York containing fifteen (15) acres, more or less, bounded and described as follows:

BEGINNING at the southerly corner of the parcel of land herein conveyed adjoining land of the heirs of Edmund Moulton at the junction of the stonewall;

THENCE running from said corner northeasterly by said heirs land and stonewall fifty-seven rods and three links to land now or formerly of Ida May Trefethen to the junction of the wall;

THENCE northwesterly by said Trefethen land and wall fifty-six rods and sixteen links to corner of wall;

THENCE southwesterly by said Trefethen land and land formerly of Wallace A. Main, thirty rods to point and pile of stones by the wall near a maple tree;

THENCE South about 20° East forty-one and eight tenths rods to a large elm tree, marked;

THENCE South about eighty-two degrees West about sixteen and three tenths rods to a point at the easterly end of a set of bars; thence southeasterly by land formerly of Alsbury J. Goodwin twenty-seven and eight tenths rods to the place of beginning. Being a portion of the Emerson Field so called.

Title reference is made to a deed recorded at York County Registry of Deeds in Book 1826, Page 492.

Excepting the land conveyed to Leo H. Cain, et ux. by deed dated June 20, 1955 and recorded in Book 1289, Page 77 at the York County Registry of Deeds.

Excepting the land conveyed to Leo H. Cain, et ux. by deed dated November 19, 1968 and recorded at Book 1969, Page 696 at the York County Registry of Deeds.

Being the same premises conveyed by Krya M. Berson and Eliot L. Berson, Co-Trustees of Heritage Realty Trust to Tide Run Development, LLC by deed dated October 18, 2016 and recorded at York County Registry of Deeds in Book 17345, Page 846.









# TOWN OF KITTERY, MAINE

SEWER DEPARTMENT 200 Rogers Road, Kittery, ME 03904 Telephone: (207) 439-4646 Fax: (207) 439-2799

Good To – Go Erik Saari 584 Route 1, Kittery, ME 03904

July 12, 2021

**RE:Sewer Availability** 

# Erik,

This letter is to confirm that there is sanitary sewer service available for the Good To-Go project Located at 584 Route 1, The sewer system (piping and pumping stations) and the treatment facility has the capacity and ability to handle the projected flow increase of 2,400 GPD.

If you have further questions or concerns please contact me.

Sincerely Yours

Recoverable Signature

Timothy Babkirk

Timothy Babkirk Superintendent Signed by: 8d59976c-e219-4963-8b87-4c42e7e470e3

Timothy Babkirk Superintendent of Sewer Services Town of Kittery 200 Rogers Rd Kittery ME 03904 1-207-439-4646 tbabkirk@kitteryme.org

Julia H. O'Connell, Secretary Michael S. Rogers, Superintendent

#### OFFICE OF

# **KITTERY WATER DISTRICT**

17 State Road Kittery, ME 03904-1565 TEL: 207-439-1128 FAX: 207-439-8549 E-Mail: kitterywater@comcast.net

Kittery Planning Board 200 Rogers Road Kittery, ME 03904

July 12, 2021

Re: Good To-Go Specialty Food Facility

Dear Planning Board Members,

Please accept this letter as verification that the Kittery Water District does have the capacity to supply municipal water service both for domestic purposes and fire protection for the proposed Good To-Go Specialty Food Facility at 524 U.S. Route 1 in Kittery.

Sincerely,

Michael A ROGL

Michael S. Rogers Superintendent

cc: Erik Saari, Altus Engineering, Inc.

# GOOD TO-GO SPECIALTY FOOD FACILITY

# Owner:

C-COAST PROPERTIES, LLC

8 Banks Rock York Harbor, Maine 03911

# Applicant:

# GOOD TO-CO

GOOD TO-GO c/o Cape House Management, LLC Architect: 484 U.S. Route 1 Kittery, Maine 03904 . . . . (207) 451-9060

# Civil Engineer:



133 Court Street (603) 433-2335

Portsmouth, NH 03801 www.altus-eng.com

# Soil and Wetland Scientist: Michael Cuomo, M.S.S. #211

6 York Pond Road York, ME 03909 (207) 363-4532

# Surveyor:



CONSULTANTS Engineers, Planners, Surveyors P.O. Box 100, South Berwick, Maine 03908 Tel. 207-384-2550 www.civcon.com



# Bild Architecture

30 Danforth St., Suite 213 Portland, Maine 004101 (207) 408-0168

# General Contractor:



Sheridan Construction Corp.

33 Sheridan Drive Fairfield, Maine 04937 (207) 453-9311

# Landscape Architect:



woodburn & c o m p a n y LANDSCAPE ARCHITECTURE

103 Kent Place Newmarket, New Hampshire Phone: 603.659.5949

VISIBLELIGHT

# Lighting Consultant:



24 STICKNEY TERRACE, SUITE 6 HAMPTON, NH 03842 603) 926-6049

524 U.S. ROUTE 1 KITTERY, MAINE

# Assessor's Parcel 67, Lot 1

Plan Issue Date:

July 22, 2021 Planning Board Submission



# Sheet Index Title

Existing Cond Right of Way Right of Way Soils Plan Site Plan Roadway Plan Highway Acce Stormwater I Erosion and Utility Plan Lighting Plan Landscape Pla Detail Sheet Front Elevation Side Elevatior

# Permit Sum

Kittery Site Pla MDEP Stormwo MDOT Entrance Notice of Inter THIS DRAWING SET HAS NOT BEEN RELEASED FOR CONSTRUCTION



		Sheet No.:	Rev.	Date
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an Approval ater Permit e Permit nt	07/22/21 -/-/- -/-/- By Contractor	r 14 day	-/-/- -/-/- -/-/- s prior to c	onstruction



PLOT DATE: 4/21/2021 10:19 AM



# NOTES

ZONING SUMMARY:

AREA:	1,040,714 S.F. (23.89± ACRES)
ZONE:	MIXED USE (MU)
	SHORELAND OVERLAY ZONE

DIMENSIONAL STANDARDS (MU)

NOTES:

- 1. THE PERIMETER BOUNDARY SHOWN HERON IS PER PLAN REFERENCE #1.
- 2. NORTH AS DEPICTED HERON IS REFERENCED TO GRID NORTH, NAD83, MAINE STATE PLAN COORDINATE SYSTEM WEST ZONE. ORIENTATION IS DERIVED FROM A GPS SURVEY COMPUTES UTILIZING THE NGS ON-LINE PROCESSING SERVICE REFERENCE FRAME IS NAD83 (2011) CORS96 EPOCH 2010.0000. THE SURVEY IS TIED TO CORS STATION BOSTON WAAS 1 CORS (ZBW1), BARLETT CORS (BARN) AND BRUNSWICK CORS (BRU1).
- 3. WETLANDS, VERNAL POOL, BUILDING, CEMETERY AND STONEWALL LOCATIONS AS SHOWN ARE BASED ON REFERENCE PLAN 2.

# PLAN REFERENCE:

- 1. "EXISTING CONDITIONS PLAN, PLAN OF LANDS OF C-COAST PROPERTIES, LLC, KITTERY TAX MAP 67, LOT 1, YORK TAX MAP 87, LOTS 67 & 68, US ROUTE 1, KITTERY AND YORK, MAINE" BY CIVIL CONSULTANTS, DATED APRIL 14, 2021, UNRECORDED.
- 2. "STANDARD BOUNDARY SURVEY FOR C-COAST PROPERTIES LLC, US ROUTE 1, YORK/KITTERY, MAINE" BY ANDERSON LIVINGSTON ENGINEERS, INC., DATED OCTOBER 26, 2018, UNRECORDED, ALE FILE NO. 6745.0000, ALE PLAN NO. 2569.181001.

# MONUMENTATION:

PRIOR TO CERTIFICATION OF OCCUPANCY OF ANY LOT SHOWN HEREON, MONUMENTS SHOWN AS "TO BE SET" MUST BE SET UNDER THE DIRECTION OF A MAINE LICENSED LAND SURVEYOR. ROADWAY MONUMENTATION SHALL BE A MINIMUM OF FOUR (4) INCHES SQUARE STONE MONUMENTS AND INSTALLED AS SHOWN ON SUBDIVISION PLAN AND PER TOWN STANDARDS.

# <u>APPROVALS:</u>

KITTERY PLANNING BOARD -PRELIMINARY SITE PLAN APPROVAL, DATED 05/27/21 ROAD NAME APPROVAL, DATED \_\_\_\_\_ FINAL APPROVAL, DATED \_\_\_\_\_ WAIVERS GRANTED, DATED \_\_\_\_\_

1. SECTION 16.8, ATTACHMENT 1, TABLE 1 (SECONDARY COLLECTOR ROAD): • SIDEWALK (NOT PROPOSED WHERE REQUIRED)

- LONGITUDINAL STREET GRADIENT (7.5% WHERE 7% REQUIRED)
- SIDE SLOPE (2:1 IN DEEP CUTS OR 1:2 IN LEDGE WHERE 3:1 REQUIRED)

• TANGENT BETWEEN REVERSE CURVES (0', 50' & 54.42' WHERE 100' REQ.) • MIN. CENTERLINE CURVE RADIUS (150', 200' & 200' WHERE 300' REQ.) MAINE DEP STORMWATER PERMIT, DATED MAINE DOT ENTRANCE PERMIT, DATED \_\_\_\_\_

TOWN OF KITTERY CONDITIONS OF APPROVAL:

- 1. NO CHANGES, ERASURES, MODIFICATIONS OR REVISIONS MAY BE MADE TO ANY PLANNING BOARD APPROVED FINAL PLAN (TITLE 16.10.9.1.2).
- 2. APPLICANT/CONTRACTOR WILL FOLLOW MAINE DEP BEST MANAGEMENT PRACTICES FOR ALL WORK ASSOCIATED WITH SITE AND BUILDING CONSTRUCTION TO ENSURE ADEQUATE EROSION CONTROL AND SLOPE STABILIZATION.
- 3. PRIOR TO THE COMMENCEMENT OF GRADING AND/OR CONSTRUCTION WITHIN A BUILDING ENVELOPE, AS SHOWN ON THE PLAN. THE OWNER AND/OR DEVELOPER MUST STAKE ALL CORNERS OF THE ENVELOPE. THESE MARKERS MUST REMAIN IN PLACE UNTIL THE CODE ENFORCEMENT OFFICER DETERMINES CONSTRUCTION IS COMPLETED AND THERE IS NO DANGER TO AREAS THAT ARE, PER PLANNING BOARD APPROVAL, TO REMAIN UNDISTURBED.
- 4. ALL NOTICES TO APPLICANT CONTAINED IN THE FINDINGS OF FACT (DATED *--/--)*.

RIGHT—OF—WAY

±441,825 S.F. (±10.14 AC.) ROW AREA







LTC LTB DxB DxB UTC DxB LTC DxB LTC DxB LTC DxB LTC DxB LTC LTC LTC LTC LTC LTC LTC LTC	LTB LTB LTC LTC LTC LTC LTC LTC LTC LTC LTC LTC	B TB LTC LTB TF #17 LTE SCB	Image: Construction of the second struct
Test Pit Number: 11 Description 2* Leaf litter. 0-7* Dark brown (10YR 3/3) silt loarn, granular, friable. 7-10* Light yellowish brown (2.5Y 6/4) silt loarn, blocky, friable, redox. 10-28* Pale olive (5Y 6/3) silt loarn, massive, friable, redox. 10-28* Pale olive (5Y 6/3) silt loarn, massive, from, massive, firm, redox. 29-44* Light yellowish brown (2.5Y 4/4) sand, massive, loose, w/ strate of firm silt, redox. Soll Name: Westbury variant Depth to Beascription 1* Leaf litter. 0-7* Dark brown (10YR 3/3) silt loarn, granular, friable. 7-11 28* Light yellowish brown (10YR 5/6) silt loarn, blocky, friable, redox. 28-64* Olive brown (10YR 5/6) silt loarn, blocky, friable. 7-11 28* Light yellowish brown (10YR 5/6) silt loarn, blocky, friable, redox. 28-64* Olive brown (2.5Y 4/4) sand, massive, loose, redox. 28-64* Olive brown (10YR 5/6) silt loarn, massive, firm, redox. 28-64* Olive brown (10YR 5/6) silt loarn, massive, firm, redox. 28-64* Olive brown (2.5Y 4/4) sand, massive, loose, redox. 28-64* Olive brown (10YR 5/6) silt loarn, massive, firm, redox. 301 Name: Nicholville variant Depth to Bearchion 1* Leaf litter. 0-10* Dark brown (10YR 3/3) stony fine sandy loarn, blocky, friable. 10-24* Strong brown (10YR 3/3) stony fine sandy loarn, blocky, firable. 24-32* Light yellowish brown (2.5Y 6/4) stony fine sandy loarn, blocky, firm, redox. 301 Name: Unbridge variant Depth to Bearchion 2* Leaf litter. 0-6* Brown (10YR 4/3) fine sandy loarn, granular, friable. 17* Yellowish brown (10YR 5/6) fine sandy loarn, blocky, firable, redox. 32* Test Pit Number: 14 Beath Description 2* Leaf litter. 0-6* Brown (10YR 4/3) fine sandy loarn, blocky, friable, redox. 32* Jight olive brown (2.5Y 5/4) stratified fine sand and silt, massive, firm, redox. 301 Name: Nicholville Depth to Bearcok: none 301 Name: Nicholville	Test Pit Number: 15 Description 1 Leef litter: 0-6 Brown (10YR 4/3) stony fine sandy loam, granular, friable. 6-12 Dark yellowish brown (10YR 5/6) stony fine sandy loam, blocky, friable. 12-18 Light yellowish brown (2.5Y 6/4) stony fine sandy loam, blocky, friable. Depth to Seasonal High Water Table: none Depth to Seasonal High Water Table: none Depth to Description 1 Leaf litter. 0-7 Very dark gray (2.5Y 3/1) silt loam, granular, friable, redox. 7-13 Light gray (2.5Y 7/1) silt loam, blocky, friable, redox. 13-22 Olive brown (2.5Y 4/4) silt loam, blocky, firm, redox. 22-50 Olive (5Y 5/4) silty clay loam, maskive, firm, redox. Soil Name: Santic Depth to Bedrock: none Test Pit Number: 17 Depth to Bedrock: none Test Pit Number: 17 Depth to Bedrock: none Test Pit Number: 18 Depth to Sasonal High Water Table: none Depth to Bedrock: 12" Test Pit Number: 18 Depth to Sasonal High Water Table: none Depth to Bedrock: 12" Test Pit Number: 19 Depth to Bedrock: 10" Table Norme: Waumbek Depth to Bedrock: 10" Depth to Bedrock: 10" Table Norme: 10 Depth to Bedrock: 10" Table Norme: 11" Depth to Bedrock: 10" Table Norme: 11" Depth to Bedrock: 10" Depth to Bedrock: 10" Table Norme: 11" Depth to Bedrock: 10" Depth	Test Pit Number: 20       (IN FEET )         Test Pit Number: 20       Dark pellowish brown (10YR 3/3) fine sandy loarn, granular, friable.         0-10       Dark brown (10YR 3/3) fine sandy loarn, granular, friable.         10-28:       Dark yellowish brown (10YR 4/4) fine sandy loarn, blocky, friable.         28-46:       Light yellowish brown (10YR 4/4) fine sandy loarn, blocky, friable.         28-46:       Light yellowish brown (2SY 6/4) gravelly loarny sand, massive, friable, redox.         Soil Name:       Waumbek         Depth to Bedrock:       46:         Test Pit Number: 21       Depth to Bedrock:         Depth to Bedrock:       46:         10-28:       Dark yellowish brown (10YR 4/6) stony fine sandy loarn, blocky, friable.         28-66:       Light olive brown (10YR 4/6) stony fine sandy loarn, blocky, friable.         0-10:       Very dark brown (10YR 4/6) stony fine sandy loarn, massive, firm, redox.         Soil Name:       Depth to Bedrock:         Depth to Bedrock:       12*         Depth to Bedrock:       12*         Soil Observation:       Lyran         Depth to Seasonal High Water Table:       none         Depth to Bedrock:       12*         Soil Observation:: A       Lyran         Depth to Seasonal High Water Table:       none         De	APPLICANT: GOOD TO-GO c/o CAPE HOUSE MANAGEMENT, LLC 484 US ROUTE 1 KITTERY, MAINE 03904 PROJECT: GOOD TO-GO SPECIALTY FOOD FACILITY TAX MAP 67, LOT 1 524 U.S. ROUTE 1 KITTERY, MAINE IITLE: SOILS PLAN SHEET NUMBER: C-2












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<ol> <li>2. DETECTABLE WARNING TAPE SHAL ALL BURIED UTILITIES, COLORS PE</li> <li>3. LIGHTING CONDUIT SHALL BE PVC</li> <li>4. ALL LIGHTING MATERIALS AND WO NATIONAL ELECTRICAL CODE AND</li> <li>5. ALL LIGHTING FIXTURES SHALL BE TEMPERATURE SO AS TO BE DARI</li> <li>6. CONTRACTOR SHALL COORDINATE CONTRACTOR FOR ALL SITE ELECTION</li> </ol>	L BE PLAC R THE RES SCH 40. RKMANSHIF LOCAL REG FULL CUT K-SKY CON WITH ARCH IRICAL WOF	ED OVER SPECTIVE U GULATIONS -OFF AND MPLIANT. HITECT ANI RK INCLUD	THE EN JTILITY CONFORM 3. 0 3000K D BUILD ING BUT	TIRE LENGTH PROVIDERS. I TO THE COLOR ING ELECTR	H OF 9. TH LIG DE IN MC CC 10. SE ICAL ED TO	IIS LIGHTIN GHT, INC., EVIATIONS STALLATION DUNTING H DNTRACTOF	G DESIGN IS BA 24 STICKNEY TE MAY SIGNIFICANT N, CRITICAL SITE EIGHT, CIRCUITR` R, ARCHITECT AN SHEETS FOR FIX	SED C RRACI ILY AF INFOI Y, ETC ID SPE TURE	DN LIMITE E, SUITE FFECT PF RMATION C.) SHALL ECIFIER. CUT SHE
7. COORDINATE WITH ARCHITECTURAL	PLANS F	OR ALL BU	JILDING-		<b>κ</b> ς,		Statistics		
FIXTURES, TYPES, LOCATIONS AND	) WIRING.						Description Outside of Park	ing S	Symbol + 0
	Schedule						Parking Lot		+ 1.
	Symbol	Label	QTY 2	Manufacturer Lithonia Lighting	Catalog Number DSXO LED P3 30K TFTM MVOLT HS SPA DDBXD with SSS 16 4C	Description DSX0 LED A houseside s	rea Fixture with hield; mounted at	Lamp LED	F
	•	S4	3	Lithonia	DM19AS DDBXD	DSX0 LED A	rea Fixture;	LED	
		S-BLC			with SSS 16 4C DM19AS DDBXD	on 2ft base	)		Ň
		w	6	Lithonia Lighting	WDGE2 LED P3 30K 80CRI MVOLT DDBXD	WDGE2 LED at 16ft	Wallpack; mounted	LED	



GRAPHIC SCALE 0 20 40 80 160	ALTUS ENGINEERING. ING.
( IN FEET )	133 Court Street (603) 433-2335Portsmouth, NH 03801 www.altus-eng.com
	VISIBLELIGHT
	ISSUED FOR:
	PLANNING BOARD
· · — · — · — · — · — · — · — ·	JULY 22, 2021
	REVISIONSNO. DESCRIPTIONBYDATE0PLANNING BOARDEBS07/22/21
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	$\frac{\text{SCALE:}}{22^{"}} \times .34^{"} - 1^{"} = 40^{'}$
	$11" \times 17" - 1" = 80'$
	OWNER:
	C-COAST PROPERTIES, LLC
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	YORK HARBOR, MAINE 03911
	APPLICANT:
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	GOOD TO-GO c/o CAPE HOUSE MANAGEMENT, LLC
	484 US ROUTE 1 KITTERY, MAINE 03904
,o <sup>°°</sup> . * 0 <sup>°</sup>	
S	PROJECT: GOOD TO-GO SPECIALTY FOOD
= = _ = _ = _	TAX MAP 67, LOT 1 524 U.S. ROUTE 1
= = = = = =	KITTERY, MAINE
	LIGHTING PLAN
	SHEET NUMBER:
	<b>C-9</b>

# *Landscape* Notes

Design is based on drawings by Altus Engineering, Inc. dated July 22, 2021 and may require adjustment due to actual field conditions. The contractor shall follow best management practices during construction and shall take all means necessary to stabilize and protect the site

US

ROUTE

-

- from erosion. Erosion Control shall be in place prior to construction.
- Erosion Control to consist of Hay Bales and Erosion Control Fabric shall be staked in place between the work and Water bodies, Wetlands and/or drainage ways prior to any construction. 5. The Contractor shall verify layout and grades and inform the Landscape Architect or Client's Representative of any discrepancies or changes in
- layout and/or grade relationships prior to construction 6. It is the contractor's responsibility to verify drawings provided are to the correct scale prior to any bid, estimate or installation. A graphic scale bar has been provided on each sheet for this purpose. If it is determined that the scale of the drawing is incorrect, the landscape architect will
- provide a set of drawings at the correct scale, at the request of the contractor. 7. Trees to Remain within the construction zone shall be protected from damage for the duration of the project by snow fence or other suitable means of protection to be approved by Landscape Architect or Client's Representative. Snow fence shall be located at the drip line at a minimum and shall include any and all surface roots. Do not fill or mulch on the trunk flare. Do not disturb roots. In order to protect the integrity of the roots, branches, trunk and bark of the tree(s) no vehicles or construction equipment shall drive or park in or on the area within the drip line(s) of the tree(s). Do not store any refuse or construction materials or portalets within the tree protection area.
- Location, support, protection, and restoration of all existing utilities and appurtenances shall be the responsibility of the Contractor. The Contractor shall verify exact location and elevation of all utilities with the respective utility owners prior to construction. Call DIGSAFE at 1-888-344-7233.
- 10. The Contractor shall procure any required permits prior to construction. 11. Prior to any landscape construction activities Contractor shall test all existing loam and loam from off-site intended to be used for lawns and plant beds using a thorough sampling throughout the supply. Soil testing shall indicate levels of pH, nitrates, macro and micro nutrients, texture, soluble salts, and organic matter. Contractor shall provide Landscape Architect with test results and recommendations from the testing facility along with soil amendment plans as necessary for the proposed plantings to thrive. All loam to be used on site shall be amended as approved by the Landscape Architect prior to placement.
- 12. Contractor shall notify landscape architect or owner's representative immediately if at any point during demolition or construction a site condition is discovered which may negatively impact the completed project. This includes, but is not limited to, unforeseen drainage problems, unknown subsurface conditions, and discrepancies between the plan and the site. If a contractor is aware of a potential issue, and does not bring it to the attention of the landscape architect or owner's representative immediately, they may be responsible for the labor and materials associated with correcting the problem.
- 13. The Contractor shall furnish and plant all plants shown on the drawings and listed thereon. All plants shall be nursery-grown under climatic conditions similar to those in the locality of the project. Plants shall conform to the botanical names and standards of size, culture, and quality for the highest grades and standards as adopted by the American Association of Nurserymen, Inc. in the American Standard of Nursery Stock, American Standards Institute, Inc. 230 Southern Building, Washington, D.C. 20005.
- 14. A complete list of plants, including a schedule of sizes, quantities, and other requirements is shown on the drawings. In the event that quantity discrepancies or material omissions occur in the plant materials list, the planting plans shall govern.
- 15. All plants shall be legibly tagged with proper botanical name. 16. The Contractor shall quarantee all plants for not less than one year from time of acceptance.
- 17. Owner or Owner's Representative will inspect plants upon delivery for conformity to Specification requirements. Such approval shall not affect the right of inspection and rejection during or after the progress of the work. The Owner reserves the right to inspect and/or select all trees at the place of growth and reserves the right to approve a representative sample of each type of shrub, herbaceous perennial, annual, and ground cover at the place of growth. Such sample will serve as a minimum standard for all plants of the same species used in this work. 18. No substitutions of plants may be made without prior approval of the Owner or the Owner's Representative for any reason.
- 19. All landscaping shall be provided with the following:
- a. Outside hose attachments spaced a maximum of 150 feet apart, and An underground irrigation system, or
- A temporary irrigation system designed for a two-year period of plant establishment.
- 20. If an automatic irrigation system is installed, all irrigation valve boxes shall be located within planting bed areas. 21. The contractor is responsible for all plant material from the time their work commences until final acceptance. This includes but is not limited to maintaining all plants in good condition, the security of the plant material once delivered to the site, and watering of plants. Plants shall be appropriately watered prior to, during and after planting. It is the contractor's responsibility to provide clean water suitable for plant health from off site, should it not be available on site.
- 22. All disturbed areas will be dressed with 6" of topsoil and planted as noted on the plans or seeded except plant beds. Plant beds shall be prepared to a depth of 12" with 75% loam and 25% compost.
- 23. Trees, ground cover, and shrub beds shall be mulched to a depth of 2" with one-year-old, well-composted, shredded native bark not longer than 4" in length and ½" in width, free of woodchips and sawdust. Mulch for ferns and herbaceous perennials shall be no longer than 1" in length. Trees in lawn areas shall be mulched in a 5' diameter min. saucer. Color of mulch shall be black.
- 24. Drip strip shall extend to 6" beyond roof overhang and shall be edged with 3/16" thick metal edger. 25. In no case shall mulch touch the stem of a plant nor shall mulch ever be more than 3" thick total (including previously applied mulch) over the root
- ball of any plant. 26. Secondary lateral branches of deciduous trees overhanging vehicular and pedestrian travel ways shall be pruned up to a height of 6' to allow clear and safe passage of vehicles and pedestrians under tree canopy. Within the sight distance triangles at vehicle intersections the canopies shall be raised to 8' min.
- 27. Snow shall be stored a minimum of 5' from shrubs and trunks of trees.
- 28. Landscape Architect is not responsible for the means and methods of the contractor.

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trees. Each wire shall be flagged with a visual marker. 5' long min, wooden stakes shall be used to anchor the wires. Stakes shall be driven at least 12" outside the edge of the planting pit into stable soil. Remove all staking NO LATER than the end of the first growing season after planting.

Do not heavily prune the tree at planting

Prune only cross-over limbs, co-dominant

nterior twigs and lateral branches may be

the crowr

leaders, and broken or dead branches. Some

pruned; however, Do NOT remove the terminal

buds of branches that extend to the edge of

Trees less than 3" in caliper shall be staked

with three stakes per tree, spaced evenly

around the trunk with 12 gauge wire. Plastic

hose sections shall be used at attachment to

Mark the north side of the tree in the nursery Rotate the tree to face north at the site whenever possible

4 in high earth saucer beyond edge of root

2 IN. max. Mulch. Do NOT place mulch in contact with tree trunk. Maintain the mulch weed-free for a minimum of three years after planting.

Tamp soil around root ball base firmly with foot pressure so that root ball does not

Place root ball on unexcavated or tamped

# Tree Planting Detail







Drawn By:	VM
Checked By:	RW
Scale:	1 = 40' - 0"
Date:	July 22, 2021
Revisions:	



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## SEDIMENT AND EROSION CONTROL NOTES

## PROJECT NAME AND LOCATION

Good To-Go, Inc. 524 U.S. Route 1 Kittery, Maine

Latitude: 043° 07' 52" N Lonaitude: 070° 42' 04" W

## DESCRIPTION

The project includes the development of a specialty food manufacturing facility with an access road, paved parking lot and associated utility and drainage improvements.

## SEQUENCE OF MAJOR ACTIVITIES

- 1. Install temporary erosion control measures, including perimeter controls and stabilized construction entrances
- 2. Clear and grub wooded areas to the limits of work and strip and stockpile loam. Stockpiles shall be temporarily stabilized with hay mulch and surrounded by a hay bale or silt fence barrier until material is removed and final grading is complete.
- Rough grade site to include stormwater facilities. Construct building foundation.
- Construct drainage structures and utilities.
- Install roadway and parking lot base materials. Install pavement binder course.
- Complete building construction.
- Install curbing. 10. Install loam where required and stormwater basin filter material where specified.
- Install pavement top course.
- 12. Install other site features and landscaping. 13 Stabilize any remaining disturbed areas
- 14. When all construction activity is complete and site is stabilized, remove perimeter controls and sediment that has been trapped by these devices.

## NAME OF RECEIVING WATER

The site drains to the Atlantic Ocean by way of Johnson Brook.

## TEMPORARY EROSION AND SEDIMENT CONTROLS AND STABILIZATION PRACTICES

All work shall be in accordance with state and local permits. Installation or construction of erosion control measures shall conform to the practices described in the "2014 Revision to the 2003 Maine Erosion and Sediment Control Field Guide for Contractors, published by the Maine Department of Environmental Protection

Minimum erosion control measures will need to be implemented and the contractor will be responsible to maintain all components of the erosion control plan until the site is fully stabilized. However, based on site and weather conditions during construction, additional erosion control measures may need to be implemented. All areas of instability and erosion must be repaired immediately during construction and need to be maintained until the site is fully stabilized or vegetation is established. A construction log must be maintained for the erosion and sedimentation control inspections and maintenance.

As indicated in the sequence of Major Activities, perimeter controls shall be installed prior to commencing any clearing or grading of the site. Structural controls shall be installed concurrently with the applicable activity. Once construction activity ceases permanently in an area, silt fences and hay bale barriers and any earth/dikes will be removed once permanent measures are established.

During construction, runoff will be diverted around the site with stabilized channels where possible channels where possible. Sheet runoff from the site will be filtered through hay bale barriers, stone check dams, and/or silt fences. All storm drain inlets shall be provided with inlet filters or stone check dams. Stone rip rap shall be provided at the outlets of drain pipes and culverts where shown on the drawings.

Temporary and permanent vegetation and mulching is an integral component of the erosion and sedimentation control plan. All areas shall be inspected and maintained until desires vegetative cover is established. These control measures are essential to erosion prevention and also reduce costly rework of graded and shaped areas.

Temporary vegetation shall be maintained in these areas until permanent seeding is applied. Additionally, erosion sedimentation measures shall be maintained until permanent vegetation is established

## INSTALLATION, MAINTENANCE AND INSPECTION PROCEDURES FOR TEMPORARY EROSION AND SEDIMENT CONTROL MEASURES

## A. GENERAL

- Perimeter controls shall be installed prior to earth moving operations. The smallest practical portion of the site will be denuded at one time and no more than be mulched in one day. All disturbed areas must be stabilized by temporary measures within 5 days of initial disturbance and stabilized by permanent measures immediately after final
- 2. Sediment barriers shall be installed downgradient of stockpiles and diversion swales installed upgradient of stockpiles to prevent movement of soil.
- Built-up sediment shall be removed from silt fence or other barriers when it has reached one-third the height of the tubular barrier or bale, or when "bulges" occur in silt fence. All diversion dikes shall be inspected and any breaches promptly repaired. Temporary seeding and planting shall be inspected for bare spots, washouts, and unhealthy 5.
- 6. The owner's authorized engineer shall inspect the site on a periodic basis to review
- compliance with the plans.
- 7. All ditches and swales shall be stabilized prior to directing runoff to them. All diversion dikes will be inspected and any breaches promptly repaired.
- 8. Temporary water diversion (swales, basins, etc) shall be used as necessary until areas are stabilized. 9. Ponds and swales shall be installed early on in the construction sequence (before rough

grading site). 10. All cut and fill slopes shall be seeded/loamed within 72 hours of achieving finished grade. 11. An area shall be considered stable if one of the following has occurred:

- a. Base coarse gravels have been installed in areas to be paved;
- A minimum of 90% vegetated growth as been established; c. A minimum of 3 inches of non-erosive material such as stone of riprap has been installed;
- d. Erosion control blankets have been properly installed.

## B. MULCHING

- <u>Application</u> \* In sensitive areas (within 100 ft of streams, wetlands and in lake watersheds) temporary mulch shall be applied within 7 days of exposing soil or prior to any storm event. Areas, which have been temporarily or permanently seeded, shall be mulched immediately
- following seeding. Areas which cannot be seeded within the growing season shall be mulched for over-winter protection and the area should be seeded at the beginning of the growing season.
- \* Mulch anchoring should be used on slopes greater than 5% in late fall (past September 15), and over-winter (September 15 - April 15).

### <u>Type of Mulch</u> Hay or Straw Mulches

Organic mulches, including hay and straw, shall be air-dried, free of undesirable seeds and coarse materials. Application rate shall be 2 bales (70-90 pounds) per 1000 sq. ft. or 1.5 to 2 tons (90-100 bales) per acre to cover 75 to 90 % of the ground surface. Hay mulch subject to wind blowing shall be anchored via: netting; peg and twine or tracking.

## Erosion Control Mix

Erosion control mix shall consist primarily of organic material and shall include any of the following: shredded bark, stump grindings, composted bark or other acceptable products based on a similar raw source. Wood or bark chips, ground construction debris or reprocessed wood products shall not be acceptable as the organic component of the mix. It can be used as a stand-alone reinforcement:

- On slopes 2 horizontal to 1 vertical or less.
- \* On frozen ground or forested areas.
- \* At the edge of gravel parking areas and areas under construction.

Other reinforcement BMPs (i.e. riprap) should be used:

- \* On slopes with groundwater seepage; At low points with concentrated flows and in gullies;
- At the bottom of steep perimeter slopes exceeding 100 feet in length; Below culvert outlet aprons; and
- \* Around catch basins and closed storm systems.
- Composition

Erosion control mix shall contain a well-graded mixture of particle sizes and may contain rocks less than 4" in diameter. Erosion control mix must be free of refuse, physical contaminants, and material toxic to plant growth. The mix composition shall meet the following standards: \* The organic matter content shall be between 80 and 100%, dry weight basis. \* Particle size by weight shall be 100% passing a 6" screen and a minimum of 70%,

- maximum of 85%, passing a 0.75" screen. \* The organic portion needs to be fibrous and elongated.

## Installatior \* Erosion control mix shall not be used on slopes steeper than 2:1.

- \* On slopes of 3:1 or less; 2 inches plus an additional 1/2 inch per 20 feet of slope up to 100 feet
- up to 100 feet.
- The thickness of the mulch at the bottom of the slope needs to be:

	<3:1 slope
<20' of slope	2.0"
<60' of slope	3.0"
<100' of slope	4.0"

\* It shall be placed evenly and must provide 100% coverage with the soil totally invisible.

Any required repairs shall be made immediately, with additional erosion control mix placed on top of the mulch to reach the recommended thickness. When the mix is decomposed, clogged with sediment, eroded or ineffective, it shall be replaced or repaired. Erosion control mix mulch shall be left in place. If the mulch needs to be removed spread it out into the landscape.

## Maintenance

All mulches must be inspected periodically, in particular after rainstorms, to check for rill erosion. If less than 90% of the soil surface is covered by mulch, additional mulch shall be immediately applied. Nets shall be inspected after rain events for dislocation or failure. If washouts or breakage occur, re-install the nets as necessary after repairing damage to the slope. Inspections shall take place until grasses are firmly established (95% soil surface covered with grass). Where mulch is used in conjunction with ornamental plantings, inspect periodically throughout the year to determine if mulch is maintaining coverage of the soil surface. Repair as needed.

## C. TEMPORARY VEGETATION

## <u>Considerations</u>

- \* Proper seedbed preparation and the use of quality seed are important in this practice just as in permanent seeding. Failure to carefully follow sound agronomic recommendations will often result in an inadequate stand of vegetation that provides little
- or no erosion control. \* Nutrients and pesticides used to establish and maintain a vegetation cover shall be
- managed to protect the surface and ground water quality.
- \* Temporary seeding shall be used extensively in sensitive areas (ponds and lake watersheds, steep slopes, streambanks, etc.).
- \* Late fall seeding may fail and cause water quality deterioration in spring runoff events, thus other measures such as mulching shall be implemented.

## <u>Specifications</u>

Seedbed Preparation Apply limestone and fertilizer according to soil test recommendations. If soil testing is not feasible on small or variable sites, or where timing is critical, fertilizer may be applied at the rate of 600 pounds per acre or 13.8 pounds per 1,000 square feet of 10-10-10 (N-P20S-K20) or equivalent. Apply limestone (equivalent to 50 percent calcium plus magnesium oxide) at a rate of 3 tons per acre (138 lb. per 1,000 square feet).

- \* Select seed from recommendations in enclosed table. \* Where the soil has been compacted by construction operations, loosen soil to a depth of
- 2 inches before applying fertilizer, lime and seed. \* Apply seed uniformly by hand, cyclone seeder, drill, cultipacker type seeder or hydroseeder (slurry including seed and fertilizer). Hydroseeding that includes mulch may be left on soil surface. Seeding rates must be increased 10% when hydroseeding.

## Mulching

Apply mulch over seeded area according to the TEMPORARY MULCHING BMP.

Temporary seeding shall be periodically inspected. At a minimum, 95% of the soil surface should be covered by vegetation. If any evidence of erosion or sedimentation is apparent, repairs shall be made and other temporary measures used in the interim (mulch, filter barriers, check dams, etc.).

<u>Temporary</u> See	<u>eding Rates and</u>	<u>d Dates</u>		
Seed	Lb./Ac	Seeding Depth	Recommended Seeding Dates	Remarks
Winter Rye	112 (2.0 bu)	1-1.5 in	8/15-10/1	Good for fall seeding. Select a hardy species, such as Aroostook Rye.
Oats	80 (2.5 bu)	1-1.5 in	4/1—7/1 Early fall 8/15— winter	Best for spring seeding. 9/15 seeding will die when weather moved in, but mulch will provide
			protection.	
Annual Ryegrass	40	.25 in	4/1-7/1	Grows quickly but is of short duration. Use where appearance is important. With mulch, seeding may be done throughout growing season.
Sudangrass	40 (1.0 bu)	.5-1 in	5/15-8/15	Good growth during hot summer periods.
Perennial	40 (2.0 bu)	.25 in	8/15-9/15	Good cover, longer lasting than Annual Ryegrass. Mulching will allow seeding throughout growing season.
Temporary mulch with	n or		10/1-4/1	Refer to TEMPORARY

### Temporary mulch with or MULCHING BMP and/or without dormant seeding PERMANENT VEGETATION BMP.

## D. FILTERS

- <u>Tubular Sediment Barrier</u>
- a. To be provided by an approved manufacturer or supplier: b. Installed per manufacturer's specifications; c. Barrier shall be removed when they have served their useful purpose but not before the
- upslope areas has been permanently stabilized. <u>Organic Filter Berm</u> See detail

- \* Sediment barriers shall be installed along the down gradient side of proposed ground disturbance areas prior to any construction activities. \* The barrier must be placed along a relatively level contour.
- <u>Maintenance</u>
- Hay bale barriers, silt fences and filter berms shall be inspected immediately after each rainfall and at least daily during prolonged rainfall. They shall be repaired immediately if there are any signs of erosion or sedimentation below them. If there are signs of undercutting at the center or the edges of the barrier, or impounding of large volumes of water behind them, sediment barriers shall be replaced with a temporary check dam.

\* Large portions of silts, clays or fine sands are not acceptable in the mix.

\* On slopes between 3:1 and 2:1, 4 inch plus an additional 1/2 inch per 20 feet of slope

slopes between 3:1 and 2:1 4.0' 5.0' 6.0'

- \* Should the fabric on a silt fence or filter barrier decompose or become ineffective prior to the end of the expected usable life and the barrier still is necessary, the fabric shall be replaced promptly.
- \* Sediment deposits should be removed when deposits reach approximately one third (1/3) the height of the barrier. Filter berms should be reshaped as needed.
- \* Any sediment deposits remaining in place after the silt fence or filter barrier is no longer required shall be dressed or removed to conform to the existing grade, prepared and
- seeded. \* Additional stone may have to be added to the construction stabilized entrance, rock barriers, stone lined swales, etc., periodically to maintain proper function of the erosion control structure.

## E. PERMANENT SEEDING

- 1. Bedding stones larger than  $1\frac{1}{2}$ ", trash, roots, and other debris that will interfere with seeding and future maintenance of the area should be removed. Where feasible, the soil should be tilled to a depth of 6" to prepare a seedbed and mix fertilizer (refer to Landscape Drawings and Specifications) into the soil.
- 2. Fertilizer (refer to Landscape Drawings and Specifications) lime and fertilizer should be applied evenly over the area prior to or at the time of seeding and incorporated into the soil. Kinds and amounts of lime and fertilizer should be based on an evaluation of soil tests.

## 3. Seed Mixture (See Landscape Drawings for additional information):

- 3.1. Lawn seed mix shall be a fresh, clean new seed crop. The Contractor shall furnish a dealer's guaranteed statement of the composition of the mixture and the percentage of purity and germination of each variety.
- 3.2. Seed mixture shall conform to landscape specifications 4. Sodding - sodding is done where it is desirable to rapidly establish cover on a disturbed area. Sodding an area may be substituted for permanent seeding procedures anywhere on
- site. Bed preparation, fertilizing, and placement of sod shall be performed according to the S.C.S. Handbook. Sodding is recommended for steep sloped areas, areas immediately adjacent to sensitive water courses, easily erodible soils (fine sand/silt), etc.

## DEWATERING

A dewatering plan shall be implemented to address excavation de-watering following heavy rainfall events or where the excavation may intercept the groundwater table during construction. The collected water needs treatment and a discharge point that will not cause downgradient erosion and offsite sedimentation or within a resource.

All dewatering discharge locations shall be located on relatively flat ground at least 75' from streams and 25' from wetlands. The contractor shall utilize dirtbags, erosion control mix berms, or similar methods for filtration of dewatering and shall conform to the Maine Erosion and Sediment Control BMPs.

## MONITORING SCHEDULE

The contractor shall be responsible for installing, monitoring, maintaining, repairing, replacing and removing all of the erosion and sedimentation controls or appointing a qualified subcontractor to do so. Maintenance measures will be applied as needed during the entire construction cycle. immediately following any significant rainfall, and at least once a week, a visual inspection will be made of all erosion and sedimentation controls as follows:

1. Silt fence shall be inspected and repaired. Sediment trapped behind these barriers shall be excavated when it reaches a depth of 6" and redistributed to areas undergoing final grading. 2. Construction entrance shall be visually inspected and repaired as needed. Any areas subject to rutting shall be stabilized immediately. If the voids of the construction entrance become filled with mud, more crushed stone shall be added as needed. The public roadway shall be swept should mud be deposited/tracked onto them.

## STANDARDS FOR STABILIZING SITES FOR THE WINTER

The following standards and methodologies shall be used for stabilizing the site during the winter construction period:

- 1. Standard for the timely stabilization of disturbed slopes (any area having a grade greater than 25%) — the contractor will seed and mulch all slopes to be vegetated by September 15th. If the contractor fails to stabilize any slope to be vegetated by September 15th, then the contractor will take one of the following actions to stabilize the slope for late fall and winter.
- A. <u>Stabilize the soil with temporary vegetation and erosion control mats</u>: by October 1st the contractor will seed the disturbed slope with winter rye at a rate of 3 pounds per 1000 square feet and then install erosion control mats or anchored hay mulch over the seeding. The contractor will monitor growth of the rye over the next 30 days.
- B. <u>Stabilize the slope with wood-waste compost</u>: the contractor will place a six-inch layer of wood-waste compost on the slope by November 15th. The contractor will not use wood-waste compost to stabilize slopes having grades greater than 50% (2h:iv) or having groundwater seeps on the slope face.
- C. Stabilize the slope with stone riprap: the contractor will place a layer of stone riprap on the slope by November 15th. The development's owner will hire a registered professional engineer to determine the stone size needed for stability on the slope and to design a filter layer for underneath the riprap.
- 2. Standard for the timely stabilization of disturbed soils by September 15th the contractor will seed and mulch all disturbed soils on the site. If the contractor fails to stabilize these soils by this date, then the contractor will take on of the following actions to stabilize the soil for late fall and winter.
- A. <u>Stabilize the soil with temporary vegetation</u>: by October 1st the contractor will seed the disturbed soil with winter rye at a seeding rate of 3 pounds per 1000 square feet, lightly mulch the seeded soil with hay or straw at 75 pounds per 1000 square feet, and anchor the mulch with plastic netting. The contractor will monitor growth of the rye over the next 30 days. If the rye fails to grow at least three inches or fails to cover at least 75% of the disturbed soil before November 1, then the contractor will mulch the area for over-winter protection as described in item iii of this standard.
- B. Stabilize the soil with sod: the contractor will stabilize the disturbed soil with properly installed sod by October 1st. proper installation includes the contractor pinning the sod onto the soil with wire pins, rolling the sod to guarantee contact between the sod and underlying soil, and watering the sod to promote root growth into the disturbed soil.
- C. <u>Stabilize the soil with mulch</u>: by November 15th the contractor will mulch the disturbed soil by spreading hay or straw at a rate of at least 150 pounds per 1000 square feet on the area so that no soil is visible through the mulch. Immediately after applying the mulch, the contractor will anchor the mulch with netting or other method to prevent wind from moving the mulch off the disturbed soil.

Winter inspections shall be preformed after, each rainfall, snowstorm or thawing and at least once a week. All areas within 75 feet of a protected natural resource must be protected with a double row of sediment barrier.

## EROSION CONTROL REMOVAL

- An area is considered stable if it is paved or if 90% growth of planted seeds is established. once an area is considered stable, the erosion control measures can be removed as follows: 1. <u>Silt Fence</u>: Silt fence shall be disposed of legally and properly off-site. all sediment trapped
- behind these controls shall be distributed to an area undergoing final grading or removed and relocated off-site. 2. <u>Stabilized Construction Entrance</u>: The stabilized construction entrance shall be removed once the compacted roadway base in in place. Stone and sediment from the construction
- entrance shall be redistributed to an area undergoing grading or removed and relocated offsite. 3. <u>Miscellaneous</u>: Once all the trapped sediments have been removed from the temporary
- sedimentation devices the disturbed areas must be regraded in an aesthetic manner to conform to the surrounding topography. Once graded these disturbed areas must be loamed (if necessary), fertilized, seeded and mulched in accordance with the rates previously stated.

The above erosion controls must be removed within 30 days of final stabilization of the site. Conformance with this plan and following these practices will result in a project that complies with the state regulations and the standards of the natural resources protection act, and will protect water quality in areas downstream from the project.

- INSPECTION AND MAINTENANCE
- Sediment Control approved by the Owner.
- area permanently stabilized.
- completion of the permanent stabilization.

# <u>HOUSEKEEPING</u>

- followed.
- Note destabilization.
  - not be used for dust control.

- Note:
- areas of the site.

## Note:

- non-stormwater discharges are:
- Fire hydrant flushings

- involve detergents
- Uncontaminated air conditioning or compressor condensate
- Uncontaminated excavation dewatering

- maintenance;

Allowable non-stormwater discharges cannot be authorized unless they are directly related to and originate from a construction site or dedicated support activity.

1. All sediment control measures shall be inspected at least once each week and following any storm event of 0.25 inches or greater. An inspection report shall be made after each inspection by a qualified inspector engaged by the Owner. The qualified inspector shall be a Professional Engineer licensed in Maine or be a Certified Professional in Erosion and

2. All measures shall be maintained in good working order; if a repair is necessary, it will be initiated within 24 hours and completed within 72 hours.

Inspection and maintenance requirements: Inspect disturbed and impervious areas, erosion and stormwater control measures, areas used for storage that are exposed to precipitation, and locations where vehicles enter or exit the site. Inspect these areas at least once a week as well as before and after a 0.5 inches or greater storm event and prior to completion of permanent stabilization measures. A person with knowledge of erosion and stormwater control, including the standards in the MCGP and any departmental companion document to the MCGP, must conduct the inspection. This person must be identified in the inspection log. If best management practices (BMPs) need to be modified or if additional BMPs are necessary, implementation must be completed within 7 calendar days and prior to any storm event (rainfall). All measures must be maintained in effective operating condition until areas

4. Inspection Log (report): A log (report) must be kept summarizing the scope of the inspection, name(s) and qualifications of the personnel making the inspection, the date(s) of the inspection, and major observations relating to operation of erosion and sedimentation controls and pollution prevention measures. Major observations must include BMPs that need maintenance, BMPs that failed to operate as designed or proved inadequate for a particular location, and locations(s) where additional BMPs are needed. For each BMP requiring maintenance, BMP needing replacement, and location needing additional BMPs, note in the inspection log the correct action taken and when it was taken. The log must be made accessible to the department staff and a copy must be provided upon request. The permittee shall retain a copy of the log for a period of at least three years from the

Spill prevention: Controls must be used to prevent pollutants from construction and waste materials stored onsite, including storage practices to minimize exposure of the materials to stormwater and appropriate spill prevention, containment, and response planning implementation. The contractor and owners need to take care with construction and waste materials such that contaminates do not enter the stormwater. The storage of materials such as paint, petroleum products, cleaning agents and the like are to be stored in watertight containers. The use of the products should be in accordance with manufacturer recommendations. When fueling equipment, including snowblowers and lawnmowers, have oil absorbent pads available below the fueling. Refueling of small engines by the owner should occur in the garage or on a paved surface. Any spill or release of toxic or hazardous substances must be reported to the department. For oil spills, call 1-800-482-0777 which is available 24 hours a day. For spills of toxic or hazardous material, call 1-800-452-4664 which is available 24 hours a day. For more information, visit the department's website at: HTTP: /WWW.MAINE.GOV/DEP/SPILLS/EMERGSPILLRESP/

2. Groundwater protection: Protection of the groundwater is required by the contractor and owner. During construction, liquid petroleum products and other hazardous materials with the potential to contaminate groundwater may not be stored or handled in areas of the site draining to an infiltration area. An "infiltration area" is any area of the site that by design or as a result of soils, topography, and other relevant factors accumulates runoff that infiltrates into the soil. Petroleum products should be stored in manufactured cans designed for the purpose. Dikes, berms, sumps, and other forms of secondary containment that prevent discharge to groundwater may be used to isolate portions of the site for the purposes of storage and handling of these materials. Spill preventions procedures should be

Lack of appropriate pollutant removal BMPs may result in violations of the groundwater quality standard established by 39 M.R.S.A. §465-C(1). Any project proposing infiltration of stormwater must provide adequate pre-treatment of stormwater prior to discharge of stormwater to the infiltration area, or provide treatment within the infiltration area, in order to prevent accumulation of fines, reductions in infiltration rate, and consequent flooding and

3. Fugitive sediment and dust: Actions must be taken to ensure that activities do not result in noticeable erosion of soils or fugitive dust emissions during or after construction. Oil may

Note: Dewatering a stream without a permit from the department violates state water quality standards and the Natural Resources Protection Act.

4. Debris and other materials: Litter, construction debris, and construction chemicals exposed to stormwater must be prevented from becoming a pollutant source. Construction materials and construction debris should be covered to prevent rainwater from washing contaminants off the site. Any fertilizers, cleaning products, herbicides should be protected from the weather and isea in accordance with manufacturers recommendations

Any contaminants that are washed off the site by rainwater is a violation of the Clean Waters Act. To prevent these materials from becoming a source of pollutants, construction activities related to a project may be required to comply with applicable provisions of rules related to solid, universal, and hazardous waste, including, but not limited to, the Maine Solid Waste and Hazardous Waste Management Rules; Maine Hazardous Waste Management Rules; Maine Oil Conveyance and Storage Rules; and Maine Pesticide requirements.

5. Trench or foundation dewatering: Trench dewatering is the removal of water from trenches, foundations, coffer dams, ponds, and other areas within the construction area that retain water after excavation. In most cases the collected water is heavily silted and hinders correct and safe construction practices. The collected water removed from the ponded area, either through gravity or pumping, must be spread through natural wooded buffers or removed to areas that are specifically designed to collect the maximum amount of sediment possible, like a cofferdam sedimentation basin. Avoid allowing the water to flow over disturbed

For guidance on dewatering controls, consult the Maine Erosion and Sediment Control BMPs, published by the Maine Department of Environmental Protection.

6. Non-stormwater discharges: Identify and prevent contamination by non-stormwater discharges. Where allowed non-stormwater discharges exist, they must be identified and steps should be taken to ensure the implementation of appropriate pollution prevention measures for the non-stormwater component(s) of the discharge. Authorized

• Discharges from firefighting activities

• Vehicle washwater if detergents are not used and washing is limited to the exterior of vehicles (engine, undercarriage, and transmission washing is prohibited • Dust control runoff in accordance with permit conditions

• Routine external building washdown, not including surface paint removal, that does not • Pavement washwater (where spills/leaks of toxic or hazardous materials have not occurred, unless all spilled material had been removed) if detergents are not used

• Uncontaminated groundwater or spring water • Foundation or footer drain-water where flows are not contaminated

• Potable water sources including waterline flushings

7. Unauthorized non-stormwater discharges: Identify and prevent contamination from discharges that is mixed with a source of non-stormwater, other than those discharges in compliance with 6. Unauthorized non-stormwater discharges are: • Wastewater from the washout or cleanout of concrete, stucco, paint, form release oils, curing compounds or other construction materials; • Fuels, oils, or other pollutants used in vehicle and equipment operations and

• Soaps, solvents or detergents used in vehicle and equipment wash; • Toxic or hazardous substances from a spill or other release.





 $\implies$ 

WORK AREA





- . PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING ANY NECESSARY APPLICATION OF LIME, FERTILIZER, AND SEED.
- 2. BEGIN AT THE TOP OF THE CHANNEL BY ANCHORING THE BLANKET IN A 6" DEEP BY 6" WIDE TRENCH WITH APPROXIMATELY 12" OF BLANKET EXTENDED BEYOND THE UP-SLOPE PORTION OF THE TRENCH. ANCHOR THE BLANKET WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN THE BOTTOM OF THE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING. APPLY SEED TO COMPACTED SOIL AND FOLD REMAINING 12" PORTION OF BLANKET BACK OVER SEED AND COMPACTED SOIL. SECURE BLANKET OVER COMPACTED SOIL WITH A ROW OF STAPLES/STAKES SPACED APPROXIMATELY 12" APART ACROSS THE WIDTH OF THE BLANKET.
- 3. ROLL CENTER BLANKET IN DIRECTION OF WATER FLOW IN BOTTOM OF CHANNEL. BLANKETS WILL UNROLL WITH APPROPRIATE SIDE AGAINST THE SOIL SURFACE. ALL BLANKETS MUST BE SECURELY FASTENED TO SOIL SURFACE BY PLACING STAPLES/STAKES IN APPROPRIATE LOCATIONS AS SHOWN IN THE STAPLE PATTERN GUIDE.
- 4. PLACE CONSECUTIVE BLANKETS END OVER END (SHINGLE STYLE) WITH A 4"-6" OVERLAP. USE A DOUBLE ROW OF STAPLES STAGGERED 4" APART AND 4" ON CENTER TO SECURE BLANKETS.
- 5. FULL LENGTH EDGE OF BLANKETS AT TOP OF SIDE SLOPES MUST BE ANCHORED WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN A 6" DEEP BY 6" WIDE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING.
- 6. ADJACENT BLANKETS MUST BE OVERLAPPED APPROXIMATELY 2"-5" (DEPENDING ON BLANKET TYPE) AND STAPLED. TO INSURE PROPER SEAM ALIGNMENT, PLACE THE EDGE OF THE OVERLAPPING BLANKET (BLANKET BEING INSTALLED ON TOP) EVEN WITH THE COLORED SEAM STITCH ON THE BLANKET BEING OVERLAPPED.
- 7. IN HIGH FLOW CHANNEL APPLICATIONS, A STAPLE CHECK SLOT IS RECOMMENDED AT 30 TO 40 FOOT INTERVALS. USE A DOUBLE ROW OF STAPLES STAGGERED 4" APART AND 4" ON CENTER OVER ENTIRE WIDTH OF THE CHANNEL.
- 8. THE TERMINAL END OF THE BLANKETS MUST BE ANCHORED WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN A 6" DEEP BY 6" WIDE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING.



CRITICAL POINTS:

. OVERLAPS AND SEAMS 3. PROJECTED WATER LINE

- C. CHANNEL BOTTOM/SIDE SLOPE VERTICES

\* HORIZONTAL STAPLE SPACING SHOULD BE ALTERED IF NECESSARY TO ALLOW STAPLES TO SECURE THE CRITICAL POINTS ALONG THE CHANNEL SURFACE.

\*\* IN LOOSE SOIL CONDITIONS, THE USE OF STAPLE OR STAKE LENGTHS GREATER THAN 6" MAY BE NECESSARY TO PROPERLY ANCHOR THE BLANKETS.

- FILTREXX® COMPOST SILT-SOXX<sup>IM</sup> SECTION PLAN VIEW SILTSOXX MAY BY USED IN PLACE OF SILT FENCE OR OTHER SEDIMENT BARRIERS. 2. ALL MATERIAL TO MEET FILTREXX SPECIFICATIONS. 3. SILTSOXX COMPOST/SOIL/ROCK/SEED FILL MATERIAL SHALL BE ADJUSTED AS NECESSARY TO MEET THE REQUIREMENTS OF THE SPECIFIC APPLICATION. 4. ALL SEDIMENT TRAPPED BY SILTSOXX SHALL BE DISPOSED OF PROPERLY **TUBULAR SEDIMENT BARRIER** NOT TO SCALE

ARFA TO BE

PROTECTED



## <u>NOTES</u>

- 1. PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING ANY NECESSARY APPLICATION OF LIME, FERTILIZER, AND SEED.
- 2. BEGIN AT THE TOP OF THE SLOPE BY ANCHORING THE BLANKET IN A 6" DEEP BY 6" WIDE TRENCH WITH APPROXIMATELY 12" OF BLANKET EXTENDED BEYOND THE UP-SLOPE PORTION OF THE TRENCH. ANCHOR THE BLANKET WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN THE BOTTOM OF THE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING. APPLY SEED TO COMPACTED SOIL AND FOLD REMAINING 12" PORTION OF BLANKET BACK OVER SEED AND COMPACTED SOIL. SECURE BLANKET OVER COMPACTED SOIL WITH A ROW OF STAPLES/STAKES SPACED APPROXIMATELY 12" APART ACROSS THE WIDTH OF THE BLANKET.
- 3. ROLL THE BLANKETS (A) DOWN OR (B) HORIZONTALLY ACROSS THE SLOPE. BLANKETS WILL UNROLL WITH APPROPRIÁTE SIDE AGÀIŃST THE SOIL SURFACE. ALL BLANKETS MUST BE SECURELY FASTENED TO SOIL SURFACE BY PLACING STAPLES/STAKES IN APPROPRIATE LOCATIONS AS SHOWN IN THE STAPLE PATTERN GUIDE.
- 4. THE EDGES OF PARALLEL BLANKETS MUST BE STAPLED WITH APPROXIMATELY 2"-5" OVERLAP DEPENDING ON BLANKET TYPE. TO ENSURE PROPER SEAM ALIGNMENT, PLACE THE EDGE OF THE OVERLAPPING BLANKET (BLANKET BEING INSTALLED ON TOP) EVEN WITH THE COLORED SEAM STITCH ON THE PREVIOUSLY INSTALLED BLANKET
- 5. CONSECUTIVE BLANKETS SPLICED DOWN THE SLOPE MUST BE PLACED END OVER END (SHINGLE STYLE) WITH AN APPROXIMATE 3" OVERLAP. STAPLE THROUGH OVERLAPPED AREA, APPROXIMATELY 12" APART ACROSS ENTIRE BLANKET WIDTH. NOTE: IN LOOSE SOIL CONDITIONS, THE USE OF STAPLE OR STAKE LENGTHS GREATER THAN 6" MAY BE NECESSARY TO PROPERLY SECURE THE BLANKETS.

EROSION CONTROL BLANKET - SWALE NOT TO SCALE

EROSION CONTROL BLANKET - SLOPE NOT TO SCALE

6





## <u>NOTES</u>

- 1. ORGANIC FILTER BERMS MAY BE UTILIZED IN LIEU OF SILT FENCE OR OTHER SEDIMENT BARRIERS.
- 2. THE EROSION CONTROL MIXTURE USED IN FILTER BERMS SHALL BE A WELL-GRADED MIX OF PARTICLE SIZES THAT MAY CONTAIN ROCKS LESS THAN 4" IN DIAMETER, STUMP GRINDINGS, SHREDDED OR COMPOSTED BARK, AND/OR ACCEPTABLE MANUFACTURED PRODUCTS AND SHALL BE FREE OF REFUSE, PHYSICAL CONTAMINANTS AND MATERIAL TOXIC TO PLANT GROWTH. EROSION CONTROL MIXTURE SHALL MEET THE FOLLOWING STANDARDS:
- a) THE ORGANIC CONTENT SHALL BE 80-100% OF DRY WEIGHT b) PARTICLE SIZE BY WEIGHT SHALL BE 100% PASSING A 6" SCREEN, AND 70-85% PASSING A 0.75" SCREEN.
- c) THE ORGANIC PORTION SHALL BE FIBROUS AND ELONGATED. d) LARGE PORTIONS OF SILTS, CLAYS, OR FINE SANDS SHALL NOT BE INCLUDED IN THE MIXTURE. e) SOLUBLE SALTS CONTENT SHALL BE >4.0mmhos/cm.
- f) THE pH SHALL BE BETWEEN 5.0 AND 8.0.
- 3. ORGANIC FILTER BERMS SHALL BE INSTALLED ALONG A RELATIVELY LEVEL CONTOUR. IT MAY BE NECESSARY TO CUT TALL GRASSES OR WOODY VEGETATION TO AVOID CREATING VOIDS AND BRIDGES THAT WOULD ENABLE FINES TO WASH UNDER THE BERM.
- 4. ON SLOPES LESS THAN 5%, OR AT THE BOTTOM OF SLOPES NO STEEPER THAN 3:1 AND UP TO 20 LONG, THE BERM SHALL BE A MINIMUM OF 12" HIGH (AS MEASURED ON THE UPHILL SIDE) AND A MINIMUM OF 36" WIDE. ON LONGER AND/OR STEEPER SLOPES, THE BERM SHALL BE TALLER AND WIDER TO ACCOMMODATE THE POTENTIAL FOR ADDITIONAL RUNOFF (MAXIMUM HEIGHT SHALL NOT EXCEED 2').
- 5. FROZEN GROUND, OUTCROPS OF BEDROCK, AND VERY ROOTED FORESTED AREAS PRESENT THE MOST PRACTICAL AND EFFECTIVE LOCATIONS FOR ORGANIC FILTER BERMS. OTHER BMP'S SHOULD BE USED AT LOW POINTS OF CONCENTRATED RUNOFF, BELOW CULVERT OUTLET APRONS, AROUND CATCH BASINS, AND AT THE BOTTOM OF STEEP PERIMETER SLOPES THAT HAVE A LARGE CONTRIBUTING ARFA
- 6. SEDIMENT SHALL BE REMOVED FROM BEHIND THE FILTER BERMS WHEN IT HAS ACCUMULATED TO ONE HALF THE ORIGINAL HEIGHT OF THE BERM.
- 7. ORGANIC FILTER BERMS MAY BE LEFT IN PLACE ONCE THE SITE IS STABILIZED PROVIDED ANY SEDIMENT DEPOSITS TRAPPED BY THEM ARE REMOVED AND DISPOSED OF PROPERLY.
- 8. FILTER BERMS ARE PROHIBITED AT THE BASE OF SLOPES STEEPER THAN 8% OR WHERE THERE IS FLOWING WATER WITHOUT THE SUPPORT OF ADDITIONAL MEASURES SUCH AS SILTFENCE.

## **ORGANIC FILTER BERM**

GRATE - LIFTING STRAP DANDY BAG II OR STANDARD FABRIC APPROVED EQUAL OF ORANGE WOVEN MONOFILAMENT DUMPING STRAP ALLOWS FOR EASY REMOVAL OF CONTENTS

## **INSTALLATION AND MAINTENANCE:**

INSTALLATION: REMOVE THE GRATE FROM CATCH BASIN. IF USING OPTIONAL OIL ABSORBENTS; PLACE ABSORBENT PILLOW IN UNIT. STAND GRATE ON END. MOVE THE TOP LIFTING STRAPS OUT OF THE WAY AND PLACE THE GRATE INTO CATCH BASIN INSERT SO THE GRATE IS BELOW THE TOP STRAPS AND ABOVE THE LOWER STRAPS. HOLDING THE LIFTING DEVICES, INSERT THE GRATE INTO THE INLET.

MAINTENANCE: REMOVE ALL ACCUMULATED SEDIMENT AND DEBRIS FROM VICINITY OF THE UNIT AFTER EACH STORM EVENT. AFTER EACH STORM EVENT AND AT REGULAR INTERVALS, LOOK INTO THE CATCH BASIN INSERT. IF THE CONTAINMENT AREA IS MORE THAN 1/3 FULL OF SEDIMENT, THE UNIT MUST BE EMPTIED. TO EMPTY THE UNIT, LIFT THE UNIT OUT OF THE INLET USING THE LIFTING STRAPS AND REMOVE THE GRATE. IF USING OPTIONAL ABSORBENTS; REPLACE ABSORBENT WHEN NEAR SATURATION.

## UNACCEPTABLE INLET PROTECTION METHOD:

A SIMPLE SHEET OF GEOTEXTILE UNDER THE GRATE IS NOT ACCEPTABLE.

## STORM DRAIN INLET PROTECTION

## NOT TO SCALE

NOT TO SCALE





![](_page_39_Figure_68.jpeg)

## MAINTENANCE

# 3' I.D. LOW PROFILE CATCH BASIN

1. STRUCTURE SHALL TO ACCOMMODATE HEAVY DUTY 24" SQ. C.I. FRAME AND GRATE.

2. "3' DIAMETER AREA DRAIN" AVAILABLE FROM PHOENIX PRECAST PRODUCTS

4. STRUCTURE SHALL BE STEEL REINFORCED MEET OR EXCEED H-20 LOADING.

5. SEAL ALL TONGUE AND GROOVE JOINTS w/BUTYL RUBBER JOINT COMPOUND.

(800-639-2199) OR APPROVED EQUAL.

3. CONCRETE: 4,000 PSI AFTER 28 DAYS

- 8' MIN.

THE SUBGRADE FOR THE GEOTEXTILE FABRIC AND RIPRAP SHALL BE PREPARED TO ACCOUNT FOR

4. GEOTEXTILE FABRICS SHALL BE PROTECTED FROM PUNCTURE OR TEARING DURING THE PLACEMENT

THE EROSION STONE MAY BE PLACED BY EQUIPMENT AND SHALL BE CONSTRUCTED TO THE FULL

LAYER THICKNESS IN ONE OPERATION AND IN SUCH A MANNER AS TO PREVENT SEGREGATION OF

OF FABRIC OVER THE DAMAGED AREA OR BY COMPLETE REPLACEMENT OF THE FABRIC. ALL

OF THE EROSION STONE. DAMAGED AREAS IN THE FABRIC SHALL BE REPAIRED BY PLACING A PIECE

OVERLAPS REQUIRED FOR REPAIRS OR JOINING TWO PIECES OF FABRIC SHALL BE A MINIMUM OF 18".

2' MIN. —

CONSTRUCT PLUNGE POOL TO THE WIDTHS AND LENGTHS SHOWN ON THE PLAN.

PERCENT PASSING BY WEIGHT

3. EROSION STONE USED FOR THE PLUNGE POOL SHALL MEET THE FOLLOWING GRADATION:

DRAIN PIPE w/FLARED

<u>NOTES</u>

END SECTION -

THE DEPTH OF RIPRAP.

100

0 - 15

90-100

<u>SIZE</u>

18"

12"

THE STONE SIZES.

PLUNGE POOL

<u>NOTES</u>

NOT TO SCALE

## PIPE INVERT IS WITHIN 4' OF FINISH GRADE. 7. FRAME AND GRATE DIMENSIONS ARE TYPICAL BUT MAY VARY BASED ON PRODUCT SELECTED OR EQUIVALENT APRROVED BY THE ENGINEER. DEEP SUMP CATCH BASIN (CB)

- RISERS OF 1', 2', 3' & 4' CAN BE USED TO REACH DESIRED DEPTH. THE STRUCTURES SHALL BE DESIGNED FOR H20 LOADING. 6. USE H20 LOADING SLAB TOP SECTION IN LIEU OF ECCENTRIC TOP WHERE
- CIRCUMFERENTIAL REINFORCEMENT EQUAL TO 0.12 SQ. IN. PER LINEAR FT.

- 3. THE TONGUE OR GROOVE OF THE JOINT SHALL CONTAIN ONE LINE OF

- 2. CIRCUMFERENTIAL REINFORCEMENT SHALL BE 0.12 SQ.IN. PER LINEAR FT. IN

<u>NOTES</u>

2.

STUMPS, AND OTHER OBJECTIONABLE MATERIAL.

PRIOR TO DIRECTING STORMWATER TO IT.

THE EROSION RESISTANCE IN THE SWALE.

**VEGETATED SWALE** 

GRADES SHOWN ON THE PLANS.

**RIPRAP LINED SWALE** 

<u>1/2</u>"

A -----

<u>PLAN</u>

22 1/4"

SECTION B-B

5 1/8" C.C. 🛌

19"

2' DIA.

2 13/16"

OR AS SHOWN ON PLANS-

**NOTES** 

PLANS

NCHES.

THE STONE SIZES.

FLOW LINE

3/8" MORTAR

<u>NOTES</u>

JOINT

-NON-WOVEN GEOTEXTILE

FABRIC (10 OZ/SY) AND

-EROSION STONE 18" MIN.

NOT TO SCALE

-HEAVY DUTY CAST

IRON GRATE

(NO BRICK)

—4" HEAVY DUTY

CAST IRON FRAME

-MORTAR ALL AROUND

TO ACCOMMODATE PIPE

12" D.I. OUTLET PIPE

w/NON-SHRINK GROUT

SEAL OPENING

-24" RISER SECTION

-36" BASE SECTION

12" BEDDING OF 3/4"

CRUSHED STONE OR AS

SPECIFIED IN GEOTECH REPORT

-COMPACTED NATIVE SUBGRADE

-MODIFY FLANGE AS NECESSARY

-6" THICK SLAB TOP

DEPTH (SEE NOTE #3)

10 MIL. POLY BARRIER

- ALL SECTIONS AND SHALL BE PLACED IN THE CENTER THIRD OF THE WALL.

- 1. ALL SECTIONS SHALL BE CONCRETE CLASS AA (4000 PSI).

PRECAST

CIRCULAR

![](_page_40_Figure_66.jpeg)

![](_page_41_Figure_0.jpeg)

## <u>NOTES</u>

ANTI-SEEP COLLARS SHALL BE CLAY, CONCRETE, PLASTIC (AGRI-DRAIN), OR EQUAL APPROVED BY THE ENGINEER.

## ANTI-SEEP COLLAR

		SOIL FILTER MEDIA
FILTER MEDIA	MIXUTRE BY VOLUME	SPECIFICATION
SAND	50-55%	MEDOT SPECICATION #703.01 FINE AGGREGATE FOR CONCRETE MODIFIED TO HAVE 8–10% PASSING THE #200 SIEVE
TOPSOIL	20-30%	SANDY LOAM TOPSOIL WITH MINIMAL CLAY CONTENT AND BETWEEN 20-70% PASSING THE #200 SIEVE
MULCH	20-30%	MODERATELY FINE, SHREDDED BARK OR WOOD FIBER MULCH WITH LESS THAN 5% PASSING #200 SIEVE

MDOT 703.22 TYPE B		MDOT 7	703.22 TYPE C
SIEVE SIZE	% BY WEIGHT	SIE VE SI ZE	% BY WEIGHT
1" 1/2" #4 #20 #50 #200	95-100 75-100 50-100 15-80 0-15 0-5	1" 3/4" 3/8" #4 #10	100 90-100 0-75 0-25 0-5

## GRASSED UNDERDRAIN SOIL FILTER (GUSF) NOTES

The contractor will retain the services of a qualified professional to inspect the construction and stabilization of all stormwater management structures. If necessary, the qualified professional shall interpret the pond's construction plan for the contractor. Once all stormwater management structures are constructed and stabilized, the qualified professional will notify the department in writing within 30 days to state that the pond has been completed. Accompanying the notification must be a log of the inspections giving the date of each inspection, the time of each inspection, and the items inspected on each visit, and include any testing data or sieve analysis data of every mineral soil and soil media specified in the plans and used on site.

**Construction Sequence:** The soil filter media and vegetation must not be installed until the area that drains to the filter has been permanently stabilized with pavement or other structure, 90% vegetation cover, or other permanent stabilization unless the runoff from the contributing drainage area is diverted around the filter until stabilization is completed.

Compaction of Soil Filter: Filter soil media and underdrain bedding material must be compacted to between 90% and 92% standard proctor. The bed should be installed in at least 2 lifts of 9 inches to prevent pockets of loose media.

- **Construction Oversight**: Inspection by a professional engineer will occur at a minimum: • After the preliminary construction of the filter grades and once the underdrain pipes are installed but not backfilled,
- After the drainage layer is constructed and prior to the installation of the filter media, • After the filter media has been installed and seeded. Bio-retention cells must be stabilized per the provided planting scheme and density for the canopy coverage of 30
- and 50%. • After one year to inspect health of the vegetation and make corrections, and

# TYPICAL GRASSED UNDERDRAINED SOIL FILTER (GUSF)

![](_page_41_Figure_15.jpeg)

![](_page_41_Figure_22.jpeg)

# NOT TO SCALE

NOT 7	TO S	A.72	L

![](_page_42_Figure_0.jpeg)

![](_page_42_Figure_1.jpeg)

- SIDEWALK, RAMP AND

AND DETAILS

SUBGRADE PER PLANS

6"-WIDE (MIN) THICKENED

NOT TO SCALE

| PER PLANS

FLUSH CURB AT RAMP DETAIL

VERTICAL GRANITE CURB -

CURB TAPER TO MATCH

TRANSITION CURB PER

RAMP DETAIL (TYP) -

PAVEMENT PER

PLANS

# CURB RAMP NOTES

- 11. CURB RAMPS SHALL HAVE A FLAT 2% MAX LANDING AT THE TOP AND BOTTOM OF THE RAMPS WHEN THERE IS A CHANGE IN DIRECTION.
- 10. NO RAMP SHALL BE LESS THAN 4' IN WIDTH.
- 9. EDGES OF SIDEWALK FOOTINGS ALONG FLUSH CURBS SHALL BE HAUNCHED SO AS TO EXTEND TO A MINIMUM DEPTH OF 1' BELOW FINISH GRADE.
- OF PAVEMENT.
- 8. FLUSH CURB SECTIONS SHALL HAVE A MAXIMUM LIP REVEAL OF 1/4" WITH A BEVEL AT THE EDGE
- (ADA) AND ALL APPLICABLE CODES.
- 7. ALL CURB RAMPS SHALL BE CONSTRUCTED IN ACCORDANCE WITH AMERICANS WITH DISABILITIES ACT

- 6. SEE CONCRETE SIDEWALK SECTION FOR RAMP CONSTRUCTION.
- 5. BASE OF RAMP SHALL BE GRADED TO PREVENT THE PONDING OF WATER.
- 4. CURB TREATMENT VARIES, SEE PLANS FOR CURB TYPE.
- SHALL BE 8.3% FOR A MAXIMUM ELEVATION CHANGE OF 6".

![](_page_42_Figure_22.jpeg)

![](_page_42_Figure_25.jpeg)

![](_page_42_Figure_26.jpeg)

![](_page_42_Figure_27.jpeg)

![](_page_42_Figure_28.jpeg)

![](_page_42_Figure_29.jpeg)

![](_page_42_Figure_30.jpeg)

![](_page_42_Figure_31.jpeg)

![](_page_42_Figure_33.jpeg)

![](_page_42_Figure_34.jpeg)

![](_page_42_Figure_35.jpeg)

![](_page_42_Figure_36.jpeg)

**ELEVATION** 

1/4" CHAMFER (TYP) -

 $\langle / / / / \rangle$ 

- 1x3 VERTICAL P.T. FACE BOARDS.

ATTACH WITH GALVANIZED NAILS.

GALVANIZED IRON PIPE

12"

TYP

FINISHED PAVEMENT GRADE

![](_page_42_Figure_43.jpeg)

SEE SITE PLAN

4 1

44

6<sup>4</sup>4 6 4 4 4

4

4 4

PITCH TO DRAIN

PER PLANS

4,000 psi CONCRETE PAD

(SEE CROSS SECTION)

⊸DOUBLE LEAF GATE -

PLAN - TYPICAL LAYOUT

DUMPSTER ENCLOSURE AND PAD

· · · · · · ·

![](_page_43_Figure_0.jpeg)

## <u>NOTES</u>

- 1. EACH GRAVEL BASE COURSE TO BE CONSTRUCTED AT THE PAVEMENT CROSS SLOPE. 2. REMOVE LEDGE 18" BELOW LOWEST WORK BEING INSTALLED.
- 3. REMOVE ALL LOAM, CLAY, MUCK, ORGANIC, YIELDING OR OTHERWISE UNSTABLE MATERIAL TO A MINIMUM OF 18" BELOW FINISHED GRADE. ADDITIONAL DEPTH MAY BE REQUIRED
- BY THE GEOTECHNICAL REPORT.
- 4. THE OVER-EXCAVATION OF UNSUITABLE MATERIAL BEYOND THAT SPECIFIED ABOVE, THE INSTALLATION OF UNDERDRAINAGE, AND/OR THE INSTALLATION OF GEOTEXTILE FABRIC SHALL BE PROVIDED UPON DETERMINATION OF THE INSPECTOR OR THE ENGINEER.
- 5. FILL BELOW PAVEMENT SUBGRADE SHALL BE SAND OR GRANULAR COMMON BORROW COMPACTED PER MDOT REQUIREMENTS.
- 6. SITEWORK CONTRACTOR SHALL COORDINATE GEOTECHNICAL ENGINEERING INSPECTIONS PRIOR TO PLACEING GRAVELS.

# **TYPICAL ROADWAY CROSS SECTION**

Specifi EPA:	cations					
EPA:	$0.95 \text{ ft}^2$		[	Ĺ		
	(.09 m <sup>2</sup> )					
Length:	(66.0 cm)	$\checkmark$		1		
Width:	(33.0 cm)		<u>.                                    </u>	)		
Height <sub>1</sub> :	(7.62 cm)			→ H, (		
Height <sub>2</sub> : Weight (max):	(17.8 cm) 16 lbs (7.25 kg)				v v	N
Orde	r <mark>ing Inform</mark> a	tion			EXAMP	LE: DSX
Series	LEDs	Color temperature	Distribution			
DSX0 LED	Forward optics           P1         P5           P2         P6           P3         P71           P41         Rotated optics           P102         P122           P112         P1312	30K 3000 K 40K 4000 K 50K 5000 K	T1STypeT2STypeT2MTypeT3STypeT3MTypeT4MTypeTFTMFormT5VSType	l short (Automoti II short III medium III short III medium IV medium rard throw mediut V very short <sup>3</sup>	ve) T5S T5M T5W BLC LCCO RCCO	Type V short <sup>3</sup> Type V medium Type V wide <sup>3</sup> Backlight contro Left corner cuto Right corner cu
Control ont	ione					
Shipped in NLTAIR2 PIRHN PER PER5 PER7 DMG	Installed InLight AIR generation 2 en Network, high/low moton, NEMA twist-lock receptacl Five-pin receptacle only (o Seven-pin receptacle only separate) <sup>UM7</sup> O -10V dimming extenc ou (control ordered separate)	abled <sup>13,14</sup> /ambient sensor <sup>15</sup> e only (control ordered sepa ontrol ordered separate) <sup>14,17</sup> (leads exit fixture) (control o t back of housing for extern <sup>14</sup>	ratej <sup>16</sup> irdered al control	PIR PIRH PIR1FC3V PIRH1FC3V FAO	Hich/low, mo height, ambie Hich/low, mo height, ambie Hich/low, mo height, ambie Field adjustat	tion/ambient senso nt sensor enabled a tion/ambient sensor int sensor enabled a tion/ambient sensor int sensor enabled a tion/ambient sensor int sensor enabled a kle output <sup>21</sup>

- COMPACTOR OPERATING AT PEAK RATED FREQUENCY OR BY OTHER MEANS APPROVED BY THE ENGINEER.

- THEIR MAXIMUM DRY DENSITIES AS DETERMINED BY ASTM D-1557.
- BY THE ENGINEER.

![](_page_43_Figure_22.jpeg)

# PAINTED HANDICAP SYMBOL

NOT TO SCALE

SYMBOL TO BE PAINTED IN ALL HANDICAPPED ACCESSIBLE SPACES IN WHITE PAINT (BLUE-1. PAINTED SQUARE BACKGROUND OPTIONAL)

![](_page_44_Figure_3.jpeg)

# 4. INLET AND OUTLET PIPE SIZES AND CONFIGURATION SHALL BE CONSTRUCTED PER THE PLANS. 1,500 GALLON GREASE TRAP

- TANK SHALL BE MANUFACTURED BY SHEA CONCRETE PRODUTS OR APPROVED EQUAL. TANK 3. DIMENSIONS MAY VARY DEPENDING ON THE MANUFACTURER.
- KEYED TANK JOINTS SHALL BE SEALED WITH BUTYL RUBBER.
- TANK SHALL BE 4,000 PSI (MIN.) STEEL REINFORCED CONCRETE. 1.

![](_page_44_Figure_9.jpeg)

![](_page_44_Figure_10.jpeg)

# BOLLARD

(TYPx3)-

NOT TO SCALE

POST OR BUILDING MOUNTED

SPACES, SEE SITE PLAN)

R7-8 (R7-8P ADDED AT VAN

# **→** 18" →

![](_page_44_Figure_13.jpeg)

![](_page_44_Figure_14.jpeg)

# **TYPICAL PAVEMENT SAWCUT** NOT TO SCALE

![](_page_44_Figure_16.jpeg)

![](_page_44_Figure_17.jpeg)

## NOTES

1. MACHINE CUT EXISTING PAVEMENT.

CURB RAMP (SEE SITE PLAN

- SIDEWALK

FOR TYPE AND LAYOUT)

**TYPICAL TRENCH PATCH** 

4"WHITE

- 2. ALL TEMPORARY, DAMAGED OR DEFECTIVE PAVEMENT SHALL BE REMOVED PRIOR TO PLACEMENT OF

- PERMANENT TRENCH REPAIRS.

![](_page_44_Figure_40.jpeg)

- 3. DIAMOND PATCHES, SHALL BE REQUIRED FOR ALL TRENCHES CROSSING ROADWAY. DIAMOND PATCHES SHALL MEET NHDOT REQUIREMENTS.

![](_page_44_Figure_48.jpeg)

## GREASE TRAP OUTLET BAFFLE DETAIL NOT TO SCALE NOT TO SCALE

![](_page_44_Figure_51.jpeg)

WEIGHT PER LINEAR FOOT: 2.50 LBS (MIN.) HOLES: 3/8" DIAMETER, 1" C-C FULL LENGTH STEEL: SHALL CONFORM TO ASTM A-499 (GRADE 60) OR ASTM A-576 (GRADE 1070 - 1080)

LENGTH: AS REQUIRED

\* IN LEDGE DRILL & GROUT TO A MIN OF 2'

# - FINISH GRADE 3,000 PSI CYLINDRICAL CONCRETE FOOTING

6" MIN. COMPACTED

6" Ø GALV. STEEL PIPE FILLED w/3000 psi CONCRETE AND PVC SLEEVE INSTALLED OVER PIPE. COLOR AT OWNERS DISCRETION

- TRENCH OR OTHER EXCAVATION PER PLANS

- CONSTRUCT BITUMINOUS CONCRETE PAVEMENT (SEE PAVEMENT CROSS SECTION)

-CLEAN VERTICAL EDGE OF SAWCUT JOINT. COAT VERTICAL EDGE OF JOINT WITH RS-1 EMULSION IMMEDIATELY PRIOR TO PLACING PAVEMENT PATCH.

![](_page_44_Figure_58.jpeg)

![](_page_44_Figure_59.jpeg)

CONTRACTOR SHALL VERIFY SPECIFIC

REQUIREMENTS PRIOR TO FABRICATION)

1. ALL SIGNS SHALL MEET THE

REQUIREMENTS OF AND BE INSTALLED

UNIFORM TRAFFIC CONTROL DEVICES,

AS INDICATED IN THE MANUAL ON

NOTES

# LEGEND

	PRO
-·-·-	RIGH
	EAS
	BUIL
	WET
	250
	250
	STO
<u> </u>	WET
	HISS
DxB	HISS
TP #11	TES
	EXIS
VGC SGC	EXIS
VGC SGC	PRO
<u>SWL SYL</u> DYL	SINC
٥ σ <del>ο</del> σ <b>ο σο σο</b>	EXIS
0 <b>00</b>	EXIS
o <b>oo</b> _	EXIS
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DD	EXIS
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F	PRO
<u>⇒</u> _S <b></b> o	PRO
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онwе	PRO
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(44) [226]	PAR
	PRO
	PRO
	PRO
<u> seber korte di Altolika di Matal</u>	

PROPERTY LINE HT OF WAY SEMENT \_DING SETBACK TLAND SETBACK VERNAL POOL SETBACK 'SHORELAND PROTECTION OVERLAY ZONE NEWALL TLAND BOUNDARY SS SOIL BOUNDARY SS SOIL DESIGNATION TPIT OR BORING LOCATION STING/PROPOSED GRAVEL STING PAVEMENT/CURB POSED PAVEMENT/VERTICAL OR SLOPED GRANITE CURB IGLE WHITE LINE/SINGLE YELLOW LINE/DOUBLE YELLOW LINE STING/PROPOSED GUARDRAIL STING/PROPOSED STOCKADE FENCE STING/PROPOSED CHAINLINK FENCE ISSUE DATE: STING CONTOUR POSED CONTOUR/INTERMEDIATE CONTOUR REVISIONS DPOSED SPOT GRADE/TOP & BOTTOM OF WALL OR CURB POSED RETAINING WALL STING WATER/CURB STOP/VALVE/HYDRANT STING SEWER/MANHOLE STING GAS/VALVE IST. OVERHEAD/UNDERGROUND UTILITIES/POLE STING DRAINAGE/CB/DMH POSED THRUST BLOCK/CURB STOP/VALVE/HYDRANT DRAWN BY: POSED DOMESTIC/FIRE WATER SERVICE LINE POSED SEWER/MANHOLE/CLEANOUT POSED SEWER FORCEMAIN/AIR RELIEF VALVE SCALE: DPOSED GAS OR PROPANE POSED OVERHEAD UTILITIES/UTILITY POLE POSED UNDERGROUND ELECTRIC/PHONE/TV OWNER: DPOSED DRAINAGE (HARD PIPE)/CB/DCB/DMH/FES POSED DRAINAGE (PERFORATED PIPE)/CLEANOUT RUGATED PLASTIC PIPE/FLARED END SECTION/HEADWALL DPOSED GROUND SLOPE/APPROX. GRADE/STONE CHECK DAM TFENCE/SEDIMENT BARRIER/CONST. FENCE BILIZED CONSTRUCTION EXIT POSED LIMIT OF DISTURBANCE/TREE CLEARING POSED SAWCUT APPLICANT: STING TREE/DRIP LINE POSED TREELINE RKING COUNT PER ROW/FOR TOTAL SITE POSED EROSION CONTROL BLANKET POSED RIPRAP POSED GRASSED UNDERDRAINED SOIL FILTER (GUSF) PROJECT: TITLE:

![](_page_44_Picture_64.jpeg)

![](_page_45_Figure_0.jpeg)

## **FIRE HYDRANT**

![](_page_45_Figure_2.jpeg)

THE CONTRACTOR IS RESPONSIBLE FOR ALL REPAIRS SHOULD SERVICE PROVIDER BE UNABLE TO INSTALL ITS CABLE IN A SUITABLE MANNER. 6. TYPICAL CONDUIT SIZES ARE 3-INCH FOR SINGLE PHASE PRIMARY AND SECONDARY VOLTAGE CABLES, 4-INCH FOR THREE PHASE SECONDARY, AND 5-INCH FOR THREE PHASE PRIMARY.

NON-PAVED AREA | PAVED AREA

" CLEAR (MIN)

3'-7" (MIN)

51" MIN. UNDER SLAB

12"

- THAN THOSE SHOWN HERE.
- HOWEVER, <u>SERVICE PROVIDERS MAY REQUIRE DIFFERENT NUMBERS, TYPES AND SIZES OF CONDUIT</u> THAN THOSE SHOWN HERE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFYING ALL CONDUIT

- SIZES, TYPES AND NUMBERS WITH EACH SERVICE PROVIDER PRIOR TO ORDERING THEM. 7. ROUTING OF CONDUIT, LOCATION OF MANHOLES, TRANSFORMERS, CABINETS, HANDHOLES, ETC., SHALL

- BE DETERMINED BY SERVICE PROVIDER DESIGN PERSONNEL. THE CONTRACTOR SHALL COORDINATE
- WITH ALL SERVICE PROVIDERS PRIOR TO THE INSTALLATION OF ANY CONDUIT.
- 8. ALL CONDUIT INSTALLATIONS MUST CONFORM TO THE CURRENT EDITION OF THE NATIONAL ELECTRIC SAFETY CODE, STATE AND LOCAL CODES AND ORDINANCES, AND WHERE APPLICABLE, THE NATIONAL
- ELECTRIC CODE. WHERE REQUIRED BY UTILITY PROVIDER, CONDUIT SHALL BE SUPPORTED IN PLACE

- USING PIPE STANCHIONS PLACED EVERY FIVE (5') FEET ALONG THE CONDUIT RUN. 9. UNDER A BUILDING SLAB THE CONDUIT SHALL BE ENCASED IN 8" OF CONCRETE ON ALL SIDES.

## SEE ROADWAY CROSS-SECTION OR BUILDING PAD DETAILS

# SAND BLANKET/BARRIER SIEVE SIZE % FINER BY WEIGHT

NON-PAVED AREA |

LOAM AND SEED OR OTHER

SURFACE TREATMENT PER PLANS -

6" GRAVEL BORROW -

SUITABLE EXCAVATED

BACKFILL OR CLEAN GRANULAR BACKFILL

AS SPECIFIED -

SURFACE

THICKNESS) -

TAPE 24" BELOW

SAND BLANKET AS

WOOD SHEETING AS

A.O.S.=70 OR LESS -

UNDISTURBED SOIL -----

REQUIRED (3" MINIMUM

NON-WOVEN GEOTEXTILE

<u>NOTES</u>

METHOD C

ARE IN TRENCH.

<u>SIEVE SIZE</u>

1/2"

200

C OR D-

NOTES

SAND BLANKET/BARRIER

<u>% FINER BY WEIGHT</u>

90 - 100

0 — 15

DRAINAGE AND SEWER TRENCH

MARINE PLYWOOD

WRAPPED IN

POLYETHYLENE -

SPECIFIED BELOW -

MATERIAL COMPACTED

"CAUTION - WARNING"

PAVED AREA

- SEE PAVEMENT SECTION

SEE PAVEMENT SECTION

SEE PAVEMENT SECTION

-SCREENED GRAVEL OR

BELOW PIPE IN ROCK

GEOTECH REPORT)

- ROCK SUBGRADE

(TEMPLATE)

SCREENED GRAVEL OR CRUSHED STONE BEDDING

<u>% PASSING BY WEIGHT</u>

100

90 - 100

20 - 55

0 - 10

0 — 5

VOLUME OF

ENGINEER

A, B OR (

CONCRETE AS

DETERMINED BY

TRENCH

' WID T⊦

NOT TO SCALE

UNDISTURBED MATERIAL

(TYP)

SIEVE SIZE

3/4"

3/8"

# 4

#8

VERTICAL BENDS

-M.J. PLUG

(TYP.)

PIPE SIZE

0.892.193.8211.1417.240.651.552.788.3812.00

0.48 | 1.19 | 2.12 | 6.02 | 9.32 |

0.25 0.60 1.06 3.08 4.74

0.13 0.30 0.54 1.54 2.38

C OR D

SQUARE FEET OF CONCRETE THRUST

1. POUR THRUST BLOCKS AGAINST UNDISTURBED MATERIAL. WHERE TRENCH WALL HAS BEEN

2. NO JOINTS SHALL BE COVERED WITH CONCRETE. POLYETHYLENE (6 MIL) SHALL BE PLACED

USED, M.J. PLUG WITH RETAINER GLAND MAY BE SUBSTITUTED FOR END BLOCKINGS.

4. PLACE BOARD IN FRONT OF ALL PLUGS BEFORE POURING THRUST BLOCKS. WHERE M.J. PIPE IS

DISTURBED, EXCAVATE LOOSE MATERIAL AND EXTEND THRUST BLOCK TO UNDISTURBED MATERIAL.

RFACTION

TYPF

90°

180°

45°

AROUND FITTINGS PRIOR TO CONCRETE PLACEMENT.

THRUST BLOCKING

22-1/2°

 $11 - 1/4^{\circ}$ 

3. ON BENDS AND TEES, EXTEND THRUST BLOCKS FULL LENGTH OF FITTING.

BLOCKING BEARING ON UNDISTURBED MATERIAL

(ADJUST AS SPECIFIED IN

CRUSHED STONE BEDDING FOR

UP TO SPRINGLINE OF PIPE, 6"

BELOW PIPE IN EARTH AND 12"

FULL WIDTH OF THE TRENCH

MIN

3'-0" (MIN) OR D+2

FOR SINGLE PIPE

1. BACKFILL MATERIAL BELOW PAVED OR CONCRETE AREAS, BEDDING MATERIAL, AND SAND BLANKET

SHALL BE COMPACTED TO NOT LESS THAN 95% OF AASHTO T 99, METHOD C. SUITABLE BACKFILL

MATERIAL BELOW LOAM AREAS SHALL BE COMPACTED TO NOT LESS THAN 90% OF AASHTO T 99,

2. INSULATE GRAVITY SEWER AND FORCEMAINS WHERE THERE IS LESS THAN 5'-0" OF COVER WITH 2"

3. MAINTAIN 12" MINIMUM HORIZONTAL SEPARATION AND WIDEN TRENCH ACCORDINGLY IF MULTIPLE PIPES

THICK CLOSED CELL RIGID BOARD INSULATION, 18" ON EACH SIDE OF PIPE.

(WHICHEVER IS GREATER)

	1/2"	90 - 100	
	200	0 - 15	
$\backslash$			

- CLEAN GRANULAR BACKFILL MATERIAL COMPACTED AS SPECIFIED
- -SELECT SAND COMPACTED TO 95% STANDARD PROCTOR
- (ADJUST BEDDING AS SPECIFIED IN GEOTECH REPORT)
- 1. ALL CONDUIT IS TO BE SCHEDULE 40 PVC, ELECTRICAL GRADE, GRAY IN COLOR AND INSTALLED PER THE MANUFACTURER'S RECOMMENDATIONS. A 10-FOOT HORIZONTAL SECTION OF RIGID GALVANIZED STEEL CONDUIT WILL BE REQUIRED AT EACH SWEEP, UNLESS IN THE OPINION OF THE SERVICE
- PROVIDER DESIGNER, THE SWEEP-PVC JOINT IS NOT SUBJECT TO FAILURE DURING PULLING OF THE
- 2. ALL 90 DEGREE SWEEPS WILL BE MADE WITH RIGID GALVANIZED STEEL WITH A MINIMUM RADIUS OF
- 36 INCHES FOR PRIMARY CABLES AND 24 INCHES FOR SECONDARY CABLES.
- UNSUITABLE BY SERVICE PROVIDER. BACKFILL SHALL BE FREE OF FROZEN LUMPS, ROCKS, DEBRIS, AND RUBBISH. ORGANIC MATERIAL SHALL NOT BE USED AS BACKFILL. BACKFILL SHALL BE IN

-INDICATOR POST

- HYDRANT SHALL BF

AFC PACER WB 67

OPEN LEFT PAINTED

TO KITTERY WATER DISTRICT SPECS

12" SAND

HRUS

BLOCK

- 6" MIN.

- HYDRANT

DRAIN SHALL

BE PLUGGED

SAND

NOT TO SCALE

└─ CONCRETE

DISTRICT REQUIREMENTS

SITTING BLOCK

PROVIDED BY KITTERY WATER

DISTRICT

- 3. BACKFILL MAY BE MADE WITH EXCAVATED MATERIAL OR COMPARABLE, UNLESS MATERIAL IS DEEMED

## STANDARD TRENCH NOTES

INCH SHALL BE USED.

TOP OF THE PIPE.

FOLLOWS:

<u>NOTES</u>

8

ORDERED EXCAVATION OF UNSUITABLE MATERIAL BELOW GRADE: BACKFILL AS STATED IN THE TECHNICAL SPECIFICATIONS OR AS SHOWN ON THE DRAWING.

BEDDING: SCREENED GRAVEL AND/OR CRUSHED STONE FREE FROM CLAY, LOAM, ORGANIC MATTER AND MEETING THE GRADATION SHOWN IN THE TRENCH DETAIL. WHERE ORDERED BY THE ENGINEER TO STABILIZE THE BASE, SCREENED GRAVEL OR CRUSHED STONE 1-1/2 INCH TO 1/2

3. SAND BLANKET: CLEAN SAND FREE FROM ORGANIC MATTER MEETING THE GRADATION SHOWN IN THE TRENCH DETAIL. BLANKET MAY BE REPLACED WITH BEDDING MATERIAL FOR CAST-IRON, DUCTILE IRON, AND REINFORCED CONCRETE PIPE PROVIDED THAT NO STONE LARGER THAN 2" IS IN CONTACT WITH THE PIPE AND THE GEOTEXTILE IS RELOCATED ACCORDINGLY.

4. SUITABLE MATERIAL: IN ROADS, ROAD SHOULDERS, WALKWAYS AND TRAVELED WAYS, SUITABLE MATERIAL FOR TRENCH BACKFILL SHALL BE THE NATURAL MATERIAL EXCAVATED DURING THE COURSE OF CONSTRUCTION, BUT SHALL EXCLUDE DEBRIS, PIECES OF PAVEMENT, ORGANIC MATTER, TOP SOIL, ALL WET OR SOFT MUCK, PEAT, OR CLAY, ALL EXCAVATED LEDGE MATERIAL, ALL ROCKS OVER 6 INCHES IN LARGEST DIMENSION, AND ANY MATERIAL WHICH, AS DETERMINED BY THE ENGINEER, WILL NOT PROVIDE SUFFICIENT SUPPORT OR MAINTAIN THE COMPLETED CONSTRUCTION IN A STABLE CONDITION. IN CROSS COUNTRY CONSTRUCTION, SUITABLE MATERIAL SHALL BE AS DESCRIBED ABOVE, EXCEPT THAT THE ENGINEER MAY PERMIT THE USE OF TOP SOIL, LOAM, MUCK, OR PEAT, IF SATISFIED THAT THE COMPLETED CONSTRUCTION WILL BE ENTIRELY STABLE AND PROVIDED THAT EASY ACCESS TO THE SEWER FOR MAINTENANCE AND POSSIBLE RECONSTRUCTION WILL BE PRESERVED.

5. BASE COURSE AND PAVEMENT SHALL MEET THE REQUIREMENTS OF THE MAINE DEPARTMENT OF TRANSPORTATION'S LATEST EDITION OF THE STANDARD SPECIFICATIONS FOR HIGHWAYS AND BRIDGES - DIVISION 700.

6. SHEETING, IF REQUIRED: WHERE SHEETING IS PLACED ALONGSIDE THE PIPE AND EXTENDS BELOW MID-DIAMETER, IT SHALL BE CUT OFF AND LEFT IN PLACE TO AN ELEVATION 1 FOOT ABOVE THE TOP OF PIPE. WHERE SHEETING IS ORDERED BY THE ENGINEER TO BE LEFT IN PLACE, IT SHALL BE CUT OFF AT LEAST 3 FEET BELOW FINISHED GRADE, BUT NOT LESS THAT 1 FOOT ABOVE THE

7. W = MAXIMUM ALLOWABLE TRENCH WIDTH TO A PLANE 12 INCHES ABOVE THE PIPE. FOR PIPES 15 INCHES NOMINAL DIAMETER OR LESS, W SHALL BE NO MORE THAN 36 INCHES. FOR PIPES GREATER THAN 15 INCHES IN NOMINAL DIAMETER, W SHALL BE 24 INCHES PLUS PIPE OUTSIDE DIAMETER (O.D.) ALSO, W SHALL BE THE PAYMENT WIDTH FOR LEDGE EXCAVATION AND FOR ORDERED EXCAVATION BELOW GRADE.

FOR CROSS COUNTRY CONSTRUCTION, BACKFILL, FILL AND/OR LOAM SHALL BE MOUNDED TO A HEIGHT OF 6 INCHES ABOVE THE ORIGINAL GROUND SURFACE.

9. CONCRETE FOR ENCASEMENT SHALL CONFORM TO THE MAINE DEPARTMENT OF PUBLIC WORKS AND HIGHWAYS STANDARD SPECIFICATION REQUIREMENTS FOR CLASS A (3000#) CONCRETE AS

CEMENT: 6.0 BAGS PER CUBIC YARD WATER: 5.75 GALLONS PER BAG CEMENT MAXIMUM SIZE OF AGGREGATE: 1 INCH CONCRETE ENCASEMENT IS NOT ALLOWED FOR PVC PIPE.

10. CONCRETE FULL ENCASEMENT: IF FULL ENCASEMENT IS UTILIZED, DEPTH OF CONCRETE BELOW

PIPE SHALL BE 1/4 I.D. (4" MINIMUM). BLOCK SUPPORT SHALL BE SOLID CONCRETE BLOCKS.

11. MAINE DEPARTMENT OF ENVIRONMENTAL PROTECTION DESIGN STANDARDS REQUIRE TEN FEET (10') SEPARATION BETWEEN WATER AND SEWER. REFER TO TOWN'S STANDARD SPECIFICATIONS FOR METHODS OF PROTECTION IN AREAS THAT CANNOT MEET THESE REQUIREMENTS.

## NOT TO SCALE

	OWNER:
6" COMPACTED LOAM <b>NON-PAVED AREA PAVED AREA</b> AND SEED OR OTHER SURFACE TREATMENT	C-COAST PROPERTIES, LLC
PER PLANS	8 BANKS ROCK YORK HARBOR, MAINE 03911
5' COVER (MIN) (7' COVER MAX) $\square$	
SUITABLE EXCAVATED BACKFILL OR CLEAN GRANULAR BACKFILL MATERIAL COMPACTED AS SPECIFIED 3" CAUTION TAPE READING "CAUTION WATER LINE BURIED BELOW" SUITABLE EXCAVATED BACKFILL MATERIAL, OR GRANULAR MATERIAL, OR GRANULAR MATERIAL, OR GRANULAR MATERIAL WHERE SPECIFIED, COMPACTED IN 12" LIFTS TO 95% STANDARD PROCTOR MAXIMUM DENSITY. TYPE "K" COPPER OR CTS PLASTIC WATER SERVICE OR HDPE DR	GOOD TO-GO c/o CAPE HOUSE MANAGEMENT, LLC 484 US ROUTE 1 KITTERY, MAINE 03904
AS SPECIFIED 6" NOMINAL (12" IN LEDGE) 3' (MIN) AS SPECIFIED 11 WATER MAIN 11 WATER MAIN 12 BELOW PIPE IN EARTH AND 12" BELOW PIPE IN LEDGE	GOOD TO-GO SPECIALTY FOOD FACILITY
	IAX MAP 67, LOI 1
<u>SAND BLANKELY BANKER</u> SIEVE SIZE <u>% FINER BY WEIGHT</u> 1/2" 90 – 100	524 U.S. ROUTE 1 KITTERY, MAINE
200 0 – 15	<u>TITLE:</u>
<ol> <li>BACKFILL MATERIAL BELOW PAVED OR CONCRETE AREAS, BEDDING MATERIAL, AND SAND BLANKET SHALL BE COMPACTED TO NOT LESS THAN 95% OF AASHTO T 99, METHOD C. SUITABLE BACKFILL MATERIAL BELOW LOAM AREAS SHALL BE COMPACTED TO NOT LESS THAN 90% OF AASHTO T 99, METHOD C.</li> <li>ALL TRENCLUNC AND BACKELL SHALL CONFORM WITH THE STANDARDS OF THE KITTERY WATER</li> </ol>	DETAILS
2. ALL INCIDING AND BACKFILL SHALL CONFORM WITH THE STANDARDS OF THE KITTERT WATER DISTRICT.	SHEET NUMBER:
WATER MAIN TRENCH NOT TO SCALE	D-8

![](_page_45_Picture_84.jpeg)

## <u>NOTES</u>

1. STYLE "DT-HD" ACCESS HATCH, AS MANUFACTURED BY SYRACUSE CASTINGS, CICERO, NEW YORK (315-699-2601) OR APPROVED EQUAL.

2. MATERIAL SHALL BE 6061-T6 ALUMINUM FOR BARS, ANGLES, AND EXTRUSIONS. 1/4" DIAMOND PLATE SHALL BE 5086 ALUMINUM.

3. UNIT DESIGNED HEAVY DUTY, FOR H-20 WHEEL LOADS, WHERE NOT SUBJECT TO HIGH DENSITY TRAFFIC. FRAME AND BEARING PLATE MUST BE CAST INTO AND SUPPORTED BY CONCRETE DESIGNED FOR H-20 WHEEL LOADS.

4. UNIT SUPPLIED WITH A HEAVY DUTY PNEU-SPRING, FOR EASE OF OPERATION WHEN OPENING COVER. COVER SHALL BE COUNTERBALANCED, SO ONE PERSON CAN EASILY OPEN THE HATCH DOOR.

5. FRAME SHALL BE OF EXTRUDED ALUMINUM WITH A CONTINUOUS 1-1/4" ANCHOR FLANGE. A DOVETAIL GROOVE SHALL BE EXTRUDED INTO THE SEAT OF THE FRAME FOR A 1/8" SILICONE GASKET.

6. EACH HATCH SHALL BE EQUIPPED WITH A STAINLESS STEEL HOLD OPEN ARM. DOOR SHALL LOCK OPEN IN THE 90 DEGREE POSITION. HOLD OPEN ARM SHALL BE FASTENED TO THE FRAME WITH A 1/2" GRADE 316 STAINLESS STEEL BOLT.

7. HINGES SHALL BE OF HEAVY DUTY DESIGN. MATERIAL SHALL BE GRADE 316 STAINLESS STEEL. EACH HINGE SHALL HAVE A GRADE 316 STAINLESS STEEL, 3/8" DIAMETER HINGE PIN. HINGE SHALL BE FASTENED TO THE CHANNEL FRAME AND DIAMOND PLATE WITH GRADE 316 STAINLESS STEEL BOLTS AND NY-LOCK NUTS.

8. ALUMINUM SHALL BE SUPPLIED WITH MILL FINISH. EXTERIOR OF FRAME WHICH COMES IN CONTACT WITH CONCRETE SHALL HAVE ONE COAT BLACK PRIMER.

9. EACH HATCH SHALL BE SUPPLIED WITH A STAINLESS STEEL SLAM LOCK, WITH THE KEY WAY PROTECTED BY A THREADED ALUMINUM PLUG. THE PLUG SHALL BE FLUSH WITH THE TOP OF THE 1/4" DIAMOND PLATE. THE SLAM LOCK SHALL BE FASTENED WITH GRADE 316 STAINLESS STEEL BOLTS AND WASHERS.

10. EACH HATCH SHALL BE EQUIPPED WITH A STAINLESS STEEL LIFT HANDLE. LIFT HANDLE SHALL BE FLUSH WITH TOP OF 1/4" DIAMOND PLATE.

11. EACH "DT-HD" STYLE HATCH IS SUPPLIED WITH A 1-1/2" THREADED DRAIN COUPLER ON THE UNDERSIDE OF CHANNEL FRAME, FOR PIPE CONNECTION.

![](_page_46_Figure_12.jpeg)

![](_page_46_Figure_13.jpeg)

![](_page_46_Figure_14.jpeg)

## OWNER'S MAINTENANCE NOTES

## PIPING check valves shall be 150 psi.

LEVEL CONTROL:

ALARM:

DOSAGE

# SLIDE RAIL ASSEMBLY: machined cast iron and support the pump four (4) inches above the floor.

CONTROLLER:

PUMPS

## shown on the Drawings. Chamber shall be rated for H-20 loading. ACCESS COVER:

shall be in compliance with local codes. PUMP CHAMBER:

PUMP STATION:

## PUMP STATION SPECIFICATIONS

13,978 CF / 154 DAYS = 90.77 CF/DAY (SUNDAYS EXCLUDED)  $90.77 \text{ CF/DAY} \times 7.48 \text{ GAL/CF} = 679 \text{ GPD}$ 679 GPD / 5,500 SF = 0.12 GPD/SF0.12 GPD/SF x 20,000 SF = 2,400 GPD DESIGN FLOW

## SPECAILTY FOOD FACILITY:

## SEWER FLOW CALCULATIONS

FLEXIBLE BOOT STANCHIONS CONCRETE FILL NOTES

## CONCRETE PIPE SUPPORTS · 2" BALL VALVE — -

1" BLOW OFF VALVE -2" BALL VALVE —

MIN.)

ADJUST FRAME AND

WITH CLAY BRICK AND MORTAR (2 COURSES

GRATE TO GRADE

![](_page_46_Figure_35.jpeg)

![](_page_47_Figure_0.jpeg)

ICLUDING THE INFORMATION HEREON, REMAINS THE PROPERTY OF S PROVIDED SOLELY FOR ERECTING THE BUILDING DESCRIBED IN THE CHASE ORDER AND MAY BE REPRODUCED ONLY FOR THAT PURPOSE. IT CONFIED, REPRODUCED OR USED FOR ANY OTHER PURPOSE WITHOUT IPPROVAL OF BUTLER MFG.		<b>,</b>	1540 G	BUTLER MANUFACTURING ENESSEE ST. KANSAS CITY, MO 64102	Single Slope Phase 1-Cove
		0418	ary:	DEBORFTICK.	RALERS The Sheridan Corporation
ONTRACTOR AND/OR ERECTOR IS SOLELY RESPONSIBLE FOR ACCURATE					CARTORNER.
VORKMANSHIP IN ERECTING THIS BUILDING IN ACCORDANCE WITH THIS IS REFERENCED IN THIS DOMINING, ALL ACPLICATION FOR THE STATES					Locartos Kittery, Maine
AND INDUSTRY STANDARDS PERTAINING TO PROPER ERECTION.					MOJEST: Good To Go Prelim 042921
XORRECT USE OF TEMPORARY BRACING.		NG-SCALE		NTS	BULDER'S POR
	697 - E	125001		10/2004 PRELIMINARY ORANING	

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![](_page_48_Figure_0.jpeg)

VPO FUEROWE INSTRUMENTS PRELIMINARY BRANING

AWING, INCLUDING THE INFORMATION HEREON, REMAINS THE PROPERTY OF MPG. IT IS PROVIDED SOLELY FOR ERECTING THE BUILDING DESCRIBED IN THE BLE PURCHASE ORDER AND MAY BE REPRODUCED ONLY FOR THAT PURPOSE. IT		B 1540 GENE		BUTLER MANUFACTURING GENESSEE ST. KANSAS CITY, MO 64102	Single Slope Pha
HALL NOT BE MODIFIED, REPRODUCED DR USED FOR ANY OTHER PURPOSE WITHOUT RIOR WRITTEN APPROVAL OF BUTLER MFG.	NEV.	DATE	HIY:	BERONFTION.	RULERS The Sheridan Corpora
E GENERAL CONTRACTOR AND/OR ERECTOR IS SOLELY RESPONSIBLE FOR ACCURATE					CUT NORMA
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# **DRAINAGE ANALYSIS**

## FOR

# Site Development for Good To-Go

524 U.S. Route 1 Kittery, Maine

Tax Map 67, Lot 1

July 22, 2021

Prepared For:

Good To-Go c/o Cape House Management, LLC 484 U.S. Route 1 Kittery, Maine 03904

Prepared By:

## ALTUS ENGINEERING, INC.

133 Court Street Portsmouth, NH 03801 Phone: (603) 433-2335

![](_page_49_Picture_11.jpeg)

![](_page_49_Picture_12.jpeg)

Altus Project 5116.1

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   Project Description
   Site Overview
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   Calculation Methods
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- Section 6 Class A High Intensity Soil Survey Test Pit Logs
- Section 7 NRCS Soils Report
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- Section 9 Stormwater Operations and Maintenance Plan
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![](_page_50_Picture_9.jpeg)

# Section 1

# Narrative

![](_page_51_Picture_2.jpeg)

## **PROJECT DESCRIPTION**

Good To-Go, a Kittery-based specialty food company focused on outdoor activities, is proposing to develop a commercial lot located at 524 U.S. Route 1 in Kittery, Maine. The 23.89 acre property is identified as Assessor's Map 47, Lot 201 and is located in the Mixed Use (MU) district. The site is primarily wooded and undeveloped save for an existing residence with several outbuildings, a woods road and several side trails.

The proposed project will construct a new public road to access a commercial specialty food facility with a 20,000 sf building serviced by municipal water and sewer, a paved parking area and new stormwater treatment measures. These measures will include two grassed underdrained soil filters. Pretreatment will be provided by catch basins with deep sumps and grease hoods.

The stormwater management system proposed for the site will reduce peak flows and treat runoff from 100% of the site's impervious areas and 75.2% of the linear access roadway prior to leaving the site.

## Site Soils

A Class A High Intensity Soils Survey (HISS) was conducted on the site which indicated that the soils are generally poor with low rates of infiltration, relatively high water tables and numerous areas of shallow ledge. These soils fall into the following primary classifications:

BrB – Brayton, Hydrologic Soil Group (HSG) D DxB – Dixfield, HSG D LTB – Lyman Tunbridge Complex, HSG C LTC – Lyman Tunbridge Complex, HSG C LTD – Lyman Tunbridge Complex, HSG C LTE – Lyman Tunbridge Complex, HSG C NiB – Nicholville, HSG D ScB – Scantic, HSG D WhB – Whately, HSG D WmB – Waumbek, HSG D

For the purposes of this analysis, offsite watershed areas beyond the limit of the HISS were classified using the USDA's NRCS Web Soil Survey.

## **Pre-Development (Existing Conditions)**

The Pre-Development Watershed Plan (Sheet WS-1) reflects the current conditions of the site which include the existing building and parking areas. The current site can be divided into two (2) subcatchments which discharge to the west to a culvert under Route 1 at Point of Analysis (POA) #1 (HydroCAD Link 100L) and south to the property boundary at Point of Analysis #2 (HydroCAD Link 200L).

## Post-Development (Proposed Conditions)

The proposed project will construct a new building, drainage system and associated site improvements.

As shown on the attached Post-Development Watershed Plan (Sheet WS-2), the site was divided into fifteen (15) subcatchment areas in the post-development conditions. The same points of analysis that were used in the Pre-Development model (POA #'s 1 and 2) were used for comparison of the Pre- and Post-development conditions.

## CALCULATION METHODS

The drainage study was completed using the USDA SCS TR-20 Method within the HydroCAD Stormwater Modeling System. Reservoir routing was performed with the Dynamic Storage Indication method with automated calculation of tailwater conditions. A Type III 24-hour rainfall distribution was utilized in analyzing the data for the 2, 10 and 25 year - 24-hour storm events using rainfall data provided by Maine DEP. Infiltration rates through biofilter media were set at 2.41 in/hr with a phase-in depth of 0.01'.

## Disclaimer

Altus Engineering, Inc. notes that stormwater modeling is limited in its capacity to precisely predict peak rates of runoff and flood elevations. Results should not be considered to represent actual storm events due to the number of variables and assumptions involved in the modeling effort. Surface roughness coefficients (n), entrance loss coefficients (ke), velocity factors (kv) and times of concentration (Tc) are based on subjective field observations and engineering judgment using available data. For design purposes, curve numbers (Cn) describe the average conditions. However, curve numbers will vary from storm to storm depending on the antecedent runoff conditions (ARC) including saturation and frozen ground. Also, higher water elevations than predicted by modeling could occur if drainage channels, closed drain systems or culverts are not maintained and/or become blocked by debris before and/or during a storm event as this will impact flow capacity of the structures. Structures should be re-evaluated if future changes occur within relevant drainage areas in order to assess any required design modifications.

## Drainage Analysis

A complete summary of the drainage model is included in the appendix of this report. The following table compares pre- and post-development peak rates at the Point of Analysis identified on the plans for the 2, 10 and 25-year storm events:

	2-Yr Storm	10-Yr Storm	25-Yr Storm
	(3.30 inch)	(4.90 inch)	(6.20 inch)
POA #1 (US 1 Culvert)			
Pre	2.74	5.55	6.75
Post	2.26	4.59	6.61
Change	-0.48	-0.96	-0.14
POA #2 (South Property Line)			
Pre	9.33	20.19	29.85
Post	9.24	19.31	29.79
Change	-0.09	-0.88	-0.06

## Stormwater Modeling Summary Peak Q (cfs) for Type III 24-Hour Storm Events

As the above table demonstrates, the proposed peak rates of runoff will be decreased from the existing conditions for all analyzed storm events.

## CONCLUSION

This proposed roadway and site development off U.S Route 1 in Kittery, ME will have minimal adverse effect on abutting properties and infrastructure as a result of stormwater runoff or siltation. Post-construction peak rates of runoff from the site will be lower than the existing conditions for all analyzed storm events. The new stormwater management system will also provide appropriate treatment to runoff from 100% of the proposed impervious surfaces from the site and 75.2% of the access road. Appropriate steps will be taken to properly mitigate erosion and sedimentation through the use of temporary and permanent Best Management Practices for sediment and erosion control, including deep sump catch basins with grease hoods and two grassed underdrained soil filters designed in accordance with the MDEP Stormwater Best Practices Manual.

# Section 2

# Aerial Photo and USGS Map

![](_page_55_Picture_2.jpeg)

![](_page_56_Picture_0.jpeg)

![](_page_57_Figure_0.jpeg)

# Section 3

# Drainage Calculations

Pre-Development 2-Year, 24-Hour Summary 10-Year, 24-Hour Complete 25-Year, 24-Hour Summary

![](_page_58_Picture_3.jpeg)

![](_page_59_Figure_0.jpeg)

Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: West Side	Runoff Area=86,228 sf 2.71% Impervious Runoff Depth>1.28" Flow Length=611' Tc=7.7 min CN=77 Runoff=2.74 cfs 0.211 af
Subcatchment 2S: East Side	Runoff Area=609,713 sf 2.66% Impervious Runoff Depth>1.09" Flow Length=1,208' Tc=32.9 min CN=74 Runoff=9.33 cfs 1.276 af
Reach 1R: 12" Steel Pipe 12.0" Round Pipe n=0.012	Avg. Flow Depth=0.45' Max Vel=8.00 fps Inflow=2.74 cfs 0.211 af L=45.0' S=0.0291 '/' Capacity=6.59 cfs Outflow=2.74 cfs 0.211 af
Link 100L: POA #1	Inflow=2.74 cfs 0.211 af Primary=2 74 cfs 0.211 af
Link 200L: POA #2	Inflow=9.33 cfs 1.276 af Primary=9.33 cfs 1.276 af

Total Runoff Area = 15.977 acRunoff Volume = 1.488 afAverage Runoff Depth = 1.12"97.34% Pervious = 15.551 ac2.66% Impervious = 0.426 ac

![](_page_61_Figure_0.jpeg)

Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: West Side	Runoff Area=86,228 sf 2.71% Impervious Runoff Depth>2.54" Flow Length=611' Tc=7.7 min CN=77 Runoff=5.55 cfs 0.418 af
Subcatchment 2S: East Side	Runoff Area=609,713 sf 2.66% Impervious Runoff Depth>2.27" Flow Length=1,208' Tc=32.9 min CN=74 Runoff=20.19 cfs 2.645 af
Reach 1R: 12" Steel Pipe 12.0" Round Pipe n=0.012	Avg. Flow Depth=0.70' Max Vel=9.40 fps Inflow=5.55 cfs 0.418 af L=45.0' S=0.0291 '/' Capacity=6.59 cfs Outflow=5.55 cfs 0.418 af
Link 100L: POA #1	Inflow=5.55 cfs 0.418 af Primary=5.55 cfs 0.418 af
Link 200L: POA #2	Inflow=20.19 cfs  2.645 af Primary=20.19 cfs  2.645 af

Total Runoff Area = 15.977 ac Runoff Volume = 3.063 af Average Runoff Depth = 2.30" 97.34% Pervious = 15.551 ac 2.66% Impervious = 0.426 ac

## Summary for Subcatchment 1S: West Side

Runoff = 5.55 cfs @ 12.11 hrs, Volume= 0.418 af, Depth> 2.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	А	rea (sf)	CN E	Description								
*		1,015	98 li	98 Impervious Existing Pavement								
*		1,318	98 li	3 Impervious Existing Building								
		1,648	96 G	Gravel surfa	ace, HŠG E	)						
		3,325	96 G	Gravel surfa	ace, HSG C							
		1,629	87 E	)irt roads, l	HSG C							
		27,302	80 >	75% Gras	s cover, Go	ood, HSG D						
		2,700	77 V	Voods, Go	od, HSG D							
		22,240	74 >	75% Gras	s cover, Go	bod, HSG C						
		25,051	70 V	Voods, Go	od, HSG C							
		86,228	77 V	Veighted A	verage							
		83,895	9	7.29% Per	vious Area							
		2,333	2	71% Impe	ervious Area	а						
	_				_							
	Τc	Length	Slope	Velocity	Capacity	Description						
(r	nin)	(feet)	(ft/ft)	(ft/sec)	(cts)							
	3.9	54	0.0579	0.23		Sheet Flow,						
						Grass: Short n= 0.150 P2= 3.30"						
	1.5	192	0.0941	2.15		Shallow Concentrated Flow,						
		<b>~</b> -				Short Grass Pasture Kv= 7.0 fps						
	0.5	97	0.0336	2.95		Shallow Concentrated Flow,						
	~ ~	0.0	0 0750			Unpaved Kv= 16.1 fps						
	0.3	80	0.0750	4.41		Shallow Concentrated Flow,						
	0.0	10	0.0000	4 57		Unpaved KV= 16.1 fps						
	0.2	10	0.0060	1.57		Shallow Concentrated Flow,						
	1 2	170	0.0214	2 10		Paved Kv= 20.3 lps						
	1.5	172	0.0214	2.19		Grassed Waterway, Ky= 15.0 fps						
	77	614	Tatal			Grasseu walerway rv- 10.0 lps						
	1.1	011	iotai									

![](_page_64_Figure_2.jpeg)

![](_page_64_Figure_3.jpeg)

## Summary for Subcatchment 2S: East Side

Runoff = 20.19 cfs @ 12.47 hrs, Volume= 2.645 af, Depth> 2.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	A	rea (sf)	CN [	Description								
*		11,834	98 I	Impervious Existing Pavement								
*		4,369	98 I	mpervious	npervious Existing Building							
		1,161	89 E	Dirt roads, I	HSG D	0						
		4,839	87 E	Dirt roads, I	HSG C							
		51,144	80 >	>75% Gras	s cover, Go	ood, HSG D						
	1	93,586	77 \	Noods, Go	od, HSG D							
		22,432	74 >	>75% Gras	s cover, Go	ood, HSG C						
	3	20,348	70 \	Noods, Go	od, HSG C							
	6	09,713	74 \	Neighted A	verage							
	5	93,510	ç	97.34% Per	vious Area							
		16,203	2	2.66% Impe	ervious Area	a						
				-								
	Тс	Length	Slope	Velocity	Capacity	Description						
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	8.8	83	0.1231	0.16		Sheet Flow,						
						Woods: Light underbrush n= 0.400 P2= 3.30"						
	1.4	121	0.0826	1.44		Shallow Concentrated Flow,						
						Woodland Kv= 5.0 fps						
	7.1	301	0.0199	0.71		Shallow Concentrated Flow,						
						Woodland Kv= 5.0 fps						
	7.8	223	0.0090	0.47		Shallow Concentrated Flow,						
						Woodland Kv= 5.0 fps						
	1.6	77	0.0250	0.79		Shallow Concentrated Flow,						
						Woodland Kv= 5.0 fps						
	1.1	98	0.0816	1.43		Shallow Concentrated Flow,						
						Woodland Kv= 5.0 fps						
	5.1	305	0.0393	0.99		Shallow Concentrated Flow,						
						Woodland Kv= 5.0 fps						
	32.9	1,208	Total									

![](_page_66_Figure_2.jpeg)

![](_page_66_Figure_3.jpeg)

## Summary for Reach 1R: 12" Steel Pipe

 Inflow Area =
 1.980 ac,
 2.71% Impervious, Inflow Depth >
 2.54" for 10-Year event

 Inflow =
 5.55 cfs @
 12.11 hrs, Volume=
 0.418 af

 Outflow =
 5.55 cfs @
 12.11 hrs, Volume=
 0.418 af, Atten= 0%, Lag= 0.1 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Max. Velocity= 9.40 fps, Min. Travel Time= 0.1 min Avg. Velocity = 3.68 fps, Avg. Travel Time= 0.2 min

Peak Storage= 27 cf @ 12.11 hrs Average Depth at Peak Storage= 0.70' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 6.59 cfs

12.0" Round Pipe n= 0.012 Length= 45.0' Slope= 0.0291 '/' Inlet Invert= 76.08', Outlet Invert= 74.77'

![](_page_67_Picture_7.jpeg)

![](_page_67_Figure_8.jpeg)

## Reach 1R: 12" Steel Pipe

## Summary for Link 100L: POA #1

Inflow /	Area	=	1.980 ac,	2.71% Impervious,	Inflow Depth > 2	.54" for 10-Year event
Inflow		=	5.55 cfs @	12.11 hrs, Volume	e 0.418 af	
Primar	у	=	5.55 cfs @	12.11 hrs, Volume	e 0.418 af	, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

![](_page_68_Figure_5.jpeg)

## Link 100L: POA #1

## Summary for Link 200L: POA #2

Inflow /	Area	=	13.997 ac,	2.66% Impervious,	Inflow Depth > 2.	27" for 10-Year event
Inflow		=	20.19 cfs @	12.47 hrs, Volume	= 2.645 af	
Primary	у	=	20.19 cfs @	12.47 hrs, Volume	= 2.645 af,	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

![](_page_69_Figure_5.jpeg)

## Link 200L: POA #2

![](_page_70_Figure_0.jpeg)

Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: West Side	Runoff Area=86,228 sf 2.71% Impervious Runoff Depth>3.65" Flow Length=611' Tc=7.7 min CN=77 Runoff=7.99 cfs 0.602 af
Subcatchment2S: East Side	Runoff Area=609,713 sf 2.66% Impervious Runoff Depth>3.33" low Length=1,208' Tc=32.9 min CN=74 Runoff=29.85 cfs 3.885 af
Reach 1R: 12" Steel Pipe 12.0" Round Pipe n=0.012	Avg. Flow Depth=1.00' Max Vel=9.55 fps Inflow=7.99 cfs 0.602 af L=45.0' S=0.0291 '/' Capacity=6.59 cfs Outflow=6.75 cfs 0.602 af
Link 100L: POA #1	Inflow=6.75 cfs 0.602 af Primary=6.75 cfs 0.602 af
Link 200L: POA #2	Inflow=29.85 cfs  3.885 af Primary=29.85 cfs  3.885 af

Total Runoff Area = 15.977 ac Runoff Volume = 4.487 af Average Runoff Depth = 3.37" 97.34% Pervious = 15.551 ac 2.66% Impervious = 0.426 ac
# Section 4

# Drainage Calculations

Post-Development 2-Year, 24-Hour Summary 10-Year, 24-Hour Complete 25-Year, 24-Hour Summary





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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: North Road Entrance,	Runoff Area=51	,236 sf 8.13	% Impervi	ious Runoff	Depth=1.28"
	Flow Length=432'	Tc=6.3 min	CN=77	Runoff=1.71	cfs 0.126 af
Subcatchment 2S: Remaining Land East	Runoff Area=279	9,061 sf 0.00	% Impervi	ious Runoff	Depth=1.05"
	ow Length=1,208'	Tc=32.9 min	CN=73	Runoff=4.01	cfs 0.559 af
Subcatchment 10S: South Road Entrance	to Runoff Area=3,	377 sf 82.44	% Impervi	ious Runoff	Depth=2.74"
	Flow Length=139'	Tc=6.0 min	CN=95	Runoff=0.24	cfs 0.018 af
Subcatchment 11S: South Route 1 Fronta	<b>ge</b> Runoff Area=6	6,211 sf 0.00	% Impervi	ious Runoff	Depth=1.48"
	Flow Length=166'	Tc=6.0 min	CN=80	Runoff=0.25	cfs 0.018 af
Subcatchment12S: Roadside to CB #4	Runoff Area=9,	746 sf 23.27	% Impervi	ious Runoff	Depth=1.55"
	Flow Length=282'	Tc=9.6 min	CN=81	Runoff=0.36	cfs 0.029 af
Subcatchment 13S: Roadside to GUSF #1	Runoff Area=13,	602 sf 16.81	% Impervi	ious Runoff	Depth=1.55"
	Flow Length=264'	Tc=6.0 min	CN=81	Runoff=0.56	cfs 0.040 af
Subcatchment 20S: Roadside to CB #3-1	Runoff Area=11,	105 sf 40.77	% Impervi	ious Runoff	Depth=2.00"
	Flow Length=390'	Tc=6.0 min	CN=87	Runoff=0.60	cfs 0.043 af
Subcatchment 21S: Woodland and	Runoff Area=40	),322 sf 6.67	% Impervi	ious Runoff	Depth=1.28"
	Flow Length=338'	Tc=6.5 min	CN=77	Runoff=1.34	cfs 0.099 af
Subcatchment 22S: Woodland and	Runoff Area=53	3,034 sf 6.79	% Impervi	ious Runoff	Depth=1.10"
	Flow Length=408'	Tc=16.0 min	CN=74	Runoff=1.10	cfs 0.112 af
Subcatchment 23S: Roadside To CB #3-4	Runoff Area=8,	495 sf 25.20	% Impervi	ious Runoff	Depth=1.48"
	Flow Length=150'	Tc=6.0 min	CN=80	Runoff=0.34	cfs 0.024 af
Subcatchment 25S: Loading Area to CB #	<b>2</b> Runoff Area=4,4	11 sf 100.00	% Impervi	ious Runoff	Depth=3.07"
	Flow Length=137'	Tc=6.0 min	CN=98	Runoff=0.32	cfs 0.026 af
Subcatchment 26S: Parking Lot to CB #1-	<b>1</b> Runoff Area=18,	776 sf 85.85	% Impervi	ious Runoff	Depth=2.74"
	Flow Length=332'	Tc=6.0 min	CN=95	Runoff=1.31	cfs 0.099 af
Subcatchment 27S: Proposed Roof	Runoff Area=20,0	00 sf 100.00 Tc=6.0 min	% Impervi CN=98	ious Runoff Runoff=1.47	Depth=3.07" cfs  0.117 af
Subcatchment 29S: Open Space to GUSF	<b>#2</b> Runoff Area=90	),054 sf 0.00	% Impervi	ious Runoff	Depth=1.10"
	Flow Length=457'	Tc=6.0 min	CN=74	Runoff=2.55	cfs_0.190 af
Subcatchment 30S: Remaining Land	Runoff Area=86,	511 sf 18.73	% Impervi	ious Runoff	Depth=1.55"
	Flow Length=760'	Tc=12.0 min	CN=81	Runoff=2.94	cfs  0.256 af
Reach 1R: 12" Steel Pipe 7	Avg. Flow Depth=0.	40' Max Vel	=7.60 fps	Inflow=2.26	cfs 0.230 af
12.0" Round Pipe n=0.012 L	=45.0' S=0.0291 '/	″Capacity=6	6.59 cfs 0	Dutflow=2.26	cfs 0.230 af

## 5116-Post-061721

Type III 24-hr 2-Year Rainfall=3.30" Printed 7/1/2021

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Reach 10R: Roadside Swale	Avg. Flow Depth=0.33' Max Vel=1.96 fps Inflow=1.94 cfs 0.144 af n=0.030 L=98.0' S=0.0104 '/' Capacity=17.99 cfs Outflow=1.93 cfs 0.144 af
Reach 13R: Swale	Avg. Flow Depth=0.08' Max Vel=1.72 fps Inflow=0.29 cfs 0.069 af n=0.030 L=41.0' S=0.0395 '/' Capacity=28.58 cfs Outflow=0.29 cfs 0.069 af
Reach 25R: 18" CPP 18.0" Round Pipe	Avg. Flow Depth=0.47' Max Vel=6.80 fps Inflow=3.27 cfs 0.304 af n=0.012 L=83.0' S=0.0175 '/' Capacity=15.04 cfs Outflow=3.27 cfs 0.304 af
Reach 27R: 12" Roof Leader 12.0" Round Pipe	Avg. Flow Depth=0.43' Max Vel=4.57 fps Inflow=1.47 cfs 0.117 af n=0.012 L=300.0' S=0.0100 '/' Capacity=3.86 cfs Outflow=1.45 cfs 0.117 af
Reach 28R: Riprap Swale	Avg. Flow Depth=0.21' Max Vel=2.82 fps Inflow=1.45 cfs 0.117 af n=0.069 L=108.0' S=0.1759 '/' Capacity=26.22 cfs Outflow=1.45 cfs 0.117 af
Pond 1P: CB #5-2	Peak Elev=78.48' Storage=12 cf Inflow=1.71 cfs 0.126 af 12.0" Round Culvert n=0.012 L=52.0' S=0.0050 '/' Outflow=1.71 cfs 0.126 af
Pond 10P: CB #5-1	Peak Elev=78.13' Storage=12 cf Inflow=1.94 cfs 0.144 af 12.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=1.94 cfs 0.144 af
Pond 12P: CB #4	Peak Elev=82.47' Storage=16 cf Inflow=0.36 cfs 0.029 af 12.0" Round Culvert n=0.120 L=50.0' S=0.0050 '/' Outflow=0.35 cfs 0.029 af
Pond 13P: GUSF #1	Peak Elev=82.34' Storage=1,664 cf Inflow=0.88 cfs 0.069 af Outflow=0.29 cfs 0.069 af
Pond 20P: CB #3-1	Peak Elev=76.93' Storage=7 cf Inflow=0.60 cfs 0.043 af 15.0" Round Culvert n=0.012 L=8.0' S=0.0100 '/' Outflow=0.59 cfs 0.043 af
Pond 21P: CB #3-2	Peak Elev=84.26' Storage=8 cf Inflow=1.34 cfs 0.099 af 12.0" Round Culvert n=0.012 L=142.0' S=0.0500 '/' Outflow=1.34 cfs 0.099 af
Pond 22P: CB #3-3	Peak Elev=79.54' Storage=7 cf Inflow=1.10 cfs 0.112 af 12.0" Round Culvert n=0.012 L=68.0' S=0.0360 '/' Outflow=1.10 cfs 0.112 af
Pond 23P: CB #3-4	Peak Elev=77.29' Storage=4 cf Inflow=0.34 cfs 0.024 af 12.0" Round Culvert n=0.012 L=45.0' S=0.0100 '/' Outflow=0.33 cfs 0.024 af
Pond 24P: DMH #3	Peak Elev=76.86' Storage=16 cf Inflow=2.96 cfs 0.278 af 18.0" Round Culvert n=0.012 L=177.0' S=0.0175 '/' Outflow=2.96 cfs 0.278 af
Pond 25P: CB #2	Peak Elev=73.84' Storage=4 cf Inflow=0.32 cfs 0.026 af 12.0" Round Culvert n=0.012 L=36.0' S=0.0100 '/' Outflow=0.32 cfs 0.026 af
Pond 26P: CB #1-1	Peak Elev=72.81' Storage=9 cf Inflow=1.31 cfs 0.099 af 12.0" Round Culvert n=0.012 L=13.0' S=0.0100 '/' Outflow=1.31 cfs 0.099 af
Pond 27P: DMH #1	Peak Elev=72.47' Storage=14 cf Inflow=4.53 cfs 0.402 af 18.0" Round Culvert n=0.012 L=50.0' S=0.0100 '/' Outflow=4.53 cfs 0.402 af
Pond 29P: GUSF #2	Peak Elev=57.96' Storage=17,547 cf Inflow=8.52 cfs 0.710 af Outflow=3.81 cfs 0.667 af

Link 100L: POA #1

Inflow=2.26 cfs 0.230 af Primary=2.26 cfs 0.230 af

Link 200L: POA #2

Inflow=9.24 cfs 1.482 af Primary=9.24 cfs 1.482 af

Total Runoff Area = 15.977 acRunoff Volume = 1.755 afAverage Runoff Depth = 1.32"88.33% Pervious = 14.113 ac11.67% Impervious = 1.864 ac



**5116-Post-061721** *Type II* Prepared by Altus Engineering, Inc. HydroCAD® 10.00-25 s/n 01222 © 2019 HydroCAD Software Solutions LLC

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method Subcatchment 1S: North Road Entrance, Runoff Area=51,236 sf 8.13% Impervious Runoff Depth=2.54" Flow Length=432' Tc=6.3 min CN=77 Runoff=3.47 cfs 0.249 af Runoff Area=279,061 sf 0.00% Impervious Runoff Depth=2.20" Subcatchment 2S: Remaining Land East Flow Length=1,208' Tc=32.9 min CN=73 Runoff=8.88 cfs 1.176 af Subcatchment 10S: South Road Entrance to Runoff Area=3,377 sf 82.44% Impervious Runoff Depth=4.32" Flow Length=139' Tc=6.0 min CN=95 Runoff=0.36 cfs 0.028 af Subcatchment 11S: South Route 1 Frontage Runoff Area=6,211 sf 0.00% Impervious Runoff Depth=2.81" Flow Length=166' Tc=6.0 min CN=80 Runoff=0.47 cfs 0.033 af Runoff Area=9,746 sf 23.27% Impervious Runoff Depth=2.90" Subcatchment 12S: Roadside to CB #4 Flow Length=282' Tc=9.6 min CN=81 Runoff=0.67 cfs 0.054 af Subcatchment 13S: Roadside to GUSF #1 Runoff Area=13,602 sf 16.81% Impervious Runoff Depth=2.90" Flow Length=264' Tc=6.0 min CN=81 Runoff=1.06 cfs 0.075 af Runoff Area=11,105 sf 40.77% Impervious Runoff Depth=3.47" Subcatchment 20S: Roadside to CB #3-1 Flow Length=390' Tc=6.0 min CN=87 Runoff=1.02 cfs 0.074 af Runoff Area=40,322 sf 6.67% Impervious Runoff Depth=2.54" Subcatchment 21S: Woodland and Flow Length=338' Tc=6.5 min CN=77 Runoff=2.71 cfs 0.196 af Runoff Area=53,034 sf 6.79% Impervious Runoff Depth=2.28" Subcatchment 22S: Woodland and Flow Length=408' Tc=16.0 min CN=74 Runoff=2.39 cfs 0.232 af Runoff Area=8,495 sf 25.20% Impervious Runoff Depth=2.81" Subcatchment 23S: Roadside To CB #3-4 Flow Length=150' Tc=6.0 min CN=80 Runoff=0.64 cfs 0.046 af Subcatchment 25S: Loading Area to CB #2 Runoff Area=4,411 sf 100.00% Impervious Runoff Depth=4.66" Flow Length=137' Tc=6.0 min CN=98 Runoff=0.49 cfs 0.039 af Subcatchment 26S: Parking Lot to CB #1-1 Runoff Area=18,776 sf 85.85% Impervious Runoff Depth=4.32" Flow Length=332' Tc=6.0 min CN=95 Runoff=2.01 cfs 0.155 af Runoff Area=20,000 sf 100.00% Impervious Runoff Depth=4.66" Subcatchment 27S: Proposed Roof Tc=6.0 min CN=98 Runoff=2.20 cfs 0.178 af Subcatchment 29S: Open Space to GUSF #2 Runoff Area=90,054 sf 0.00% Impervious Runoff Depth=2.28" Flow Length=457' Tc=6.0 min CN=74 Runoff=5.51 cfs 0.394 af Runoff Area=86,511 sf 18.73% Impervious Runoff Depth=2.90" Subcatchment 30S: Remaining Land Flow Length=760' Tc=12.0 min CN=81 Runoff=5.54 cfs 0.479 af Avg. Flow Depth=0.62' Max Vel=9.07 fps Inflow=4.59 cfs 0.439 af Reach 1R: 12" Steel Pipe 12.0" Round Pipe n=0.012 L=45.0' S=0.0291 '/' Capacity=6.59 cfs Outflow=4.59 cfs 0.439 af

Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points

## 5116-Post-061721

Type III 24-hr 10-Year Rainfall=4.90" Printed 7/1/2021

Prepared by Altus Engineering, Inc. HydroCAD® 10.00-25 s/n 01222 © 2019 HydroCAD Software Solutions LLC

Reach 10R: Roadside Swale	Avg. Flow Depth=0.47' Max Vel=2.37 fps Inflow=3.78 cfs 0.277 af n=0.030 L=98.0' S=0.0104 '/' Capacity=17.99 cfs Outflow=3.76 cfs 0.277 af
Reach 13R: Swale	Avg. Flow Depth=0.12' Max Vel=2.26 fps Inflow=0.63 cfs 0.129 af n=0.030 L=41.0' S=0.0395 '/' Capacity=28.58 cfs Outflow=0.63 cfs 0.129 af
Reach 25R: 18" CPP 18.0" Round Pipe	Avg. Flow Depth=0.69' Max Vel=8.18 fps Inflow=6.43 cfs 0.586 af n=0.012 L=83.0' S=0.0175 '/' Capacity=15.04 cfs Outflow=6.43 cfs 0.586 af
Reach 27R: 12" Roof Leader 12.0" Round Pipe	Avg. Flow Depth=0.54' Max Vel=5.06 fps Inflow=2.20 cfs 0.178 af n=0.012 L=300.0' S=0.0100 '/' Capacity=3.86 cfs Outflow=2.17 cfs 0.178 af
Reach 28R: Riprap Swale	Avg. Flow Depth=0.27' Max Vel=3.21 fps Inflow=2.17 cfs 0.178 af n=0.069 L=108.0' S=0.1759 '/' Capacity=26.22 cfs Outflow=2.17 cfs 0.178 af
Pond 1P: CB #5-2	Peak Elev=79.68' Storage=26 cf Inflow=3.47 cfs 0.249 af 12.0" Round Culvert n=0.012 L=52.0' S=0.0050 '/' Outflow=3.43 cfs 0.249 af
Pond 10P: CB #5-1	Peak Elev=78.83' Storage=20 cf Inflow=3.77 cfs 0.277 af 12.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=3.78 cfs 0.277 af
Pond 12P: CB #4	Peak Elev=84.16' Storage=38 cf Inflow=0.67 cfs 0.054 af 12.0" Round Culvert n=0.120 L=50.0' S=0.0050 '/' Outflow=0.65 cfs 0.054 af
Pond 13P: GUSF #1	Peak Elev=82.99' Storage=2,543 cf Inflow=1.63 cfs 0.129 af Outflow=0.63 cfs 0.129 af
Pond 20P: CB #3-1	Peak Elev=77.34' Storage=12 cf Inflow=1.02 cfs 0.074 af 15.0" Round Culvert n=0.012 L=8.0' S=0.0100 '/' Outflow=1.01 cfs 0.074 af
Pond 21P: CB #3-2	Peak Elev=84.66' Storage=13 cf Inflow=2.71 cfs 0.196 af 12.0" Round Culvert n=0.012 L=142.0' S=0.0500 '/' Outflow=2.71 cfs 0.196 af
Pond 22P: CB #3-3	Peak Elev=79.89' Storage=12 cf Inflow=2.39 cfs 0.232 af 12.0" Round Culvert n=0.012 L=68.0' S=0.0360 '/' Outflow=2.39 cfs 0.232 af
Pond 23P: CB #3-4	Peak Elev=77.52' Storage=7 cf Inflow=0.64 cfs 0.046 af 12.0" Round Culvert n=0.012 L=45.0' S=0.0100 '/' Outflow=0.64 cfs 0.046 af
Pond 24P: DMH #3	Peak Elev=77.30' Storage=25 cf Inflow=5.97 cfs 0.547 af 18.0" Round Culvert n=0.012 L=177.0' S=0.0175 '/' Outflow=5.97 cfs 0.547 af
Pond 25P: CB #2	Peak Elev=73.94' Storage=5 cf Inflow=0.49 cfs 0.039 af 12.0" Round Culvert n=0.012 L=36.0' S=0.0100 '/' Outflow=0.48 cfs 0.039 af
Pond 26P: CB #1-1	Peak Elev=73.37' Storage=16 cf Inflow=2.01 cfs 0.155 af 12.0" Round Culvert n=0.012 L=13.0' S=0.0100 '/' Outflow=1.98 cfs 0.155 af
Pond 27P: DMH #1	Peak Elev=73.12' Storage=22 cf Inflow=8.36 cfs 0.742 af 18.0" Round Culvert n=0.012 L=50.0' S=0.0100 '/' Outflow=8.36 cfs 0.742 af
Pond 29P: GUSF #2	Peak Elev=58.66' Storage=24,031 cf Inflow=16.00 cfs 1.314 af Outflow=7.85 cfs 1.270 af

Link 100L: POA #1

Inflow=4.59 cfs 0.439 af Primary=4.59 cfs 0.439 af

Link 200L: POA #2

Inflow=19.31 cfs 2.926 af Primary=19.31 cfs 2.926 af

Total Runoff Area = 15.977 ac Runoff Volume = 3.408 af Average Runoff Depth = 2.56" 88.33% Pervious = 14.113 ac 11.67% Impervious = 1.864 ac

## Summary for Subcatchment 1S: North Road Entrance, House and Yard to CB #5-2

Runoff = 3.47 cfs @ 12.09 hrs, Volume= 0.249 af, Depth= 2.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	А	rea (sf)	CN E	Description		
*		741	98 l	mpervious	Existing Pa	avement
*		1,318	98 l	mpervious	Existing Bu	uilding
*		2,105	98 l	mpervious	Proposed I	Pavement
		333	96 C	Gravel surfa	ace, HSG D	)
		3,755	96 C	Gravel surfa	ace, HSG (	
		1,629	87 E	Dirt roads, I	HSG C	
		7,139	80 >	75% Gras	s cover, Go	bod, HSG D
		818	77 V	Voods, Go	od, HSG D	
		14,145	74 >	•75% Gras	s cover, Go	ood, HSG C
		19,253	70 V	Voods, Go	od, HSG C	
		51,236	77 V	Veighted A	verage	
		47,072	ç	1.87% Pei	vious Area	
		4,164	8	3.13% Impe	ervious Are	a
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.9	54	0.0579	0.23		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.30"
	1.5	192	0.0941	2.15		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.5	97	0.0336	2.95		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.3	80	0.0750	4.41		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.1	9	0.0075	1.76		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
	6.3	432	Total			



## Subcatchment 1S: North Road Entrance, House and Yard to CB #5-2

### Summary for Subcatchment 2S: Remaining Land East Side

Runoff = 8.88 cfs @ 12.47 hrs, Volume= 1.176 af, Depth= 2.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

_	A	rea (sf)	CN D	Description		
		1,161	89 E	)irt roads, H	HSG D	
		2,559	87 E	)irt roads, l	HSG C	
		2,459	80 >	75% Gras	s cover, Go	ood, HSG D
		93,993	77 V	Voods, Go	od, HSG D	
		3,899	74 >	75% Gras	s cover, Go	ood, HSG C
_	1	74,990	70 V	Voods, Go	od, HSG C	
	2	79,061	73 V	Veighted A	verage	
	2	79,061	1	00.00% Pe	ervious Are	а
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	8.8	83	0.1231	0.16		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.30"
	1.4	121	0.0826	1.44		Shallow Concentrated Flow,
				a = (		Woodland Kv= 5.0 fps
	7.1	301	0.0199	0.71		Shallow Concentrated Flow,
	7.0	000	0 0000	0.47		Woodland Kv= 5.0 fps
	7.8	223	0.0090	0.47		Shallow Concentrated Flow,
	10	77	0 0050	0.70		Woodland Kv= 5.0 fps
	1.6	11	0.0250	0.79		Shallow Concentrated Flow,
	1 1	00	0.0016	1 4 2		shallow Concentrated Flow
	1.1	90	0.0010	1.43		Moodland Ky= 5.0 fpc
	51	305	0 0303	0.00		Shallow Concentrated Flow
	J. I	305	0.0393	0.99		Woodland Ky= 5.0 fps
-	22.0	1 200	Total			
	JZ.9	1,∠∪0	rotal			



## Subcatchment 2S: Remaining Land East Side

Printed 7/1/2021

#### Summary for Subcatchment 10S: South Road Entrance to CB #5-1

0.36 cfs @ 12.08 hrs, Volume= 0.028 af, Depth= 4.32" Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	A	rea (sf)	CN	Description		
*		129	98	Impervious	Existing Pa	avement
*		2,655	98	Impervious	Proposed I	Pavement
		593	80	>7 <sup>5</sup> % Gras	s cover, Go	bod, HSG D
		3,377	95	Weighted A	verage	
		593		17.56% Pei	rvious Area	
		2,784		82.44% Imp	pervious Are	ea
	Тс	Length	Slope	e Velocity	Capacity	Description
(m	in)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
C	).4	50	0.0801	2.12		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.30"
C	).1	34	0.0783	5.68		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
C	).1	37	0.0543	4.73		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
C	).1	18	0.0444	4.28		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps



#### Subcatchment 10S: South Road Entrance to CB #5-1



### Summary for Subcatchment 11S: South Route 1 Frontage

Runoff = 0.47 cfs @ 12.09 hrs, Volume= 0.033 af, Depth= 2.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

A	rea (sf)	CN [	Description							
	5,206	80 >	80 >75% Grass cover, Good, HSG D							
	1,005	<u> </u>	/voods, Go	od, HSG D						
	6,211	80 V	Neighted A	verage						
	6.211	1	100.00% Pe	ervious Are	а					
	- /									
Тс	Lenath	Slope	Velocitv	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
3.4	50	0.0660	0.24	(0.0)	Shoot Flow					
5.4	50	0.0000	0.24		Crease Short = 0.150  D2= 2.20"					
					Grass: Short $n=0.150 PZ=3.30$					
0.6	98	0.1326	2.55		Shallow Concentrated Flow,					
					Short Grass Pasture Kv= 7.0 fps					
0.2	18	0.0142	1.79		Shallow Concentrated Flow,					
					Grassed Waterway Kv= 15.0 fps					
1 2	166	Total	Incroaced t	o minimum	$T_{0} = 6.0 min$					

4.2 166 Total, Increased to minimum Tc = 6.0 min

#### Subcatchment 11S: South Route 1 Frontage



## Summary for Subcatchment 12S: Roadside to CB #4

Runoff = 0.67 cfs @ 12.13 hrs, Volume= 0.054 af, Depth= 2.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	A	rea (sf)	CN	Description						
*		2,268	98	Impervious	Proposed I	Pavement				
		1,740	80	>75% Grass cover, Good, HSG D						
		1,668	77	Woods, Go	od, HSG D					
		3,711	74	>75% Gras	s cover, Go	bod, HSG C				
		359	70	Woods, Go	od, HSG C					
		9.746	81	Weighted A	verade					
		7,478	-	76.73% Pe	rvious Area					
		2,268		23.27% Im	pervious Ar	ea				
		,		•						
	Тс	Length	Slop	e Velocity	Capacity	Description				
(r	nin)	(feet)	(ft/ft	) (ft/sec)	(cfs)					
	7.9	41	0.039	9 0.09		Sheet Flow.				
						Woods: Light underbrush n= 0.400 P2= 3.30"				
	0.9	61	0.0492	2 1.11		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
	0.3	37	0.084	9 2.04		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.1	11	0.040	0 1.40		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.4	132	0.0614	4 5.03		Shallow Concentrated Flow,				
						Paved Kv= 20.3 fps				
	9.6	282	Total							



## Subcatchment 12S: Roadside to CB #4

Printed 7/1/2021

## Summary for Subcatchment 13S: Roadside to GUSF #1

Runoff = 1.06 cfs @ 12.09 hrs, Volume= 0.075 af, Depth= 2.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	A	rea (sf)	CN E	Description		
*		2,286	98 l	mpervious	Proposed I	Pavement
		7,996	80 >	75% Gras	s cover, Go	ood, HSG D
		33	77 V	Voods, Go	od, HSG D	
		2,443	74 >	•75% Gras	s cover, Go	ood, HSG C
		844	70 V	Voods, Go	od, HSG C	
		13,602	81 V	Veighted A	verage	
		11,316	8	3.19% Per	vious Area	
		2,286	1	6.81% Imp	pervious Ar	ea
	_				_	
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	0.2	12	0.0200	0.91		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.30"
	0.0	8	0.3333	4.04		Shallow Concentrated Flow,
	0.0	00	0.0450	4.00		Short Grass Pasture Kv= 7.0 fps
	0.6	63	0.0159	1.89		Shallow Concentrated Flow,
	0.0	<b>F7</b>	0.0054	0.04		Grassed Waterway KV= 15.0 fps
	0.3	57	0.0351	2.81		Shallow Concentrated Flow,
	0.4	00	0.0610	2 70		Grassed Waterway KV= 15.0 lps
	0.4	02	0.0610	3.70		Shallow Concentrated Flow, Creased Weterway, Ky= 15.0 fps
	0.2	40	0.0052	4.62		Shallow Concentrated Flow
	0.2	42	0.0952	4.03		Grassed Waterway, Ky= 15.0 fps
_	17	264	Tatal	norocod 4	o minimum	$T_{0} = 6.0 \text{ min}$
	1.7	204	i otal, i	ncreased t	ommmum	1 I C – 0.0 IIIIII





## Subcatchment 13S: Roadside to GUSF #1

## Summary for Subcatchment 20S: Roadside to CB #3-1

Runoff = 1.02 cfs @ 12.09 hrs, Volume= 0.074 af, Depth= 3.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	A	rea (sf)	CN E	Description		
*		4,527	98 li	mpervious	Proposed I	Pavement
		6,371	80 >	75% Gras	s cover, Go	ood, HSG D
		207	74 >	75% Gras	s cover, Go	ood, HSG C
		11,105	87 V	Veighted A	verage	
		6,578	5	9.23% Per	vious Area	
		4,527	4	0.77% Imp	ervious Ar	ea
				-		
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	0.2	12	0.0200	0.91		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.30"
	0.0	8	0.3333	4.04		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.6	63	0.0159	1.89		Shallow Concentrated Flow,
						Grassed Waterway Kv= 15.0 fps
	1.5	257	0.0350	2.81		Shallow Concentrated Flow,
						Grassed Waterway Kv= 15.0 fps
	0.2	50	0.0650	3.82		Shallow Concentrated Flow,
						Grassed Waterway Kv= 15.0 fps
	2.5	390	Total, I	ncreased t	o minimum	Tc = 6.0 min





#### Summary for Subcatchment 21S: Woodland and Roadside to CB #3-2

Runoff 2.71 cfs @ 12.10 hrs, Volume= 0.196 af, Depth= 2.54" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

/	Area (sf)	CN [	Description			
*	2,690	98 I	mpervious	Proposed I	Pavement	
	304	87 I	Dirt roads, l	HSG C		
	14,485	80 >	>75% Gras	s cover, Go	ood, HSG D	
	873	77 \	Noods, Go	od, HSG D		
	15,967	74 >	>75% Gras	s cover, Go	bod, HSG C	
	6,003	70 \	Noods, Go	od, HSG C		
	40,322	77 \	Neighted A	verage		
	37,632	ę	93.33% Pei	vious Area		
	2,690	6	6.67% Impe	ervious Area	а	
			-			
Tc	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
3.9	50	0.0493	0.22		Sheet Flow,	
					Grass: Short n= 0.150 P2= 3.30"	
2.1	180	0.0402	1.40		Shallow Concentrated Flow,	
					Short Grass Pasture Kv= 7.0 fps	
0.1	11	0.0402	1.40		Shallow Concentrated Flow,	
					Short Grass Pasture Kv= 7.0 fps	
0.4	97	0.0341	3.75		Shallow Concentrated Flow,	
					Paved Kv= 20.3 fps	
6.5	338	Total				



## Subcatchment 21S: Woodland and Roadside to CB #3-2

### Summary for Subcatchment 22S: Woodland and Roadside to CB #3-3

Runoff 2.39 cfs @ 12.22 hrs, Volume= 0.232 af, Depth= 2.28" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	A	rea (sf)	CN	Description			
*	* 3,603 98 Impervious Proposed Pavement						
		1,976	87	Dirt roads, I	HSG C		
		3,978	80	>75% Gras	s cover, Go	ood, HSG D	
		442	77	Woods, Go	od, HSG D		
	8,850 74 >75% Grass cover, Good, HSG C						
		34,185	70	Woods, Go	od, HSG C		
		53,034	74	Weighted A	verage		
		49,431	9	93.21% Pei	vious Area		
		3,603	(	6.79% Impe	ervious Area	а	
	Тс	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	12.4	50	0.0191	0.07		Sheet Flow,	
						Woods: Light underbrush n= 0.400 P2= 3.30"	
	1.9	185	0.1017	1.59		Shallow Concentrated Flow,	
						Woodland Kv= 5.0 fps	
	0.4	52	0.0769	1.94		Shallow Concentrated Flow,	
						Short Grass Pasture Kv= 7.0 fps	
	0.7	44	0.0471	1.09		Shallow Concentrated Flow,	
						Woodland Kv= 5.0 fps	
	0.1	8	0.0350	1.31		Shallow Concentrated Flow,	
						Short Grass Pasture Kv= 7.0 fps	
	0.5	69	0.0140	2.40		Shallow Concentrated Flow,	
						Paved Kv= 20.3 fps	
	16.0	408	Total				



## Subcatchment 22S: Woodland and Roadside to CB #3-3

#### Summary for Subcatchment 23S: Roadside To CB #3-4

Runoff = 0.64 cfs @ 12.09 hrs, Volume= 0.046 af, Depth= 2.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Area (sf)	CN	Description					
*	2,141	98	Impervoius Proposed Pavement					
	224	80	>75% Gras	s cover, Go	ood, HSG D			
	6,130	74	>75% Gras	s cover, Go	ood, HSG C			
	8,495	80	Weighted A	verage				
	6,354		74.80% Pei	rvious Area				
	2,141		25.20% Imp	pervious Are	ea			
Т	c Length	Slope	Velocity	Capacity	Description			
(min	) (feet)	(ft/ft)	(ft/sec)	(cfs)				
0.2	2 14	0.0200	0.94		Sheet Flow,			
					Smooth surfaces n= 0.011 P2= 3.30"			
0.0	) 4	0.0400	1.40		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
0.0	) 5	0.3333	4.04		Shallow Concentrated Flow,			
_					Short Grass Pasture Kv= 7.0 fps			
0.9	9 127	0.0222	2.23		Shallow Concentrated Flow,			
					Grassed Waterway Kv= 15.0 fps			



## Subcatchment 23S: Roadside To CB #3-4



## Summary for Subcatchment 25S: Loading Area to CB #2

Runoff = 0.49 cfs @ 12.08 hrs, Volume= 0.039 af, Depth= 4.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

_	A	rea (sf)	CN D	Description			
*		4,411	98 Ir	mpervious	Proposed F	Pavement	
		4,411	100.00% Impervious Are		pervious A	rea	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	0.5	44	0.0316	1.42		Sheet Flow,	
	0.1	24	0.0238	3.13		Smooth surfaces n= 0.011 P2= 3.30" <b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps	
	0.3	60	0.0200	2.87		Shallow Concentrated Flow,	
	0.1	9	0.0040	1.28		Paved Kv= 20.3 fps <b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps	
	4.0	407	<b>—</b> · · · ·			T 00 '	

1.0 137 Total, Increased to minimum Tc = 6.0 min

## Subcatchment 25S: Loading Area to CB #2



## Summary for Subcatchment 26S: Parking Lot to CB #1-1

Runoff = 2.01 cfs @ 12.08 hrs, Volume= 0.155 af, Depth= 4.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	A	rea (sf)	CN E	Description					
*		16,120	98 li	98 Impervious Proposed Pavement					
		2,295	80 >	75% Gras	s cover, Go	ood, HSG D			
		361	74 >	75% Gras	s cover, Go	bod, HSG C			
		18,776	95 V	Veighted A	verage				
		2,656	1	4.15% Per	vious Area				
16,120 85.85% Impervious Area									
	Тс	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	0.5	50	0.0444	1.67		Sheet Flow,			
						Smooth surfaces n= 0.011 P2= 3.30"			
	0.2	48	0.0334	3.71		Shallow Concentrated Flow,			
						Paved Kv= 20.3 fps			
	1.4	234	0.0200	2.87		Shallow Concentrated Flow,			
						Paved Kv= 20.3 fps			
	2.1	332	Total, I	ncreased t	o minimum	1 Tc = 6.0 min			

## Subcatchment 26S: Parking Lot to CB #1-1



## Summary for Subcatchment 27S: Proposed Roof

Runoff = 2.20 cfs @ 12.08 hrs, Volume= 0.178 af, Depth= 4.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"



## Summary for Subcatchment 29S: Open Space to GUSF #2

Runoff = 5.51 cfs @ 12.09 hrs, Volume= 0.394 af, Depth= 2.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

A	<u>rea (sf)</u>	<u>CN</u> D	escription					
	13,841	80 >	75% Gras	s cover, Go	ood, HSG D			
	18,593	77 V	77 Woods, Good, HSG D					
	31,340	74 >	74 >75% Grass cover, Good, HSG C					
	26,280	70 Woods, Good, HSG C						
	90,054	74 Weighted Average						
	90,054	1	00.00% Pe	ervious Are	а			
_								
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
1.5	16	0.0582	0.18		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.30"			
3.5	319	0.0100	1.50		Shallow Concentrated Flow,			
					Grassed Waterway Kv= 15.0 fps			
0.1	27	0.1290	5.44	13.61	Trap/Vee/Rect Channel Flow,			
					Bot.W=2.00' D=1.00' Z= 0.5 '/' Top.W=3.00'			
					n= 0.069 Riprap, 6-inch			
0.1	48	0.2800	8.02	20.05	Trap/Vee/Rect Channel Flow,			
					Bot.W=2.00' D=1.00' Z= 0.5 '/' Top.W=3.00'			
	. –				n= 0.069 Riprap, 6-inch			
0.2	47	0.0950	4.67	11.68	Trap/Vee/Rect Channel Flow,			
					Bot.W=2.00' D=1.00' Z= 0.5 '/' Top.W=3.00'			
					n= 0.069 Kiprap, 6-inch			
5.4	457	Total, li	ncreased t	o minimum	Tc = 6.0 min			



# Subcatchment 29S: Open Space to GUSF #2

## Summary for Subcatchment 30S: Remaining Land Southwest Side

Runoff 5.54 cfs @ 12.17 hrs, Volume= 0.479 af, Depth= 2.90" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	A	rea (sf)	CN E	Description		
*		11,834	98 l	mpervious	Existing Pa	avement
* 4,369 98 Impervious Existing Roof						pof
		27,369	80 >	•75% Gras	s cover, Go	ood, HSG D
		35,628	77 V	Voods, Go	od, HSG D	
		1,815	74 >	•75% Gras	s cover, Go	ood, HSG C
		5,496	70 V	Voods, Go	od, HSG C	
		86,511	81 V	Veighted A	verage	
		70,308	8	31.27% Pei	vious Area	
		16,203	1	8.73% Imp	pervious Are	ea
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.8	31	0.0200	0.14		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.30"
	0.1	15	0.0200	2.87		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
	1.2	74	0.0203	1.00		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	3.8	209	0.0335	0.92		Shallow Concentrated Flow,
		~~-				Woodland Kv= 5.0 fps
	1.4	207	0.0290	2.55		Shallow Concentrated Flow,
	0.0	75	0 0000	4 50		Grassed Waterway Kv= 15.0 fps
	0.3	75	0.0933	4.58		Shallow Concentrated Flow,
	4 4	140	0 4000	4 74		Grassed Waterway KV= 15.0 fps
	1.4	149	0.1208	1.74		Shahow Concentrated Flow,
	40.0	700	<b>T</b> ( )			
	12.0	760	Total			



## Subcatchment 30S: Remaining Land Southwest Side

## Summary for Reach 1R: 12" Steel Pipe

 Inflow Area =
 1.932 ac, 13.66% Impervious, Inflow Depth =
 2.73" for 10-Year event

 Inflow =
 4.59 cfs @
 12.11 hrs, Volume=
 0.439 af

 Outflow =
 4.59 cfs @
 12.11 hrs, Volume=
 0.439 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Max. Velocity= 9.07 fps, Min. Travel Time= 0.1 min Avg. Velocity = 2.07 fps, Avg. Travel Time= 0.4 min

Peak Storage= 23 cf @ 12.11 hrs Average Depth at Peak Storage= 0.62' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 6.59 cfs

12.0" Round Pipe n= 0.012 Length= 45.0' Slope= 0.0291 '/' Inlet Invert= 76.08', Outlet Invert= 74.77'





## Reach 1R: 12" Steel Pipe

#### Summary for Reach 10R: Roadside Swale

Inflow Area = 1.254 ac, 12.72% Impervious, Inflow Depth = 2.65" for 10-Year event Inflow 3.78 cfs @ 12.09 hrs, Volume= 0.277 af = Outflow 3.76 cfs @ 12.11 hrs, Volume= = 0.277 af, Atten= 0%, Lag= 1.1 min Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Max. Velocity= 2.37 fps, Min. Travel Time= 0.7 min Avg. Velocity = 0.63 fps, Avg. Travel Time= 2.6 min Peak Storage= 156 cf @ 12.11 hrs Average Depth at Peak Storage= 0.47' Bank-Full Depth= 1.00' Flow Area= 5.0 sf, Capacity= 17.99 cfs 2.00' x 1.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 3.0 '/' Top Width= 8.00' Length= 98.0' Slope= 0.0104 '/' Inlet Invert= 77.10', Outlet Invert= 76.08' ‡ Reach 10R: Roadside Swale Hydrograph Inflow
Outflow <u>3 78 cfs</u> 4 3.76 cfs Inflow Area=1.254 ac Avg. Flow Depth=0.47' Max Vel=2.37 fps 3 n=0.030 <sup>-</sup>low (cfs) L=98.0' 2 S=0.0104 '/' Capacity=17.99 cfs 1 0 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 0 2

Time (hours)

#### Summary for Reach 13R: Swale

 Inflow Area =
 0.536 ac, 19.50% Impervious, Inflow Depth > 2.89" for 10-Year event

 Inflow =
 0.63 cfs @ 12.41 hrs, Volume=
 0.129 af

 Outflow =
 0.63 cfs @ 12.42 hrs, Volume=
 0.129 af, Atten= 0%, Lag= 0.2 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Max. Velocity= 2.26 fps, Min. Travel Time= 0.3 min Avg. Velocity = 0.66 fps, Avg. Travel Time= 1.0 min

Peak Storage= 12 cf @ 12.42 hrs Average Depth at Peak Storage= 0.12' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 28.58 cfs

2.00' x 1.00' deep channel, n= 0.030 Earth, grassed & winding Side Slope Z-value= 2.0 '/' Top Width= 6.00' Length= 41.0' Slope= 0.0395 '/' Inlet Invert= 77.70', Outlet Invert= 76.08'

Reach 13R: Swale


## Summary for Reach 25R: 18" CPP

 Inflow Area =
 2.694 ac, 14.80% Impervious, Inflow Depth = 2.61" for 10-Year event

 Inflow =
 6.43 cfs @ 12.11 hrs, Volume=
 0.586 af

 Outflow =
 6.43 cfs @ 12.11 hrs, Volume=
 0.586 af, Atten= 0%, Lag= 0.1 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Max. Velocity= 8.18 fps, Min. Travel Time= 0.2 min Avg. Velocity = 2.49 fps, Avg. Travel Time= 0.6 min

Peak Storage= 65 cf @ 12.11 hrs Average Depth at Peak Storage= 0.69' Bank-Full Depth= 1.50' Flow Area= 1.8 sf, Capacity= 15.04 cfs

18.0" Round Pipe n= 0.012 Length= 83.0' Slope= 0.0175 '/' Inlet Invert= 72.95', Outlet Invert= 71.50'





### Reach 25R: 18" CPP

## Summary for Reach 27R: 12" Roof Leader

 Inflow Area =
 0.459 ac,100.00% Impervious, Inflow Depth =
 4.66" for 10-Year event

 Inflow =
 2.20 cfs @
 12.08 hrs, Volume=
 0.178 af

 Outflow =
 2.17 cfs @
 12.10 hrs, Volume=
 0.178 af, Atten= 1%, Lag= 0.8 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Max. Velocity= 5.06 fps, Min. Travel Time= 1.0 min Avg. Velocity = 1.70 fps, Avg. Travel Time= 2.9 min

Peak Storage= 129 cf @ 12.10 hrs Average Depth at Peak Storage= 0.54' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 3.86 cfs

12.0" Round Pipe n= 0.012 Length= 300.0' Slope= 0.0100 '/' Inlet Invert= 78.50', Outlet Invert= 75.50'





## Reach 27R: 12" Roof Leader

#### Summary for Reach 28R: Riprap Swale

Inflow Area = 0.459 ac,100.00% Impervious, Inflow Depth = 4.66" for 10-Year event Inflow 2.17 cfs @ 12.10 hrs, Volume= 0.178 af = Outflow 2.17 cfs @ 12.10 hrs, Volume= = 0.178 af, Atten= 0%, Lag= 0.4 min Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Max. Velocity= 3.21 fps, Min. Travel Time= 0.6 min Avg. Velocity = 0.86 fps, Avg. Travel Time= 2.1 min Peak Storage= 73 cf @ 12.10 hrs Average Depth at Peak Storage= 0.27' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 26.22 cfs 2.00' x 1.00' deep channel, n= 0.069 Riprap, 6-inch Side Slope Z-value= 2.0 '/' Top Width= 6.00' Length= 108.0' Slope= 0.1759 '/' Inlet Invert= 75.50', Outlet Invert= 56.50' **Reach 28R: Riprap Swale** Hydrograph Inflow
Outflow 2 17 cfs 2.17 cfs Inflow Area=0.459 ac Avg. Flow Depth=0.27' 2 Max Vel=3.21 fps n=0.069 <sup>-</sup>low (cfs) L=108.0' S=0.1759 '/' Capacity=26.22 cfs 0 Ó Ż 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 Time (hours)

## Summary for Pond 1P: CB #5-2

Inflow Area	=	1.176 ac,	8.13% Impervious,	Inflow Depth =	2.54" for	10-Year event
Inflow	=	3.47 cfs @	12.09 hrs, Volume	= 0.249 a	af	
Outflow	=	3.43 cfs @	12.11 hrs, Volume	= 0.249 a	af, Atten= 1	%, Lag= 0.9 min
Primary	=	3.43 cfs @	12.11 hrs, Volume	= 0.249 a	af	-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 79.68' @ 12.11 hrs Surf.Area= 228 sf Storage= 26 cf

Plug-Flow detention time= 0.2 min calculated for 0.249 af (100% of inflow) Center-of-Mass det. time= 0.2 min (831.2 - 830.9)

Volume	Inv	ert Avail.Sto	orage Stora	ge Description	
#1	77.	56' 1	10 cf Custo	om Stage Data (Pri	ismatic)Listed below (Recalc)
Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
77.9 78.0 79.0 79.8	56 65 65 80	13 13 4 1,155	0 14 9 87	0 14 23 110	
Device	Routing	Invert	Outlet Devi	ces	
#1	Primary	77.56'	<b>12.0" Rou</b> L= 52.0' C Inlet / Outle n= 0.012,	<b>nd Culvert</b> CPP, square edge h et Invert= 77.56' / 77 Flow Area= 0.79 sf	eadwall, Ke= 0.500 7.30' S= 0.0050 '/' Cc= 0.900

**Primary OutFlow** Max=3.42 cfs @ 12.11 hrs HW=79.68' TW=78.83' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 3.42 cfs @ 4.35 fps) Pond 1P: CB #5-2



## Summary for Pond 10P: CB #5-1

Inflow Area	=	1.254 ac,	12.72% Imper	vious, Inflow	Depth =	2.65"	for 10-`	Year event
Inflow	=	3.77 cfs @	12.11 hrs, V	/olume=	0.277	af		
Outflow	=	3.78 cfs @	12.09 hrs, V	/olume=	0.277	af, Attei	n= 0%,	Lag= 0.0 min
Primary	=	3.78 cfs @	12.09 hrs, V	/olume=	0.277	af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 78.83' @ 12.09 hrs Surf.Area= 8 sf Storage= 20 cf

Plug-Flow detention time= 0.2 min calculated for 0.277 af (100% of inflow) Center-of-Mass det. time= 0.2 min (825.1 - 824.9)

Volume	Inv	vert Avail.Sto	rage Storage	Description	
#1	77.	20'	65 cf Custom	Stage Data (Prismatio	)Listed below (Recalc)
Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
77.2 78.3 79.3 79.3	20 30 30 50	13 13 4 416	0 14 9 42	0 14 23 65	
Device	Routing	Invert	Outlet Devices	6	
#1	Primary	77.20'	<b>12.0" Round</b> L= 20.0' CPF Inlet / Outlet Ir n= 0.012, Flo	<b>Culvert</b> , square edge headwal wert= 77.20' / 77.10' S w Area= 0.79 sf	ll, Ke= 0.500 δ= 0.0050 '/' Cc= 0.900

Primary OutFlow Max=3.78 cfs @ 12.09 hrs HW=78.83' TW=77.57' (Dynamic Tailwater) ☐ 1=Culvert (Barrel Controls 3.78 cfs @ 4.81 fps)

Type III 24-hr 10-Year Rainfall=4.90" Printed 7/1/2021

Pond 10P: CB #5-1



# Summary for Pond 12P: CB #4

Inflow A	rea =	0.224 ac, 23.	27% Impe	ervious,	Inflow Dep	oth = 2	.90"	for	10-Y	ear ev	ent
Inflow	=	0.67 cfs @ 1	2.13 hrs,	Volume	= (	).054 af					
Outflow	=	0.65 cfs @ 1	2.15 hrs.	Volume	= (	).054 af	. Atte	en= 3	%. L	_ag= 1	.0 min
Primary	=	0.65 cfs @ 1	2.15 hrs,	Volume	= (	0.054 af		-	,	5	-
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs											
Peak Ele	ev= 84.16'	@ 12.16 hrs S	Surf.Area=	= 13 sf	Storage= 3	88 cf					
Plug-Flo	w detentio	on time= 4.4 min	n calculate	ed for 0.0	)54 af (100	% of inf	low)				
Center-c	of-Mass de	et. time= 4.3 mir	n ( 827.6 -	823.3)							
Volume	Inve	ert Avail Sto	rade St	orade Di	escription						
	04.0					(D.:!	41 - 11	ام ما ما			1 - )
#1	81.2	25	bici Cl	istom S	tage Data	(Prisma	atic)∟	istea	Delo	w (Red	caic)
Elevatio	on	Surf.Area	Inc.Sto	ore	Cum.Sto	re					
(fee	et)	(sq-ft)	(cubic-fe	et)	(cubic-fee	et)					
81.2	25	13		0		0					
84.5	50	13		42	2	12					
85.5	50	4		9	5	51					
Device	Routing	Invert	Outlet D	evices							
#1	Primary	81.25'	12.0" F	Round C	ulvert						
	,, <b>,</b>	• · · - •	I = 50.0	CPP	square edo	ne head	wall	Ke=	0 500	0	
			Inlet / O	utlet Inv	ert= 81 25'	/ 81 00	' S=	0.00	50 '/'	$C_{C} = 0$	0 900
					A 01.20	, 01.00	0	5.000	,	00	0.000

n= 0.120, Flow Area= 0.79 sf

Primary OutFlow Max=0.65 cfs @ 12.15 hrs HW=84.14' TW=82.72' (Dynamic Tailwater) -1=Culvert (Outlet Controls 0.65 cfs @ 0.82 fps) Pond 12P: CB #4



## Summary for Pond 13P: GUSF #1

Inflow Area	=	0.536 ac,	19.50% Impe	ervious,	Inflow Depth =	2.90"	for 10-Y	ear event
Inflow	=	1.63 cfs @	12.10 hrs,	Volume	= 0.129	af		
Outflow	=	0.63 cfs @	12.41 hrs,	Volume	= 0.129	af, Atte	en= 61%,	Lag= 18.5 min
Primary	=	0.63 cfs @	12.41 hrs,	Volume	= 0.129	af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Starting Elev= 81.00' Surf.Area= 464 sf Storage= 601 cf Peak Elev= 82.99' @ 12.41 hrs Surf.Area= 1,551 sf Storage= 2,543 cf (1,942 cf above start) Flood Elev= 84.25' Surf.Area= 2,475 sf Storage= 5,079 cf (4,478 cf above start)

Plug-Flow detention time= 218.1 min calculated for 0.115 af (89% of inflow) Center-of-Mass det. time= 136.5 min (959.6 - 823.1)

Volume	Invert	Avai	il.Stora	ge Storage Descr	iption	
#1	77.50'		5,079	cf Custom Stage	e Data (Prismatic)	Listed below (Recalc)
Elevatio	n Si	urf.Area	Voids	Inc.Store	Cum.Store	
(fee	t)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
77.5	0	464	0.0	0	0	
79.0	0	464	40.0	278	278	
79.5	60	464	40.0	93	371	
81.0	0	464	33.0	230	601	
81.8	0	850	100.0	526	1,126	
82.0	0	955	100.0	181	1,307	
83.0	0	1,559	100.0	1,257	2,564	
84.0	0	2,282	100.0	1,921	4,484	
84.2	25	2,475	100.0	595	5,079	
Device	Routing	In	vert	Outlet Devices		
#1	Primary	78	.00' ′	12.0" Round Culve	ert	
	-		I	_= 30.0' CPP, squa	are edge headwall,	Ke= 0.500
			I	nlet / Outlet Invert=	78.00' / 77.70' S	= 0.0100 '/' Cc= 0.900
			I	n= 0.012, Flow Area	a= 0.79 sf	
#2	Device 1	78	.00'	6.0" Vert. Orifice/G	rate C= 0.600	
#3	Device 1	81	.80' 4	4.0" Vert. Orifice/G	rate C= 0.600	
#4	Device 1	82	.83' 9	9.0" W x 5.0" H Ver	t. Orifice/Grate	C= 0.600
#5	Device 1	83	.25' 2	24.0" Horiz. Orifice	/Grate C= 0.600	
#6	Device 2	81	.00' 2	2.410 in/hr Exfiltrat Excluded Surface ar	ion over Surface ea = 464 sf Phase	<b>area above 81.00'</b> e-In= 0.01'

Primary OutFlow Max=0.63 cfs @ 12.41 hrs HW=82.99' TW=77.82' (Dynamic Tailwater) **1=Culvert** (Passes 0.63 cfs of 8.01 cfs potential flow)

**2=Orifice/Grate** (Passes 0.06 cfs of 2.06 cfs potential flow) **6=Exfiltration** (Exfiltration Controls 0.06 cfs)

-3=Orifice/Grate (Orifice Controls 0.42 cfs @ 4.86 fps)

-4=Orifice/Grate (Orifice Controls 0.15 cfs @ 1.27 fps)

-5=Orifice/Grate (Controls 0.00 cfs)

Type III 24-hr 10-Year Rainfall=4.90" Printed 7/1/2021

Pond 13P: GUSF #1



## Summary for Pond 20P: CB #3-1

Inflow Area	=	0.255 ac, 4	0.77% Imper	rvious, Inflow D	epth = 3.4	47" for 10	-Year event
Inflow	=	1.02 cfs @	12.09 hrs, \	/olume=	0.074 af		
Outflow	=	1.01 cfs @	12.09 hrs, \	/olume=	0.074 af,	Atten= 1%	, Lag= 0.1 min
Primary	=	1.01 cfs @	12.09 hrs,  \	/olume=	0.074 af		-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 77.34' @ 12.12 hrs Surf.Area= 13 sf Storage= 12 cf

Plug-Flow detention time= 0.6 min calculated for 0.074 af (100% of inflow) Center-of-Mass det. time= 0.4 min (802.4 - 802.0)

nvert Avail.Sto	orage Storage	Description	
6.38' 1	06 cf Custom	Stage Data (Pris	matic)Listed below (Recalc)
Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
13 13 4 40 131	0 31 9 6 61	0 31 39 45 106	
g Invert	Outlet Devices	3	
<sup>-</sup> y 76.38'	<b>15.0" Round</b> L= 8.0' CPP, Inlet / Outlet Ir n= 0.012, Flor	<b>Culvert</b> square edge head overt= 76.38' / 76.3 w Area= 1.23 sf	dwall, Ke= 0.500 30' S= 0.0100 '/' Cc= 0.900
	<u>vvert Avail.Sto</u> 3.38' 1 Surf.Area (sq-ft) 13 13 4 40 131 13 13 4 70 131 13 13 13 13 4 13 13 13 13 13 13 13 13 13 13	nvert         Avail.Storage         Storage           3.38'         106 cf         Custom           Surf.Area         Inc.Store           (sq-ft)         (cubic-feet)           13         0           13         31           4         9           40         6           131         61           ig         Invert         Outlet Devices           ry         76.38'         15.0" Round           L= 8.0'         CPP,           Inlet / Outlet Ir         n= 0.012, Flor	nvertAvail.StorageStorage Description $3.38'$ 106 cfCustom Stage Data (PrisSurf.AreaInc.StoreCum.Store(sq-ft)(cubic-feet)(cubic-feet)130013313149394064513161106ngInvertOutlet Devicesry76.38' <b>15.0'' Round Culvert</b> L= 8.0'CPP, square edge headInlet / Outlet Invert=76.38' / 76.3'n= 0.012, Flow Area=1.23 sf

Primary OutFlow Max=0.75 cfs @ 12.09 hrs HW=77.30' TW=77.27' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 0.75 cfs @ 1.07 fps)

## 5116-Post-061721

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Pond 20P: CB #3-1



# Summary for Pond 21P: CB #3-2

Inflow -			or viouo,		pui – 2.	J <del>4</del>	101	10-16	ai eve	110	
IIIIIOW –	2.71 cfs @	12.10 hrs,	Volume	=	0.196 af						
Outflow =	2.71 cfs @	12.10 hrs,	Volume	=	0.196 af,	Atte	n= 09	%, La	ag= 0.1	min	
Primary =	2.71 cfs @	12.10 hrs,	Volume	=	0.196 af						
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs											
Peak Elev= 84.66'	@ 12.10 hrs	Surf.Area	= 13 sf	Storage=	13 cf						
Plug-Flow detention time= 0.4 min calculated for 0.196 af (100% of inflow)											
Center-of-Mass de	et. time= 0.2 r	nin ( 831.3	- 831.1 )								
Volume Inve	ert Avail.S	Storage S	torage D	escription							
#1 83.6	65'	48 cf <b>C</b>	ustom S	tage Data	(Prisma	itic)Li	sted	belov	v (Reca	alc)	
Elevation	Surf.Area	Inc.St	ore	Cum.Sto	ore						
(feet)	(sq-ft)	(cubic-fe	eet)	(cubic-fe	<u>et)</u>						
83.65	13		0		0						
86 70	13		40		40						
83.65	13		0	10001010	0						

Device	Routing	Invert	Outlet Devices
#1	Primary	83.65'	<b>12.0" Round Culvert</b> L= 142.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 83.65' / 76.55' S= 0.0500 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

48

Primary OutFlow Max=2.70 cfs @ 12.10 hrs HW=84.66' TW=77.29' (Dynamic Tailwater) -1=Culvert (Inlet Controls 2.70 cfs @ 3.44 fps)

9

4

87.70

Type III 24-hr 10-Year Rainfall=4.90" Printed 7/1/2021

Pond 21P: CB #3-2



## Summary for Pond 22P: CB #3-3

Inflow Area	=	1.217 ac,	6.79% Impervious,	Inflow Depth =	2.28"	for 10-Ye	ear event
Inflow	=	2.39 cfs @	12.22 hrs, Volume	= 0.232	af		
Outflow	=	2.39 cfs @	12.22 hrs, Volume	= 0.232	af, Atte	n= 0%, L	ag= 0.0 min
Primary	=	2.39 cfs @	12.22 hrs, Volume	= 0.232	af		-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 79.89' @ 12.22 hrs Surf.Area= 13 sf Storage= 12 cf

Plug-Flow detention time= 0.4 min calculated for 0.232 af (100% of inflow) Center-of-Mass det. time= 0.2 min (847.9 - 847.7)

Volume	Inve	ert Avail.Sto	rage Storage	ge Storage Description						
#1	79.0	0' 4	48 cf Custon	n Stage Data (Pr	<b>rismatic)</b> Listed below (Recalc)					
Elevation (feet)		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)						
79.00 82.00 83.00		13 13 4	0 39 9	0 39 48						
Device R	Routing	Invert	Outlet Device	es						
#1 P	rimary	79.00'	<b>12.0" Round</b> L= 68.0' CP Inlet / Outlet n= 0.012, Fle	<b>d Culvert</b> P, square edge h Invert= 79.00' / 7 ow Area= 0.79 sf	neadwall, Ke= 0.500 6.55' S= 0.0360 '/' Cc= 0.900					

Primary OutFlow Max=2.38 cfs @ 12.22 hrs HW=79.89' TW=77.13' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 2.38 cfs @ 3.22 fps)

Type III 24-hr 10-Year Rainfall=4.90" Printed 7/1/2021

Pond 22P: CB #3-3



## Summary for Pond 23P: CB #3-4

Inflow Area	=	0.195 ac, 2	25.20% Impe	ervious,	Inflow Dep	oth =	2.81"	for 10-	-Year event	
Inflow	=	0.64 cfs @	12.09 hrs,	Volume	= (	0.046	af			
Outflow	=	0.64 cfs @	12.09 hrs,	Volume	= (	0.046	af, Atte	en= 1%,	Lag= 0.1 mi	n
Primary	=	0.64 cfs @	12.09 hrs,	Volume	= (	0.046	af		-	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 77.52' @ 12.11 hrs Surf.Area= 13 sf Storage= 7 cf

Plug-Flow detention time= 0.5 min calculated for 0.046 af (100% of inflow) Center-of-Mass det. time= 0.5 min (823.2 - 822.7)

Volume	Inv	vert Avail.Sto	rage Storage	ge Storage Description					
#1	77.0	00' 1:	33 cf Custon	n Stage Data (Prismatic)Listed below (Red	alc)				
Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)					
77.0 79.0 80.0 80.9	00 00 00 50	13 13 4 388	0 26 9 98	0 26 35 133					
Device	Routing	Invert	Outlet Device	es					
#1	Primary	77.00'	<b>12.0" Round</b> L= 45.0' CP Inlet / Outlet n= 0.012, Flo	<b>d Culvert</b> P, square edge headwall, Ke= 0.500 Invert= 77.00' / 76.55' S= 0.0100 '/' Cc= ow Area= 0.79 sf	0.900				

**Primary OutFlow** Max=0.61 cfs @ 12.09 hrs HW=77.51' TW=77.28' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 0.61 cfs @ 2.21 fps)

Type III 24-hr 10-Year Rainfall=4.90" Printed 7/1/2021

Pond 23P: CB #3-4



# Summary for Pond 24P: DMH #3

Inflow Are Inflow Outflow Primary	a = = = =	2.593 ac, 11. 5.97 cfs @ 12 5.97 cfs @ 12 5.97 cfs @ 12	47% Imperviou 2.11 hrs, Volu 2.11 hrs, Volu 2.11 hrs, Volu	us, Inflow Depth = me= 0.547 me= 0.547 me= 0.547	2.53" for 10-Year event af af, Atten= 0%, Lag= 0.0 min af				
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 77.30' @ 12.11 hrs Surf.Area= 20 sf Storage= 25 cf									
Plug-Flow Center-of-	detentio Mass de	n time= 0.2 min t. time= 0.2 min	calculated for ( 834.0 - 833.	0.547 af (100% of 8)	inflow)				
Volume	Inve	ert Avail.Sto	rage Storage	e Description					
#1	76.0	5' 10	03 cf Custor	n Stage Data (Pris	matic)Listed below (Recalc)				
Elevation (feet)		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)					
76.05		20 20	0 91	0 91					
81.60		4	12	103					
Device I	Routing	Invert	Outlet Device	es					
#1 I	Primary	76.05'	<b>18.0" Roun</b> L= 177.0' C Inlet / Outlet n= 0.012, Fl	<b>d Culvert</b> PP, square edge h Invert= 76.05' / 72. ow Area= 1.77 sf	eadwall, Ke= 0.500 95' S= 0.0175 '/' Cc= 0.900				
D									

Primary OutFlow Max=5.97 cfs @ 12.11 hrs HW=77.30' TW=73.63' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 5.97 cfs @ 3.80 fps) Pond 24P: DMH #3



## Summary for Pond 25P: CB #2

Inflow Area =	0.101 ac,100.00% Imperv	vious, Inflow Depth =	4.66" for 10-Year event
Inflow =	0.49 cfs @ 12.08 hrs, Vo	olume= 0.039	af
Outflow =	0.48 cfs @12.08 hrs, Vo	olume= 0.039	af, Atten= 0%, Lag= 0.1 min
Primary =	0.48 cfs @ 12.08 hrs, Vo	olume= 0.039	af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 73.94' @ 12.10 hrs Surf.Area= 13 sf Storage= 5 cf

Plug-Flow detention time= 0.8 min calculated for 0.039 af (100% of inflow) Center-of-Mass det. time= 0.6 min (749.0 - 748.4)

Volume	Inv	ert Avail.Sto	rage Storage	e Storage Description						
#1	73.	56'	56 cf Custom	Stage Data (Pri	smatic)Listed below (Recalc)					
Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)						
73.5 77.2 78.2	56 25 25	13 13 4	0 48 9	0 48 56						
Device	Routing	Invert	Outlet Devices	3						
#1	Primary	73.56'	<b>12.0" Round</b> L= 36.0' CPP Inlet / Outlet Ir n= 0.012, Flow	<b>Culvert</b> P, square edge ho overt= 73.56' / 73 w Area= 0.79 sf	eadwall, Ke= 0.500 .20' S= 0.0100 '/' Cc= 0.900					

Primary OutFlow Max=0.47 cfs @ 12.08 hrs HW=73.94' TW=73.62' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 0.47 cfs @ 2.55 fps)

Hydrograph InflowPrimary 0 49 cfs 0.48 cfs Inflow Area=0.101 ac 0.5 Peak Elev=73.94' 0.45 Storage=5 cf 0.4 12.0" 0.35 Flow (cfs) **Round Culvert** 0.3 0.25 n=0.012 L=36.0' 0.2 0.15 S=0.0100 '/' 0.1 0.05 0-2 10 12 14 16 18 20 Ó 4 8 22 24 26 28 30 32 34 36 38 40 42 44 46 48 6 Time (hours)

#### Pond 25P: CB #2

## Summary for Pond 26P: CB #1-1

Inflow Area	ı =	0.431 ac, 8	85.85% Imper	vious, Inflow [	Depth =	4.32" for	10-Year event
Inflow	=	2.01 cfs @	12.08 hrs, V	/olume=	0.155	af	
Outflow	=	1.98 cfs @	12.09 hrs, V	/olume=	0.155 a	af, Atten= <sup>·</sup>	1%, Lag= 0.1 min
Primary	=	1.98 cfs @	12.09 hrs,  V	/olume=	0.155	af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 73.37' @ 12.11 hrs Surf.Area= 13 sf Storage= 16 cf

Plug-Flow detention time= 0.5 min calculated for 0.155 af (100% of inflow) Center-of-Mass det. time= 0.3 min (769.1 - 768.8)

Volume	Inv	ert Avail.Sto	rage Storage	e Storage Description					
#1	72.	13'	66 cf Custom	Stage Data (Prismatic)Listed be	elow (Recalc)				
Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)					
72. <sup>-</sup> 74.0 75.0 76.0	13 65 65 00	13 13 4 136	0 33 9 24	0 33 41 66					
Device	Routing	Invert	Outlet Device	5					
#1	Primary	72.13'	<b>12.0" Round</b> L= 13.0' CPI Inlet / Outlet I n= 0.012, Flo	<b>Culvert</b> P, square edge headwall, Ke= 0.8 hvert= 72.13' / 72.00' S= 0.0100 w Area= 0.79 sf	500 '/' Cc= 0.900				

Primary OutFlow Max=1.80 cfs @ 12.09 hrs HW=73.30' TW=73.08' (Dynamic Tailwater) -1=Culvert (Inlet Controls 1.80 cfs @ 2.29 fps)

Type III 24-hr 10-Year Rainfall=4.90" Printed 7/1/2021

Pond 26P: CB #1-1



## Summary for Pond 27P: DMH #1

Inflow Area	= 3	3.125 ac,24	1.60% In	pervious,	Inflow De	pth = 2.8	5" for	10-Year ev	rent
Inflow	= 8.	.36 cfs @	12.10 hr	s, Volume	)=	0.742 af			
Outflow	= 8	.36 cfs 🥘	12.10 hr	s, Volume	)=	0.742 af, .	Atten= (	0%, Lag= 0	.1 min
Primary	= 8	.36 cfs 🥘	12.10 hr	s, Volume	)= _	0.742 af		ý <b>U</b>	
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 73 12' @ 12 10 hrs_Surf Area= 13 sf_Storage= 22 cf									
Plug-Flow detention time= 0.1 min calculated for 0.741 af (100% of inflow) Center-of-Mass det. time= 0.1 min ( 816.3 - 816.1 )									
Volume	Invert	Avail.St	orage	Storage D	escription				
#1	71.40'		56 cf	Custom S	Stage Data	(Prismati	<b>ic)</b> Listed	d below (Re	calc)
Elevation	Su	rf.Area	Inc.	Store	Cum.Sto	ore			
(feet)		(sq-ft)	(cubic	-feet)	(cubic-fe	et)			
71.40		13		0		0			
75.05		13		47		47			
76.05		4		9		56			
Device Ro	outing	Invert	t Outle	t Devices					
	•								

#1 Primary 71.40' **18.0" Round Culvert** L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 71.40' / 70.90' S= 0.0100 '/' Cc= 0.900 n= 0.012, Flow Area= 1.77 sf

Primary OutFlow Max=8.35 cfs @ 12.10 hrs HW=73.11' TW=58.29' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 8.35 cfs @ 4.73 fps) Pond 27P: DMH #1



## Summary for Pond 29P: GUSF #2

Inflow Ar	ea =	5.652 ac, 21.73% Impervious, Inflow	Depth = 2.79" for 10-Year event
Inflow	=	16.00 cfs @ 12.10 hrs, Volume=	1.314 af
Outflow	=	7.85 cfs @ 12.34 hrs, Volume=	1.270 af, Atten= 51%, Lag= 14.4 min
Primary	=	7.85 cfs @ 12.34 hrs, Volume=	1.270 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Starting Elev= 56.50' Surf.Area= 5,832 sf Storage= 7,395 cf Peak Elev= 58.66' @ 12.34 hrs Surf.Area= 9,986 sf Storage= 24,031 cf (16,636 cf above start) Flood Elev= 60.00' Surf.Area= 13,062 sf Storage= 39,412 cf (32,017 cf above start)

Plug-Flow detention time= 225.4 min calculated for 1.100 af (84% of inflow) Center-of-Mass det. time= 121.5 min (935.6 - 814.1)

Volume	Inver	t Ava	il.Storage	Storage Descript	ion	
#1	53.00	)'	39,412 cf	Custom Stage D	<b>ata (Prismatic)</b> Listed b	elow (Recalc)
Elevatio	on S	Surf.Area	Voids	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
53.0	00	5,682	0.0	0	0	
54.8	50	5,682	40.0	3,409	3,409	
55.0	00	5,682	40.0	1,136	4,546	
56.5	50	5,832	33.0	2,850	7,395	
57.0	00	6,496	100.0	3,082	10,477	
57.2	25	6,886	100.0	1,673	12,150	
57.3	30	6,974	100.0	346	12,497	
57.3	35	7,061	100.0	351	12,847	
57.5	50	7,354	100.0	1,081	13,929	
58.0	00	8,503	100.0	3,964	17,893	
59.0	00	10,737	100.0	9,620	27,513	
60.0	00	13,062	100.0	11,900	39,412	
Device	Routing	In	vert Out	let Devices		
#1	Primary	53	.50' <b>18.</b>	0" Round Culvert		
	-		L= :	25.0' CPP, square	edge headwall, Ke= 0.	.500
			Inle	t / Outlet Invert= 53	8.50 <sup>°</sup> / 53.25' S= 0.0100	) '/' Cc= 0.900
			n= (	0.012, Flow Area=	1.77 sf	
#2	Device 1	53	5.50' <b>6.0</b> '	" Vert. Orifice/Grat	te C= 0.600	
#3	Device 1	57	'.30' <b>33.</b> (	0" W x 5.0" H Vert	Orifice/Grate C= 0.60	00
#4	Device 1	58	3.35' <b>36.</b> 0	0" W x 6.0" H Vert	Orifice/Grate C= 0.60	00
#5	Device 1	58	6.85' <b>48.</b> 0 Lim	0" x 48.0" Horiz. O ited to weir flow at	rifice/Grate C= 0.600	
#6	Device 2	56	5.50' <b>2.4</b> '	10 in/hr Exfiltratio	n over Surface area ab	ove 56.50'
			Exc	luded Surface area	ı = 5,832 sf Phase-In= (	0.01'
#7	Primary	59	0.00' <b>4.0'</b> Hea 2.50 Coe	long         x 6.0'         bread           ad (feet)         0.20         0.40           0         3.00         3.50         4.00           ef. (English)         2.37         2           5         2.66         2.66         2.67	th Broad-Crested Rect 0.60 0.80 1.00 1.20 4.50 5.00 5.50 2.51 2.70 2.68 2.68 2. 2 69 2.72 2.76 2.83	t <b>angular Weir</b> 1.40 1.60 1.80 2.00 67 2.65 2.65 2.65
			2.00	2.00 2.00 2.01		

Primary OutFlow Max=7.85 cfs @ 12.34 hrs HW=58.66' TW=0.00' (Dynamic Tailwater)

-**1=Culvert** (Passes 7.85 cfs of 17.88 cfs potential flow)

**2=Orifice/Grate** (Passes 0.23 cfs of 2.10 cfs potential flow)

**6=Exfiltration** (Exfiltration Controls 0.23 cfs)

-3=Orifice/Grate (Orifice Controls 5.92 cfs @ 5.17 fps)

-4=Orifice/Grate (Orifice Controls 1.69 cfs @ 1.80 fps)

-7=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

## Pond 29P: GUSF #2



# Summary for Link 100L: POA #1

Inflow A	Area	=	1.932 ac,	13.66% Impe	ervious,	Inflow Depth =	2.7	73" for 10-	Year event
Inflow		=	4.59 cfs @	12.11 hrs,	Volume	= 0.439	) af		
Primar	у	=	4.59 cfs @	12.11 hrs,	Volume	= 0.439	) af,	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs



# Link 100L: POA #1

# Summary for Link 200L: POA #2

Inflow /	Area =	=	14.044 ac, 1	11.39% Impe	ervious,	Inflow Depth >	2.5	50" for 10-	Year event
Inflow	=		19.31 cfs @	12.39 hrs,	Volume	= 2.926	3 af		
Primar	y =		19.31 cfs @	12.39 hrs,	Volume	= 2.926	6 af,	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs



## Link 200L: POA #2



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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: North Road Entrance,	Runoff Area=51,236 sf 8.13% Impervious Runoff Depth=3.65" Flow Length=432' Tc=6.3 min CN=77 Runoff=4.99 cfs 0.358 af
Subcatchment 2S: Remaining Land East Flor	Runoff Area=279,061 sf 0.00% Impervious Runoff Depth=3.26" w Length=1,208' Tc=32.9 min CN=73 Runoff=13.25 cfs 1.738 af
Subcatchment 10S: South Road Entrance	e to Runoff Area=3,377 sf 82.44% Impervious Runoff Depth=5.61" Flow Length=139' Tc=6.0 min CN=95 Runoff=0.46 cfs 0.036 af
Subcatchment 11S: South Route 1 Fronta	age Runoff Area=6,211 sf 0.00% Impervious Runoff Depth=3.96" Flow Length=166' Tc=6.0 min CN=80 Runoff=0.66 cfs 0.047 af
Subcatchment12S: Roadside to CB #4	Runoff Area=9,746 sf 23.27% Impervious Runoff Depth=4.07" Flow Length=282' Tc=9.6 min CN=81 Runoff=0.94 cfs 0.076 af
Subcatchment 13S: Roadside to GUSF #1	Runoff Area=13,602 sf 16.81% Impervious Runoff Depth=4.07" Flow Length=264' Tc=6.0 min CN=81 Runoff=1.48 cfs 0.106 af
Subcatchment 20S: Roadside to CB #3-1	Runoff Area=11,105 sf 40.77% Impervious Runoff Depth=4.71" Flow Length=390' Tc=6.0 min CN=87 Runoff=1.36 cfs 0.100 af
Subcatchment 21S: Woodland and	Runoff Area=40,322 sf 6.67% Impervious Runoff Depth=3.65" Flow Length=338' Tc=6.5 min CN=77 Runoff=3.89 cfs 0.282 af
Subcatchment 22S: Woodland and	Runoff Area=53,034 sf 6.79% Impervious Runoff Depth=3.35" Flow Length=408' Tc=16.0 min CN=74 Runoff=3.53 cfs 0.340 af
Subcatchment 23S: Roadside To CB #3-4	Runoff Area=8,495 sf 25.20% Impervious Runoff Depth=3.96" Flow Length=150' Tc=6.0 min CN=80 Runoff=0.90 cfs 0.064 af
Subcatchment 25S: Loading Area to CB #	<b>#2</b> Runoff Area=4,411 sf 100.00% Impervious Runoff Depth=5.96" Flow Length=137' Tc=6.0 min CN=98 Runoff=0.62 cfs 0.050 af
Subcatchment 26S: Parking Lot to CB #1-	-1 Runoff Area=18,776 sf 85.85% Impervious Runoff Depth=5.61" Flow Length=332' Tc=6.0 min CN=95 Runoff=2.57 cfs 0.202 af
Subcatchment 27S: Proposed Roof	Runoff Area=20,000 sf 100.00% Impervious Runoff Depth=5.96" Tc=6.0 min CN=98 Runoff=2.79 cfs 0.228 af
Subcatchment 29S: Open Space to GUSF	<b>#2</b> Runoff Area=90,054 sf 0.00% Impervious Runoff Depth=3.35" Flow Length=457' Tc=6.0 min CN=74 Runoff=8.13 cfs 0.578 af
Subcatchment 30S: Remaining Land	Runoff Area=86,511 sf 18.73% Impervious Runoff Depth=4.07" Flow Length=760' Tc=12.0 min CN=81 Runoff=7.73 cfs 0.673 af
Reach 1R: 12" Steel Pipe 7 12.0" Round Pipe n=0.012 L	Avg. Flow Depth=0.82' Max Vel=9.56 fps Inflow=6.59 cfs 0.623 af _=45.0' S=0.0291 '/' Capacity=6.59 cfs Outflow=6.61 cfs 0.623 af

## 5116-Post-061721

Type III 24-hr 25-Year Rainfall=6.20" Printed 7/1/2021

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Reach 10R: Roadside Swale	Avg. Flow Depth=0.56' Max Vel=2.61 fps Inflow=5.74 cfs n=0.030 L=98.0' S=0.0104 '/' Capacity=17.99 cfs Outflow=5.39 cfs	0.394 af 0.394 af
Reach 13R: Swale	Avg. Flow Depth=0.18' Max Vel=2.80 fps Inflow=1.19 cfs n=0.030 L=41.0' S=0.0395 '/' Capacity=28.58 cfs Outflow=1.19 cfs	0.181 af 0.181 af
Reach 25R: 18" CPP 18.0" Round Pipe	Avg. Flow Depth=0.85' Max Vel=8.93 fps Inflow=9.17 cfs n=0.012 L=83.0' S=0.0175 '/' Capacity=15.04 cfs Outflow=9.16 cfs	0.837 af 0.837 af
Reach 27R: 12" Roof Leader 12.0" Round Pipe	Avg. Flow Depth=0.63' Max Vel=5.34 fps Inflow=2.79 cfs n=0.012 L=300.0' S=0.0100 '/' Capacity=3.86 cfs Outflow=2.76 cfs	0.228 af 0.228 af
Reach 28R: Riprap Swale	Avg. Flow Depth=0.31' Max Vel=3.46 fps Inflow=2.76 cfs n=0.069 L=108.0' S=0.1759 '/' Capacity=26.22 cfs Outflow=2.75 cfs	0.228 af 0.228 af
Pond 1P: CB #5-2	Peak Elev=82.27' Storage=110 cf Inflow=4.99 cfs 12.0" Round Culvert n=0.012 L=52.0' S=0.0050 '/' Outflow=5.69 cfs	0.358 af 0.358 af
Pond 10P: CB #5-1	Peak Elev=80.00' Storage=65 cf Inflow=6.15 cfs 12.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=5.74 cfs	0.394 af 0.394 af
Pond 12P: CB #4	Peak Elev=86.23' Storage=51 cf Inflow=0.94 cfs 12.0" Round Culvert n=0.120 L=50.0' S=0.0050 '/' Outflow=0.97 cfs	0.076 af 0.076 af
Pond 13P: GUSF #1	Peak Elev=83.25' Storage=2,968 cf Inflow=2.34 cfs Outflow=1.19 cfs	0.182 af 0.181 af
Pond 20P: CB #3-1	Peak Elev=77.86' Storage=19 cf Inflow=1.36 cfs 15.0" Round Culvert n=0.012 L=8.0' S=0.0100 '/' Outflow=1.34 cfs	0.100 af 0.100 af
Pond 21P: CB #3-2	Peak Elev=85.21' Storage=20 cf Inflow=3.89 cfs 12.0" Round Culvert n=0.012 L=142.0' S=0.0500 '/' Outflow=3.89 cfs	0.282 af 0.282 af
Pond 22P: CB #3-3	Peak Elev=80.37' Storage=18 cf Inflow=3.53 cfs 12.0" Round Culvert n=0.012 L=68.0' S=0.0360 '/' Outflow=3.53 cfs	0.340 af 0.340 af
Pond 23P: CB #3-4	Peak Elev=77.90' Storage=12 cf Inflow=0.90 cfs 12.0" Round Culvert n=0.012 L=45.0' S=0.0100 '/' Outflow=0.88 cfs	0.064 af 0.064 af
Pond 24P: DMH #3	Peak Elev=77.82' Storage=35 cf Inflow=8.58 cfs 18.0" Round Culvert n=0.012 L=177.0' S=0.0175 '/' Outflow=8.58 cfs	0.787 af 0.787 af
Pond 25P: CB #2	Peak Elev=74.04' Storage=6 cf Inflow=0.62 cfs 12.0" Round Culvert n=0.012 L=36.0' S=0.0100 '/' Outflow=0.61 cfs	0.050 af 0.050 af
Pond 26P: CB #1-1	Peak Elev=74.43' Storage=30 cf Inflow=2.57 cfs 12.0" Round Culvert n=0.012 L=13.0' S=0.0100 '/' Outflow=2.53 cfs	0.202 af 0.202 af
Pond 27P: DMH #1	Peak Elev=74.01' Storage=34 cf Inflow=11.62 cfs 18.0" Round Culvert n=0.012 L=50.0' S=0.0100 '/' Outflow=11.62 cfs	1.038 af 1.038 af
Pond 29P: GUSF #2	Peak Elev=58.98' Storage=27,340 cf Inflow=22.42 cfs Outflow=13.92 cfs	1.844 af 1.801 af

Link 100L: POA #1

Inflow=6.61 cfs 0.623 af Primary=6.61 cfs 0.623 af

Link 200L: POA #2

Inflow=29.79 cfs 4.212 af Primary=29.79 cfs 4.212 af

Total Runoff Area = 15.977 ac Runoff Volume = 4.878 af Average Runoff Depth = 3.66" 88.33% Pervious = 14.113 ac 11.67% Impervious = 1.864 ac

# Section 5

Precipitation Table


#### APPENDIX H. 24-hour duration rainfalls for various return periods

COUNTY	Storm Type	1-YR	2- YR	5- YR	10- YR	25- YR	50- YR	100- YR	500- YR
ANDROSCOGGIN	III	2.5	3.0	3.7	4.3	5.4	6.4	7.6	11.1
AROOSTOOK C	П	1.9	2.3	2.8	3.2	3.9	4.6	5.3	7.6
(Presque Isle Area)					•	• • •			
(Fort Kent Area)	II	1.9	2.2	2.7	3.1	3.7	4.3	5.0	7.0
AROOSTOOK S				•					
(Houlton Area)	11	2.1	2.5	3.0	3.4	4.1	4.7	5.4	7.5
CUMBERLAND									
NW	III	2.5	3.0	3.7	4.3	5.4	6.3	7.5	10.9
(Bridgton Area)									
CUMBERLAND SF	ш	26	3.1	3.0	16	5 8	6.0	<b>Q</b> 1	12.1
(N Windham Area)	111	2.0	5.1	5.9	4.0	5.8	0.9	0.1	12.1
FRANKLIN	II	2.0	2.4	2.9	3.4	4.2	4.9	5.7	8.2
HANCOCK	III	2.5	2.9	3.6	4.2	5.2	6.1	7.2	10.5
KENNEBEC	III	2.4	2.8	3.5	4.2	5.2	6.1	7.2	10.6
KNOX	III	2.6	3.2	3.9	4.6	5.7	6.7	7.9	11.5
LINCOLN	III	2.5	3.1	3.8	4.5	5.5	6.5	7.6	11.1
OXFORD E	$\mathrm{II}^{1}$	2.3	2.7	3.3	3.9	4.8	5.7	6.7	9.7
(Rumford Area)									
(Gilead Area)	II	2.2	2.7	3.4	4.0	4.9	5.8	6.9	10.1
PENOBSCOT N					• •				
(Millinocket Area)	II	2.2	2.6	3.2	3.8	4.7	5.6	6.5	9.5
PENOBSCOT S	п	2.2	27	2.4	2.0	4.0	57	67	0.7
(Hudson Area)	11	2.3	2.1	5.4	5.9	4.9	5.7	0.7	9.7
PISCATAQUIS N	Π	2.0	2.4	2.9	3.4	4.2	5.0	5.8	8.5
(Chesuncook Area)					••••				
(Monson Area)	II	2.2	2.7	3.3	3.9	4.8	5.7	6.8	10.0
SAGADAHOC	Ш	26	32	39	46	57	67	78	114
SOMERSET N		2.0	0.2	0.0	1.0	5.7	0.7	7.0	
(Pittston Farm Area)	11	2.0	2.3	2.8	3.3	4.0	4.7	5.4	7.8
SOMERSET S	П	23	27	3.4	3.0	49	57	67	9.8
(Solon Area)		2.5	2.1	5.7	5.7	т.)	5.1	0.7	2.0
WALDO	III	2.4	2.9	3.6	4.2	5.2	6.1	7.2	10.5
WASHINGTON		2.5	2.8	3.4	3.9	4.8	5.5	6.4	9.0
YUKK	111	2.6	5.5	4.1	4.9	6.2	1.5	8./	13.2

1 Use Type III rainfall for the towns of Brownfield, Buckfield, Denmark, Hartford, Hebron, Hiram, Oxford, and Porter.

Source: Data extracted by the Maine Department of Environmental Protection from the Northeast Regional Climate Center website (http://precip.eas.cornell.edu), Extreme Precipitation Tables. Data from this website was obtained from the National Oceanic and Atmospheric Administration's Regional Climate Center Program. June 2014

# Section 6

# Class A High Intensity Soil Survey Test Pit Logs



Michael Cuomo, Soil Scientist 6 York Pond Road, York, Maine 03909 207 363 4532 mcuomosoil@gmail.com

### Class A

### High Intensity Soil Survey Report

Tax map 67, Lot 1

US Route One

Kittery, Maine

prepared for:

Altus Engineering 133 Court Street Portsmouth, NH 03801



17 May 2021

This report is in reference to this +/32 acre property at 514 US Route One in Kittery, Maine. In May of 2021 a class 'A' High Intensity Soil Survey of this property was completed in compliance with the standards created by the Maine Association of Professional Soil Scientists. The purpose of this soil investigation is to assist in planning a commercial development served by municipal water and sewer service. This report will explain the methods, limitations, and results of this work.

A high intensity soil survey is comprised of two components: a soil map and this report. The soil map is made by traversing the property and observing the soil at locations thought to be representative of the landform. Because soil is highly variable, it is not possible to represent every soil variation on the map. The map is a simplified two-dimensional interpretation of the complex three dimensional soil-landscape relationship. Class A standards allow for inclusions of soils other than those named in the map unit label, so long as no inclusion limiting for the proposed land use is greater than one-eighth acre in size. Boundaries between different soils are shown as lines on the soil map, but may be diffuse transition zones.

Soil names were selected using best fit with soils already researched in detail and found to occur extensively in Maine by the United States Department of Agriculture's Natural Resource Conservation Service. The map unit design and the interpretations of soil properties in this report are specific to this site and were selected considering the proposed use. Therefore, the interpretations and limitations described in this report may be insufficient for other uses. For example, soil suitability for on-site wastewater disposal was ignored in map unit design.

This soil map is based on 22 test pits dug with an excavator and two hand dug soil observations. The data for these is attached at the rear of this report, and their locations are shown on the base map. Other shallow soil observations were previously made to determine the edge of the wetland soils, but the data and locations of these were not recorded.

Hydrologic soil groups were assigned using the "HSG Triangle" developed by the University of Rhode Island.

The soil map is presented on a base plan: a two foot contour interval topographic and boundary survey with wetland flag locations prepared by Altus Engineering.

Eight different soils were mapped on the property and are described below.

#### Brayton (BrB)

Drainage class: poorly drained. Parent material: basal till or loose till. Texture range: stony fine sandy loam. Description: see soil observation B. Landscape position: lowland. Landform: ground moraine. Slope range: 0 to 8%. Permeability: moderate in the upper layers and slow in the lower layers. Bedrock class: moderately deep to deep. Hydrologic soil group: D. Saturated hydraulic conductivity: 0.0 to 0.6 in/hr in the most restrictive horizons. Flood hazard: water ponds at the surface seasonally. Inclusions: on this site Brayton map units represents poorly drained basal till soils which have variable bedrock depth. Use and management: Land uses are limited by wetness close to the surface for prolonged periods of time during an average year. These are wetland soils and may not be drained or filled without permits.

#### <u>Dixfield (DxB)</u>

Drainage class: moderately well drained.

Parent material: basal till.

Texture range: stony fine sandy loam.

Description: see test pit one.

Landscape position: upland.

Landform: gently rolling.

Slope range: 0 to 8%.

Permeability: moderate in the upper layers and slow in the lower layers.

Bedrock class: very deep.

Hydrologic group: D.

Flood hazard: none.

Inclusions: test pit 5 has some horizons which are more sandy; Test pit 21 is an inclusion of the similar Marlow soil.

Use and management: land uses are slightly limited by the presence of basal till, which causes the ground water to perch after rain events and snow melt. This limitation can be overcome by appropriate grading and drainage.

#### <u>Lyman-Tunbridge (LT)</u>

Drainage class: somewhat excessively well and well drained. Parent material: loose glacial till. Texture range: stony fine sandy loam. Description: Lyman is described in test pit 3 and Tunbridge in test pit 9. Landscape position: upland. Landform: gently rolling to steep. Slope range: 0 to greater than 25%. Permeability: moderately rapid. Bedrock class: shallow and moderately deep. Hydrologic soil group: the predominant HSG is C. Saturated hydraulic conductivity: 0.1 to 14 in/hr in the most restrictive horizon.

Flood hazard: none.

- Inclusions: This soil map unit represents upland soils with variable bedrock depth. Inclusions are the very shallow Abram soils in test pit 8; test pit 6, which has basal till over moderately deep bedrock; and few bedrock outcroppings at the surface.
- Use and management: land uses are limited by bedrock 0 to 40 inches from the soil surface, which can be overcome by blasting and filling.

#### <u>Nicholville (NiB)</u>

Drainage class: somewhat poorly and moderately well drained. Parent material: lacustrine and shallow marine sediments. Texture range: very fine sandy loam in the upper part over silt

loam in the lower part.

Description: test pits 12 and 14.

Landscape position: lowland.

Landform: gently rolling to nearly level plains.

Slope range: 0 to 8%.

Permeability: moderate in the upper part and slow in the lower part.

-

Bedrock class: very deep.

Hydrologic group: D.

Flood hazard: none.

- Inclusions: Nicholville is typically a moderately well drained soil, but on this site the name includes the extensive somewhat poorly drained variant.
- Use and management: Land uses are limited by seasonal wetness close to the surface. These are not wetland soils and may be drained or filled to overcome this limitation. The Nicholville soils are highly erosive and have low bearing strength when wet.

Scantic (ScB) Drainage class: poorly drained. Parent material: marine. Texture range: silt loam over silty clay loam. Description: see test pit 16. Landscape position: wetland. Landform: glacial deltas, bays. Slope range: 0 to 8%. Permeability: slow in the upper layers and very slow in the lower layers. Bedrock class: very deep. Hydrologic group: D. Flood hazard: water ponds at the surface seasonally. Inclusions: none noted. Use and management: Land uses are limited by frequent saturation to the surface and fine texture of the soil which makes it difficult to work in when wet. These are wetlands soils and may be not be drained or filled without permits. Waumbek (WmB) Drainage class: moderately well drained. Parent material: loose glacial till. Texture range: stony fine sandy loam over gravelly sand. Description: see test pit 20. Landscape position: upland. Landform: sideslopes. Slope range: 0 to 8%. Permeability: moderately rapid in the upper layers and rapid in the lower layers. Bedrock class: very deep. Hydrologic group: D. Flood hazard: none. Inclusions: none noted. Use and management: land uses are slightly limited by the presence of brief duration ground water within 2 feet of the surface. This limitation can be overcome by appropriate grading and drainage. Westbury (WsB) Drainage class: somewhat poorly drained. Parent material: basal till and loose till. Texture range: fine sandy loam to loamy sand. Description: see test pit 4. Landscape position: lowland. Landform: nearly level. Slope range: 0 to 8%. Permeability: moderate in the upper layers and slow to rapid in

the lower layers.

Hydrologic group: D.

Bedrock class: moderately deep to deep.

Flood hazard: water will pond at the surface briefly after significant rainstorms or snow melt. Inclusions: Though typically deep to bedrock, on this site the Westbury soils have significant area which is moderately deep to bedrock. Use and management: land uses are limited by seasonal wetness close to the surface. These are not wetland soils and may drained or filled to overcome this limitation. be Whately (WhB) Drainage class: very poorly drained. Parent material: glacial lacustrine or aeolian. Texture range: very fine sandy loam to sand. Description: see soil observation A. Landscape position: wetland. Landform: deltas, bays. Slope range: 0 to 8%. Permeability: moderately rapid in the upper layers and very slow in the lower layers. Bedrock class: very deep. Hydrologic soil group: D. Saturated hydraulic conductivity: 0.6 to 20 in/hr. Flood hazard: water ponds at the surface frequently. Inclusions: none noted. Use and management: Land uses are limited by near constant saturation to the surface and low bearing strength. These are regulated wetlands and may be not be drained or filled without permits. Conclusion The soils on this site are similar to those encountered elsewhere in York County. The limitations that the non-wetland soils present can be overcome by: 1) identifying the soils and their limitations, as has been done in this report; 2) engineering and designing measures such as construction sequencing, material specifications, drainage structures, grading, blasting, and erosion/sediment control in response to the limitations identified; and

3) implementing the designed measures properly.

The Brayton, Scantic, and Whately soils are regulated wetlands. No filling is allowed without permits. Proper erosion and sediment techniques must be employed to protect the wetlands during construction. THIS LEGEND MUST APPEAR ON THE PLAN WHICH CONTAINS THE SOIL MAP.

High Intensity Soil Map Legend

BrB Brayton, 0-8% slopes\* DxB Dixfield, 0-8% slopes LTB Lyman Tunbridge complex, 0-8% slopes LTC Lyman Tunbridge complex, 8-15% slopes LTD Lyman Tunbridge complex, 15-25% slopes LTE Lyman Tunbridge complex, +25% slopes NiB Nicholville, 0-8% slopes ScB Scantic, 0-8% slopes WmB Waumbek, 0-8% slopes WhB Whately, 0-8% slopes WsB Westbury, 0-8% slopes

\* These are wetland soils.

This soil survey complies with Class A standards as defined by the Maine Association of Professional Soil Scientists. See report dated 17 May 2021, for complete description of methods, soils, and results.

Michael Cuomo Maine Soil Scientist #211

#### Michael Cuomo, Soil Scientist

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#### TEST PIT DATA

Client: Altus Engineering

Location: 514 US Route One, Kittery Date: 10 May 2021 Test Pit Number: 1 Description Depth 2" Leaf litter. Dark brown (10YR 3/3) fine sandy loam, granular, friable. 0-9" Dark yellowish brown (10YR 4/6) fine sandy loam, blocky, 9-24" friable. Light olive brown (2.5Y 5/4) fine sandy loam, blocky, friable, 24-35" redox. Dark olive brown (2.5Y 3/3) stony fine sandy loam, massive, 35-48" firm, redox. Dixfield Soil Name: 24" Depth to Seasonal High Water Table: Depth to Bedrock: 48" Test Pit Number: 2 Description Depth 1" Leaf litter. Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 0-8" Dark yellowish brown (10YR 4/6) stony fine sandy loam, blocky, 8-20" friable. Soil Name: Tunbridge Depth to Seasonal High Water Table: none Depth to Bedrock: 20" Test Pit Number: 3 Description Depth 2" Leaf litter. Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 0-8" Dark yellowish brown (10YR 4/6) stony fine sandy loam, blocky, 8-18" friable. Lyman Soil Name: Depth to Seasonal High Water Table: none Depth to Bedrock: 18" Test Pit Number: 4 Description Depth 2" Leaf litter. 0-8" Dark grayish brown (2.5Y 4/2) fine sandy loam, granular, friable. Dark yellowish brown (10YR 4/6) fine sandy loam, blocky, 8-16" friable, redox. Light yellowish brown (2.5¥ 6/4) fine sandy loam, blocky, firm, 16-24" redox. Westbury variant Soil Name: 8" Depth to Seasonal High Water Table: 24" Depth to Bedrock:

Test Pit Number: 5 Description Depth 1" Leaf litter. Yellowish brown (10YR 5/4) fine sandy loam, blocky, friable. 0-22" Dark yellowish brown (10YR 4/6) gravelly loamy sand, blocky, 22-32" friable, redox. Dark olive brown (2.5Y 3/3) gravelly sand, loose, massive, 32-44" redox. Light olive brown (2.5Y 5/4)stony fine sandy loam, massive, 44-56" firm, redox. Dixfield Soil Name: Depth to Seasonal High Water Table: 22" 56" Depth to Bedrock: Test Pit Number: 6 Depth Description 1" Leaf litter. Dark brown (10YR 3/3) fine sandy loam, granular, friable. 0 - 10''10-24" Dark yellowish brown (10YR 4/6) fine sandy loam, blocky, friable. Light yellowish brown (2.5Y 6/4) stony fine sandy loam, massive, 24-38" firm, redox. Tunbridge variant Soil Name: 24" Depth to Seasonal High Water Table: Depth to Bedrock: 38" Test Pit Number: 7 Depth Description 1" Leaf litter. 0-7" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. Yellowish brown (10YR 5/6) stony fine sandy loam, blocky, 7-18" friable. Lyman Soil Name: Depth to Seasonal High Water Table: none Depth to Bedrock: 18" Test Pit Number: 8 Depth Description 2" Leaf litter. Very dark gray (10YR 3/1) stony fine sandy loam, granular, 0-3" friable. Soil Name: Abram Depth to Seasonal High Water Table: none 3" Depth to Bedrock: -Test Pit Number: 9 Description Depth 2" Leaf litter. Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 0-6" Yellowish brown (10YR 5/6) stony fine sandy loam, blocky, 6-27" friable. Tunbridge Soil Name: Depth to Seasonal High Water Table: none 27" Depth to Bedrock:

Test Pit Number: 10 Description Depth 2" Leaf litter. 0-6" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. Soil Name: Abram Depth to Seasonal High Water Table: none Depth to Bedrock: 6" Test Pit Number: 11 Description Depth 2" Leaf litter. 0-7" Dark brown (10YR 3/3) silt loam, granular, friable. 7-10" Light yellowish brown (2.5Y 6/4) silt loam, blocky, friable, redox. Pale olive (5Y 6/3) silt loam, massive, friable, redox. 10-28" 29-44" Light yellowish brown (2.5Y 6/4) fine sandy loam, massive, firm, redox. 44-96" Olive brown (2.5Y 4/4) sand, massive, loose, with strata of firm silt, redox. Soil Name: Westbury variant Depth to Seasonal High Water Table: 7" Depth to Bedrock: none Test Pit Number: 12 Depth Description 1" Leaf litter. 0 - 7''Dark brown (10YR 3/3) silt loam, granular, friable. 7-11" Yellowish brown (10YR 5/6) silt loam, blocky, friable. 11-28" Light yellowish brown (2.5Y 6/4) silt loam, blocky, friable, redox. 28-64" Olive brown (2.5Y 4/4) sand, massive, loose, redox. 64-96" Olive brown (2.5Y 4/4) silt loam, massive, firm, redox. Soil Name: Nicholville variant Depth to Seasonal High Water Table: 11" Depth to Bedrock: none Test Pit Number: 13 Depth Description 1" Leaf litter. 0-10" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 10-24" Strong brown (7.5YR 4/6) stony fine sandy loam, blocky, friable. Light yellowish brown (2.5Y 6/4) stony fine sandy loam, blocky, 24-32" firm, redox. Soil Name: Tunbridge variant Depth to Seasonal High Water Table: 24" Depth to Bedrock: 32" Test Pit Number: 14 Depth Description 2″ Leaf litter. 0-6" Brown (10YR 4/3) fine sandy loam, granular, friable. 6-17" Yellowish brown (10YR 5/6) fine sandy loam, blocky, friable, redox. Olive brown (2.5Y 4/4) sand, massive, loose, redox. 17-24" 24-52" Light olive brown (2.5Y 5/4) stratified fine sand and silt, massive, firm, redox. Soil Name: Nicholville

Depth to Seasonal High Water Table: 17" Depth to Bedrock: none Test Pit Number: 15 Description Depth 1″ Leaf litter. 0-6" Brown (10YR 4/3) stony fine sandy loam, granular, friable. Dark yellowish brown (10YR 5/6) stony fine sandy loam, blocky, 6-12" friable. 12-18" Light yellowish brown (2.5Y 6/4) stony fine sandy loam, blocky, friable. Soil Name: Lyman Depth to Seasonal High Water Table: none Depth to Bedrock: 18" Test Pit Number: 16 Depth Description 1" Leaf litter. 0-7" Very dark gray (2.5Y 3/1) silt loam, granular, friable, redox. 7-13" Light gray (2.5Y 7/1) silt loam, blocky, friable, redox. 13-22" Olive brown (2.5Y 4/4) silt loam, blocky, firm, redox. 22-50" Olive (5Y 5/4) silty clay loam, massive, firm, redox. Soil Name: Scantic Depth to Seasonal High Water Table: surface Depth to Bedrock: none Test Pit Number: 17 Depth Description 2" Leaf litter. 0-5" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 5-12" Strong brown (7.5YR 4/6) stony fine sandy loam, blocky, friable. Soil Name: Lyman Depth to Seasonal High Water Table: none Depth to Bedrock: 12" Test Pit Number: 18 Depth Description 1" Leaf litter. 0-5 Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 5-17" Yellowish brown (10YR 5/4) fine sandy loam, blocky, friable. Light olive brown (2.5Y 5/4) stony fine sandy loam, blocky, 17-24" friable, redox. 24-54" Light yellowish brown (2.5Y 6/4) sand, massive, loose, redox. Soil Name: Waumbek Depth to Seasonal High Water Table: 17" Depth to Bedrock: none Test Pit Number: 19 Depth Description 0" Leaf litter. 0-8" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 8-28" Dark yellowish brown (10YR 4/4) stony fine sandy loam, blocky, friable. Soil Name: Tunbridge Depth to Seasonal High Water Table: none Depth to Bedrock: 28"

Test Pit Number: 20 Depth Description 0 " Leaf litter. 0 - 10Dark brown (10YR 3/3) fine sandy loam, granular, friable. 10-28" Dark yellowish brown (10YR 4/4) fine sandy loam, blocky, friable. 28-46" Light yellowish brown (2.5Y 6/4) gravelly loamy sand, massive, friable, redox. Waumbek Soil Name: Depth to Seasonal High Water Table: 28" Depth to Bedrock: 46" Test Pit Number: 21 Depth Description 0" Leaf litter. 0-10" Very dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 10-28" Dark yellowish brown (10YR 4/6) stony fine sandy loam, blocky, friable. 28-66" Light olive brown (2.5Y 5/4) stony fine sandy loam, massive, firm, redox. Soil Name: Marlow Depth to Seasonal High Water Table: 28" 66" Depth to Bedrock: Test Pit Number: 22 Depth Description 0" Leaf litter. 0-6" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 6-12" Yellowish brown (10YR 5/6) stony fine sandy loam, blocky, friable. Soil Name: Lyman Depth to Seasonal High Water Table: none Depth to Bedrock: 12"

Soil Observation: A Depth Description 3" Leaf litter. 0-10" Black (10YR2/1) mucky peat, massive, friable, redox. 10-20" Gray (2.5Y 5/1) loamy fine sand, massive, friable, redox. Olive gray (5Y 5/2) very fine sandy loam, massive, friable, 20-28" redox. Gray (2.5Y 5/1) fine sand, massive, friable, redox. 28-36" 36-42" Olive brown (2.5Y 4/4) very fine sandy loam, massive, firm, redox. Soil Name: Whately Depth to Seasonal High Water Table: surface Depth to Bedrock: none Soil Observation: B Description Depth 4" Leaf litter. 0-8" Very dark gray (2.5Y 3/1) stony fine sandy loam, massive, friable, redox. Dark gray (2.5Y 4/1) stony fine sandy loam, massive, friable, 8-14" redox. Light yellowish brown (2.5Y 6/3) stony fine sandy loam, massive, 14-28" friable, redox. Soil Name: Brayton variant Depth to Seasonal High Water Table: surface Depth to Bedrock: 28"

# Section 7

# NRCS Soils Report





United States Department of Agriculture

Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

## Custom Soil Resource Report for York County, Maine



## Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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## Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



Γ

MAP INFORMATION	The soil surveys that comprise your AOI were mapped at 1:20,000.	Warning: Soil Map may not be valid at this scale.	Enlargement of maps beyond the scale of mapping can cause	misunderstanding of the detail of mapping and accuracy of soil line placement The maps do not show the small areas of	contrasting soils that could have been shown at a more detailed	scale.		Please rely on the bar scale on each map sheet for map measurements.	· · · · · · · · · · · · · · · · · · ·	Source of Map: Natural Resources Conservation Service Web Soil Survev URL:	Coordinate System: Web Mercator (EPSG:3857)	Maps from the Web Soil Survey are based on the Web Mercator	projection, which preserves direction and shape but distorts	ubidance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more	accurate calculations of distance or area are required.	This product is generated from the USDA-NRCS certified data as	of the version date(s) listed below.	Soil Survey Area: York County, Maine	Survey Area Data: Version 19, May 29, 2020	Soil map units are labeled (as space allows) for map scales	1:50,000 or larger.	Date(s) aerial images were photographed: Dec 31, 2009—Sep	9, 2017	The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.
MAP LEGEND	Area of Interest (AOI) Soli Area Area of Interest (AOI) Area of Interest (AOI)	Solis Soli Map Unit Polygons 💮 Wery Stony Spot	Soil Map Unit Lines	Soil Map Unit Points	Special Point Features	Blowout water reatives Streams and Canals	Borrow Pit	Clay Spot	<ul> <li>Closed Depression</li> <li>Interstate Highways</li> </ul>	Gravel Pit US Routes	** Gravelly Spot	🕸 Landfill Local Roads	🙏 Lava Flow Background	👞 Marsh or swamp 🜉 Aerial Photography	🙊 Mine or Quarry	Miscellaneous Water	Perennial Water	Rock Outcrop		Sandy Spot	Severely Eroded Spot	Sinkhole Sinkhole	Slide or Slip	Ø Sodic Spot

### **Map Unit Legend**

Man Unit Symbol	Man Unit Name	Acres in AOI	Percent of AOI				
Bm	Biddeford mucky peat, 0 to 3 percent slopes	11.1	8.2%				
BrB	Brayton and Westbury fine sandy loams, 0 to 8 percent slopes	3.6	2.7%				
BuB	Buxton silt loam, 3 to 8 percent slopes	1.2	0.9%				
HeC	Hermon sandy loam, 8 to 15 percent slopes	21.2	15.7%				
LnB	Lyman loam, 3 to 8 percent slopes, rocky	10.5	7.8%				
LnC	Lyman loam, 8 to 15 percent slopes, rocky	20.0	14.8%				
LnD	Lyman loam, 15 to 25 percent slopes, rocky	1.1	0.8%				
LyC	Lyman-Rock outcrop complex, 8 to 15 percent slopes	1.2	0.9%				
LyE	Lyman-Rock outcrop complex, 15 to 80 percent slopes	8.3	6.2%				
MrB	Marlow fine sandy loam, 3 to 8 percent slopes	16.4	12.1%				
MrC2	Marlow fine sandy loam, 8 to 15 percent slopes	4.7	3.5%				
PeB	Peru fine sandy loam, 3 to 8 percent slopes	11.0	8.2%				
Sa	Saco mucky silt loam	0.0	0.0%				
Sc	Scantic silt loam, 0 to 3 percent slopes	25.0	18.5%				
Totals for Area of Interest		135.1	100.0%				

### **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class.

Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

#### York County, Maine

#### Bm—Biddeford mucky peat, 0 to 3 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2t0jn Elevation: 10 to 1,200 feet Mean annual precipitation: 33 to 60 inches Mean annual air temperature: 39 to 45 degrees F Frost-free period: 90 to 160 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

Biddeford and similar soils: 82 percent Minor components: 18 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Biddeford**

#### Setting

Landform: Marine terraces, river valleys Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave, linear Parent material: Organic material over glaciomarine deposits

#### **Typical profile**

*Oe - 0 to 12 inches:* mucky peat *Eg - 12 to 16 inches:* silt loam *Bg - 16 to 45 inches:* silty clay *Cg - 45 to 65 inches:* clay

#### **Properties and qualities**

Slope: 0 to 3 percent
Surface area covered with cobbles, stones or boulders: 0.0 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.14 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Available water capacity: High (about 11.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 5w Hydrologic Soil Group: D Ecological site: F144BY002ME - Marine Terrace Depression Hydric soil rating: Yes

#### **Minor Components**

#### Scantic

Percent of map unit: 9 percent

Landform: Marine terraces, river valleys Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Ecological site: F144BY001ME - Marine Terrace Flat Hydric soil rating: Yes

#### Wonsqueak

Percent of map unit: 6 percent Landform: Marine terraces, river valleys Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

#### Swanville

Percent of map unit: 2 percent Landform: Lake plains, marine terraces Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

#### Lamoine

Percent of map unit: 1 percent Landform: Marine terraces, river valleys Landform position (two-dimensional): Footslope Landform position (three-dimensional): Rise Down-slope shape: Linear Across-slope shape: Convex Hydric soil rating: No

#### BrB—Brayton and Westbury fine sandy loams, 0 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 9k52 Elevation: 10 to 2,500 feet Mean annual precipitation: 34 to 48 inches Mean annual air temperature: 37 to 46 degrees F Frost-free period: 90 to 160 days Farmland classification: Not prime farmland

#### Map Unit Composition

Brayton and similar soils: 70 percent Westbury and similar soils: 25 percent Minor components: 5 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Brayton**

#### Setting

Landform: Till plains Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf Down-slope shape: Concave Across-slope shape: Linear Parent material: Coarse-loamy lodgment till derived from mica schist and/or coarse-loamy lodgment till derived from gneiss

#### **Typical profile**

*H1 - 0 to 8 inches:* fine sandy loam *H2 - 8 to 14 inches:* fine sandy loam *H3 - 14 to 65 inches:* fine sandy loam

#### **Properties and qualities**

Slope: 0 to 8 percent
Depth to restrictive feature: 10 to 20 inches to densic material
Drainage class: Poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.60 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Low (about 3.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: D Hydric soil rating: Yes

#### **Description of Westbury**

#### Setting

Landform: Till plains Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Coarse-loamy lodgment till derived from granite and gneiss

#### **Typical profile**

H1 - 0 to 4 inches: fine sandy loam

- H2 4 to 23 inches: fine sandy loam
- H3 23 to 36 inches: fine sandy loam
- H4 36 to 65 inches: sandy loam

#### Properties and qualities

Slope: 0 to 8 percent
Depth to restrictive feature: 13 to 24 inches to densic material
Drainage class: Somewhat poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: About 7 to 18 inches
Frequency of flooding: None

*Frequency of ponding:* None *Available water capacity:* Very low (about 2.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: D Hydric soil rating: No

#### **Minor Components**

#### Skerry

Percent of map unit: 3 percent Landform: Till plains Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Peru

Percent of map unit: 1 percent Landform: Till plains Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Westbury, slopes >8%

Percent of map unit: 1 percent Landform: Till plains Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### BuB—Buxton silt loam, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 9k54 Elevation: 10 to 900 feet Mean annual precipitation: 34 to 48 inches Mean annual air temperature: 43 to 46 degrees F Frost-free period: 90 to 160 days Farmland classification: Farmland of statewide importance

#### Map Unit Composition

Buxton and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Buxton**

#### Setting

Landform: Coastal plains Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Linear Parent material: Glaciolacustrine deposits derived from siltstone and/or fine-silty marine deposits

#### **Typical profile**

H1 - 0 to 7 inches: silt loam H2 - 7 to 19 inches: silt loam H3 - 19 to 37 inches: silty clay H4 - 37 to 65 inches: silty clay

#### Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: About 7 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: High (about 9.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: D Hydric soil rating: No

#### **Minor Components**

#### Scantic

Percent of map unit: 5 percent Landform: Coastal plains Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: Yes

#### Buxton mod well drained

Percent of map unit: 5 percent Landform: Coastal plains Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### Biddeford

Percent of map unit: 2 percent Landform: Coastal plains Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

#### Scio

Percent of map unit: 1 percent Landform: Coastal plains Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Buxton, slopes >8%

Percent of map unit: 1 percent Landform: Coastal plains Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### Buxton, 0.1 to 3% stone cover

Percent of map unit: 1 percent Landform: Coastal plains Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### HeC—Hermon sandy loam, 8 to 15 percent slopes

#### Map Unit Setting

National map unit symbol: 2w9r9 Elevation: 0 to 980 feet Mean annual precipitation: 31 to 65 inches Mean annual air temperature: 36 to 52 degrees F Frost-free period: 90 to 160 days Farmland classification: Farmland of statewide importance

#### Map Unit Composition

*Hermon and similar soils:* 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Hermon**

#### Setting

Landform: Hills, mountains

Landform position (two-dimensional): Backslope, summit, shoulder

*Landform position (three-dimensional):* Mountainbase, mountainflank, side slope, nose slope, interfluve

Down-slope shape: Convex

Across-slope shape: Convex

*Parent material:* Sandy and gravelly supraglacial meltout till derived from granite and gneiss

#### **Typical profile**

Ap - 0 to 9 inches: sandy loam

Bs1 - 9 to 16 inches: very gravelly sandy loam

Bs2 - 16 to 32 inches: extremely gravelly loamy sand

C - 32 to 65 inches: very gravelly coarse sand

#### **Properties and qualities**

Slope: 8 to 15 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (1.42 to 14.17 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water capacity: Low (about 3.9 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: A Hydric soil rating: No

#### **Minor Components**

#### Monadnock

Percent of map unit: 4 percent Landform: Hills, mountains Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Mountainflank, mountainbase, side slope, nose slope, interfluve Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Peru

Percent of map unit: 4 percent Landform: Mountains, hills Landform position (two-dimensional): Footslope, backslope Landform position (three-dimensional): Mountainflank, mountainbase, side slope, nose slope, interfluve Microfeatures of landform position: Open depressions, closed depressions, closed depressions, open depressions *Down-slope shape:* Convex, concave *Across-slope shape:* Linear, concave *Hydric soil rating:* No

#### Tunbridge

Percent of map unit: 1 percent Landform: Mountains, hills Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Mountainbase, mountainflank, side slope, nose slope, interfluve Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Brayton

Percent of map unit: 1 percent
Landform: Mountains, hills
Landform position (two-dimensional): Toeslope, footslope
Landform position (three-dimensional): Mountainflank, mountainbase, side slope, nose slope, interfluve
Microfeatures of landform position: Closed depressions, open depressions, closed depressions, open depressions
Down-slope shape: Concave
Across-slope shape: Concave
Hydric soil rating: Yes

#### LnB—Lyman loam, 3 to 8 percent slopes, rocky

#### Map Unit Setting

National map unit symbol: 2trq7 Elevation: 0 to 520 feet Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F Frost-free period: 60 to 160 days Farmland classification: Farmland of statewide importance

#### Map Unit Composition

*Lyman, rocky, and similar soils:* 86 percent *Minor components:* 14 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Lyman, Rocky**

#### Setting

Landform: Mountains, hills Landform position (two-dimensional): Shoulder, summit, backslope Landform position (three-dimensional): Mountaintop, mountainbase, crest, side slope Down-slope shape: Convex Across-slope shape: Convex *Parent material:* Loamy supraglacial till derived from granite and gneiss and/or loamy supraglacial till derived from phyllite and/or loamy supraglacial till derived from mica schist

#### **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loam

*E* - 3 to 5 inches: fine sandy loam

Bhs - 5 to 7 inches: loam

Bs1 - 7 to 11 inches: loam

Bs2 - 11 to 18 inches: channery loam

R - 18 to 28 inches: bedrock

#### **Properties and qualities**

Slope: 3 to 8 percent
Depth to restrictive feature: 11 to 24 inches to lithic bedrock
Drainage class: Somewhat excessively drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00 to 14.03 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: D Hydric soil rating: No

#### **Minor Components**

#### Tunbridge, rocky

Percent of map unit: 6 percent Landform: Hills, mountains Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Mountaintop, mountainbase, side slope, crest Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Skerry, rocky

Percent of map unit: 5 percent Landform: Hills, mountains Landform position (two-dimensional): Footslope, backslope Landform position (three-dimensional): Mountaintop, mountainbase, crest, side slope Microfeatures of landform position: Closed depressions, closed depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: No

#### Hermon, rocky

*Percent of map unit:* 2 percent *Landform:* Hills, mountains *Landform position (two-dimensional):* Backslope, summit, shoulder Landform position (three-dimensional): Mountaintop, mountainbase, side slope, crest Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Brayton, rocky

Percent of map unit: 1 percent
Landform: Hills, mountains
Landform position (two-dimensional): Toeslope, footslope
Landform position (three-dimensional): Mountaintop, mountainbase, crest, side slope
Microfeatures of landform position: Closed depressions, closed depressions
Down-slope shape: Concave
Across-slope shape: Concave
Hydric soil rating: Yes

#### LnC—Lyman loam, 8 to 15 percent slopes, rocky

#### **Map Unit Setting**

National map unit symbol: 2trq9 Elevation: 0 to 690 feet Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F Frost-free period: 60 to 160 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Lyman, rocky, and similar soils:* 86 percent *Minor components:* 14 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Lyman, Rocky**

#### Setting

Landform: Hills, mountains Landform position (two-dimensional): Shoulder, summit, backslope Landform position (three-dimensional): Mountaintop, mountainbase, mountainflank, crest, side slope Down-slope shape: Convex Across-slope shape: Convex Parent material: Loamy supraglacial till derived from granite and gneiss and/or

loamy supraglacial till derived from phyllite and/or loamy supraglacial till derived from mica schist

#### **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

- A 1 to 3 inches: loam
- *E* 3 to 5 inches: fine sandy loam
- Bhs 5 to 7 inches: loam
Bs1 - 7 to 11 inches: loam

- Bs2 11 to 18 inches: channery loam
- R 18 to 28 inches: bedrock

## **Properties and qualities**

Slope: 8 to 15 percent
Depth to restrictive feature: 11 to 24 inches to lithic bedrock
Drainage class: Somewhat excessively drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00 to 14.03 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: D Hydric soil rating: No

#### **Minor Components**

#### Tunbridge, rocky

Percent of map unit: 6 percent Landform: Mountains, hills Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Mountaintop, mountainbase, mountainflank, side slope, crest Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

## Skerry, rocky

Percent of map unit: 5 percent

Landform: Hills, mountains

Landform position (two-dimensional): Footslope, backslope

Landform position (three-dimensional): Mountaintop, mountainbase,

mountainflank, crest, side slope

*Microfeatures of landform position:* Closed depressions, closed depressions, open depressions

*Down-slope shape:* Concave

Across-slope shape: Concave

Hydric soil rating: No

#### Hermon, rocky

Percent of map unit: 2 percent

Landform: Hills, mountains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Mountaintop, mountainbase,

mountainflank, side slope, crest

Down-slope shape: Convex

Across-slope shape: Convex

Hydric soil rating: No

#### Brayton, rocky

Percent of map unit: 1 percent

Landform: Hills, mountains Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Mountaintop, mountainbase, mountainflank, crest, side slope Microfeatures of landform position: Open depressions, open depressions, closed depressions, closed depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## LnD—Lyman loam, 15 to 25 percent slopes, rocky

#### **Map Unit Setting**

National map unit symbol: 2trqd Elevation: 0 to 850 feet Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F Frost-free period: 60 to 160 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Lyman, rocky, and similar soils:* 92 percent *Minor components:* 8 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Lyman, Rocky**

#### Setting

Landform: Hills, mountains

Landform position (two-dimensional): Shoulder, summit, backslope

Landform position (three-dimensional): Mountaintop, mountainflank, crest, side slope

*Down-slope shape:* Convex

Across-slope shape: Convex

*Parent material:* Loamy supraglacial till derived from granite and gneiss and/or loamy supraglacial till derived from phyllite and/or loamy supraglacial till derived from mica schist

#### **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loam

*E* - 3 to 5 inches: fine sandy loam

Bhs - 5 to 7 inches: loam

Bs1 - 7 to 11 inches: loam

Bs2 - 11 to 18 inches: channery loam

R - 18 to 28 inches: bedrock

#### **Properties and qualities**

*Slope:* 15 to 25 percent *Depth to restrictive feature:* 11 to 24 inches to lithic bedrock Drainage class: Somewhat excessively drained Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00 to 14.03 in/hr) Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Available water capacity: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4e Hydrologic Soil Group: D Hydric soil rating: No

#### **Minor Components**

#### Tunbridge, rocky

Percent of map unit: 3 percent Landform: Hills, mountains Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Mountaintop, mountainflank, side slope, crest Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Hermon, rocky

Percent of map unit: 2 percent Landform: Hills, mountains Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Mountainflank, mountaintop, side slope, crest Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Skerry, rocky

Percent of map unit: 2 percent Landform: Mountains, hills Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Mountaintop, mountainflank, crest, side slope Microfeatures of landform position: Open depressions, open depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: No

#### Brayton, rocky

Percent of map unit: 1 percent Landform: Hills, mountains Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Mountaintop, mountainflank, side slope, crest Microfeatures of landform position: Open depressions, open depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## LyC—Lyman-Rock outcrop complex, 8 to 15 percent slopes

#### Map Unit Setting

National map unit symbol: 2trqj Elevation: 0 to 790 feet Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F Frost-free period: 60 to 160 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Lyman, very stony, and similar soils:* 62 percent *Rock outcrop:* 25 percent *Minor components:* 13 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### Description of Lyman, Very Stony

#### Setting

Landform: Hills, mountains

Landform position (two-dimensional): Shoulder, summit, backslope Landform position (three-dimensional): Mountaintop, mountainbase, crest, side slope

*Down-slope shape:* Convex

Across-slope shape: Convex

*Parent material:* Loamy supraglacial till derived from granite and gneiss and/or loamy supraglacial till derived from phyllite and/or loamy supraglacial till derived from mica schist

#### **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loam

E - 3 to 5 inches: fine sandy loam

Bhs - 5 to 7 inches: loam

Bs1 - 7 to 11 inches: loam

Bs2 - 11 to 18 inches: channery loam

R - 18 to 28 inches: bedrock

## **Properties and qualities**

Slope: 8 to 15 percent
Surface area covered with cobbles, stones or boulders: 1.5 percent
Depth to restrictive feature: 11 to 24 inches to lithic bedrock
Drainage class: Somewhat excessively drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00 to 14.03 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: D Hydric soil rating: No

#### **Description of Rock Outcrop**

#### Setting

Landform: Hills, mountains Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Mountaintop, mountainbase, crest, side slope Down-slope shape: Convex Across-slope shape: Convex Parent material: Igneous and metamorphic rock

#### **Typical profile**

R - 0 to 10 inches: bedrock

#### **Properties and qualities**

Slope: 8 to 15 percent Depth to restrictive feature: 0 inches to lithic bedrock Capacity of the most limiting layer to transmit water (Ksat): Very low to very high (0.00 to 14.17 in/hr)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8s Hydric soil rating: Unranked

#### **Minor Components**

#### Skerry, very stony

Percent of map unit: 4 percent
Landform: Hills, mountains
Landform position (two-dimensional): Backslope, footslope
Landform position (three-dimensional): Mountaintop, mountainbase, crest, side slope
Microfeatures of landform position: Closed depressions, closed depressions, open depressions
Down-slope shape: Concave
Across-slope shape: Concave

Hydric soil rating: No

#### Hermon, very stony

Percent of map unit: 4 percent

Landform: Mountains, hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Mountaintop, mountainbase, side slope,

crest

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

## Tunbridge, very stony

Percent of map unit: 3 percent

Landform: Mountains, hills

Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Mountaintop, mountainbase, side slope, crest

*Down-slope shape:* Convex *Across-slope shape:* Convex *Hydric soil rating:* No

#### Brayton, very stony

Percent of map unit: 2 percent
Landform: Hills, mountains
Landform position (two-dimensional): Toeslope, footslope
Landform position (three-dimensional): Mountaintop, mountainbase, crest, side slope
Microfeatures of landform position: Closed depressions, closed depressions, open depressions, open depressions
Down-slope shape: Concave
Across-slope shape: Concave
Hydric soil rating: Yes

## LyE—Lyman-Rock outcrop complex, 15 to 80 percent slopes

#### Map Unit Setting

National map unit symbol: 2trqp Elevation: 0 to 980 feet Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F Frost-free period: 60 to 160 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Lyman, very stony, and similar soils:* 60 percent *Rock outcrop:* 30 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### Description of Lyman, Very Stony

#### Setting

Landform: Mountains, hills Landform position (two-dimensional): Shoulder, summit, backslope Landform position (three-dimensional): Mountaintop, mountainflank, crest, side slope

Down-slope shape: Convex

Across-slope shape: Convex

*Parent material:* Loamy supraglacial till derived from granite and gneiss and/or loamy supraglacial till derived from phyllite and/or loamy supraglacial till derived from mica schist

#### **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loam

E - 3 to 5 inches: fine sandy loam

Bhs - 5 to 7 inches: loam

Bs1 - 7 to 11 inches: loam

Bs2 - 11 to 18 inches: channery loam

R - 18 to 28 inches: bedrock

#### **Properties and qualities**

Slope: 15 to 80 percent
Surface area covered with cobbles, stones or boulders: 1.5 percent
Depth to restrictive feature: 11 to 24 inches to lithic bedrock
Drainage class: Somewhat excessively drained
Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00 to 14.03 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: D Hydric soil rating: No

#### Description of Rock Outcrop

#### Setting

Landform: Hills, mountains Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Mountaintop, mountainflank, crest, side slope, free face Down-slope shape: Convex Across-slope shape: Convex Parent material: Igneous and metamorphic rock

## **Typical profile**

R - 0 to 10 inches: bedrock

## **Properties and qualities**

Slope: 15 to 80 percent Depth to restrictive feature: 0 inches to lithic bedrock Capacity of the most limiting layer to transmit water (Ksat): Very low to very high (0.00 to 14.17 in/hr)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8s Hydric soil rating: Unranked

## **Minor Components**

#### Tunbridge, very stony

Percent of map unit: 4 percent Landform: Hills, mountains

#### **Custom Soil Resource Report**

Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Mountaintop, mountainflank, side slope, crest Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Hermon, very stony

Percent of map unit: 3 percent Landform: Mountains, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Mountaintop, mountainflank, side slope, crest Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Skerry, very stony

Percent of map unit: 2 percent Landform: Mountains, hills Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Mountaintop, mountainflank, crest, side slope Microfeatures of landform position: Open depressions, open depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: No

#### Brayton, very stony

Percent of map unit: 1 percent Landform: Hills, mountains Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Mountaintop, mountainflank, crest, side slope Microfeatures of landform position: Open depressions, open depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

#### MrB—Marlow fine sandy loam, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 2ty5d Elevation: 0 to 690 feet Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F Frost-free period: 90 to 160 days Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Marlow and similar soils: 87 percent Minor components: 13 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Marlow**

#### Setting

Landform: Mountains, hills Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Mountainbase, side slope, nose slope, interfluve Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Loamy lodgment till derived from granite and/or loamy lodgment till derived from mica schist and/or loamy lodgment till derived from phyllite

#### **Typical profile**

Ap - 0 to 4 inches: fine sandy loam E - 4 to 6 inches: fine sandy loam Bs1 - 6 to 10 inches: fine sandy loam Bs2 - 10 to 15 inches: fine sandy loam Bs3 - 15 to 20 inches: fine sandy loam BC - 20 to 24 inches: fine sandy loam Cd - 24 to 65 inches: fine sandy loam

#### **Properties and qualities**

Slope: 3 to 8 percent
Depth to restrictive feature: 20 to 39 inches to densic material
Drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.01 to 1.42 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water capacity: Low (about 3.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2e Hydrologic Soil Group: C Hydric soil rating: No

#### **Minor Components**

#### Peru

Percent of map unit: 6 percent Landform: Hills, mountains Landform position (two-dimensional): Footslope, backslope Landform position (three-dimensional): Mountainbase, side slope, nose slope, interfluve Microfeatures of landform position: Closed depressions, closed depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: No

## Tunbridge

Percent of map unit: 4 percent Landform: Mountains, hills Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Mountainbase, side slope, nose slope, interfluve Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Brayton

Percent of map unit: 2 percent Landform: Hills, mountains Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Mountainbase, side slope, nose slope, interfluve Microfeatures of landform position: Closed depressions, closed depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## Colonel

Percent of map unit: 1 percent Landform: Hills, mountains Landform position (two-dimensional): Footslope Landform position (three-dimensional): Mountainbase, side slope, nose slope, interfluve Microfeatures of landform position: Closed depressions, closed depressions Down-slope shape: Linear Across-slope shape: Concave Hydric soil rating: No

## MrC2—Marlow fine sandy loam, 8 to 15 percent slopes

## **Map Unit Setting**

National map unit symbol: 2ty5g Elevation: 0 to 820 feet Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F Frost-free period: 90 to 160 days Farmland classification: Not prime farmland

## **Map Unit Composition**

Marlow and similar soils: 88 percent Minor components: 12 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Marlow**

#### Setting

Landform: Hills, mountains

Landform position (two-dimensional): Summit, shoulder, backslope

*Landform position (three-dimensional):* Mountainbase, mountainflank, side slope, nose slope, interfluve

Down-slope shape: Convex

Across-slope shape: Convex

*Parent material:* Loamy lodgment till derived from granite and/or loamy lodgment till derived from mica schist and/or loamy lodgment till derived from phyllite

#### **Typical profile**

Ap - 0 to 4 inches: fine sandy loam

*E - 4 to 6 inches:* fine sandy loam

Bs1 - 6 to 10 inches: fine sandy loam

Bs2 - 10 to 15 inches: fine sandy loam

Bs3 - 15 to 20 inches: fine sandy loam

BC - 20 to 24 inches: fine sandy loam

Cd - 24 to 65 inches: fine sandy loam

#### **Properties and qualities**

Slope: 8 to 15 percent
Depth to restrictive feature: 20 to 39 inches to densic material
Drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.01 to 1.42 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water capacity: Low (about 3.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: C Hydric soil rating: No

#### **Minor Components**

#### Tunbridge

Percent of map unit: 5 percent Landform: Hills, mountains Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Mountainbase, mountainflank, side slope, nose slope, interfluve Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Peru

Percent of map unit: 5 percent Landform: Hills, mountains Landform position (two-dimensional): Footslope, backslope

#### **Custom Soil Resource Report**

Landform position (three-dimensional): Mountainbase, mountainflank, side slope, nose slope, interfluve Microfeatures of landform position: Closed depressions, closed depressions, open depressions, open depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: No

#### Brayton

Percent of map unit: 2 percent Landform: Mountains, hills Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Mountainbase, mountainflank, side slope, nose slope, interfluve Microfeatures of landform position: Open depressions, open depressions, closed depressions, closed depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## PeB—Peru fine sandy loam, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 2ty5x Elevation: 0 to 720 feet Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F Frost-free period: 90 to 160 days Farmland classification: All areas are prime farmland

#### Map Unit Composition

*Peru and similar soils:* 88 percent *Minor components:* 12 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Peru**

#### Setting

Landform: Hills, mountains Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Mountainbase, interfluve Down-slope shape: Convex Across-slope shape: Linear Parent material: Loamy lodgment till derived from granite and/or loamy lodgment till derived from mica schist and/or loamy lodgment till derived from phyllite

#### **Typical profile**

*Ap - 0 to 6 inches:* fine sandy loam *Bhs - 6 to 8 inches:* fine sandy loam *Bs1 - 8 to 12 inches:* fine sandy loam *Bs2 - 12 to 18 inches:* fine sandy loam *Bs3 - 18 to 21 inches:* fine sandy loam *BC - 21 to 24 inches:* fine sandy loam *Cd - 24 to 65 inches:* sandy loam

#### **Properties and qualities**

Slope: 3 to 8 percent
Depth to restrictive feature: 20 to 39 inches to densic material
Drainage class: Moderately well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.01 to 1.42 in/hr)
Depth to water table: About 16 to 30 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water capacity: Low (about 3.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2e Hydrologic Soil Group: C/D Hydric soil rating: No

#### **Minor Components**

#### Brayton

Percent of map unit: 5 percent Landform: Hills, mountains Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Mountainbase, interfluve Microfeatures of landform position: Closed depressions, closed depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

#### Sunapee

Percent of map unit: 3 percent Landform: Hills, mountains Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Mountainbase, interfluve Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Marlow

Percent of map unit: 3 percent Landform: Hills, mountains Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Mountainbase, interfluve Microfeatures of landform position: Rises, rises Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Colonel

*Percent of map unit:* 1 percent *Landform:* Hills, mountains

#### **Custom Soil Resource Report**

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Mountainbase, interfluve Microfeatures of landform position: Closed depressions, closed depressions Down-slope shape: Linear, concave Across-slope shape: Concave Hydric soil rating: No

## Sa—Saco mucky silt loam

#### Map Unit Setting

National map unit symbol: 9k6j Elevation: 10 to 2,000 feet Mean annual precipitation: 34 to 48 inches Mean annual air temperature: 37 to 46 degrees F Frost-free period: 80 to 160 days Farmland classification: Not prime farmland

#### Map Unit Composition

Saco and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### Description of Saco

#### Setting

Landform: Flood plains Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Coarse-silty alluvium

#### **Typical profile**

H1 - 0 to 13 inches: mucky silt loam
H2 - 13 to 24 inches: silt loam
H3 - 24 to 65 inches: very fine sandy loam

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: FrequentNone
Frequency of ponding: None
Available water capacity: Very high (about 16.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6w

Hydrologic Soil Group: B/D Hydric soil rating: Yes

#### **Minor Components**

#### Rumney

Percent of map unit: 8 percent Landform: Flood plains Landform position (two-dimensional): Summit Landform position (three-dimensional): Rise Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: Yes

#### Chocorua

Percent of map unit: 7 percent Landform: Bogs Hydric soil rating: Yes

## Sc—Scantic silt loam, 0 to 3 percent slopes

#### Map Unit Setting

National map unit symbol: 2slv3 Elevation: 10 to 900 feet Mean annual precipitation: 33 to 60 inches Mean annual air temperature: 39 to 45 degrees F Frost-free period: 90 to 160 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Scantic and similar soils:* 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Scantic**

#### Setting

Landform: Marine terraces, river valleys Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Glaciomarine deposits

#### **Typical profile**

Ap - 0 to 9 inches: silt loam Bg1 - 9 to 16 inches: silty clay loam Bg2 - 16 to 29 inches: silty clay Cg - 29 to 65 inches: silty clay

## **Properties and qualities**

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches Drainage class: Poorly drained Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr) Depth to water table: About 0 to 12 inches Frequency of flooding: None Frequency of ponding: None Available water capacity: Moderate (about 6.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: D Hydric soil rating: Yes

#### **Minor Components**

#### Lamoine

Percent of map unit: 8 percent Landform: River valleys, marine terraces Landform position (three-dimensional): Riser, rise Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Biddeford

Percent of map unit: 3 percent Landform: Marine terraces, river valleys Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave, linear Ecological site: F144BY002ME - Marine Terrace Depression Hydric soil rating: Yes

#### Buxton

Percent of map unit: 2 percent Landform: Marine terraces, river valleys Landform position (three-dimensional): Riser, rise Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Roundabout

Percent of map unit: 2 percent Landform: River valleys, marine terraces Landform position (three-dimensional): Tread, talf Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

# Section 8

# BMP Sizing Calculations Riprap Calculations



## **BMP Water Quality Volume (WQV) Calculations**

## BMP: Grassed Underdrained Soil Filter #1 (Pond 13P)

	Area (sf)	Ratio (in/sf)	WQV (cf)	
Impervious	4554	1	380	cf
Landscape	8462	0.4	282	cf
25% Pretreatme	-165	cf		
Total W0	QV Required:		496	cf

Available Storage (cf):

Surplus/Deficit:	29	cf
Total Storage Provided:	525	cf
Surface to Lowest Outlet:	525	cf
		cf

Filter Area:	%	Area Req.		
Impervious	4554	5%	228	sf
Landscape	8462	2%	169	sf
Total Filter Are	a Required:		397	sf
Filter Are	a Provided:		464	sf
	Surp	olus/Deficit:	67	sf



## **BMP Water Quality Volume (WQV) Calculations**

## BMP: Grassed Underdrained Soil Filter #1 (Pond 13P)

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Landscape	8462	2%	169	sf
Total Filter Are	a Required:		397	sf
Filter Are	a Provided:		464	sf
	Surp	olus/Deficit:	67	sf



		<u>R</u>	IPRAP CA	LCULATI	ONS			
Location:	CB #5-1.	12" Culvert	(HvdroCA	D Pond #1	0P)	I - I		
	,				,			
Date	6/29/2021	By:	FBS					
Date.	0/20/2021	By.	LDS					
Та	Apron Leng	th Ft	Calculated					
Tw	Tailwater	Ft	0.5					
0	Flow 10 Y	r Storm, CFS	3 78					
$\Sigma$	Median Stor	ne Dia Ft	Calculated					
D	Depth of Ste	one. In	Calculated					
Do	Pine Diame	ter. Ft	1.00					
W1	Width @ St	art. Ft.	Calculated					
W2	Width @ En	nd, Ft	Calculated					
W	Width of C	hannel	2					
W1:								
	3(Do)=		3	Ft.				
					Widt	th @ Start:	3	Ft.
D50:	$0.02(O)^{4/3}$			D50=	0.23	Ft.		
2001	Tw(Do)			200	0.20			
	1(2.0)			or	2.8	In.		
					Median	Stone Size:	6	In.
					1/1Cului		U	111.
D.	2.25*D50				Donth	of Dingons	14	In
D:	2.25*D50				Deptii	of Riprap:	14	111.
т		/2		D /2	0.5	<b>E</b> 4		
La:	If $IW \le DO$	/2:		D0/2=	0.5	Ft.		
		La=1.8Q/Do <sup>3/2</sup>	+ 7Do	Tw=	0.5	Ft.		
	and	W2=width of c	hannel					
		or						
		W2=3Do+La						
	If Two Da/2	-						
	II I W>D0/2	3/2						
		$La=3Q/Do^{3/2} +$	· 7Do					
	and	W2=width of c	hannel					
		or			Length	of Apron:	14	Ft.
		W2=3Do+0.4I	la		Wid	th @ End:	2	Ft.
	1	1						
Á T/T	TIC							
ALI	US T							
ENGINEE	RING, INC							

		R	IPRAP CA	LCULATI	ONS			
Location:	CB #4, 12	" Culvert (I	IvdroCAD	Pond #12]	P)			
	- )		<b>J</b>		/			
Data	12/31/2020	Dave	EDS					
Date.	12/31/2020	Dy.	LDS					
La	Apron Leng	th Ft	Calculated					
La Tw	Tailwater	, 11, 1 t. Ft						
0	Flow 10 V	r Storm CFS	0.5					
D50	Median Stor	ne Dia Et	Calculated					
D	Depth of Sto	one In	Calculated					
Do	Pine Diame	one, m eter. Ft	1 00					
W1	Width @ St	art Ft	Calculated					
W2	Width @ Er	nd Ft	Calculated					
W	Width of C	hannel	2					
•••	Whath of C		_					
W1:								
	3(Do)=		3	Ft.				
	- ( )				Widt	h @ Start.	3	Ft
					··· iui	in w Start.	5	1
	0.00 (0) 4/3					-		
D50:	$0.02(Q)^{13}$			D50=	0.02	Ft.		
	Tw(Do)					-		
				or	0.3	ln.		
						~ ~ ~		-
					Median	Stone Size:	6	ln.
D:	2.25*D50				Depth	of Riprap:	14	In.
La:	If Tw<= Do	/2:		Do/2=	0.5	Ft.		
		$L_{a=1} 80/Do^{3/2}$	+7Do	Tw=	0.5	Ft		
	and	W2=width of c	hannel	1.00	0.0	1.0		
		or						
		W2=3Do+La						
	If Tw>Do/2	:						
		$I_{a}=30/Do^{3/2}+$	7Do					
	and	$W^2 = width of c$	hannel					
	ana	width of e			Longth	of Annone	0	E4
		or			Length	of Apron:	9	гι.
		W2=3Do+0.4L	La		Wid	th @ End:	2	Ft.
		I						
Á T/T	TIC							
ALI	US							
ENGINEE	RING, INC							

	RIPRAP CALCULATIONS							
Location:	GUSF #1	. 12" Culver	t (HvdroC	AD Pond #	(13P)	U		
		,			- /			
Date:	12/31/2020	By:	EBS					
Date.	12/31/2020	By.	LDS					
La	Apron Leng	th Ft	Calculated					
Tw	Tailwater.	Ft.	0.5					
0	Flow, 10 Y	r Storm, CFS	0.63					
<u>2</u> D50	Median Stor	ne Dia Ft.	Calculated					
D	Depth of Sto	one. In	Calculated					
 Do	Pipe Diame	eter. Ft	1.00					
W1	Width @ St	art. Ft.	Calculated					
W2	Width @ Er	nd. Ft	Calculated					
W	Width of C	hannel	2					
			•					
W1:								
	3(Do)=		3	Ft.				
					Widt	h @ Start:	3	Ft.
							-	
D50·	$0.02(0)^{4/3}$			D50=	0.02	Ft		
D30.	$\overline{\mathrm{Tw}(\mathrm{Do})}$			D30-	0.02	1't.		
	1 W(D0)			or	0.3	In		
				01	0.5			
					Modian	Stone Size:	6	In
					WICUIAII	Stolic Size.	0	111.
	0.05+10.50					CD'	14	т
D:	2.25*D50				Deptn	of Riprap:	14	In.
T	LOT D			D (2		D.		
La:	If Tw<= Do	/2:		Do/2=	0.5	Ft.		
		La=1.8Q/Do <sup>3/2</sup>	+ 7Do	Tw=	0.5	Ft.		
	and	W2=width of c	hannel					
		or						
		W2=3Do+La						
	If Tw>Do/2	:						
		$La=3Q/Do^{3/2} +$	· 7Do					
	and	W2=width of c	hannel					
		or			Length	of Apron:	9	Ft.
		W2=3Do+0.4L	a		Wid	th @ End:	2	Ft.
	TIO							
AĽĽ	$US^{-}$	<u> </u>						
ENGINEE	RING, INC							

		R	IPRAP CA	LCULATI	<b>IONS</b>			
Location:	Roof Lea	der - 12" Cu	lvert (Hvd	roCAD Re	ach #27R	)		
Data	12/21/2020	Drv	EDS					
Date.	12/31/2020	By.	LDS					
La	Aprop Leng	th Ft	Calculated					
	Tailwater	,111, 1°t. Ff						
$\frac{1}{0}$	Flow 10 V	rt. r Storm CFS	0.3					
Q D50	Median Stor	ne Dia Et	Calculated					
D30	Depth of Sto	one In	Calculated					
Do	Pine Diame	one, m oter Ft						
W1	Width @ St	art Ft	Calculated					
W2	Width @ Er	nd Ft	Calculated					
W	Width of C	hannel	2					
•••	which of C	hanner	-					
W1:								
	3(Do)=		3	Ft.				
	- ( )				Widt	h @ Start.	3	Ft
					Wiu	in w Start.	5	1' ι.
	a a <b>a</b> ( a) 4/3				0.44	-		
D50:	$0.02(Q)^{+3}$			D50=	0.11	Ft.		
	Tw(Do)					-		
				or	1.3	ln.		<u> </u>
					Median	Stone Size:	6	ln.
D:	2.25*D50				Depth	of Riprap:	14	In.
La:	If Tw<= Do	/2:		Do/2=	0.5	Ft.		
		La=1.80/Do3/2	+ 7Do	Tw=	0.5	Ft.		
	and	W2=width of c	hannel					
		or						
		W2=3Do+La						
	If Tw>Do/2	:						
		$La=30/Do^{3/2} +$	· 7Do					
	and	W2=width of c	hannel					
		or			Length	of Aprop.	11	Ft
					Tength MV			F4
		w2=3Do+0.4L	La		Wid	un a Ena:	2	гt.
	1	·						
	TIC	<						
	UJ							
ENGINEE	KING, INC	••						

		<u>R</u>	IPRAP CA	LCULATI	ONS			
Location:	GUSF #2	, 18" Culver	t (HvdroC	AD Pond #	29P)			
					,			
Date	12/31/2020	By:	EBS					
Date.	12/31/2020	By.	LDS					
Та	Apron Leng	th Ft	Calculated					
Tw	Tailwater	Ft	0.5					
0	Flow 10 Y	r Storm, CFS	7.85					
$\overline{\mathbf{D}}$	Median Stor	ne Dia Ft	Calculated					
D	Depth of Ste	one. In	Calculated					
Do	Pine Diame	ter. Ft	1.50					
W1	Width @ St	art. Ft.	Calculated					
W2	Width @ Er	nd. Ft	Calculated					
W	Width of C	hannel	2					
W1:								
	3(Do)=		4.5	Ft.				
					Widt	th @ Start:	5	Ft.
D50.	$0.02(0)^{4/3}$			D50-	0.41	E+		
D30.	$\frac{0.02(Q)}{Tw(D_2)}$			D30-	0.41	г.		
	Tw(D0)			or	5.0	In		
				01	5.0	111.		
					Madian	Stone Sizes	6	In
					Wieulali	stone size.	0	111.
						<b>6D!</b>	14	T
D:	2.25*D50				Depth	of Riprap:	14	ln.
-								
La:	If $Tw \le Do$	/2:		Do/2=	0.75	Ft.		
		La=1.8Q/Do <sup>3/2</sup>	+ 7Do	Tw=	0.5	Ft.		
	and	W2=width of c	hannel					
		or						
		W2=3Do+La						
	If Tw>Do/2	:						
		$La=3Q/Do^{3/2} +$	· 7Do					
	and	W2=width of c	hannel					
		or			Length	of Apron:	19	Ft.
		$W_{2=3D_{0}+0.4I}$	а		Wid	th @ End·	2	Ft
					** 10		-	- **
	IIS	<						
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	and the second second in the local second		1					

# Section 9

Stormwater Operations & Maintenance Plan



## **STORMWATER INSPECTION AND MAINTENANCE MANUAL**

## **Good To-Go** Kittery Assessor's Map 67, Lot 1

## OWNER AT TIME OF APPROVAL: Good To-Go c/o Cape House Management, LLC 484 U.S. Route 1 Kittery, Maine 03904

Proper inspection, maintenance, and repair are key elements in maintaining a successful stormwater management program on a developed property. Routine inspections ensure permit compliance and reduce the potential for deterioration of infrastructure or reduced water quality. The following responsible parties shall be in charge of managing the stormwater facilities:

## **RESPONSIBLE PARTIES:**

Owner:	<u>Good To-Go c/o Cape Ho</u>	use Management	(207) 451-9060
	Name	Company	Phone
Inspection:	<u>Good To-Go c/o Cape Ho</u>	use Management	(207) 451-9060
	Name	Company	Phone
Maintenance	: <u>Good To-Go c/o Cape Ho</u>	ouse Management	(207) 451-9060
	Name	Company	Phone

## <u>NOTES:</u>

Inspection and maintenance responsibilities shall transfer to any future property owner(s).

This manual shall be updated as needed to reflect any changes related to any transfer of ownership and/or any delegation of inspection and maintenance responsibilities to any entity other than those listed above.



## **GRASSED UNDERDRAINED SOIL FILTERS**

Underdrain soil filters control stormwater quality by capturing and retaining runoff and passing it through a filter bed comprised of a specific media. The basin shall be inspected semi-annually and following major storm events for evidence of erosion, clogging or of bypass conditions.

## Maintenance

- *Drainage:* The filter should within 24 to 48 hours following a one-inch storm or greater. If the system drains too fast, adjust the outlet release valve opening to regulate the outflow.
- *Sediment Removal*: Sediment and plant debris should be removed from the pretreatment structure at least annually.
- *Mowing*: If mowing is desired, only hand-held string trimmers or push-mowers are allowed on the filter (no tractor) and the grass bed should be mowed no more than 2 times per growing season to maintain grass heights of no less than 6 inches.
- *Fertilization:* Fertilization of the underdrained filter area should be avoided unless absolutely necessary to establish vegetation.
- *Weeding:* Weeding to control unwanted or invasive plants if necessary.
- *Grass cover:* Maintaining a healthy cover of grass will minimize clogging with fine sediments. If ponding exceeds 48 hours, the top of the filter bed should be rototilled to reestablish the soil's filtration capacity.
- *Soil Filter Replacement:* The top several inches of the filter can be replaced with fresh material if water is ponding for more than 72 hours, or the basin can be rototilled, seeded and mulched. Once the filter is mature, adding new material (a 1-inch to 2-inch cover of mature compost) can compensate for subsidence.

## **CULVERTS AND DRAINAGE PIPES**

*Function* – Culverts and drainage pipes convey stormwater away from buildings, walkways, and parking areas and to surface waters or closed drainage systems.

Maintenance

- Culverts and drainage pipes shall be inspected semi-annually, or more often as needed, for accumulation of debris and structural integrity. Leaves and other debris shall be removed from the inlet and outlet to insure the functionality of drainage structures. Debris shall be disposed of on site where it will not concentrate back at the drainage structures or at a solid waste disposal facility.
- Riprap Areas Culvert outlets and inlets shall be inspected during annual maintenance and operations for erosion and scour. If scour or erosion is identified, the owner shall take appropriate means to prevent further erosion.

## **DEEP SUMP CATCH BASINS**

*Function* – Catch basins collect stormwater, primarily from paved surfaces and roofs. Stormwater from paved areas often contains sediment and contaminants. Catch basin sumps serve to trap sediment, trace metals, nutrients and debris. Hooded catch basins trap hydrocarbons and floating debris.

Maintenance

- Remove leaves and debris from structure grates on an as-needed basis.
- Sumps shall be inspected and cleaned annually and any removed sediment and debris shall be disposed of at a solid waste disposal facility.

## LANDSCAPED AREAS - FERTILIZER MANAGEMENT

*Function* – Fertilizer management involves controlling the rate, timing and method of fertilizer application so that the nutrients are taken up by the plants thereby reducing the chance of polluting the surface and ground waters. Fertilizer management can be effective in reducing the amounts of phosphorus and nitrogen in runoff from landscaped areas, particularly lawns.

Maintenance

- Have the soil tested by your landscaper or local Soil Conservation Service for nutrient requirements and follow the recommendations.
- Do not apply fertilizer to frozen ground.
- Clean up any fertilizer spills.
- Do not allow fertilizer to be broadcast into water bodies.
- When fertilizing a lawn, water thoroughly, but do not create a situation where water runs off the surface of the lawn.

## LANDSCAPED AREAS - LITTER CONTROL

*Function* – Landscaped areas tend to filter debris and contaminates that may block drainage systems and pollute the surface and ground waters.

Maintenance

- Litter Control and lawn maintenance involves removing litter such as trash, leaves, lawn clippings, pet wastes, oil and chemicals from streets, parking lots, and lawns before materials are transported into surface waters.
- Litter control shall be implemented as part of the grounds maintenance program.

## **VEGETATIVE SWALES**

*Function* – Vegetative swales filter sediment from stormwater, promote infiltration, and the uptake of contaminates. They are designed to treat runoff and dispose of it safely into the natural drainage system.

Maintenance

- Timely maintenance is important to keep a swale in good working condition. Mowing of grassed swales shall be monthly to keep the vegetation in vigorous condition. The cut vegetation shall be removed to prevent the decaying organic litter from adding pollutants to the discharge from the swale.
- Fertilizing shall be bi-annual or as recommended from soil testing.
- Inspect swales following significant rainfall events.
- Woody vegetation shall not be allowed to become established in the swales or rock riprap outlet protection and if present shall be removed.
- Accumulated debris disrupts flow and leads to clogging and erosion. Remove debris and litter as necessary.
- Inspect for eroded areas. Determine cause of erosion and correct deficiency as required. Monitor repaired areas.

## Page 4 of 4

## **RIP RAP OUTLETS**

*Function* – Rip rap outlets slow the velocity of runoff, minimizing erosion and maximizing the treatment capabilities of associated buffers. Vegetated buffers, either forested or meadow, slow runoff which promotes and reduces peak rates of runoff. The reduced velocities and the presence of vegetation encourage the filtration of sediment and the limited bio-uptake of nutrients.

Maintenance

- Inspect level spreaders and buffers at least annually for signs of erosion, sediment buildup, or vegetation loss.
- Inspect level for signs of condensed flows. Level spreader and rip rap shall be maintained to disperse flows evenly over level spreader.
- If a meadow buffer, provide periodic mowing as needed to maintain a healthy stand of herbaceous vegetation.
- If a forested buffer, then the buffer should be maintained in an undisturbed condition, unless erosion occurs.
- If erosion of the buffer (forested or meadow) occurs, eroded areas should be repaired and replanted with vegetation similar to the remaining buffer. Corrective action should include eliminating the source of the erosion problem and may require retrofit or reconstruction of the level spreader.
- Remove debris and accumulated sediment and dispose of properly.

## **GENERAL CLEAN UP**

- Upon completion of the project, the contractor shall remove all temporary stormwater structures (i.e., temporary stone check dams, silt fence, temporary diversion swales, catch basin inlet filter, etc.). Any sediment deposits remaining in place after the silt fence or filter barrier is no longer required shall be dressed to conform to the existing grade, prepared, and seeded. Remove any sediment in catch basins and clean drain pipes that may have accumulated during construction.
- Once in operation, all paved areas of the site should be swept at least once annually at the end of winter/early spring prior to significant spring rains.

## APPPENDIX

- A. Stormwater System Operations and Maintenance Report
- B. Site Grading and Drainage Plan

## STORM WATER SYSTEM OPERATION AND MAINTENANCE REPORT

General Information					
Project Name					
Owner					
Inspector's Name(s)					
Inspector's Contact Information					
Date of Inspection			Start Time:	End Time:	
Type of Inspection:         Annual Report       Post-storm event         Due to a discharge of significant amounts of sediment					
Notes:					

General Site Questions and Discharges of Significant Amounts of Sediment						
Subject		Status	Notes			
A d	A discharge of significant amounts of sediment may be indicated by (but is not limited to) observations of the following.					
Not	Note whether any are observed during this inspection:					
	Notes/ Action taken:					
1	Do the current site conditions reflect	□Yes				
	the attached site plan?	□No				
2	Is the site permanently stabilized,	□Yes				
	temporary erosion and sediment	□No				
	controls are removed, and stormwater					
	discharges from construction activity					
	are eliminated?					
3	Is there evidence of the discharge of	□Yes				
	significant amounts of sediment to	□No				
	surface waters, or conveyance					
	systems leading to surface waters?					

Permit Coverage and Plans						
#	BMP/Facility	Inspected	Corrective Action Needed and Notes	Date Corrected		
	Grassed Underdrained Soil Filters	□Yes □No				
	Catch Basins	□Yes □No				
	Drainage Pipes	□Yes □No				
	Riprap Aprons	□Yes □No				
		□Yes □No				
		□Yes □No				
		□Yes □No				



# Section 10

# Watershed Plans

Pre-Development Drainage Area Plan Post-Development Drainage Area Plan









## TRAFFIC IMPACT STUDY PROPOSED FOOD MANUFACTURING FACILITY KITTERY, MAINE

July 22, 2021

**Prepared For:** 

Altus Engineering, Inc. 133 Court Street Portsmouth, NH 03801

Prepared by:





ATFC Company

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## **INTRODUCTION**

The purpose of this report is to summarize a traffic impact study performed by James W. Sewall Company (Sewall) for a proposed specialty food manufacturing facility, Good to Go, to be located off Route 1 in Kittery, Maine. The site location, on the easterly side of Route 1 is located is between Landmark Hill Lane and Parson's Lane, as shown on the map in Figure 1. The facility will be 20,000 square feet (S.F.) in size and will employ 30 persons. Access to the site will be provided by a single full-movement access drive to Route 1.

This report details the traffic analysis which determines the expected number of trips to be generated by the manufacturing facility and any off-site impacts on level of service or safety for the local Town of Kittery approval process.

It is understood that construction is expected to begin in fall of 2021 with completion and occupancy planned for summer 2022. Hence, 2022 was selected as the study year for traffic analysis puposes.

## **TRIP GENERATION ANALYSIS**

The number of trips to be generated by the proposed manufacturing facility was estimated utilizing the latest Institute of Transportation Engineers (ITE) "Trip Generation, 10<sup>th</sup> edition". Land use code (LUC) 140 – Manufacturing was utilized on the basis of both 20,000 S.F. and 30 employees. The results are summarized below:

	ITE TRIP GENERATION		
Time Period	<u>S.F.</u>	<u>Employees</u>	<u>Average</u>
Weekday	80	74	78
AM Peak Hour – Adjacent Street	13	11	12
Entering	10	8	9
Exiting	3	3	3
AM Peak Hour – Generator	16	13	15
Entering	12	11	12
Exiting	4	2	3
PM Peak Hour – Adjacent Street	14	10	12
Entering	4	4	4
Exiting	10	6	8
PM Peak Hour – Generator	16	14	15
Entering	7	6	6
Exiting	9	8	9
The results were similar on both the square footage and employee bases so they were averaged together to best estimate trips. These results show that the proposed manufacturing facility is expected to generate 78 one-way trips (39 round-trips) on a daily basis. Twelve one-way trips are projected for the AM and PM peak hours of the adjacent street system. Fifteen one-way trips will be generated during the peak hours of the facility. This level of traffic would not be expected to have a significant impact off-site on traffic operations beyond the site drives.

However, to assess level of service to meet the requirements of the Kittery ordinances, traffic analysis was conducted for the site drive intersection to demonstrate level of service.

### **TRAFFIC VOLUMES**

Turning movement/classification counts were conducted by Sewall during the weekday AM (7:00 – 9:00) and PM peak hour periods (3:00- 6:00) on June 3, 2021 at the intersection of Route 1 and Landmark Hill Lane to determine existing volumes and traffic patterns. The AM peak hour occurred from 8:00 to 9:00 while the PM peak hour occurred from 3:45 – 4:45. The counts were factored to 30<sup>th</sup> highest hour conditions using MaineDOT group mean factors. These volumes typically occur under peak summer conditions in July and August in Maine. The results are shown in Figure 2. The PM peak hour volumes are 40 % higher than the AM peak hour volumes. Given this and the similar site trip generation during both peak hours, the PM peak hour was selected as the analysis period, when the additional trips are expected to have the greatest impact.

Existing average annual daily traffic (AADT) data for the area was obtained from "Traffic Volume Counts, 2019 and 2014 Annual Reports", published by MaineDOT. This data is summarized in the following table:

	Average	Annual	Daily Traf	fic
Location Description	<u>2010</u>	<u>2013</u>	<u>2016</u>	<u>2019</u>
Route 1, northeast of Cutts Road	11,340			10,550
Route 1, northeast of Haley Road	12,330	10,940	10,260	10,780
Route 1, southwest of Beechridge Road in York	11,450	9 <i>,</i> 370	9,490	9,440

As seen above, traffic volumes have generally been declining along this section of Route 1 over the period 2010 to 2019. As a result, a conservative ½ % annual traffic growth rate was utilized to project the 2021 volumes to base 2022 conditions.

The Town of Kittery Planner was contacted to determine if there are any other approved (but unbuilt) developments, expected to significantly impact future Route 1 volumes in the area, which should be considered in the traffic analysis. The only other development project identified is the Homestead Subdivision project, which is located on Route 1 opposite Lewis Road. The trips to be generated by this development were obtained from the Traffic Impact study prepared by Maine Traffic Resources (now Sewall) and dated 9/7/2018. Those other development volumes expected to be passing by the site during the PM peak hour are shown in Figure 3. The resulting 2022 No Build volumes, allowing for 1/2 % annual traffic growth and the Homestead Subdivision to be fully occupied, are shown in Figure 4.

The trip assignments for the manufacturing facility were assigned based upon the travel patterns recorded during the counts. The resulting trip assignments are shown in Figure 5. Based upon the trip assignments the facility is expected to have a minimal impact on offsite traffic operations. Generally, a project won't have an impact on traffic operations unless it generates in excess of twenty-five (25) lane hour trips. Based upon the trip assignments, the manufacturing facility will generate just four (4) lane hour trips during the PM peak hour analysis period. Given these trip assignments the study area would be limited to the site drive intersection but it was extended southerly through the intersection of Landmark Hill Lane to evaluate impact on nearby intersections. Lastly, the projected Build 2022 volumes are shown in Figure 6.

### **CAPACITY ANALYSIS**

Traffic operations are evaluated in terms of level of service (LOS). Level of service is a qualitative measure that describes operations by letter designation. The levels range from A - very little delay to F - extreme delays. Level of service "D" is generally considered acceptable in urban locations while LOS "E" is generally considered the capacity of a facility and the minimum tolerable level. The level of service for unsignalized intersections is based upon average control delay per vehicle for each minor, opposed movement, as defined in the following table excerpted from the 2010 "Highway Capacity Manual":

#### **Unsignalized Intersection Level of Service**

LOS	<u>Delay Range</u>
А	< = 10.0 seconds
В	> 10.0 and <= 15.0
С	> 15.0 and <= 25.0
D	> 25.0 and <= 35.0
E	> 35.0 and <= 50.0
F	> 50.0

### **UNSIGNALIZED INTERSECTION ANALYSIS**

The level of service (LOS) was determined for the unsignalized study area intersection for existing 2021 and projected 2022 conditions using Synchro 10 and SimTraffic. The results are provided in the appendix and are summarized in the following tables:

	Route 1 PM Peak	& Landmark H Hour Level of	lill Lane f Service
Approach/Movement	Existing <u>2021</u>	No Build <u>2022</u>	Build <u>2022</u>
Westbound Landmark Hill Lane	A (6.5)	A (8.1)	A (9.3)
Northbound Route 1	A (1.2)	A (1.2)	A (1.3)
Southbound Route 1	A (0.3)	A (0.3)	A (0.4)
Overall Intersection	A (0.8)	A (0.9)	A (1.0)

As seen above, Landmark Hill Lane currently operates at a good LOS "A" during the PM peak hour with no significant delay. The same LOS is expected in 2022 allowing for ½ % annual traffic growth and the Homestead Subdivision project. Lastly under projected build volumes, with the Good to Go facility fully occupied, it will continue to operate at LOS "A" with no capacity concerns. The increase in delay from No Build to Build conditions is negligible at 0.10 second demonstrating the minimal impact of the project on traffic operations off-site.

Approach/Movement	Route 1 & Site Drive PM Peak Hour Level of Service Build <u>2022</u>
Westbound Site Drive	A (6.5)
Northbound Route 1	A (0.3)
Southbound Route 1	A (0.8)
Overall Intersection	A (0.6)

As seen above, there are also no capacity concerns at the unsignalized site drive intersection, which will also function at a very good LOS "A" in 2022 under full Build volumes.

# SAFETY ANAYSIS ACCIDENT REVIEW

The Maine Department of Transportation uses two criteria to determine high crash locations (HCLs). The first is the critical rate factor (CRF), which is a measure of the accident rate. A CRF greater than one indicates a location which has a higher than expected crash rate. The expected rate is calculated as a statewide average of similar facilities.

The second criterion, which must also be met, is based upon the number of accidents that occur at a particular location. Eight or more accidents must occur over the three-year study period for the location to be considered a high crash location.

The MaineDOT Map Viewer was reviewed for high crash locations in the vicinity of the site for the most recent 3-year period (2018 – 2020). There are no high crash locations along Route 1 from Cutts Road in Kittery northerly to the intersection of Beech Ridge Road and Southside Road in York. As a result, no additional accident review or evaluation is necessary.

## **DRIVEWAY SIGHT DISTANCE**

One of the most important safety factors to consider for a project is sight distance from the access drives. This sight distance is measured ten feet back from the edge of travel way at a driver's eye height of 3.5 feet to an object height of 4.25 feet. Sewall recommends a minimum sight distance of 450 feet for the posted 45 mile per hour speed limit on this segment of Route 1. The Kittery ordinance also requires 450' of sight distance while MaineDOT Entrance Rules require a lesser 425'.

Sewall field checked the sight distances from the proposed drive location and found it exceeds 500' to the left (south) and was approximately 450' to the right (north). Altus Engineering prepared a sight distance analysis, shown on their Highway Access Plan provided in this study, which confirms that the sight distance to the right exceeds 450'. Hence, sight distance will be adequate to provide for safe access. It is important that no signage or landscaping be located in the driveway sight triangle which could obscure or limit the driveway sight distances in the future.

### **SUMMARY AND RECOMMENDATIONS**

The proposed specialty food manufacturing facility is expected to generate between 12 and 15 one-way trips during peak hours. Based upon both trip generation results and the peak hour volumes, the weekday PM peak hour of the adjacent street was selected as the analysis period. Also based upon the trip assignments, the study area for capacity purposes was defined as extending from the site drive through the intersection of Landmark Hill Lane to evaluate off-site impact.

In terms of capacity, the unsignalized intersection of Landmark Hill Lane currently operates at a good level of service "A" during the weekday PM peak hour. Under projected Build volumes the LOS will remain at this level with no capacity concerns. The site drive is also expected to operate at LOS "A", again showing no capacity concerns.

In terms of safety, there are no high crash locations within an extended study area so no further accident review or evaluation is necessary. Sight distances from the proposed site drive exceed the recommended standard providing for safe access. It is important that no signage or landscaping be located in the sight triangle which could obstruct driveway sight distance in the future.



Site Location Map Kittery Food Manufacturing Kittery, Maine













# APPENDIX

Turning Movement Counts Capacity Analysis Highway Access Plan

40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill Road TOWN: Kittery, ME COUNTER: WD WEATHER: Sun/clouds File Name : KitteryLandmarkHill1AM2021 Site Code : 00000000 Start Date : 6/3/2021 Page No : 1

					Grou	ps Pri	inted-	Pass	enger	Vehicle	es - Li	ight Ti	rucks	- Heav	vy Truc	ks					
			Route	1			Lan	dmar	k Hill				Route	1	-		Lan	dmar	k Hill		
		So	uthbo	und			W	estbo	und			No	rthbo	und			Ea	astbo	und		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
07:00 AM	0	52	0	0	52	0	0	0	0	0	0	48	0	0	48	0	0	0	0	0	100
07:15 AM	0	55	0	0	55	0	0	0	1	1	0	50	0	0	50	0	0	0	0	0	106
07:30 AM	0	67	3	0	70	0	0	0	0	0	6	70	0	0	76	0	0	0	0	0	146
07:45 AM	0	75	4	0	79	0	0	0	1	1	8	59	0	0	67	0	0	0	0	0	147
Total	0	249	7	0	256	0	0	0	2	2	14	227	0	0	241	0	0	0	0	0	499
08:00 AM	0	70	4	0	74	1	0	0	0	1	5	82	0	0	87	0	0	0	0	0	162
08:15 AM	0	76	4	0	80	0	0	0	0	0	1	78	0	0	79	0	0	0	0	0	159
08:30 AM	0	96	3	0	99	1	0	1	0	2	2	85	0	0	87	0	0	0	0	0	188
08:45 AM	0	93	6	0	99	0	0	1	0	1	3	81	0	0	84	0	0	0	0	0	184
Total	0	335	17	0	352	2	0	2	0	4	11	326	0	0	337	0	0	0	0	0	693
Grand Total	0	584	24	0	608	2	0	2	2	6	25	553	0	0	578	0	0	0	0	0	1192
Apprch %	0	96.1	3.9	0		33.3	0	33.3	33.3		4.3	95.7	0	0		0	0	0	0		
Total %	0	49	2	0	51	0.2	0	0.2	0.2	0.5	2.1	46.4	0	0	48.5	0	0	0	0	0	
Passenger Vehicles																					
% Passenger Vehicles	0	95.2	100	0	95.4	100	0	100	100	100	96	91.5	0	0	91.7	0	0	0	0	0	93.6
Light Trucks																					
% Light Trucks	0	4.5	0	0	4.3	0	0	0	0	0	0	6.5	0	0	6.2	0	0	0	0	0	5.2
Heavy Trucks	0	2	0	0	2	0	0	0	0	0	1	11	0	0	12	0	0	0	0	0	14
% Heavy Trucks																					

40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill Road TOWN: Kittery, ME COUNTER: WD WEATHER: Sun/clouds File Name : KitteryLandmarkHill1AM2021 Site Code : 00000000 Start Date : 6/3/2021 Page No : 2

		ļ	Route	1			Lan	dmar	k Hill				Route	1			Lan	dmar	k Hill		
		So	uthbo	und			W	estbo	und			No	rthbo	und			Ea	astbo	und		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour A	Analysi	s From	n 07:00	O AM to	o 08:45	AM - F	Peak 1	of 1													
Peak Hour for	or Enti	re Inte	rsectio	on Beg	ins at 0	8:00 A	M														
08:00 AM	0	70	4	0	74	1	0	0	0	1	5	82	0	0	87	0	0	0	0	0	162
08:15 AM	A 0 76 4 0 80 0 0 0 0 0 1 78 0 0 79 0 0 0 0 0										0	159									
08:30 AM	0	96	3	0	99	1	0	1	0	2	2	85	0	0	87	0	0	0	0	0	188
08:45 AM	0	93	6	0	99	0	0	1	0	1	3	81	0	0	84	0	0	0	0	0	184
Total Volume	0	335	17	0	352	2	0	2	0	4	11	326	0	0	337	0	0	0	0	0	693
% App. Total	0	95.2	4.8	0		50	0	50	0		3.3	96.7	0	0		0	0	0	0		
PHF	.000	.872	.708	.000	.889	.500	.000	.500	.000	.500	.550	.959	.000	.000	.968	.000	.000	.000	.000	.000	.922
Passenger Vehicles																					
% Passenger Vehicles	0	95.2	100	0	95.5	100	0	100	0	100	100	91.4	0	0	91.7	0	0	0	0	0	93.7
Light Trucks																					
% Light Trucks	0	4.8	0	0	4.5	0	0	0	0	0	0	6.4	0	0	6.2	0	0	0	0	0	5.3
Heavy Trucks	0	0	0	0	0	0	0	0	0	0	0	7	0	0	7	0	0	0	0	0	7
% Heavy Trucks																					



40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill Road TOWN: Kittery, ME COUNTER: WD WEATHER: Sun/clouds File Name : KitteryLandmarkHill1AM2021 Site Code : 00000000 Start Date : 6/3/2021 Page No : 3

40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill TOWN: Kittery, ME COUNTER: WD WEATHER: Sun/clouds File Name : KitteryLandmarkHill1PM2021 Site Code : 00000000 Start Date : 6/3/2021 Page No : 1

					Grou	ps Pr	inted-	Pass	enger	Vehicl	es - L	ight Ti	rucks	- Heav	vy Truc	ks					
			Route	1			Lan	dmar	k Hill			- 1	Route	1	-						
		So	uthbo	ound			W	estbo	und			No	<u>rthb</u> o	und			Ea	astbo	und		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
03:00 PM	0	103	0	0	103	0	0	0	0	0	7	126	0	0	133	0	0	0	0	0	236
03:15 PM	0	95	4	0	99	2	0	1	0	3	3	115	0	0	118	0	0	0	0	0	220
03:30 PM	0	94	4	0	98	3	0	2	0	5	5	134	0	0	139	0	0	0	0	0	242
03:45 PM	0	87	2	0	89	1	0	2	0	3	3	120	0	0	123	0	0	0	0	0	215
Total	0	379	10	0	389	6	0	5	0	11	18	495	0	0	513	0	0	0	0	0	913
04:00 PM	0	103	0	0	103	4	0	2	0	6	2	116	0	0	118	0	0	0	0	0	227
04:15 PM	0	102	3	0	105	0	0	2	1	3	0	145	0	0	145	0	0	0	0	0	253
04:30 PM	0	130	4	0	134	1	0	1	0	2	2	135	0	0	137	0	0	0	0	0	273
04:45 PM	0	96	1	0	97	3	0	0	0	3	0	110	0	0	110	0	0	0	0	0	210
Total	0	431	8	0	439	8	0	5	1	14	4	506	0	0	510	0	0	0	0	0	963
05:00 PM	0	85	3	0	88	3	0	0	0	3	1	101	0	0	102	0	0	0	0	0	193
05:15 PM	0	106	0	0	106	1	0	0	0	1	3	105	0	0	108	0	0	0	0	0	215
05:30 PM	0	70	2	0	72	0	0	0	0	0	3	102	0	0	105	0	0	0	0	0	177
05:45 PM	0	81	0	0	81	2	0	0	0	2	3	121	0	0	124	0	0	0	0	0	207
Total	0	342	5	0	347	6	0	0	0	6	10	429	0	0	439	0	0	0	0	0	792
Grand Total	0	1152	23	0	1175	20	0	10	1	31	32	1430	0	0	1462	0	0	0	0	0	2668
Apprch %	0	98	2	0		64.5	0	32.3	3.2		2.2	97.8	0	0		0	0	0	0		
Total %	0	43.2	0.9	0	44	0.7	0	0.4	0	1.2	1.2	53.6	0	0	54.8	0	0	0	0	0	
Passenger Vehicles		1135										1397									
% Passenger Vehicles	0	98.5	100	0	98.6	100	0	100	100	100	93.8	97.7	0	0	97.6	0	0	0	0	0	98.1
Light Trucks																					
% Light Trucks	0	1	0	0	1	0	0	0	0	0	6.2	2	0	0	2.1	0	0	0	0	0	1.6
Heavy Trucks	0	5	0	0	5	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	9
% Heavy Trucks																					

40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill TOWN: Kittery, ME COUNTER: WD WEATHER: Sun/clouds File Name : KitteryLandmarkHill1PM2021 Site Code : 00000000 Start Date : 6/3/2021 Page No : 2

		F	Route	1			Lan	dmar	k Hill				Route	1							
		So	uthbo	und			W	estbo	und			No	rthbo	und			Ea	astbou	und		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour A	Analysi	s From	n 03:00	D PM to	05:45	PM - F	Peak 1	of 1													
Peak Hour for	or Enti	re Inte	rsectic	on Begi	ins at 0	3:45 P	M														
03:45 PM	0	87	2	0	89	1	0	2	0	3	3	120	0	0	123	0	0	0	0	0	215
04:00 PM	<i>I</i> 0 103 0 0 103 <b>4</b> 0 2 0 <b>6</b> 2 116 0 0 118 0 0 0 0 0										227										
04:15 PM	O 102 3 0 145 0 <td>0</td> <td>253</td>										0	253									
04:30 PM	0	130	4	0	134	1	0	1	0	2	2	135	0	0	137	0	0	0	0	0	273
Total Volume	0	422	9	0	431	6	0	7	1	14	7	516	0	0	523	0	0	0	0	0	968
% App. Total	0	97.9	2.1	0		42.9	0	50	7.1		1.3	98.7	0	0		0	0	0	0		
PHF	.000	.812	.563	.000	.804	.375	.000	.875	.250	.583	.583	.890	.000	.000	.902	.000	.000	.000	.000	.000	.886
Passenger Vehicles																					
% Passenger Vehicles	0	98.1	100	0	98.1	100	0	100	100	100	100	96.1	0	0	96.2	0	0	0	0	0	97.1
Light Trucks																					
% Light Trucks	0	1.2	0	0	1.2	0	0	0	0	0	0	3.3	0	0	3.3	0	0	0	0	0	2.3
Heavy Trucks	0	3	0	0	3	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	6
% Heavy Trucks																					



40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill TOWN: Kittery, ME COUNTER: WD WEATHER: Sun/clouds File Name : KitteryLandmarkHill1PM2021 Site Code : 00000000 Start Date : 6/3/2021 Page No : 3

		50	Route	1			Lan	dmar	k Hill und			No	Route	1 und			F	etho	und		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	Ann Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App Total	Int Total
Peak Hour A	Analysi	s Fror	n 03:0	0 PM to	0 05:45	PM - F	Peak 1	of 1		APP. TUIdl	,gin			. 545	App. Total	·gin				App. Total	an. Tutdl
Peak Hour f	or Eacl	h App	roach l	Begins	at:																
	04:00 PM					03:15 PM	-				03:30 PN	1				03:00 PN					
+0 mins.	0	103	0	0	103	2	0	1	0	3	5	134	0	0	139	0	0	0	0	0	
+15 mins.	0	102	3	0	105	3	0	2	0	5	3	120	0	0	123	0	0	0	0	0	
+30 mins. +45 mins		96	4	0	97	4	0	2	0	ა 6		145	0	0	145	0	0	0	0	0	
Total Volume	0	431	8	0	439	10	0	7	0	17	10	515	0	0	525	0	0	0	0	0	
% App. Total	0	98.2	1.8	0		58.8	0	41.2	0		1.9	98.1	0	0		0	0	0	0		
PHF	.000	.829	.500	.000	.819	.625	.000	.875	.000	.708	.500	.888	.000	.000	.905	.000	.000	.000	.000	.000	
Passenger Vehicles		00										06									
% Passenger Vehicles	0	90. 1	100	0	98.2	100	0	100	0	100	90	90. .3	0	0	96.2	0	0	0	0	0	
Light Trucks	0	5	0	0	5	0	0	0	0	0	1	16	0	0	17	0	0	0	0	0	
% Light Trucks	0	1.2	Ō	Ō	1.1	0	Ō	Ō	Ō	Ő	10	3.1	Ő	Ō	3.2	0	Ō	Ō	Ō	Ō	
Heavy Trucks	0	3	0	0	3	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	
% Heavy Trucks																					
		ſ							In - P	Route eak Hou	e 1 <u>:</u> 04:00	PM									
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#### Summary of All Intervals

Run Number	1	2	3	4	5	Avg	
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	
End Time	8:00	8:00	8:00	8:00	8:00	8:00	
Total Time (min)	70	70	70	70	70	70	
Time Recorded (min)	60	60	60	60	60	60	
# of Intervals	2	2	2	2	2	2	
# of Recorded Intervals	1	1	1	1	1	1	
Vehs Entered	1198	1172	1164	1155	1258	1190	
Vehs Exited	1193	1166	1157	1145	1259	1185	
Starting Vehs	14	9	11	11	14	12	
Ending Vehs	19	15	18	21	13	17	
Travel Distance (mi)	637	623	619	609	673	632	
Travel Time (hr)	15.3	15.0	14.8	14.7	16.3	15.2	
Total Delay (hr)	1.0	0.9	0.9	0.9	1.0	0.9	
Total Stops	19	11	17	16	22	17	
Fuel Used (gal)	17.0	16.4	16.5	16.2	17.8	16.8	

#### Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Volumes adjusted by Grow	vth Factors.
No data recorded this inter	rval.

#### Interval #1 Information Recording

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	1	2	3	4	5	Avg	
Vehs Entered	1198	1172	1164	1155	1258	1190	
Vehs Exited	1193	1166	1157	1145	1259	1185	
Starting Vehs	14	9	11	11	14	12	
Ending Vehs	19	15	18	21	13	17	
Travel Distance (mi)	637	623	619	609	673	632	
Travel Time (hr)	15.3	15.0	14.8	14.7	16.3	15.2	
Total Delay (hr)	1.0	0.9	0.9	0.9	1.0	0.9	
Total Stops	19	11	17	16	22	17	
Fuel Used (gal)	17.0	16.4	16.5	16.2	17.8	16.8	

#### 3: Route 1 & Landmark Hill Lane Performance by lane

Lane	WB	NB	SB	All	
Movements Served	LR	TR	LT		
Denied Del/Veh (s)				0.3	
Total Del/Veh (s)	6.5	1.2	0.3	0.8	

#### Intersection: 3: Route 1 & Landmark Hill Lane

Movement	WB	NB	SB
Directions Served	LR	TR	LT
Maximum Queue (ft)	35	6	44
Average Queue (ft)	9	0	5
95th Queue (ft)	33	4	24
Link Distance (ft)	546	1435	172
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

#### Summary of All Intervals

Run Number	1	2	3	4	5	Avg	
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	
End Time	8:00	8:00	8:00	8:00	8:00	8:00	
Total Time (min)	70	70	70	70	70	70	
Time Recorded (min)	60	60	60	60	60	60	
# of Intervals	2	2	2	2	2	2	
# of Recorded Intervals	1	1	1	1	1	1	
Vehs Entered	1341	1317	1240	1209	1203	1263	
Vehs Exited	1347	1302	1242	1197	1197	1257	
Starting Vehs	22	8	20	9	11	14	
Ending Vehs	16	23	18	21	17	19	
Travel Distance (mi)	708	688	651	630	631	662	
Travel Time (hr)	17.1	16.8	15.6	15.2	15.1	16.0	
Total Delay (hr)	1.1	1.2	1.0	1.0	0.9	1.0	
Total Stops	18	16	20	18	18	18	
Fuel Used (gal)	18.7	18.4	17.5	16.7	16.8	17.6	

#### Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Volumes adjusted by Grow	wth Factors.
No data recorded this inte	erval.

### Interval #1 Information Recording

Volumes adjusted by Growth Factors.

Run Number	1	2	3	4	5	Avg	
Vehs Entered	1341	1317	1240	1209	1203	1263	
Vehs Exited	1347	1302	1242	1197	1197	1257	
Starting Vehs	22	8	20	9	11	14	
Ending Vehs	16	23	18	21	17	19	
Travel Distance (mi)	708	688	651	630	631	662	
Travel Time (hr)	17.1	16.8	15.6	15.2	15.1	16.0	
Total Delay (hr)	1.1	1.2	1.0	1.0	0.9	1.0	
Total Stops	18	16	20	18	18	18	
Fuel Used (gal)	18.7	18.4	17.5	16.7	16.8	17.6	

#### 3: Route 1 & Landmark Hill Lane Performance by lane

Lane	WB	NB	SB	All	
Movements Served	LR	TR	LT		
Denied Del/Veh (s)				0.3	
Total Del/Veh (s)	8.1	1.2	0.3	0.9	

#### Intersection: 3: Route 1 & Landmark Hill Lane

Movement	WB	NB	SB
Directions Served	LR	TR	LT
Maximum Queue (ft)	40	11	59
Average Queue (ft)	10	0	5
95th Queue (ft)	34	8	28
Link Distance (ft)	546	1435	171
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

#### Summary of All Intervals

Run Number	1	2	3	4	5	Avg	
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	
End Time	8:00	8:00	8:00	8:00	8:00	8:00	
Total Time (min)	70	70	70	70	70	70	
Time Recorded (min)	60	60	60	60	60	60	
# of Intervals	2	2	2	2	2	2	
# of Recorded Intervals	1	1	1	1	1	1	
Vehs Entered	1185	1273	1232	1245	1291	1246	
Vehs Exited	1186	1276	1229	1240	1283	1242	
Starting Vehs	15	17	14	12	10	13	
Ending Vehs	14	14	17	17	18	15	
Travel Distance (mi)	632	680	659	664	689	665	
Travel Time (hr)	15.2	16.6	15.9	16.1	16.7	16.1	
Total Delay (hr)	1.0	1.2	1.0	1.1	1.2	1.1	
Total Stops	30	36	25	27	28	29	
Fuel Used (gal)	17.0	18.3	17.5	17.8	18.4	17.8	

### Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Volumes adjusted by Gro	owth Factors.
No data recorded this int	erval.

#### Interval #1 Information Recording

Start Time	7.00
	1.00
End Time	0.00
	0.00
Total Time (min)	60
rotar rime (min)	00

Volumes adjusted by Growth Factors.

Run Number	1	2	3	4	5	Avg	
Vehs Entered	1185	1273	1232	1245	1291	1246	
Vehs Exited	1186	1276	1229	1240	1283	1242	
Starting Vehs	15	17	14	12	10	13	
Ending Vehs	14	14	17	17	18	15	
Travel Distance (mi)	632	680	659	664	689	665	
Travel Time (hr)	15.2	16.6	15.9	16.1	16.7	16.1	
Total Delay (hr)	1.0	1.2	1.0	1.1	1.2	1.1	
Total Stops	30	36	25	27	28	29	
Fuel Used (gal)	17.0	18.3	17.5	17.8	18.4	17.8	

#### 3: Route 1 & Landmark Hill Lane Performance by lane

Lane	WB	NB	SB	All
Movements Served	LR	TR	LT	
Denied Del/Veh (s)				0.3
Total Del/Veh (s)	9.3	1.3	0.4	1.0

#### 4: Route 1 & Site Drive Performance by lane

Lane	WB	NB	SB	All
Movements Served	LR	TR	LT	
Denied Del/Veh (s)				0.2
Total Del/Veh (s)	6.5	0.3	0.8	0.6

### **Total Network Performance**

Denied Del/Veh (s)	0.5	
Total Del/Veh (s)	2.7	

#### Intersection: 3: Route 1 & Landmark Hill Lane

Movement	WB	SB
Directions Served	LR	LT
Maximum Queue (ft)	35	74
Average Queue (ft)	13	6
95th Queue (ft)	37	34
Link Distance (ft)	546	171
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

#### Intersection: 4: Route 1 & Site Drive

Movement	WB	SB
Directions Served	LR	LT
Maximum Queue (ft)	31	25
Average Queue (ft)	8	1
95th Queue (ft)	29	11
Link Distance (ft)	416	1133
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

#### Network Summary

Network wide Queuing Penalty: 0

