

Civil Site Planning Environmental Engineering

133 Court Street Portsmouth, NH 03801-4413

July 22, 2021

Kittery Planning Board 200 Rogers Road Kittery, Maine 03904

Re: Site Plan Review and Right of Way Applications

Good To-Go 524 U.S. Route 1 Kittery, Maine

Dear Members of the Board,

On behalf of the applicant, C-Coast Properties and Good To-Go c/o Cape House Management, LLC, we respectfully submit Site Plan Review and Right of Way applications for property located at 524 U.S. Route 1. The property currently hosts a residential dwelling and is primarily wooded except for a few small sections of meadow around the existing house. The applications contemplate the construction of a public right of way to access a private site consisting of a 20,000 sf specialty food manufacturing facility. Good To-Go, a Kittery-based company currently located at 484 U.S. Route 1, makes dehydrated foods for hiking, camping and other outdoor activity. With this new facility, they anticipate being able to quadruple production to meet explosive demand for their award-winning creations.

If you have any questions or need additional information, please contact us. Thank you for your time and consideration.

Sincerely,

ALTUS ENGINEERING, INC.

Erik B. Saari Vice President

ebs/5116-00-CoverLetter-072221

Enclosures

Tel: (603) 433-2335 E-mail: Altus@altus-eng.com



TOWN OF KITTERY, MAINE TOWN PLANNING AND DEVELOPMENT DEPARTMENT

200 Rogers Road, Kittery, Maine 03904 PHONE: (207) 475-1323 - FAX: (207) 439-6806 www.kittery.org

APPLICATION: SITE PLAN REVIEW

					\$50/USE OF UNIT; OR			, ,	•	00 SQ FT OF GROSS AREA \$1,000		Application	ate:
FEE FO SITE PLA REVIEW	AN	\$300. 00 THE GR OF	EATER	\$0.50/LINEAR FOOT OF DOCK, SLIP & FLOAT; OR				PROV	IDE	NIT INTENDED TO OVERNIGHT SLEEPIN ODATIONS	IG	ASA Fee Po	
PROPERTY DESCRIPTION		Parcel ID	Map	67	Lot	1		Zone: Base: Overlay: MS4:		YES _XNO		al Land Area uare Feet)	1,040,714 sf (23.89 acres)
		Physical Address	524 l	J.S. Ro	ute 1								
PROPERTY	,	Name		ast Prop		LLC			8	Banks Rock			
OWNER'S INFORMATION		Phone Fax						Mailing Address		ork, Maine 03911			
Email			kevin	kevinwerikson@gmail.com									
		Name	Erik S	aari				me of iness	Α	Itus Engineering,	Inc.		
APPLICAN' AGENT	T'S	Phone	(603) 433-2335										
INFORMAT	TION	Fax					Mailing Address						
		Email	esaar	esaari@altus-eng.com									
	Existing	Use: The	site cu	rrently h	osts a	single-far	nily	residence	and	d some sections o	of fie	ld with the re	emainder
		of th	e site b	eing w	oded.								
7													
TION													
SCRIF	Project	Name: G	ood To	o-Go									
r DE	Propose	ed Use: S	pecialt	y Food	Facility	/							
Project Name: Good To-Go Proposed Use: Specialty Food Facility 20,000 sf building with as					associate	d pa	arking and	inf	rastructure				
PR(

REV. 6-2014 Page **1** of **9**

WAIVER REQUEST

Ordinance Section	Describe why this request is being made.
EXAMPLE 16.32.560 (B)- OFFSTREET PARKING.	***EXAMPLE*** Requesting a waiver of this ordinance since the proposed professional offices have a written agreement with the abutting Church owned property to share parking.
	See attached Waiver Request Letter
	EXAMPLE 16.32.560 (B)- OFFSTREET

Related Kittery Land Use Code concerning waivers and modifications:

16.10.8.2.5 Conditions or Waivers.

Conditions required by the Planning Board at the final plan review phase must have been met before the final plan may be given final approval unless so specified in the condition or specifically waived, upon written request by the applicant, by formal Planning Board action wherein the character and extent of such waivers which may have been requested are such that they may be waived without jeopardy to the public health, safety and general welfare.

16.7.4.1 Objectives Met. In granting modifications or waivers, the Planning Board must require such conditions as will, in its judgment, substantially meet the objectives of the requirements so waived or modified.

I certify that, to the best of my knowledge, the information provided in this application is true and correct and will not deviate from						
the plans submitted without notifying the Kittery Planning Department of any changes.						
Applicant's	23: 6	Owner's	See attached LOA			
Signature: Date:	07/22/21	Signature: Date:	07/22/21			

COMPLETED BY OFFICE STAFF

ASA CHARGE		AMOUNT	ASA CHARGE	AMOUNT
REVIEW			SERVICES	
LEGAL FEES	ΓBD)		RECORDER	\$35
ENGINEERS REVIEW	TBD)		FACT FINDING (TBD)	
ABUTTER NOTICES			3 RD PARTY INSPECTIONS (TBD)	
Postage		\$20	OTHER PROFESSIONAL SERVICES	\$50
LEGAL NOTICES			PERSONNEL	
ADVERTISING		\$300	SALARY CHARGES IN EXCESS OF 20 HOURS	
SUPPLIES				
OFFICE		\$5		
SUB	TOTAL		SUB TOTAL	
			TOTAL ASA REVIEW FEES	

REV. 6-2014 Page **2** of **9**



TOWN OF KITTERY MAINE TOWN PLANNING DEPARTMENT

200 Rogers Road, Kittery, Maine 03904 PHONE: (207) 475-1323 Fax: (207) 439-6806 www.kittery.org

APPLICATION: RIGHT-OF WAY PLAN REVIEW (APPLICABLE FOR A SINGLE LOT)

FEE FOR REVIEW		1	□ \$3	00.00		Am	ount Paid:	\$	Date: _			
PROP DESC	ERTY RIPTION	Parcel ID	Мар	67	Lot	1	Zone(S): Base Overlay MS4	YESXNO	Total Land Area	1,040,714 sf (23.86 acres)		
		Physical Address	524 L	J.S. Ro	ute 1							
		Name	C-Coa	ıst Prop	erties	, LLC						
PROP OWN		Phone	(207)	321-95	69		Mailing	8 Banks Rock				
	RMATION	Fax	,				Address	York, Maine 03911	York, Maine 03911			
		Email	keviny	verikso	n@gm	nail.com						
		Name	Erik S	Erik Saari			Name of Business	Altus Engineering, Ir	nc.			
APPL	ICANT'S IT	Phone	(603)	433-23	35			422 Ozvet Chrast	133 Court Stroot			
INFO	RMATION	Fax					Mailing Address	133 Court Street Portsmouth, NH 03	8 01			
		Email	esaar	i@altus	s-eng.c	om		Fortsmodin, Ni 1 03				
	Existing Cond	itions: The	e site cu	ırrently	hosts	a single-fa	amily reside	nce and some sections o	of field with	the remainder		
			he site l	•		· ·	•					
z												
PTIO	B	al and alamate	1									
DESCRIPTION	Proposed legal (Documents for				intenan	ce agreemer	nts, riders to d	eeds, grading, drainage and pa	vement, etc	.)		
DE	The propo	sal adds a	60'-wic	le publ	ic right	of way to	access two	private sites. One site is	s currently	for sale while the		
	other is inc	luded in t	he acco	mpany	ing site	e plan revi	ew applicat	on. Said site will include	a new 20	,000 sf		
	building with associated parking and infrastructure.											
	-		-	_		-		application is true and co	rrect and v	vill not deviate from		
	cant's	9 (L.)	Curying	THE KILL	lery 10		Owner's	See attached LOA				
Signa Date:	ture:	07/22/2	1			——	Signature: Date:	07/22/21				
Date.		_					Date.		_			

hundred (100) feet of the property line. The APPLICATN IS RESPONSIBLE TO CLEARLY DESCRIBE THE PROJECT. Structural pavement sections Erosion control detail Roadway cross sections Trenching details Structural pavement sections Erosion control detail Roadway cross sections Trenching details Structural pavement sections Trenching details Structural pavement sections Trenching details Structural pavement sections Erosion control detail Roadway cross sections Trenching details Structural pavement sections Erosion control detail Roadway cross sections Trenching details Structural pavement sections Erosion control detail Roadway cross sections Trenching details Structural pavement sections Erosion control detail Roadway cross sections Trenching details Structural pavement sections Erosion control detail Roadway cross sections Trenching details Structural pavement sections Erosion control detail Roadway cross sections Trenching details Structural pavement sections Erosion control detail Roadway cross sections Trenching details Structural pavement sections Erosion control detail Roadway cross sections Trenching details Erosion control detail Roadway cross sections Trenching details Erosion control paves Roadway cross sections Trenching details Erosion control paves Roadway cross sections Trenching details Erosion control paves Erosion control paves Erosion control paves Erosion control paves Erosion control paves	iviinimum Submissi	on kequirements
PLANNING BOARD WILL DECIDE WHETHER SUFFICIENT INFORMATION HAS BEEN PROVIDED AND WILL VOTE TO DETERMINE COMPLETENESS/ACCEPTANCE. See Section 16.10.5.2 THE APPLICATN IS RESPONSIBLE TO CLEARLY DESCRIBE THE PROJECT. A) Paper size: (Including: PROJECT. A) Provide application of all structures and address and town staff decision of the	☐ 15 COPIES OF THE RIGHT OF PLAN – 5 OF WHICH MUST BI	E 24"X 36"
Structural pavement sections Erosion control detail	PLANNING BOARD WILL DECIDE WHETHER SUFFICIENT INFORMATION HAS BEEN PROVIDED AND WILL VOTE TO DETERMINE COMPLETENESS/ACCEPTANCE. See Section	☐ existing and proposed signage☐ details of all structures and accesses located within one
No less than 11" X 17" (reduced) or greater than 24" X 36" (full).		☐ Structural pavement sections ☐ Erosion control detail ☐ Roadway cross sections ☐ Trenching details
Scale size:	No less than 11" X 17" (reduced) or greater than 24" X 36"	documents:
Copy of documents showing owner's legal interest Agne of preparer of plans with professional information and professional seal Paracel's tax map identification (map – lot) Date of plan preparation Date of plan preparation Survey performed and sealed by licensed surveyor: Identify all existing property/R.O.W. markers Show all proposed boundary monuments (per ordinance) Provide orientation: Arrow showing true north and magnetic declination Graphic scale Signature block Area of R.O.W. Length of lot frontage; Zoning and zone boundaries Front yard setbacks Deed docket and page numbers Intersecting lot lines Size of the parcel minus the area in the R.O.W. Area of R.O.W. Length of lot frontage; Zoning and zone boundaries Front yard setbacks Deed docket and page numbers Intersecting lot lines Sixing topography Horizontal alignment Vertical profile (existing ground and proposed grades) Given deviation of all natural features or site elements to be preserved.	☐ Under 10 acres: no greater than 1" = 30'	☐ A maintenance agreement for R.O.W. as a rider to the deed.
D) Survey performed and sealed by licensed surveyor:	 □ Applicant's name and address □ Name of preparer of plans with professional information and professional seal □ Parcel's tax map identification (map – lot) 	 □ Copy of documents showing owner's legal interest □ Copy of any existing or proposed property encumbrances □ Erosion control plan and sedimentation endorsed by York County Soil and Water District □ A plan for stormwater management prepared by a registered professional engineer
Arrow showing true north and magnetic declination Graphic scale Signature block The right of way plans must include: Size of the parcel minus the area in the R.O.W. Area of R.O.W. Length of lot frontage; Zoning and zone boundaries Front yard setbacks Deed docket and page numbers Intersecting lot lines Sidewalks Sidewalks Sidewalks Sidewalks Sidewalks Storm drainage systems and structures Parks Open space Conservation easements The location of all natural features or site elements to be preserved. Show and locate on the plans the names and addresses of all owners of record of contiguous property, including those across the street. WITH THE FIRST SUBMITTAL, PROVIDE 2 SETS OF MAILING LABLES. MN) An estimate of the amount and type of vehicular traffic on a daily basis and during peak hours. Where it is anticipated that four hundred (400) vehicle trips per day or more, a traffic impact analysis must be conducted in accordance with section 16.10.5.2.D.1. Additional Requirements. In its consideration of an application/plan, the Board may at any point in during the review, require the applicant to submit additional materials, studies, analyses, and agreement proposals as it may deem necessary for complete understanding of the application. Such materials may include those listed below. Fiscal Impact Analysis. An analysis of the relationship of the revenues to the town from the development and the costs of additional publicly funded resources; Traffic impact Study (see Section 16.10.5.2.D.1) NOTE TO APPLICANT: THE PLANNING BOARD MAY CHOOSE TO CONDUCT A SITE WALK. PRIOR TO THE SITE WALK, TEMPORARY MARKERS MUST BE ADEQUATELY PLACED THAT ENABLE THE LAYOUT OF DEVELOPMENT.	☐ Identify all existing property/R.O.W. markers	York County Where the soil survey shows soils with severe restrictions for development, a high intensity Class A soil
□ Size of the parcel minus the area in the R.O.W. □ Area of R.O.W. □ Length of lot frontage; □ Zoning and zone boundaries □ Front yard setbacks □ Deed docket and page numbers □ Intersecting lot lines □ Existing topography □ Horizontal alignment □ Vertical profile (existing ground and proposed grades) □ Sidewalks □ Watercourses □ forest cover □ Ledge outcroppings □ Proposed areas of blasting □ Utilities (above and below ground) □ Above ground utilities (poles) that may be relocated □ Storm drainage systems and structures □ Parks □ Open space □ Conservation easements □ The location of all natural features or site elements to be preserved. □ Show and locate on the plans the names and addresses of all owners of record of contiguous property, including those across the street. WITH THE FIRST SUBMITTAL, PROVIDE 2 SETS OF MAILING LABLES. H) Provide sufficient information to identify and locate each interior lot line, right of way lines, and street alignments.	☐ Arrow showing true north and magnetic declination☐ Graphic scale☐ Signature block☐	on a daily basis and during peak hours. Where it is anticipated that four hundred (400) vehicle trips per day or more, a traffic impact analysis must be conducted in
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lot line, right of way lines, and street alignments.	owners of record of contiguous property, including those across the street. WITH THE FIRST SUBMITTAL, PROVIDE 2 SETS OF	TO CONDUCT A SITE WALK. PRIOR TO THE SITE WALK, TEMPORARY MARKERS MUST BE ADEQUATELY PLACED
SUBMITTALS THE TOWN PLANNER DEEMS SUFFICIENTLY LACKING IN CONTENT WILL NOT BE SCHEDULED FOR PLANNING BOARD REVIEW.	lot line, right of way lines, and street alignments. ☐ curve geometry ☐ bearings and distances ☐ widths	AND APPRAISE THE LAYOUT OF DEVELOPMENT.



TOWN OF KITTERY ~ MAINE PLANNING OFFICE

200 Rogers Road, Kittery, Maine 03904 PHONE: (207) 475-1323 Fax: (207) 439-6806 www.kittery.org

APPLICATION: REQUEST FOR WAIVER

THE REVIEW PROCESS PROJURES ARRESTAL FROM ROTH THE TOWN RIANNER AND THE CORE ENFORCEMENT OFF

ППІЗ	KEVIEW FKC	CL33 KEC	VOIKES	AIIKO	VALI	KOM BOI	II IIIL IOWIN	PLANNER AND THE	L CODE LIVI OKCI	MENT OFFICER	
PROPERTY DESCRIPTION		Parcel ID	Мар	67	Lot	1	Zone Base Overlay	<u>MU</u>	Total Land Area	1,040,714 sf (23.89 ac.)	
		Physical Address	524 (J.S. Ro	oute 1						
		Name	C-Coa	ast Prop	erties	, LLC					
_	PERTY	Phone		321-95		,	Mailing	8 Banks Rock			
_	NER'S DRMATION	Fax					Address	York, Maine 0391	1		
		Email	kevinv	verikso	n@gm	ail.com	-				
		Name	Erik Saari				Name of Business	Altus Engineering	Inc		
	LICANT'S	Phone		433-23	35		200111000	133 Court Street	,		
AGEI INFO	N I DRMATION	Fax					Mailing Address	Portsmouth, NH 03801			
		Email	esaar	i@altus	eng.c	com					
	Ordinance Section Describe why this request i					request is	being made.				
	EXAMPLE 16.32.560 (B)- OFFSTREET PARKING.		***EXAMPLE*** Requesting a waiver of this ordinance since the proposed professional offices have a written agreement with the abutting Church owned property to share parking.								
DESCRIPTION			Se	e attac	hed W	aiver Req	uest Letter				
DESCR											
									_		
	-		-	_		_	ovided in this a	application is true an	d correct and will n	ot deviate from	
Applicant's Signature: Date: 07/22/21			. C		•		Owner's Signature: Date:		tter of Authorizatio	n	



Civil Site Planning Environmental Engineering

133 Court Street Portsmouth, NH 03801-4413

July 22, 2021

Kittery Planning Board 200 Rogers Road Kittery, Maine 03904

Re: Waiver Request Good To-Go 524 U.S. Route 1 Kittery, Maine

Dear Members of the Board,

On behalf of the applicant, we respectfully request that the following five provisions of Section 16.8, Attachment 1, Table 1 (Design and Construction Standards for Streets and Pedestrian Ways) for Secondary Collector streets be waived:

- Sidewalk (not proposed where required)
- Longitudinal Street Gradient (7.5% proposed where 7% required)
- Side Slope (2:1 in deep cuts and 1:2 in ledge proposed where 3:1 required)
- Tangent Between Reverse Curves (0', 50' & 54.42' proposed where 100' required)
- Min. Centerline Curve Radius (150', 200' & 200' proposed where 300' required)

The property has a number of unique characteristics that make a strict application of the standards impractical. Due to the need for the proposed roadway to be placed away from the abutting Landmark Hill driveway, the location of the existing house, the presence of a cemetery and the existing topography, adequate space for a roadway fully compliant with the standards is lacking.

The existing slope of the site requires a slightly steeper roadway than permitted. Even with relief from the street gradient requirement, the roadway will still require substantial cutting in some areas. By maintaining a 2:1 slope in these deep cut areas, the overall area of disturbance and tree clearing will be minimized. In addition, initial subsurface investigations indicate the presence of shallow ledge over the majority of the site. We expect that the deepest cut sections will require ledge removal which will leave a stable, near-vertical rock face that will have little potential for erosion. Were the exact letter of the standards applied, the design would result in significantly deeper cuts and longer side slopes that would require more extensive grading activities and ledge removal.

As for horizontal geometry, reduced tangents and centerline radii allow the road to navigate the existing obstacles while maintaining an adequate and safe public accessway. The knock-on effect of this is that the roadway design will promote slower vehicular speeds and will in essence become self-regulating in that respect. In addition, shorter tangents and radii will let the project maintain more of the existing buffer to the abutting property to the south by allowing the road to turn away from the property line more quickly once it passes below the cemetery.

Tel: (603) 433-2335 E-mail: Altus@altus-eng.com

Regarding the sidewalk, installing one at this location would not serve any purpose as the proposed use is not a retail establishment and will therefore not require pedestrian access. There is also no sidewalk network along this section of Route 1 for any new sidewalk to connect to. That said, we have designed the road to be able to easily accommodate a sidewalk in the future if additional development in the vicinity requires it.

We appreciate your time and consideration and hope that you will conclude that these waivers are justified given the nature of the project site. If you have any questions or need additional information, please contact us. We would be happy to address any concerns you may have.

Sincerely,

ALTUS ENGINEERING, INC.

Erik B. Saari Vice President

ebs/5116-WaiverRequest-072221

Letter of Authorization

I, Kevin W. Erikson of C-Coast Properties, LLC ("LLC"), hereby authorize Altus Engineering, Inc. of Portsmouth, NH to represent the LLC as the Owner in all matters concerning the engineering and related permitting of a site plan on Kittery Tax Map 67, Lot 1 located at 524 U.S Route 1 in Kittery Maine. This authorization shall include any signatures required for Federal, State and Municipal permit applications.

Kevin W. Erikson

Testav Suarson
Witness

Telstav Swarson
Print Name

5/6/21

Date

Letter of Authorization

We, Jennifer Scism and David Koorits of Good To-Go c/o Cape House Management, LLC hereby authorize Altus Engineering, Inc. of Portsmouth, NH to represent us as the Applicant in all matters concerning the engineering and related permitting of a site plan on Kittery Tax Map 67, Lot 1 located at 524 U.S Route 1 in Kittery Maine. This authorization shall include any signatures required for Federal, State and Municipal permit applications.

Signature

Signature

Dand Koonts

Date

7/8/21

Date

Date

Date

Print Name

Print Name

Date

Date

DEBRA L. ANDERSON, REGISTER OF DEEDS E-RECORDED **Bk 17807 PG 929**

Instr # 2018040395 09/25/2018 10:59:49 AM Pages 4 YORK CO

WARRANTY DEED

Know all by these presents that TIDE RUN DEVELOPMENT, LLC, a Maine limited liability company, with a business mailing address of 70 Cider Hill Road, York, Maine 03909, for consideration paid, grants to C-COAST PROPERTIES LLC, a Maine limited liability company, with a business mailing address of P.O. Box 603, York Harbor, Maine 03911, with Warranty Covenants, the real property, situated partially in the Town of York and partially in the Town of Kittery, County of York and State of Maine, described as follows:

SEE EXHIBIT A ATTACHED HERETO

IN WITNESS WHEREOF, the said TIDE RUN DEVELOPMENT, LLC, has caused this instrument to be signed in its company name, under seal, by DEBORAH E. ERIKSON, its Manager, duly authorized, this 24 day of September 2018.

TIDE RUN DEVELOPMENT, LLC

DEBORAH E. ERIKSON, MANAGER

September 24.

J. Ballow

STATE OF MAINE

York, ss.

Then personally appeared the above named Deborah E. Erikson and acknowledged the foregoing instrument to be her free act and deed in her said capacity and the free act and deed of said limited liability company.

Before me,

Attorney at Law/Notary

Commission Expires

EXHIBIT A

PARCEL 1

A certain lot or parcel of land together with the buildings thereon situate in said Kittery and in part in the Town of York. Both in the County of York and State of Maine bounded and described as follows:

BEGINNING on U.S. Highway No. 1 at land of Leo H. and Barbara L. Cain;

THENCE running South 27° East by land of said Cains to a marked tree in line of a stone wall;

THENCE continuing on a southeasterly course on the line of land formerly conveyed to said Leo and Barbara Cain to a stone wall on line of land now or formerly owned by Leon W. Main;

THENCE turning and running southwesterly as the wall runs by other land now or formerly of said Main to a corner in the wall;

THENCE turning and running southeasterly as the wall runs to land now or formerly of one Fuller, being the southeasterly boundary of the farm herein conveyed;

THENCE southwesterly by said Fuller land to land of William Crawford;

THENCE northwesterly land of said Crawford to land of Sheldon Doody;

THENCE northeasterly, four hundred (400) feet, by land of said Doody;

THENCE northwesterly, five hundred forty-four (544) feet, by land of said Doody to said U.S. Highway No. 1;

THENCE northeasterly by said Highway, seven hundred (700) feet, more or less, to the PLACE OF BEGINNING.

Containing forty acres, more or less.

Subject to a pole easement granted to New England Tel. & Tel. Co. by Wallace A. Main, by instrument dated September 3, 1925 and recorded at York County Registry of Deeds in Book 755, Page 21. Title reference is made to a deed recorded at York County Registry of Deeds in Book 1826, Page 490.

PARCEL 2

A certain lot or parcel of land situate in the Town of York, County of York and State of Maine, being a woodlot lying adjacent to and north of the Kittery-York town line; being a portion of the

"Emerson Field", and delineated on Plan of Land of Kyra M. Kaplan by Moulton Engineering Co., dated 10/18/72, recorded in York County Registry of Deeds in Plan Book 59. Page 18, bounded and described as follows:

BEGINNING at a pipe in the ground beside an old set of bars at the southeasterly corner of said parcel, and running North eighty-five degrees forty-one minutes thirty seconds East (N 85° 41′ 30" E) two hundred eighty-nine and thirty hundredths (289.30) feet to a pipe in the ground beside an old elm tree with spike in it;

THENCE running North twenty-two degrees thirty-eight minutes forty-five seconds West (N 22° 38' 45" W) six hundred ninety-nine and forty-six hundredths (699.46) feet to a pipe driven in a pile of stones;

THENCE running southwesterly by and along a stone wall four hundred forty-eight and forty-nine hundredths (448.49) feet to a pipe in the corner of said stone wall;

THENCE running southeasterly by and along another stone wall four hundred sixty-seven and sixty-seven hundredths (467.67) feet to the POINT OF BEGINNING.

Together with the right of way, leading from said woodlot through land of heirs of Wallace A. Main to the highway known as U.S. Route 1.

Meaning and intending and hereby conveying the second parcel only described and conveyed in deed of Jack A. Drobish et ux. to Frank G. Leighton, Jr. et al., dated May 27, 1972, recorded at said Registry in Book 1950, Page 88. Title reference is made to a deed recorded at York County Registry of Deeds in Book 2010, Page 193.

PARCEL 3

A certain lot or parcel of land situated in said York containing fifteen (15) acres, more or less, bounded and described as follows:

BEGINNING at the southerly corner of the parcel of land herein conveyed adjoining land of the heirs of Edmund Moulton at the junction of the stonewall;

THENCE running from said corner northeasterly by said heirs land and stonewall fifty-seven rods and three links to land now or formerly of Ida May Trefethen to the junction of the wall;

THENCE northwesterly by said Trefethen land and wall fifty-six rods and sixteen links to corner of wall;

THENCE southwesterly by said Trefethen land and land formerly of Wallace A. Main, thirty rods to point and pile of stones by the wall near a maple tree;

THENCE South about 20° East forty-one and eight tenths rods to a large elm tree, marked;

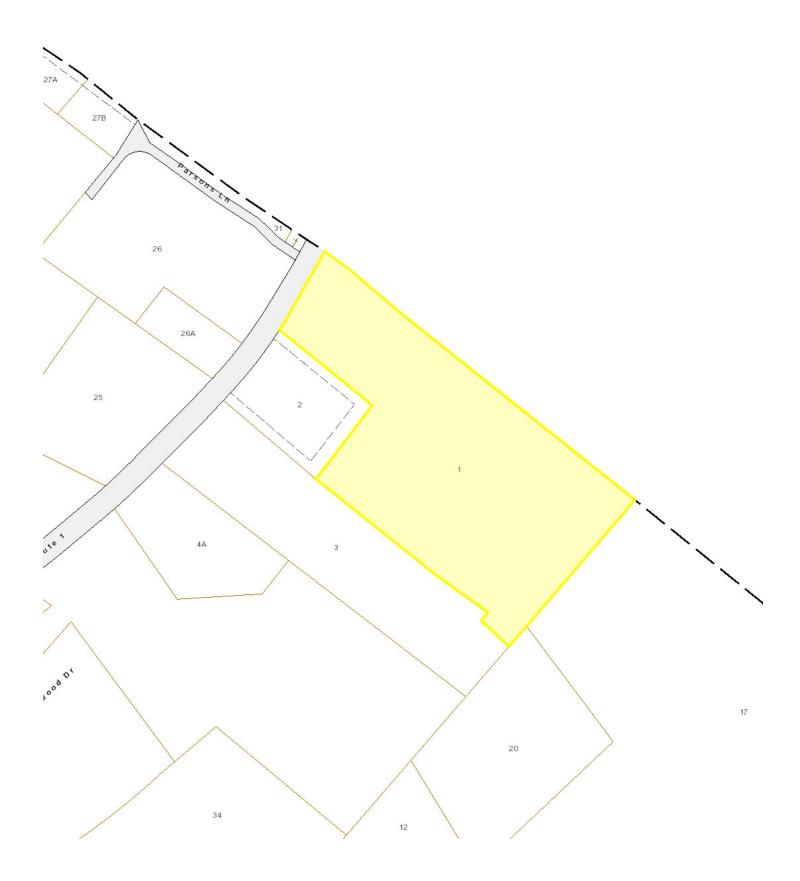
THENCE South about eighty-two degrees West about sixteen and three tenths rods to a point at the easterly end of a set of bars; thence southeasterly by land formerly of Alsbury J. Goodwin twenty-seven and eight tenths rods to the place of beginning. Being a portion of the Emerson Field so called.

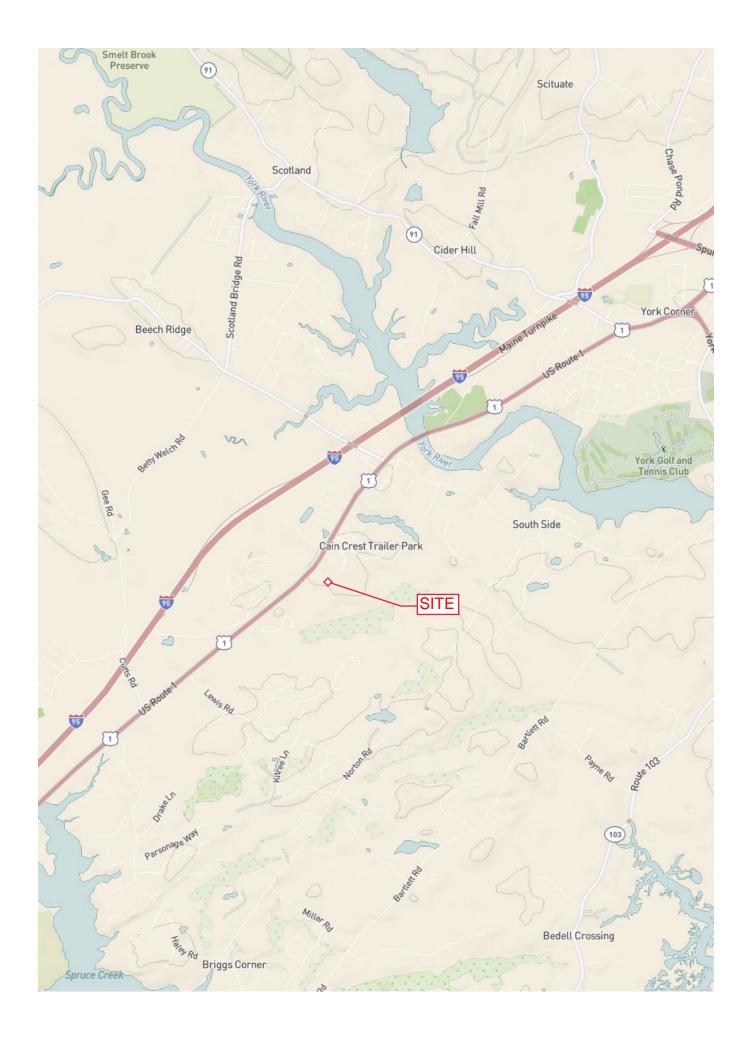
Title reference is made to a deed recorded at York County Registry of Deeds in Book 1826, Page 492.

Excepting the land conveyed to Leo H. Cain, et ux. by deed dated June 20, 1955 and recorded in Book 1289, Page 77 at the York County Registry of Deeds.

Excepting the land conveyed to Leo H. Cain, et ux. by deed dated November 19, 1968 and recorded at Book 1969, Page 696 at the York County Registry of Deeds.

Being the same premises conveyed by Krya M. Berson and Eliot L. Berson, Co-Trustees of Heritage Realty Trust to Tide Run Development, LLC by deed dated October 18, 2016 and recorded at York County Registry of Deeds in Book 17345, Page 846.









TOWN OF KITTERY, MAINE

SEWER DEPARTMENT

200 Rogers Road, Kittery, ME 03904 Telephone: (207) 439-4646 Fax: (207) 439-2799

Good To – Go Erik Saari 584 Route 1, Kittery, ME 03904

July 12, 2021

RE:Sewer Availability

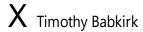
Erik,

This letter is to confirm that there is sanitary sewer service available for the Good To-Go project Located at 584 Route 1, The sewer system (piping and pumping stations) and the treatment facility has the capacity and ability to handle the projected flow increase of 2,400 GPD.

If you have further questions or concerns please contact me.

Sincerely Yours





Timothy Babkirk
Superintendent
Signed by: 8d59976c-e219-4963-8b87-4c42e7e470e3

Timothy Babkirk
Superintendent of Sewer Services
Town of Kittery
200 Rogers Rd
Kittery ME 03904
1-207-439-4646
tbabkirk@kitteryme.org

OFFICE OF

KITTERY WATER DISTRICT

17 State Road Kittery, ME 03904-1565 TEL: 207-439-1128 FAX: 207-439-8549

E-Mail: kitterywater@comcast.net

Kittery Planning Board 200 Rogers Road Kittery, ME 03904

July 12, 2021

Re: Good To-Go Specialty Food Facility

Dear Planning Board Members,

Please accept this letter as verification that the Kittery Water District does have the capacity to supply municipal water service both for domestic purposes and fire protection for the proposed Good To-Go Specialty Food Facility at 524 U.S. Route 1 in Kittery.

Sincerely,

Michael S. Rogers

Superintendent

cc: Erik Saari, Altus Engineering, Inc.

GOOD TO-GO SPECIALTY FOOD FACILITY

524 U.S. ROUTE 1 KITTERY, MAINE

Owner:

C-COAST PROPERTIES, LLC

8 Banks Rock York Harbor, Maine 03911 Assessor's Parcel 67, Lot 1

Applicant:



GOOD TO-GO

(207) 451-9060

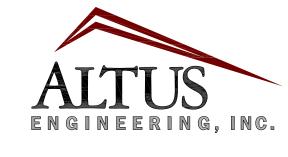
c/o Cape House Management, LLC *Architect:*



Bild Architecture

Portland, Maine 004101 (207) 408-0168

Civil Engineer:



www.altus-eng.com

Soil and Wetland Scientist: Michael Cuomo, M.S.S. #211

6 York Pond Road York, ME 03909 (207) 363-4532

Surveyor:



Engineers, Planners, Surveyors www.civcon.com



30 Danforth St., Suite 213

General Contractor:



Sheridan Construction Corp. 33 Sheridan Drive Fairfield, Maine 04937 (207) 453-9311

Landscape Architect:

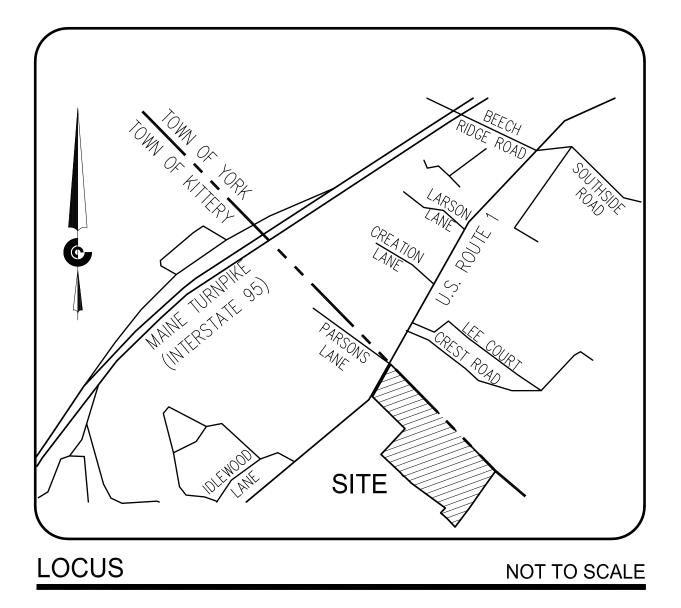


Lighting Consultant:

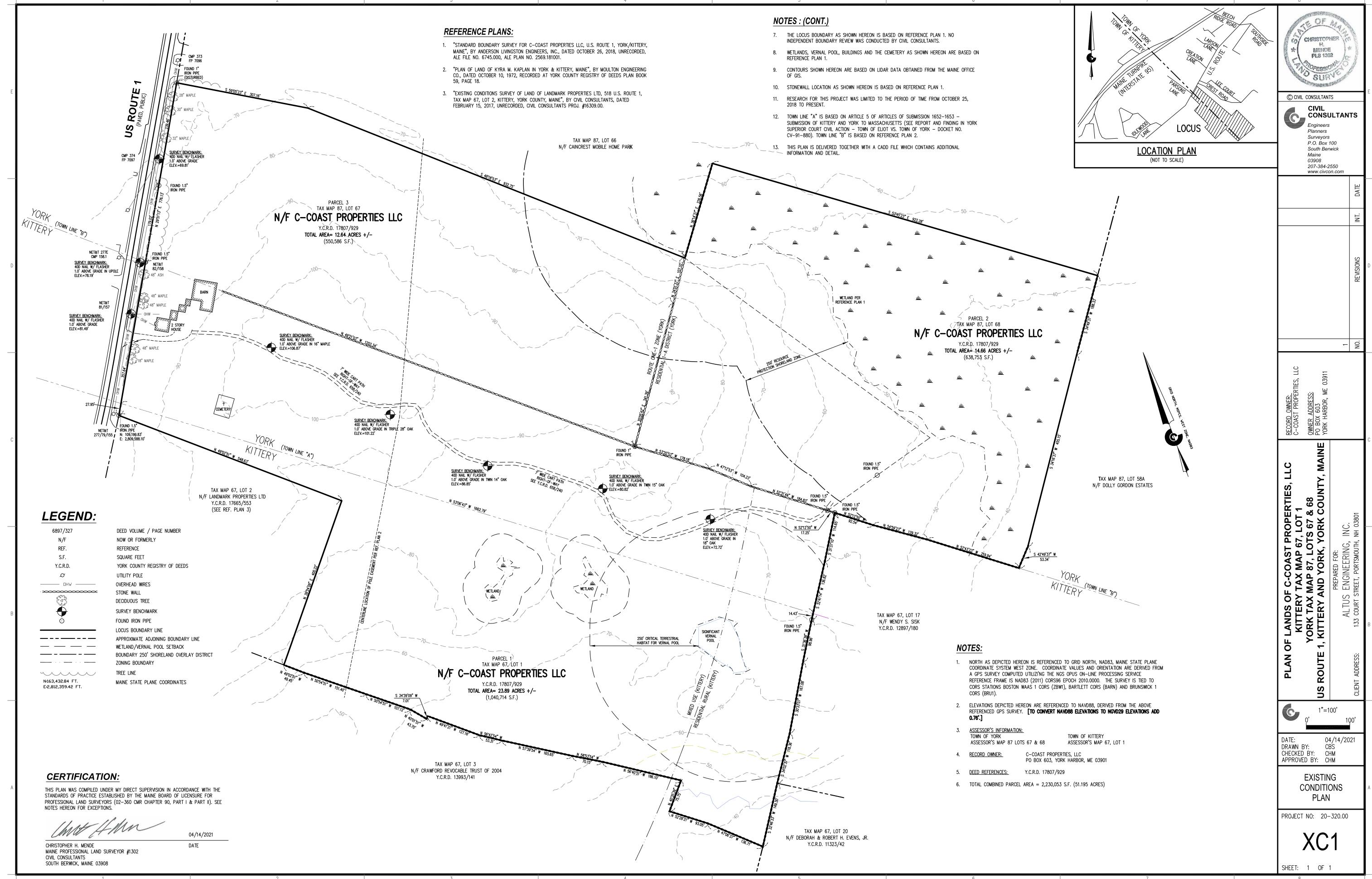


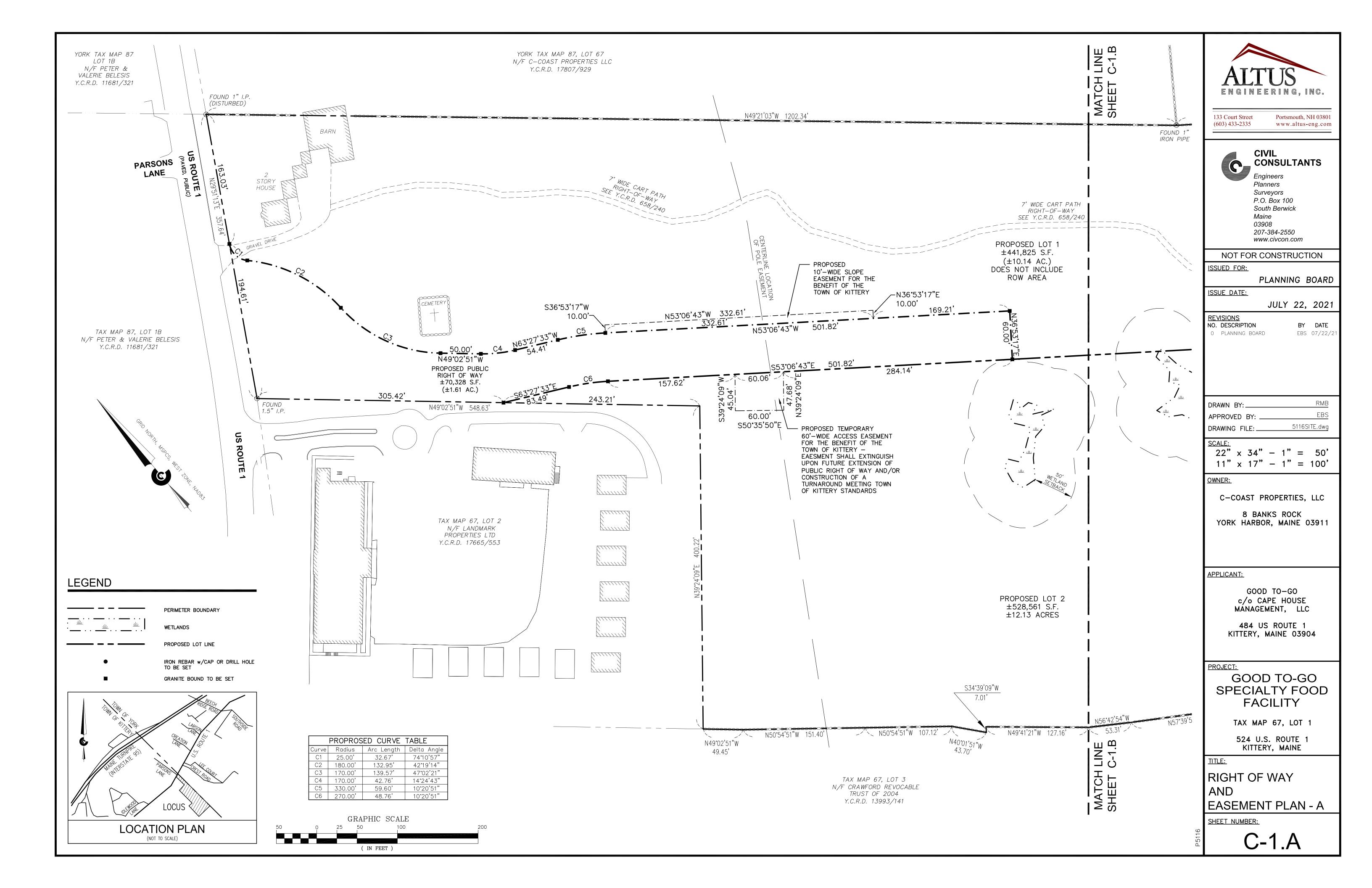
Plan Issue Date:

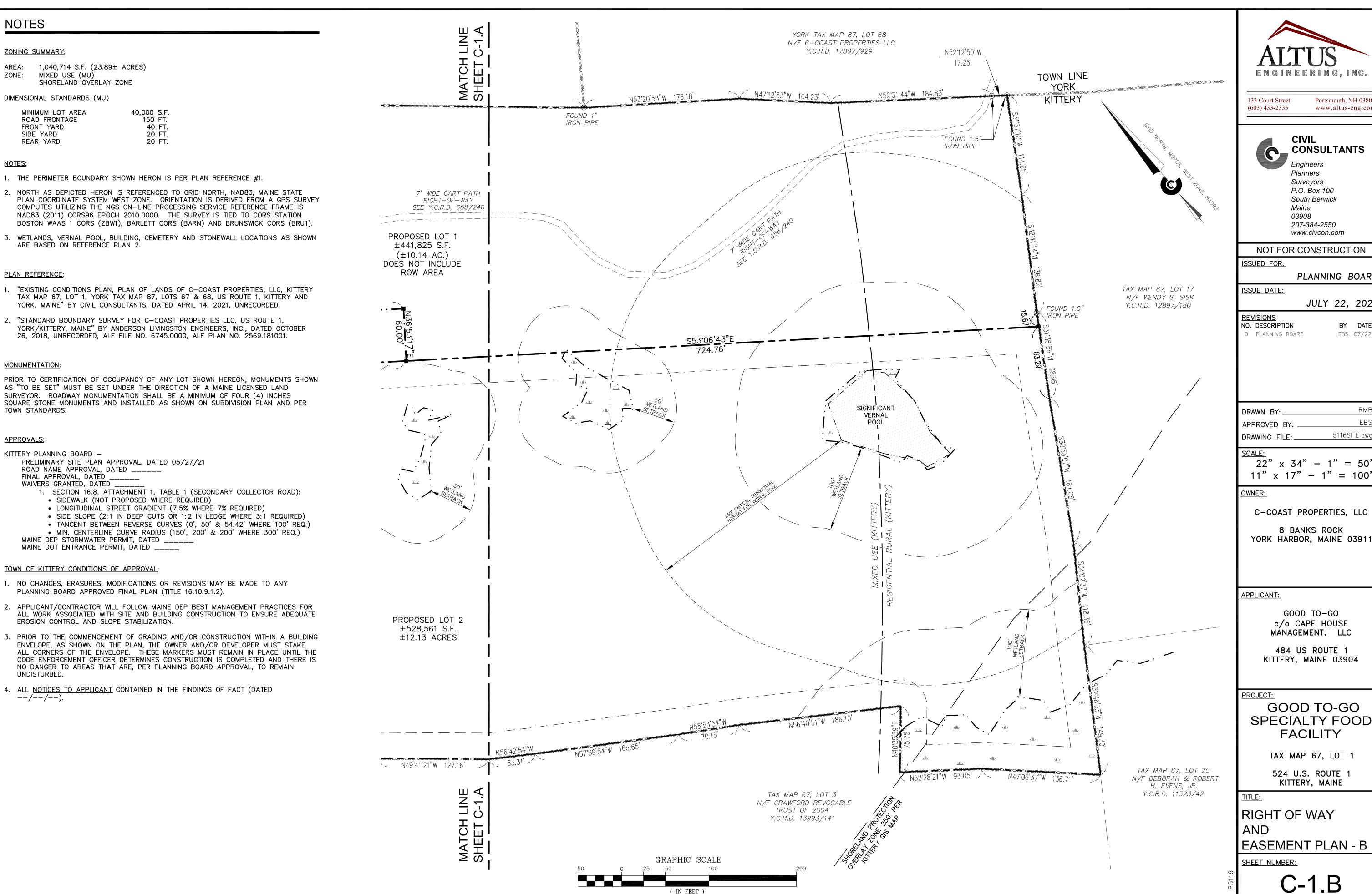
July 22, 2021 Planning Board Submission

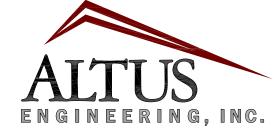


Sheet Index Title	Sheet No.:	Rev.	Date
Existing Conditions Plan	XC1	0	04/14/21
Right of Way and Easement Plan — A	C-1.A	0	07/22/21
Right of Way and Easement Plan — B	C-1.B	Ο	07/22/21
Soils Plan	C-2	Ο	07/22/21
Site Plan	C-3	Ο	07/22/21
Roadway Plan and Profile	C-4	Ο	07/22/21
Highway Access Plan	C-5	0	07/22/21
Stormwater Management Plan	C-6	Ο	07/22/21
Erosion and Sediment Control Plan	C - 7	Ο	07/22/21
Utility Plan	C-8	Ο	07/22/21
Lighting Plan	C-9	Ο	07/22/21
Landscape Plan	L-1	Ο	07/22/21
Detail Sheet	D-1	Ο	07/22/21
Detail Sheet	D-2	Ο	07/22/21
Detail Sheet	D-3	Ο	07/22/21
Detail Sheet	D-4	Ο	07/22/21
Detail Sheet	D-5	Ο	07/22/21
Detail Sheet	D-6	Ο	07/22/21
Detail Sheet	D-7	Ο	07/22/21
Detail Sheet	D-8	Ο	07/22/21
Detail Sheet	D - 9	Ο	07/22/21
Front Elevation	SK-2	Ο	07/12/21
Side Elevation	SK-3	0	07/12/21
Permit Summary: Submitte	d	Received	!
Kittery Site Plan Approval $07/22/21$ MDEP Stormwater Permit $-/-/-$ MDOT Entrance Permit $-/-/-$ By Contractions	tor 14 day	-/-/- -/-/- -/-/-	construction









133 Court Street (603) 433-2335

Portsmouth, NH 03801 www.altus-eng.com



CONSULTANTS

Engineers Planners Surveyors P.O. Box 100 South Berwick Maine 03908 207-384-2550 www.civcon.com

NOT FOR CONSTRUCTION

ISSUED FOR:

PLANNING BOARD

ISSUE DATE:

JULY 22, 2021

BY DATE

EBS 07/22/2

NO. DESCRIPTION

O PLANNING BOARD

DRAWN BY: APPROVED BY: ___ 5116SITE.dwg

 $22" \times 34" - 1" = 50"$ $11" \times 17" - 1" = 100"$

C-COAST PROPERTIES, LLC

8 BANKS ROCK YORK HARBOR, MAINE 03911

APPLICANT:

GOOD TO-GO c/o CAPE HOUSE MÁNAGEMENT, LLC

484 US ROUTE 1 KITTERY, MAINE 03904

PROJECT:

GOOD TO-GO SPECIALTY FOOD **FACILITY**

TAX MAP 67, LOT 1

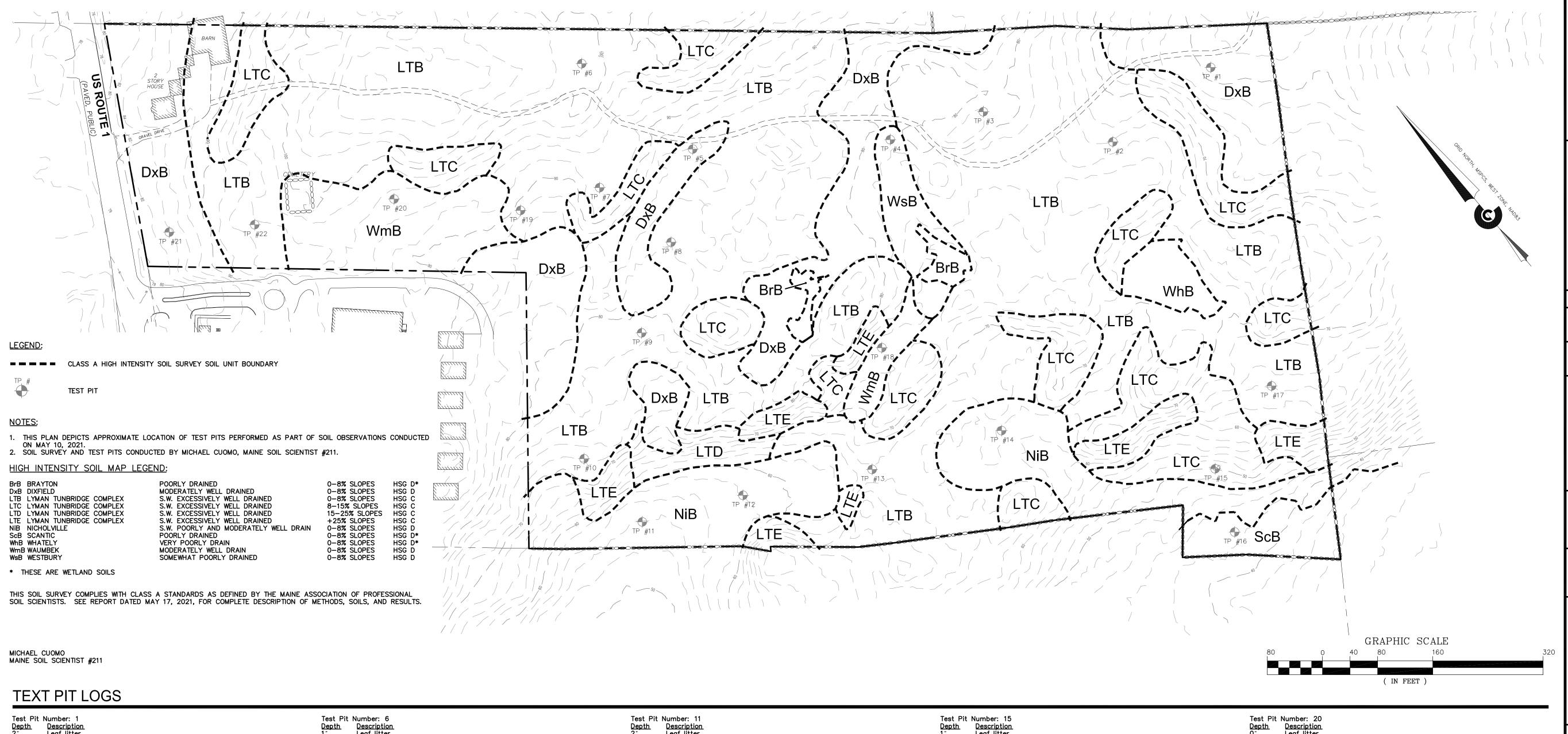
KITTERY, MAINE

524 U.S. ROUTE 1

RIGHT OF WAY AND

SHEET NUMBER:

C-1.B



```
<u>Depth</u> <u>Description</u>
2" Leaf litter.
0-9" Dark brown (10YR 3/3) fine sandy loam, granular, friable.
9-24" Dark yellowish brown (10YR 4/6) fine sandy loam, blocky, friable.
24-35" Light olive brown (2.5Y 5/4) fine sandy loam, blocky, friable, redox.
35-48" Dark olive brown (2.5Y 3/3) stony fine sandy loam, massive, firm, redox. Soil Name:
 Soil Name:
Depth to Seasonal High Water Table: 24"
 Depth to Bedrock:
 Test Pit Number: 2
 <u>Depth</u> <u>Description</u>
         Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.
8-20" Dark yellowish brown (10YR 4/6) stony fine sandy loam, blocky, friable.
                                           Tunbridge
Depth to Seasonal High Water Table: none
 Depth to Bedrock:
Test Pit Number: 3
Depth Description 2" Leaf litter.
          Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.
8-18" Dark yellowish brown (10YR 4/6) stony fine sandy loam, blocky, friable.
Soil Name: Lyma
Depth to Seasonal High Water Table: none
Depth to Bedrock:
 Test Pit Number: 4
<u>Depth</u> <u>Description</u>
2" <u>Leaf litter.</u>
 0-8" Dark grayish brown (2.5Y 4/2) fine sandy loam, granular, friable.
8-16" Dark yellowish brown (10YR 4/6) fine sandy loam, blocky, friable, redox.
16-24" Light yellowish brown (2.5Y 6/4) fine sandy loam, blocky, firm, redox.
Soil Name:
                                          Westbury variant
Depth to Seasonal High Water Table: 8"
 Depth to Bedrock:
Test Pit Number: 5
         <u>Description</u>
Leaf litter.
0-22" Yellowish brown (10YR 5/4) fine sandy loam, blocky, friable.
22-32" Dark yellowish brown (10YR 4/6) gravelly loamy sand, blocky, friable, redox.
32-44" Dark olive brown (2.5Y 3/3) gravelly sand, loose, massive, redox.
44-56" Light olive brown (2.5Y 5/4)stony fine sandy loam, massive, firm, redox.
Depth to Seasonal High Water Table: 22"
```

Depth to Bedrock:

```
0-10" Dark brown (10YR 3/3) fine sandy loam, granular, friable.
10-24" Dark yellowish brown (10YR 4/6) fine sandy loam, blocky, friable.
                                                                                        0-7"
                                                                                                 Dark brown (10YR 3/3) silt loam, granular, friable.
                                                                                                 Light yellowish brown (2.5Y 6/4) silt loam, blocky, friable, redox.
24-38" Light yellowish brown (2.5Y 6/4) stony fine sandy loam, massive, firm,
                                                                                        10-28" Pale olive (5Y 6/3) silt loam, massive, friable, redox.
                                                                                        29-44" Light yellowish brown (2.5Y 6/4) fine sandy loam, massive, firm, redox.
Soil Name:
                                         Tunbridge variant
                                                                                        44-96" Olive brown (2.5Y 4/4)
Depth to Seasonal High Water Table: 24"
                                                                                        Soil Name:
Depth to Bedrock:
                                                                                        Depth to Seasonal High Water Tab
                                                                                        Depth to Bedrock:
Test Pit Number: 7
        <u>Description</u>
Leaf litter.
                                                                                        Test Pit Number: 12
                                                                                        <u>Depth</u>
                                                                                                 Description
         Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.
7-18" Yellowish brown (10YR 5/6) stony fine sandy loam, blocky, friable.
                                                                                        0-7"
                                                                                                 Dark brown (10YR 3/3)
Soil Name:
                                                                                        7-11"
                                                                                                  Yellowish brown (10YR
Depth to Seasonal High Water Table: none
                                                                                        11-28" Light yellowish brown (2
Depth to Bedrock:
                                                                                        28-64" Olive brown (2.5Y 4/4)
                                                                                        64-96" Olive brown (2.5Y 4/4)
Test Pit Number: 8
                                                                                        Soil Name:
Depth Description 2" Leaf litter.
                                                                                        Depth to Seasonal High Water Tab
                                                                                        Depth to Bedrock:
0-3" Very dark gray (10YR 3/1) stony fine sandy loam, granular, friable.
Soil Name:
                                                                                        Test Pit Number: 13
Depth to Seasonal High Water Table: none
                                                                                        Depth Description Leaf litter.
Depth to Bedrock:
                                                                                        0-10" Dark brown (10YR 3/3)
Test Pit Number: 9
                                                                                        10-24" Strong brown (7.5YR 4)
<u>Depth</u> <u>Description</u>
                                                                                        24-32" Light yellowish brown (2
                                                                                        redox.
         Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.
                                                                                        Soil Name:
6-27" Yellowish brown (10YR 5/6) stony fine sandy loam, blocky, friable.
                                                                                        Depth to Seasonal High Water Tab
                                         Tunbridge
                                                                                        Depth to Bedrock:
Depth to Seasonal High Water Table: none
Depth to Bedrock:
                                                                                        Test Pit Number: 14
                                                                                                 <u>Description</u>
Leaf litter.
                                                                                        <u>Depth</u>
Test Pit Number: 10
Depth Description 2" Leaf litter.
                                                                                                 Brown (10YR 4/3) fine
                                                                                                 Yellowish brown (10YR 5
0-6" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.
                                                                                        17-24" Olive brown (2.5Y 4/4)
Depth to Seasonal High Water Table: none
                                                                                        24-52" Light olive brown (2.5Y
Depth to Bedrock:
                                                                                        Soil Name:
```

	d, massive, loose, w/ strata of firm silt, redox. Westbury variant 7"	Depth to S
Depth to Bedrock:	none	Test Pit N <u>Depth</u>
Test Pit Number: 12		1"
Depth Description		0-7"
1" Leaf litter.	In any commenters frields	7–13"
0-7" Dark brown (10YR 3/3) silt	ioam, granular, triable.	13-22"
7-11" Yellowish brown (10YR 5/6)		22-50" Soil Name:
	6/4) silt loam, blocky, friable, redox.	Depth to S
		Depth to E
64-96" Olive brown (2.5Y 4/4) silt Soil Name:	Nicholville variant	
Depth to Seasonal High Water Table:	11"	Test Pit N
Depth to Bedrock:	none	<u>Depth</u>
-		2"
Test Pit Number: 13		0-5"
Depth Description		5-12"
1" Leaf litter.		Soil Name: Depth to S
10-24" Strong brown (7.5YR 4/6) s	ny fine sandy loam, granular, friable. stony fine sandy loam, blocky, friable.	Depth to E
	6/4) stony fine sandy loam, blocky, firm,	Test Pit N
redox. Soil Name:	Tunbridge variant	<u>Depth</u>
Depth to Seasonal High Water Table:	Tunbridge variant 24"	1"
Depth to Bedrock:	32"	0-5
		5-17"
Test Pit Number: 14		17 –24 " (
<u>Depth</u> <u>Description</u>		24-54"
2" Leaf litter.		Soil Name:
0-6" Brown (10YR 4/3) fine sand		Depth to S
17-24" Olive brown (2.5Y 4/4) sand		Depth to E
) stratified fine sand and silt, massive, firm,	Test Pit N
redox.	N2-L-1.21-	Depth 1
Soil Name:	Nicholville 17"	0"
Depth to Seasonal High Water Table: Depth to Bedrock:	17 none	0-8"
Doptil to bedicok.	110110	8-28"
		Soil Name:
		Depth to S
		L/ 1 L/ 1

Depth Description 1" Leaf litter.	<u>Depth</u> <u>Description</u> 0" Leaf litter.
0-6" Brown (10YR 4/3) stony fine sandy loam, granular, friable.	0-10 Dark brown (10YR 3/3) fine sandy loam, granular, friable.
6-12" Dark yellowish brown (10YR 5/6) stony fine sandy loam, blocky, friable.	10-28" Dark yellowish brown (10YR 4/4) fine sandy loam, blocky, friable.
12-18" Light yellowish brown (2.5Y 6/4) stony fine sandy loam, blocky, friable.	28-46" Light yellowish brown (2.5Y 6/4) gravelly loamy sand, massive, friable,
Soil Name: Lyman	redox.
Depth to Seasonal High Water Table: none	Soil Name: Waumbek
Depth to Bedrock: 18"	Depth to Seasonal High Water Table: 28"
	Depth to Bedrock: 46"
Test Pit Number: 16	
Depth Description	Test Pit Number: 21
1" Leaf litter.	<u>Depth</u> <u>Description</u> O" Leaf litter.
0-7" Very dark gray (2.5Y 3/1) silt loam, granular, friable, redox.	
7-13" Light gray (2.5Y 7/1) silt loam, blocky, friable, redox.	0-10" Very dark brown (10YR 3/3) stony fine sandy loam, granular, friable.
13-22" Olive brown (2.5Y 4/4) silt loam, blocky, firm, redox.	10-28" Dark yellowish brown (10YR 4/6) stony fine sandy loam, blocky, friable.
22-50" Olive (5Y 5/4) silty clay loam, massive, firm, redox.	28—66" Light olive brown (2.5Y 5/4) stony fine sandy loam, massive, firm, red Soil Name:
Soil Name: Scantic	
Depth to Seasonal High Water Table: surface	Depth to Seasonal High Water Table: 28" Depth to Bedrock: 66"
Depth to Bedrock: none	bepth to bedrock.
Test Pit Number: 17	Test Pit Number: 22
Depth Description	<u>Depth</u> <u>Description</u>
2" Leaf litter.	0" Leaf litter.
0-5" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.	0-6" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.
5—12" Strong brown (7.5YR 4/6) stony fine sandy loam, blocky, friable.	6-12" Yellowish brown (10YR 5/6) stony fine sandy loam, blocky, friable.
Soil Name: Lyman	Soil Name: Lyman
Depth to Seasonal High Water Table: none	Depth to Seasonal High Water Table: none
Depth to Bedrock: 12"	Depth to Bedrock: 12"
Test Pit Number: 18	Soil Observation: A
Depth Description	<u>Depth</u> <u>Description</u>
1" Leaf litter.	3" Leaf litter.
0-5 Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.	0-10" Black (10YR2/1) mucky peat, massive, friable, redox.
5-17" Yellowish brown (10YR 5/4) fine sandy loam, blocky, friable.	10-20" Gray (2.5Y 5/1) loamy fine sand, massive, friable, redox.
17-24" Light olive brown (2.5Y 5/4) stony fine sandy loam, blocky, friable, redo	
24-54" Light yellowish brown (2.5Y 6/4) sand, massive, loose, redox.	28—36" Gray (2.5Y 5/1) fine sand, massive, friable, redox.
Soil Name: Waumbek	36-42" Olive brown (2.5Y 4/4) very fine sandy loam, massive, firm, redox.
Depth to Seasonal High Water Table: 17"	Soil Name: Whately
Depth to Bedrock: none	Depth to Seasonal High Water Table: surface
	Depth to Bedrock: none
Test Pit Number: 19	Soil Observation: B
Depth Description	Depth Description
0" Leaf litter.	4" Leaf litter.

pth to Seasonal High Water Table: 17	/aumbek 7" one	Soil Name Depth to	Seasonal High Water Table	very fine sandy Whately		n, redox.
st Pit Number: 19 <u>pth Description</u> Leaf litter.		Depth to Soil Obser Depth 4"		none		
	ine sandy loam, granular, friable.	0-8"	Very dark gray (2.5Y 3/1	l) stony fine so	andv loam, massive	, friable, redox.
			Dark gray (2.5Y 4/1) sto			
il Name: Ti			Light yellowish brown (2.5			
pth to Seasonal High Water Table: no	one	redox.	,		•	
pth to Bedrock: 2	8"	Soil Name	:	Brayton v	variant	
		Depth to	Seasonal High Water Table	e: surface		

> igh Water Table: surface none PLAN Very dark gray (2.5Y 3/1) stony fine sandy loam, massive, friable, redox.

Depth to Bedrock:

SHEET NUMBER:

133 Court Street Portsmouth, NH 03801 (603) 433-2335 www.altus-eng.com

NOT FOR CONSTRUCTION

ISSUED FOR:

O PLANNING BOARD

ISSUE DATE:

PLANNING BOARD

JULY 22, 2021

<u>REVISIONS</u> NO. DESCRIPTION BY DATE

EBS 07/22/2

RMB DRAWN BY: 5116SITE.dwg DRAWING FILE:

 $11" \times 17" - 1" = 160"$

C-COAST PROPERTIES, LLC

8 BANKS ROCK YORK HARBOR, MAINE 03911

APPLICANT:

GOOD TO-GO c/o CAPE HOUSE MÁNAGEMENT, LLC

484 US ROUTE 1 KITTERY, MAINE 03904

PROJECT:

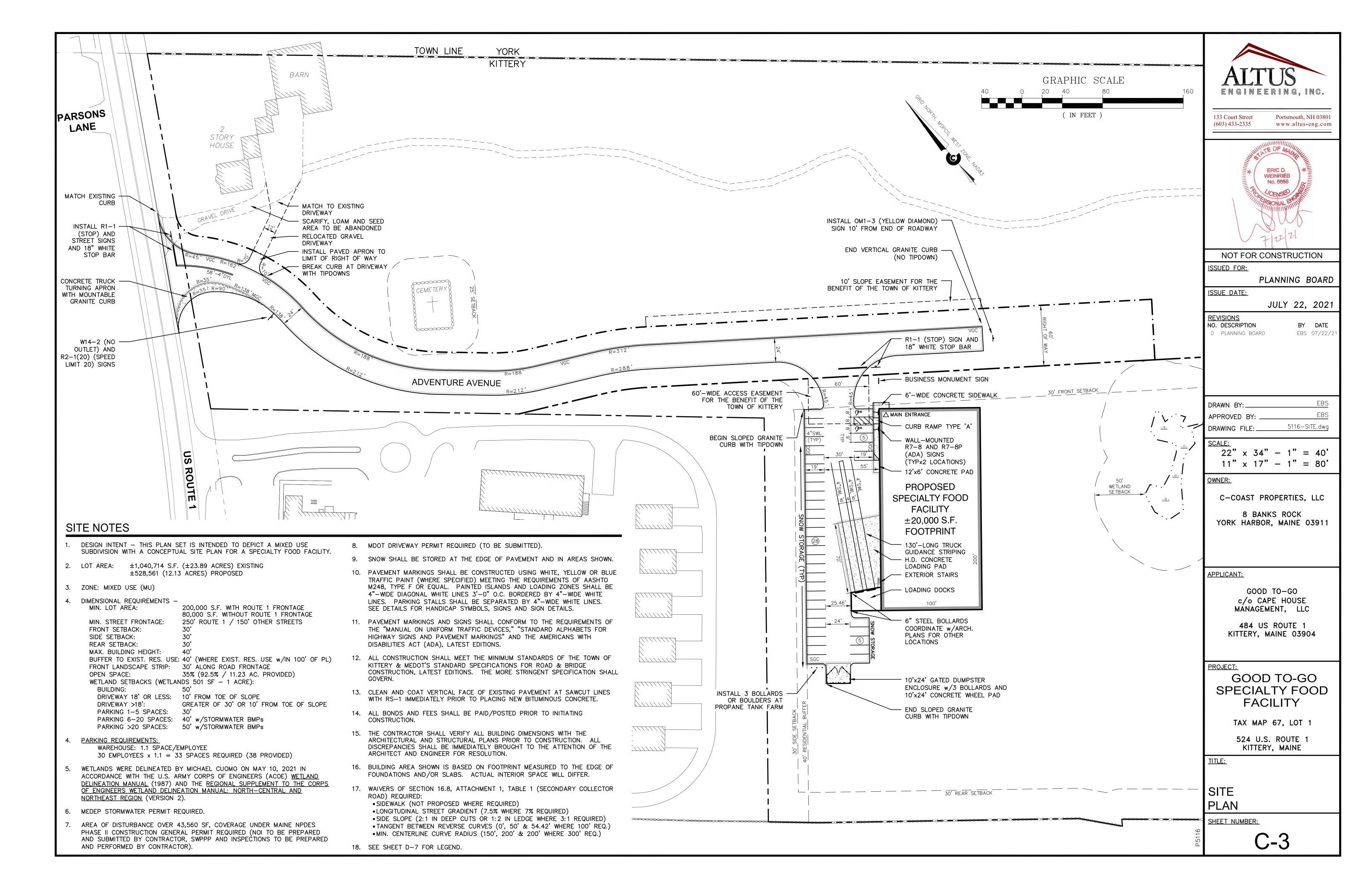
GOOD TO-GO SPECIALTY FOOD **FACILITY**

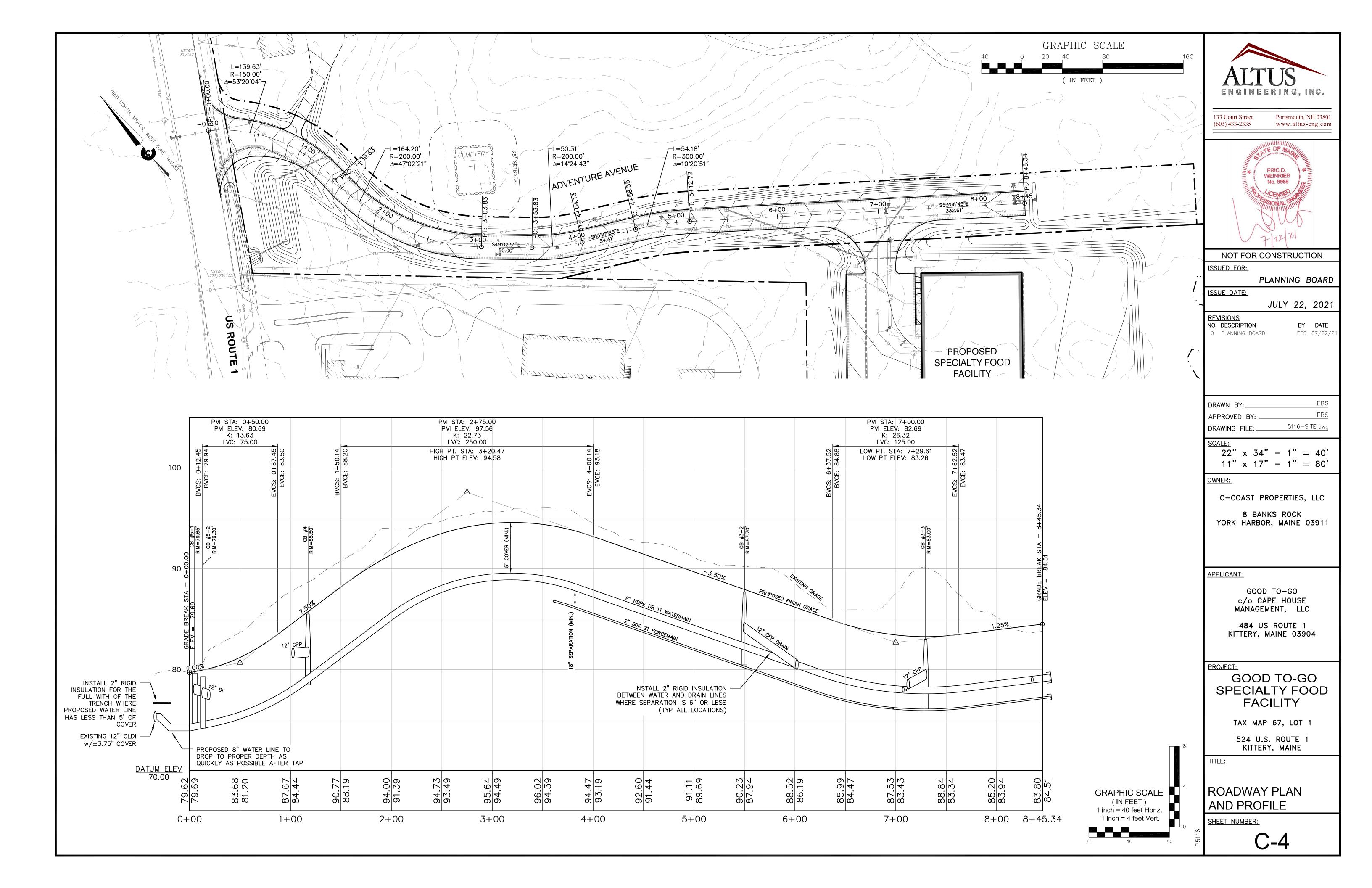
TAX MAP 67, LOT 1

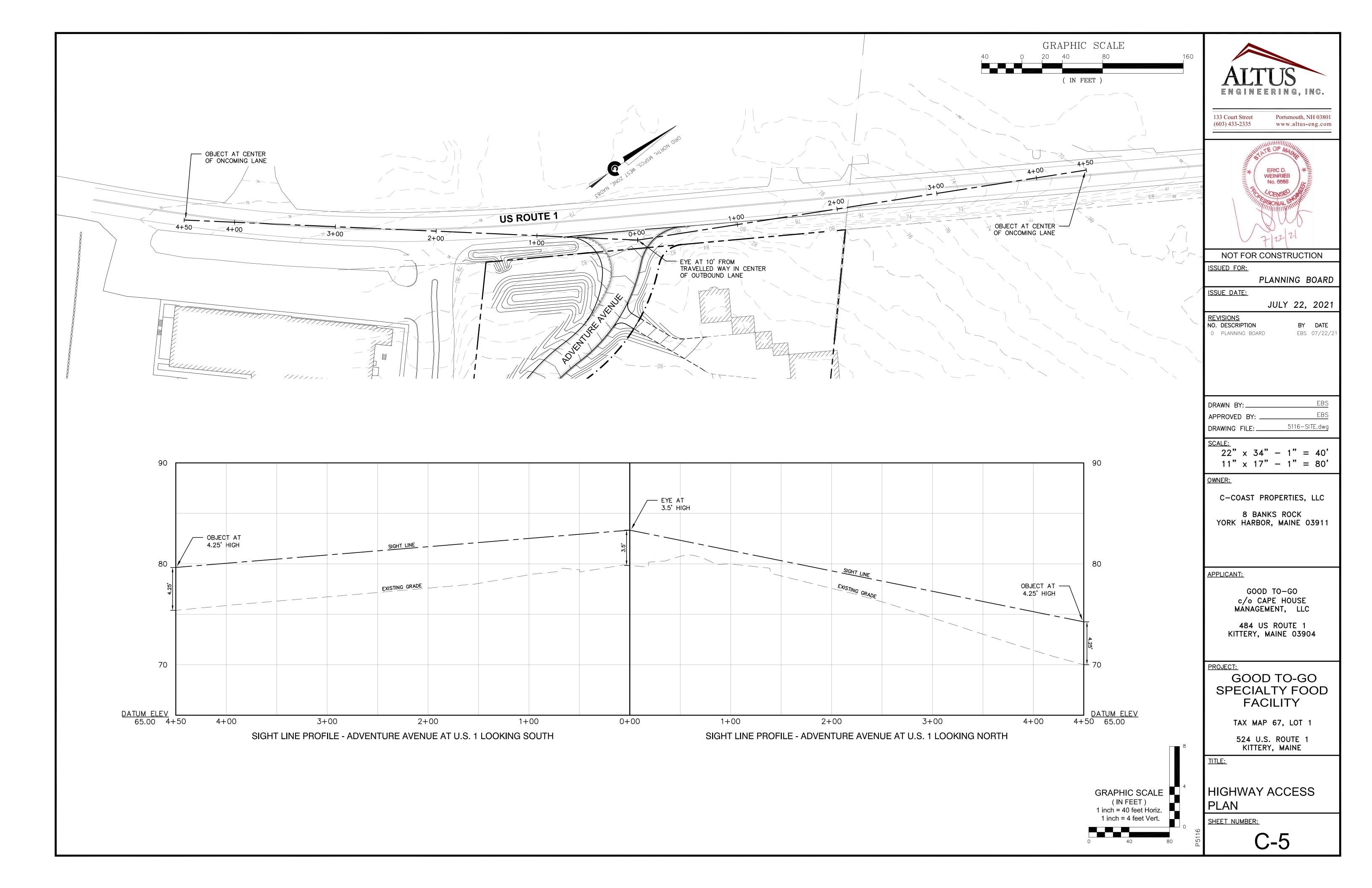
524 U.S. ROUTE 1

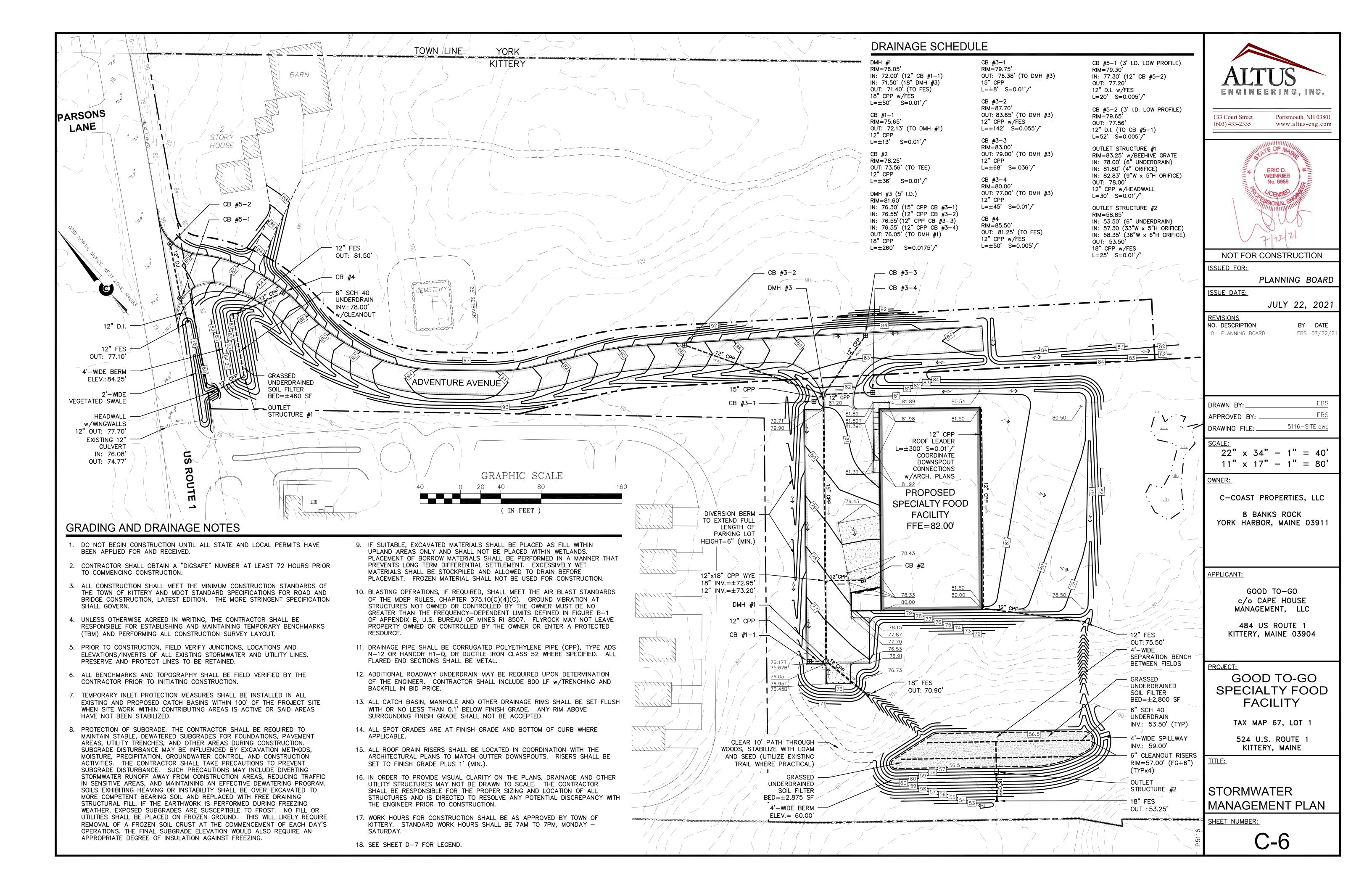
KITTERY, MAINE

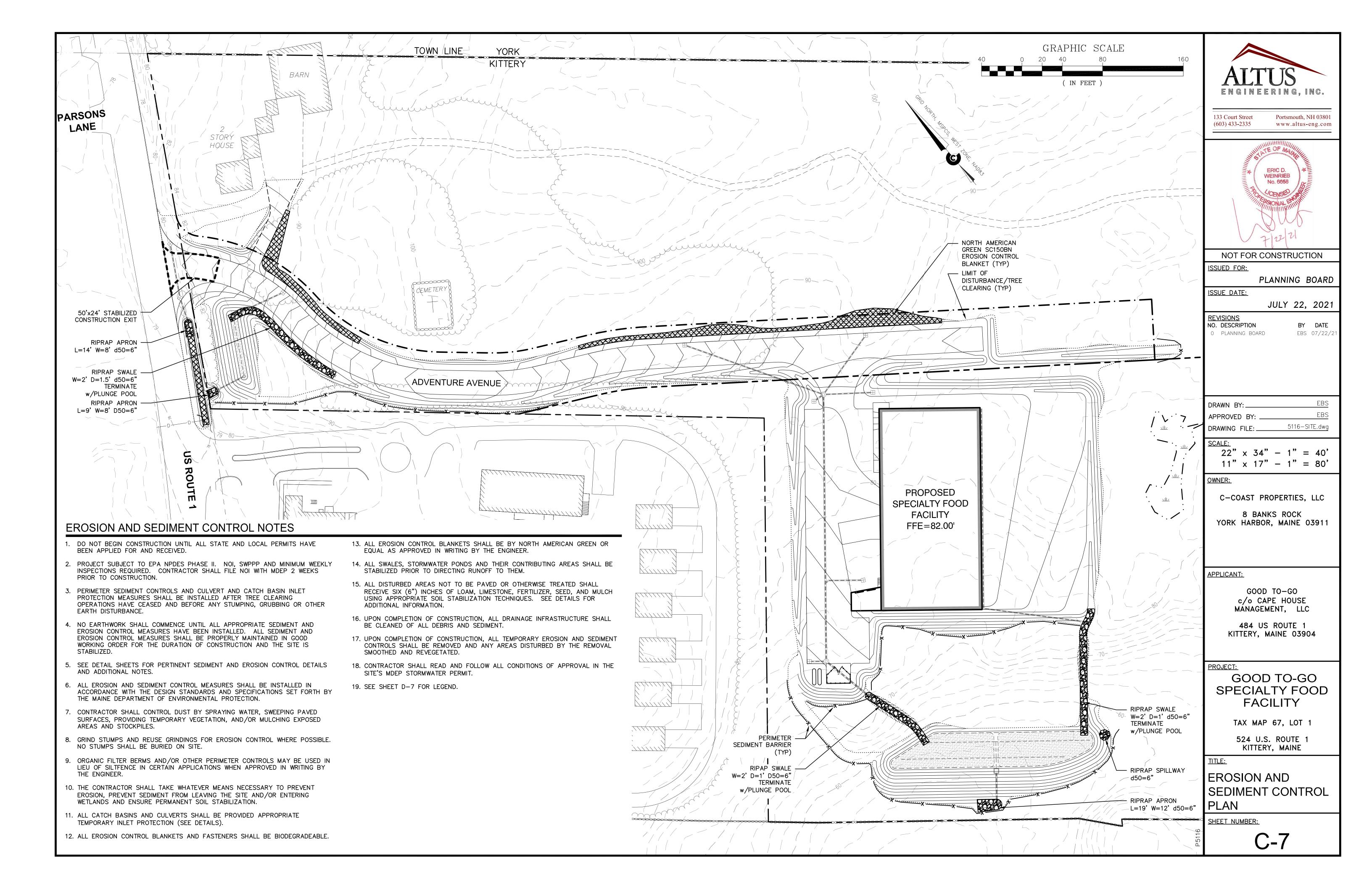
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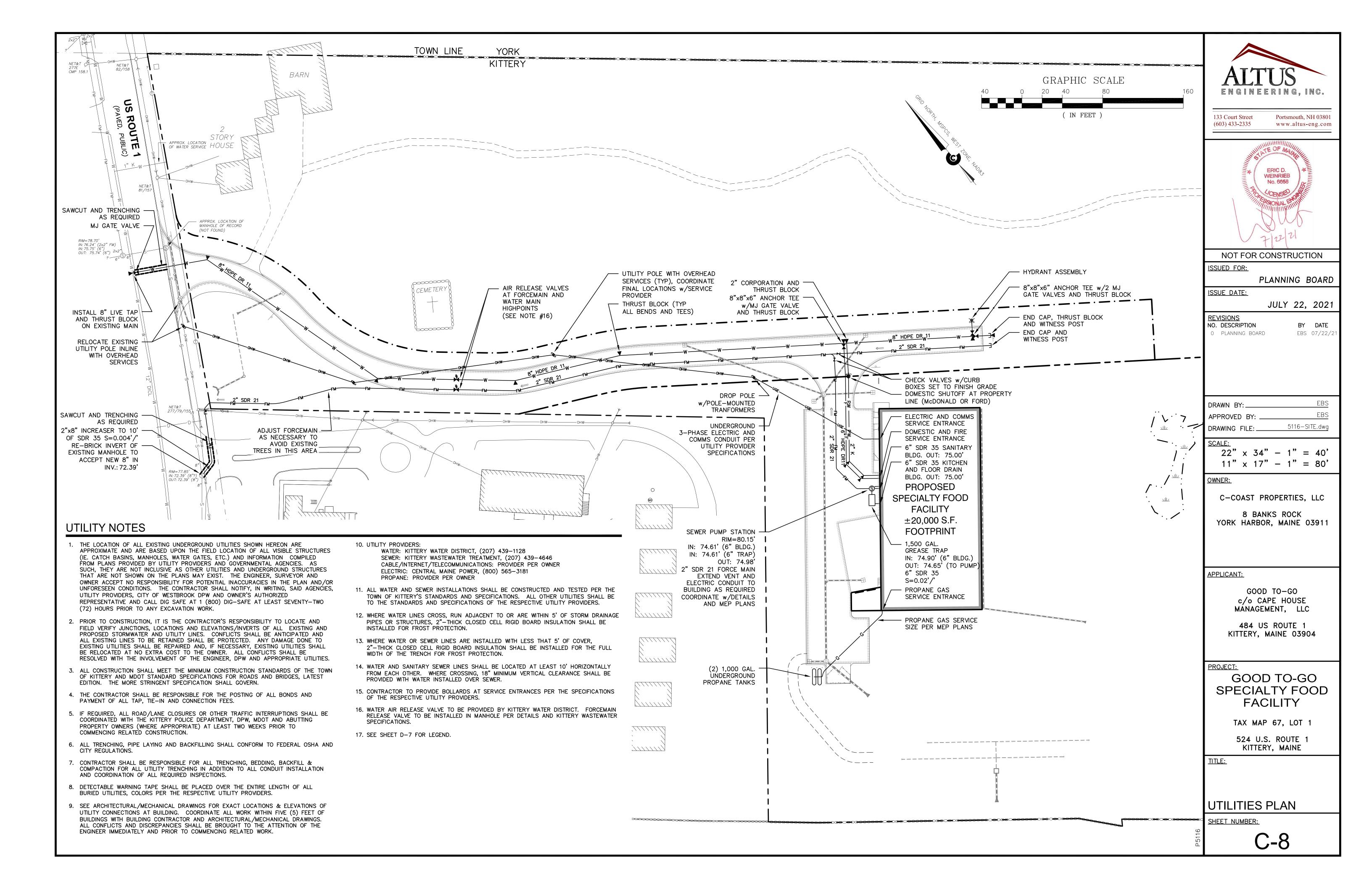


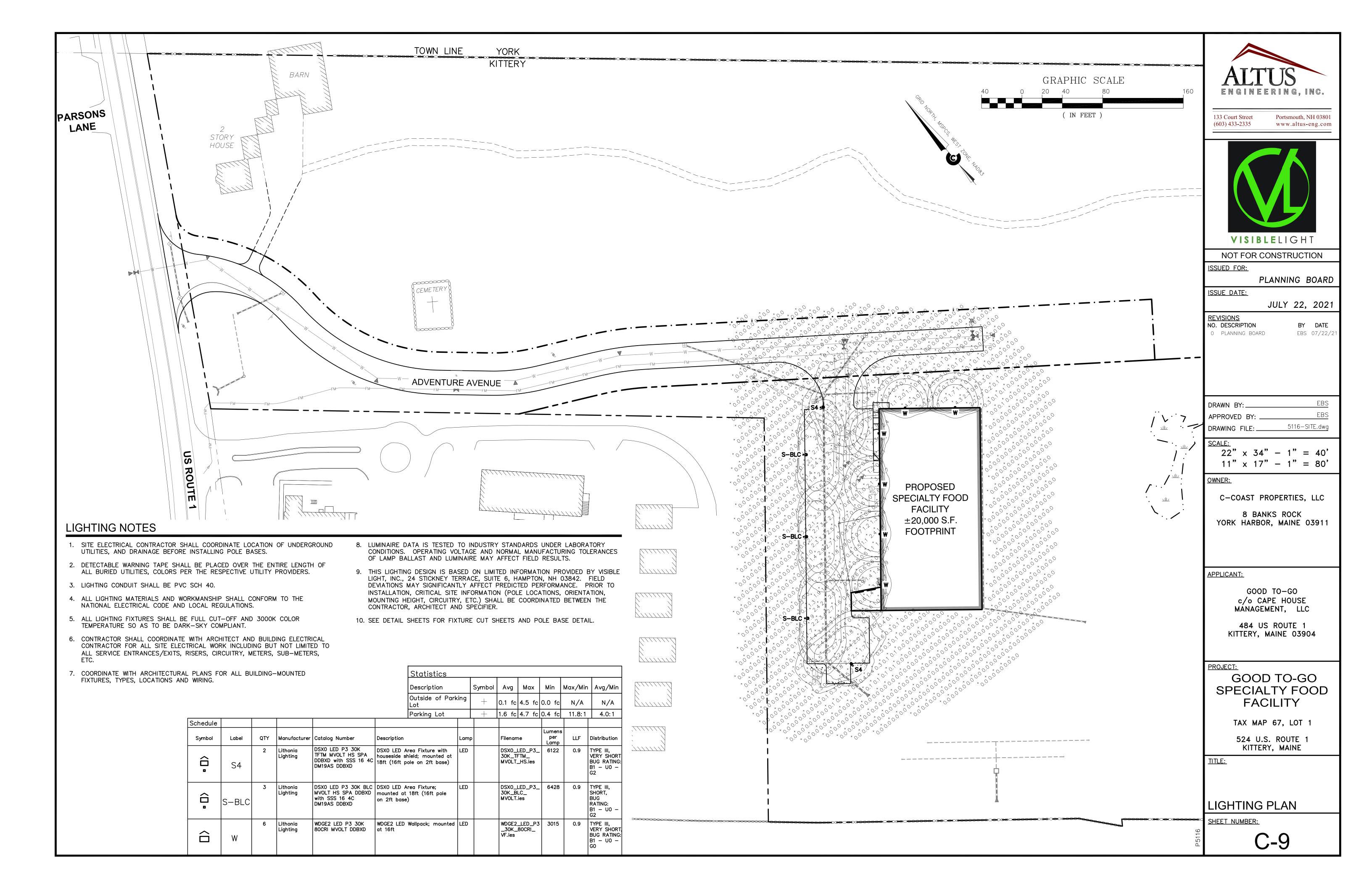


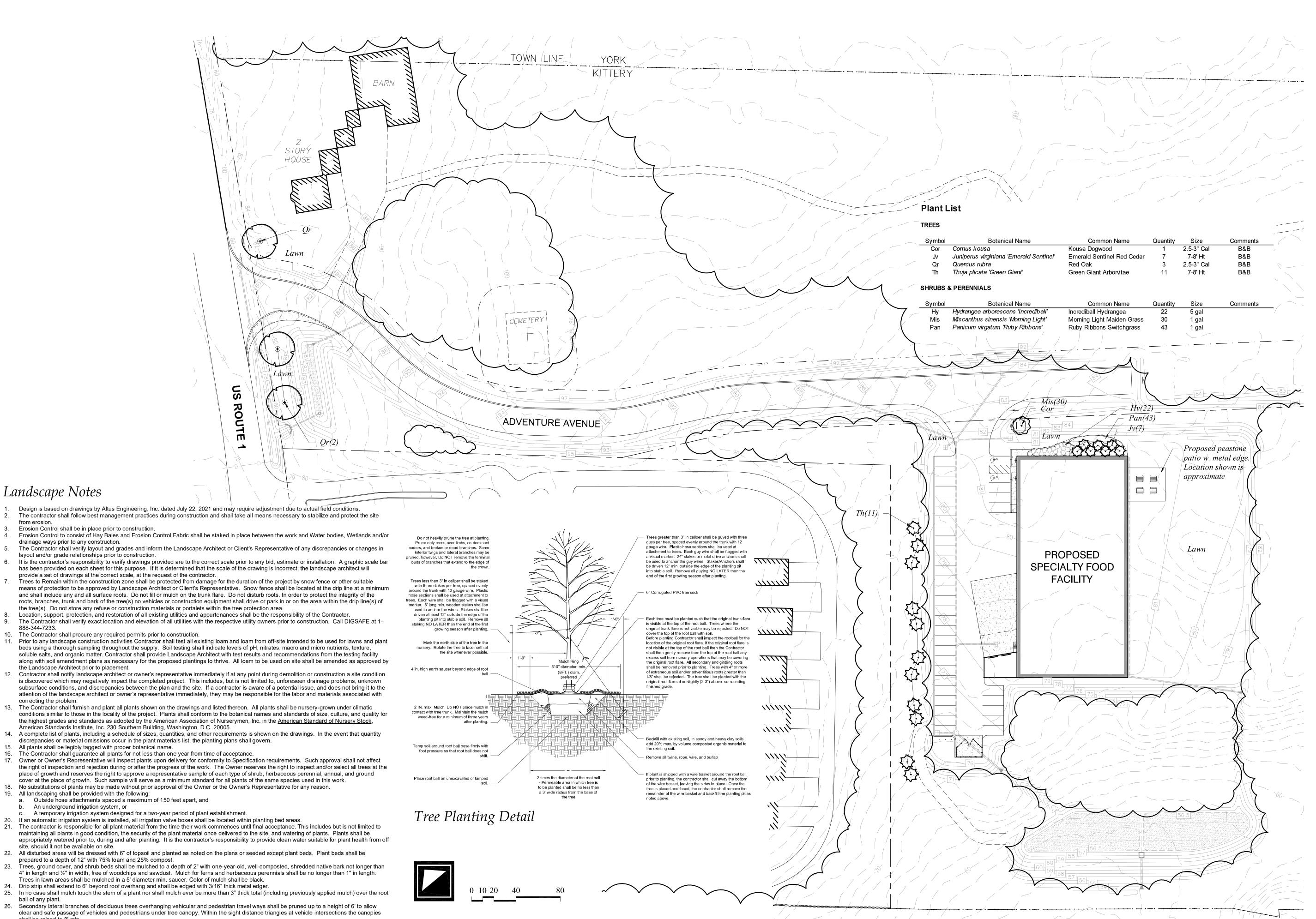












Landscape Notes

drainage ways prior to any construction.

the Landscape Architect prior to placement.

An underground irrigation system, or

27. Snow shall be stored a minimum of 5' from shrubs and trunks of trees.

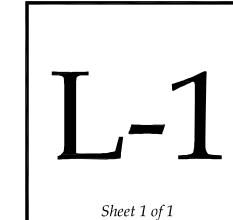
28. Landscape Architect is not responsible for the means and methods of the contractor.

site, should it not be available on site.



Facility **F00** alty 0

Drawn By: Checked By: $1 = 40^{\circ} - 0^{\circ}$ July 22, 2021 Date: Revisions:



SEDIMENT AND EROSION CONTROL NOTES

PROJECT NAME AND LOCATION

Good To-Go, Inc. 524 U.S. Route 1 Kittery, Maine

Latitude: 043° 07′ 52″ N Longitude: 070° 42′ 04″ W

DESCRIPTION

The project includes the development of a specialty food manufacturing facility with an access road, paved parking lot and associated utility and drainage improvements.

SEQUENCE OF MAJOR ACTIVITIES

- 1. Install temporary erosion control measures, including perimeter controls and stabilized
- construction entrances 2. Clear and grub wooded areas to the limits of work and strip and stockpile loam. Stockpiles shall be temporarily stabilized with hay mulch and surrounded by a hay bale or silt fence
- barrier until material is removed and final grading is complete.
- Rough grade site to include stormwater facilities. Construct building foundation.
- Construct drainage structures and utilities.
- Install roadway and parking lot base materials. Install pavement binder course.
- Complete building construction.
- Install curbing. 10. Install loam where required and stormwater basin filter material where specified.
- Install pavement top course.
- 12. Install other site features and landscaping.
- 13 Stabilize any remaining disturbed areas.
- 14. When all construction activity is complete and site is stabilized, remove perimeter controls and sediment that has been trapped by these devices.

NAME OF RECEIVING WATER

The site drains to the Atlantic Ocean by way of Johnson Brook.

TEMPORARY EROSION AND SEDIMENT CONTROLS AND STABILIZATION PRACTICES

All work shall be in accordance with state and local permits. Installation or construction of erosion control measures shall conform to the practices described in the "2014 Revision to the 2003 Maine Erosion and Sediment Control Field Guide for Contractors, published by the Maine Department of Environmental Protection

Minimum erosion control measures will need to be implemented and the contractor will be responsible to maintain all components of the erosion control plan until the site is fully stabilized. However, based on site and weather conditions during construction, additional erosion control measures may need to be implemented. All areas of instability and erosion must be repaired immediately during construction and need to be maintained until the site is fully stabilized or vegetation is established. A construction log must be maintained for the erosion and sedimentation control inspections and maintenance.

As indicated in the sequence of Major Activities, perimeter controls shall be installed prior to commencing any clearing or grading of the site. Structural controls shall be installed concurrently with the applicable activity. Once construction activity ceases permanently in an area, silt fences and hay bale barriers and any earth/dikes will be removed once permanent measures are established.

During construction, runoff will be diverted around the site with stabilized channels where possible channels where possible. Sheet runoff from the site will be filtered through hay bale barriers, stone check dams, and/or silt fences. All storm drain inlets shall be provided with inlet filters or stone check dams. Stone rip rap shall be provided at the outlets of drain pipes and culverts where shown

Temporary and permanent vegetation and mulching is an integral component of the erosion and sedimentation control plan. All areas shall be inspected and maintained until desires vegetative cover is established. These control measures are essential to erosion prevention and also reduce costly rework of graded and shaped areas.

Temporary vegetation shall be maintained in these areas until permanent seeding is applied. Additionally, erosion sedimentation measures shall be maintained until permanent vegetation is

INSTALLATION, MAINTENANCE AND INSPECTION PROCEDURES FOR TEMPORARY EROSION AND SEDIMENT CONTROL MEASURES

A. GENERAL

- Perimeter controls shall be installed prior to earth moving operations.
- The smallest practical portion of the site will be denuded at one time and no more than be mulched in one day. All disturbed areas must be stabilized by temporary measures within 5 days of initial disturbance and stabilized by permanent measures immediately after final
- Sediment barriers shall be installed downgradient of stockpiles and diversion swales installed upgradient of stockpiles to prevent movement of soil.
- Built—up sediment shall be removed from silt fence or other barriers when it has reached one—third the height of the tubular barrier or bale, or when "bulges" occur in silt fence.
- All diversion dikes shall be inspected and any breaches promptly repaired. Temporary seeding and planting shall be inspected for bare spots, washouts, and unhealthy
- 6. The owner's authorized engineer shall inspect the site on a periodic basis to review compliance with the plans.
- 7. All ditches and swales shall be stabilized prior to directing runoff to them. All diversion dikes will be inspected and any breaches promptly repaired.
- 8. Temporary water diversion (swales, basins, etc) shall be used as necessary until areas are
- 9. Ponds and swales shall be installed early on in the construction sequence (before rough grading site).
- 10. All cut and fill slopes shall be seeded/loamed within 72 hours of achieving finished grade. 11. An area shall be considered stable if one of the following has occurred:
- a. Base coarse gravels have been installed in areas to be paved;
- A minimum of 90% vegetated growth as been established; c. A minimum of 3 inches of non-erosive material such as stone of riprap has been installed;
- d. Erosion control blankets have been properly installed.

15), and over—winter (September 15 — April 15).

B. MULCHING

- <u>Application</u>
- * In sensitive areas (within 100 ft of streams, wetlands and in lake watersheds) temporary mulch shall be applied within 7 days of exposing soil or prior to any storm event. Areas, which have been temporarily or permanently seeded, shall be mulched immediately following seeding.
- Areas which cannot be seeded within the growing season shall be mulched for over—winter protection and the area should be seeded at the beginning of the growing season. * Mulch anchoring should be used on slopes greater than 5% in late fall (past September

Type of Mulch Hay or Straw Mulches

Organic mulches, including hay and straw, shall be air—dried, free of undesirable seeds and coarse materials. Application rate shall be 2 bales (70—90 pounds) per 1000 sq. ft. or 1.5 to 2 tons (90-100 bales) per acre to cover 75 to 90 % of the ground surface. Hay mulch subject to wind blowing shall be anchored via: netting; peg and twine or tracking.

Erosion control mix shall consist primarily of organic material and shall include any of the following: shredded bark, stump grindings, composted bark or other acceptable products based on a similar raw source. Wood or bark chips, ground construction debris or reprocessed wood products shall not be acceptable as the organic component of the mix. It can be used as a stand—alone reinforcement:

- On slopes 2 horizontal to 1 vertical or less.
- * On frozen ground or forested areas. * At the edge of gravel parking areas and areas under construction.

- Other reinforcement BMPs (i.e. riprap) should be used:
- * On slopes with groundwater seepage; At low points with concentrated flows and in gullies;
- At the bottom of steep perimeter slopes exceeding 100 feet in length;
- Below culvert outlet aprons; and * Around catch basins and closed storm systems.

Erosion control mix shall contain a well—graded mixture of particle sizes and may contain rocks less than 4" in diameter. Erosion control mix must be free of refuse, physical contaminants, and material toxic to plant growth. The mix composition shall meet the following standards:

- * The organic matter content shall be between 80 and 100%, dry weight basis. * Particle size by weight shall be 100% passing a 6" screen and a minimum of 70%,
- maximum of 85%, passing a 0.75" screen.
- * The organic portion needs to be fibrous and elongated. * Large portions of silts, clays or fine sands are not acceptable in the mix.

- * Erosion control mix shall not be used on slopes steeper than 2:1. * On slopes of 3:1 or less; 2 inches plus an additional 1/2 inch per 20 feet of slope up
- * On slopes between 3:1 and 2:1, 4 inch plus an additional 1/2 inch per 20 feet of slope up to 100 feet.
- The thickness of the mulch at the bottom of the slope needs to be: <3:1 slope slopes between 3:1 and 2:1 2.0" <20' of slope <60' of slope 3.0"
- <100' of slope 4.0" 6.0' * It shall be placed evenly and must provide 100% coverage with the soil totally invisible.

Any required repairs shall be made immediately, with additional erosion control mix placed on top of the mulch to reach the recommended thickness. When the mix is decomposed, clogged with sediment, eroded or ineffective, it shall be replaced or repaired. Erosion control mix mulch shall be left in place. If the mulch needs to be removed spread it out into the landscape.

All mulches must be inspected periodically, in particular after rainstorms, to check for rill erosion. If less than 90% of the soil surface is covered by mulch, additional mulch shall be immediately applied. Nets shall be inspected after rain events for dislocation or failure. If washouts or breakage occur, re-install the nets as necessary after repairing damage to the slope. Inspections shall take place until grasses are firmly established (95% soil surface covered with grass). Where mulch is used in conjunction with ornamental plantings, inspect periodically throughout the year to determine if mulch is maintaining coverage of the soil surface. Repair as

C. TEMPORARY VEGETATION

<u>Considerations</u>

- * Proper seedbed preparation and the use of quality seed are important in this practice just as in permanent seeding. Failure to carefully follow sound agronomic recommendations will often result in an inadequate stand of vegetation that provides little
- or no erosion control. * Nutrients and pesticides used to establish and maintain a vegetation cover shall be
- managed to protect the surface and ground water quality. * Temporary seeding shall be used extensively in sensitive areas (ponds and lake
- watersheds, steep slopes, streambanks, etc.). * Late fall seeding may fail and cause water quality deterioration in spring runoff events,
- thus other measures such as mulching shall be implemented.

<u>Specifications</u>

Apply limestone and fertilizer according to soil test recommendations. If soil testing is not feasible on small or variable sites, or where timing is critical, fertilizer may be applied at the rate of 600 pounds per acre or 13.8 pounds per 1,000 square feet of 10-10-10(N—P20S—K20) or equivalent. Apply limestone (equivalent to 50 percent calcium plus

magnesium oxide) at a rate of 3 tons per acre (138 lb. per 1,000 square feet).

- * Select seed from recommendations in enclosed table.
- * Where the soil has been compacted by construction operations, loosen soil to a depth of 2 inches before applying fertilizer, lime and seed. * Apply seed uniformly by hand, cyclone seeder, drill, cultipacker type seeder or hydroseeder (slurry including seed and fertilizer). Hydroseeding that includes mulch may be left on

Temporary seeding shall be periodically inspected. At a minimum, 95% of the soil surface should be covered by vegetation. If any evidence of erosion or sedimentation is apparent, repairs shall be made and other temporary measures used in the interim (mulch, filter barriers, check dams,

soil surface. Seeding rates must be increased 10% when hydroseeding.

Apply mulch over seeded area according to the TEMPORARY MULCHING BMP.

<u>Temporary</u> S	<u>Seeding Rates an</u>	<u>d Dates</u>		
Seed	Lb./Ac	Seeding Depth	Recommended Seeding Dates	Remarks
Winter Rye	112 (2.0 bu)	1-1.5 in	8/15-10/1	Good for fall seeding. Select a hardy species, such as Aroostook Rye.
Oats	80 (2.5 bu)	1-1.5 in		Best for spring seeding. -9/15 seeding will die when weather moved in, but mulch will provide
Annual Ryegrass	40	.25 in	4/1-7/1	Grows quickly but is of short duration. Use where appearance is important. With mulch, seeding may be done throughout growing season.
Sudangrass	40 (1.0 bu)	.5-1 in	5/15-8/15	Good growth during hot summer periods.
Perennial	40 (2.0 bu)	.25 in	8/15-9/15	Good cover, longer lasting than Annual Ryegrass. Mulching will allow seeding throughout growing season.
Temporary mulch v	vith or		10/1-4/1	Refer to TEMPORARY

D. FILTERS

<u>Tubular Sediment Barrier</u>

a. To be provided by an approved manufacturer or supplier:

MULCHING BMP and/or without dormant seeding

b. Installed per manufacturer's specifications; c. Barrier shall be removed when they have served their useful purpose but not before the upslope areas has been permanently stabilized.

<u>Organic Filter Berm</u> See detail

PERMANENT VEGETATION BMP.

* Sediment barriers shall be installed along the down gradient side of proposed ground disturbance areas prior to any construction activities. * The barrier must be placed along a relatively level contour.

<u>Maintenance</u>

Hay bale barriers, silt fences and filter berms shall be inspected immediately after each rainfall and at least daily during prolonged rainfall. They shall be repaired immediately if there are any signs of erosion or sedimentation below them. If there are signs of undercutting at the center or the edges of the barrier, or impounding of large volumes of water behind them, sediment barriers shall be replaced with a temporary check dam.

- * Should the fabric on a silt fence or filter barrier decompose or become ineffective prior to the end of the expected usable life and the barrier still is necessary, the fabric shall
- * Sediment deposits should be removed when deposits reach approximately one third (1/3)
- the height of the barrier. Filter berms should be reshaped as needed. * Any sediment deposits remaining in place after the silt fence or filter barrier is no longer
- required shall be dressed or removed to conform to the existing grade, prepared and * Additional stone may have to be added to the construction stabilized entrance, rock barriers, stone lined swales, etc., periodically to maintain proper function of the erosion

E. PERMANENT SEEDING

- 1. Bedding stones larger than $1\frac{1}{2}$, trash, roots, and other debris that will interfere with seeding and future maintenance of the area should be removed. Where feasible, the soil should be tilled to a depth of 6" to prepare a seedbed and mix fertilizer (refer to Landscape Drawings and Specifications) into the soil.
- 2. Fertilizer (refer to Landscape Drawings and Specifications) lime and fertilizer should be applied evenly over the area prior to or at the time of seeding and incorporated into the soil. Kinds and amounts of lime and fertilizer should be based on an evaluation of soil
- 3. Seed Mixture (See Landscape Drawings for additional information): 3.1. Lawn seed mix shall be a fresh, clean new seed crop. The Contractor shall furnish a dealer's quaranteed statement of the composition of the mixture and the percentage

of purity and germination of each variety.

3.2. Seed mixture shall conform to landscape specifications 4. Sodding — sodding is done where it is desirable to rapidly establish cover on a disturbed area. Sodding an area may be substituted for permanent seeding procedures anywhere on site. Bed preparation, fertilizing, and placement of sod shall be performed according to the S.C.S. Handbook. Sodding is recommended for steep sloped areas, areas immediately adjacent to sensitive water courses, easily erodible soils (fine sand/silt), etc.

A dewatering plan shall be implemented to address excavation de—watering following heavy rainfall events or where the excavation may intercept the groundwater table during construction. The collected water needs treatment and a discharge point that will not cause downgradient erosion and offsite sedimentation or within a resource.

All dewatering discharge locations shall be located on relatively flat ground at least 75' from streams and 25' from wetlands. The contractor shall utilize dirtbags, erosion control mix berms, or similar methods for filtration of dewatering and shall conform to the Maine Erosion and Sediment Control BMPs.

MONITORING SCHEDULE

The contractor shall be responsible for installing, monitoring, maintaining, repairing, replacing and removing all of the erosion and sedimentation controls or appointing a qualified subcontractor to do so. Maintenance measures will be applied as needed during the entire construction cycle. immediately following any significant rainfall, and at least once a week, a visual inspection will be made of all erosion and sedimentation controls as follows:

excavated when it reaches a depth of 6" and redistributed to areas undergoing final grading. 2. Construction entrance shall be visually inspected and repaired as needed. Any areas subject to rutting shall be stabilized immediately. If the voids of the construction entrance become filled with mud, more crushed stone shall be added as needed. The public roadway shall be swept should mud be deposited/tracked onto them.

1. Silt fence shall be inspected and repaired. Sediment trapped behind these barriers shall be

STANDARDS FOR STABILIZING SITES FOR THE WINTER

- The following standards and methodologies shall be used for stabilizing the site during the winter construction period:
- 1. Standard for the timely stabilization of disturbed slopes (any area having a grade greater than 25%) — the contractor will seed and mulch all slopes to be vegetated by September 15th. If the contractor fails to stabilize any slope to be vegetated by September 15th, then the contractor will take one of the following actions to stabilize the slope for late fall and
- A. Stabilize the soil with temporary vegetation and erosion control mats: by October 1st the contractor will seed the disturbed slope with winter rye at a rate of 3 pounds per 1000 square feet and then install erosion control mats or anchored hay mulch over the seeding. The contractor will monitor growth of the rye over the next 30 days.
- B. <u>Stabilize the slope with wood-waste compost</u>: the contractor will place a six-inch layer of wood-waste compost on the slope by November 15th. The contractor will not use wood-waste compost to stabilize slopes having grades greater than 50% (2h:iv) or having groundwater seeps on the slope face.
- C. Stabilize the slope with stone riprap: the contractor will place a layer of stone riprap on the slope by November 15th. The development's owner will hire a registered professional engineer to determine the stone size needed for stability on the slope and to design a filter layer for

2. Standard for the timely stabilization of disturbed soils — by September 15th the contractor

- will seed and mulch all disturbed soils on the site. If the contractor fails to stabilize these soils by this date, then the contractor will take on of the following actions to stabilize the soil for late fall and winter. A. <u>Stabilize the soil with temporary vegetation</u>: by October 1st the contractor will seed the disturbed soil with winter rye at a seeding rate of 3 pounds per 1000 square feet, lightly mulch the seeded soil with hay or straw at 75 pounds per 1000 square feet, and anchor the mulch with plastic netting. The contractor will monitor growth of the rye over the next 30 days. If the rye fails to
- then the contractor will mulch the area for over-winter protection as described in item iii of this B. Stabilize the soil with sod: the contractor will stabilize the disturbed soil with properly installed sod by October 1st. proper installation includes the contractor pinning the sod onto the soil with wire pins, rolling the sod to guarantee contact between the sod and underlying soil, and watering the sod to promote root growth into the disturbed soil.

grow at least three inches or fails to cover at least 75% of the disturbed soil before November 1,

C. <u>Stabilize the soil with mulch</u>: by November 15th the contractor will mulch the disturbed soil by spreading hay or straw at a rate of at least 150 pounds per 1000 square feet on the area so that no soil is visible through the mulch. Immediately after applying the mulch, the contractor will anchor the mulch with netting or other method to prevent wind from moving the mulch off

Winter inspections shall be preformed after, each rainfall, snowstorm or thawing and at least once a week. All areas within 75 feet of a protected natural resource must be protected with a double row of sediment barrier.

EROSION CONTROL REMOVAL

- An area is considered stable if it is paved or if 90% growth of planted seeds is established. once an area is considered stable, the erosion control measures can be removed as follows: 1. <u>Silt Fence</u>: Silt fence shall be disposed of legally and properly off—site. all sediment trapped behind these controls shall be distributed to an area undergoing final grading or removed and
- relocated off-site. 2. <u>Stabilized Construction Entrance</u>: The stabilized construction entrance shall be removed once the compacted roadway base in in place. Stone and sediment from the construction entrance shall be redistributed to an area undergoing grading or removed and relocated
- 3. <u>Miscellaneous</u>: Once all the trapped sediments have been removed from the temporary sedimentation devices the disturbed areas must be regraded in an aesthetic manner to conform to the surrounding topography. Once graded these disturbed areas must be loamed (if necessary), fertilized, seeded and mulched in accordance with the rates previously stated.

The above erosion controls must be removed within 30 days of final stabilization of the site. Conformance with this plan and following these practices will result in a project that complies with the state regulations and the standards of the natural resources protection act, and will protect water quality in areas downstream from the project.

INSPECTION AND MAINTENANCE

- 1. All sediment control measures shall be inspected at least once each week and following any storm event of 0.25 inches or greater. An inspection report shall be made after each inspection by a qualified inspector engaged by the Owner. The qualified inspector shall be a Professional Engineer licensed in Maine or be a Certified Professional in Erosion and Sediment Control approved by the Owner.
- 2. All measures shall be maintained in good working order; if a repair is necessary, it will be
- initiated within 24 hours and completed within 72 hours. Inspection and maintenance requirements: Inspect disturbed and impervious areas, erosion and stormwater control measures, areas used for storage that are exposed to precipitation, and locations where vehicles enter or exit the site. Inspect these areas at least once a week as well as before and after a 0.5 inches or greater storm event and prior to completion of permanent stabilization measures. A person with knowledge of erosion and stormwater control, including the standards in the MCGP and any departmental companion document to the MCGP, must conduct the inspection. This person must be identified in the inspection log. If best management practices (BMPs) need to be modified or if additional BMPs are necessary, implementation must be completed within 7 calendar days and prior to any storm event (rainfall). All measures must be maintained in effective operating condition until areas area permanently stabilized.
- 4. Inspection Log (report): A log (report) must be kept summarizing the scope of the inspection, name(s) and qualifications of the personnel making the inspection, the date(s) of the inspection, and major observations relating to operation of erosion and sedimentation controls and pollution prevention measures. Major observations must include BMPs that need maintenance, BMPs that failed to operate as designed or proved inadequate for a particular location, and locations(s) where additional BMPs are needed. For each BMP requiring maintenance, BMP needing replacement, and location needing additional BMPs, note in the inspection log the correct action taken and when it was taken. The log must be made accessible to the department staff and a copy must be provided upon request. The permittee shall retain a copy of the log for a period of at least three years from the completion of the permanent stabilization.

Spill prevention: Controls must be used to prevent pollutants from construction and waste materials stored onsite, including storage practices to minimize exposure of the materials to stormwater and appropriate spill prevention, containment, and response planning implementation. The contractor and owners need to take care with construction and waste materials such that contaminates do not enter the stormwater. The storage of materials such as paint, petroleum products, cleaning agents and the like are to be stored in watertight containers. The use of the products should be in accordance with manufacturer recommendations. When fueling equipment, including snowblowers and lawnmowers, have oil absorbent pads available below the fueling. Refueling of small engines by the owner should occur in the garage or on a paved surface. Any spill or release of toxic or hazardous substances must be reported to the department. For oil spills, call 1-800-482-0777 which is available 24 hours a day. For spills of toxic or hazardous material, call 1—800—452—4664 which is available 24 hours a day. For more information, visit the department's website at: HTTP: /WWW.MAINE.GOV/DEP/SPILLS/EMERGSPILLRESP/

- 2. Groundwater protection: Protection of the groundwater is required by the contractor and owner. During construction, liquid petroleum products and other hazardous materials with the potential to contaminate groundwater may not be stored or handled in areas of the site draining to an infiltration area. An "infiltration area" is any area of the site that by design or as a result of soils, topography, and other relevant factors accumulates runoff that infiltrates into the soil. Petroleum products should be stored in manufactured cans designed for the purpose. Dikes, berms, sumps, and other forms of secondary containment that prevent discharge to groundwater may be used to isolate portions of the site for the purposes of storage and handling of these materials. Spill preventions procedures should be
- Lack of appropriate pollutant removal BMPs may result in violations of the groundwater quality standard established by 39 M.R.S.A. §465-C(1). Any project proposing infiltration of stormwater must provide adequate pre-treatment of stormwater prior to discharge of stormwater to the infiltration area, or provide treatment within the infiltration area, in order to prevent accumulation of fines, reductions in infiltration rate, and consequent flooding and
- 3. Fugitive sediment and dust: Actions must be taken to ensure that activities do not result in noticeable erosion of soils or fugitive dust emissions during or after construction. Oil may not be used for dust control.
- Note: Dewatering a stream without a permit from the department violates state water quality standards and the Natural Resources Protection Act.
- 4. Debris and other materials: Litter, construction debris, and construction chemicals exposed to stormwater must be prevented from becoming a pollutant source. Construction materials and construction debris should be covered to prevent rainwater from washing contaminants off the site. Any fertilizers, cleaning products, herbicides should be protected from the weather and
- Any contaminants that are washed off the site by rainwater is a violation of the Clean Waters Act. To prevent these materials from becoming a source of pollutants, construction activities related to a project may be required to comply with applicable provisions of rules related to solid, universal, and hazardous waste, including, but not limited to, the Maine Solid Waste and Hazardous Waste Management Rules; Maine Hazardous Waste Management Rules; Maine Oil Conveyance and Storage Rules; and Maine Pesticide requirements.
- 5. Trench or foundation dewatering: Trench dewatering is the removal of water from trenches, foundations, coffer dams, ponds, and other areas within the construction area that retain water after excavation. In most cases the collected water is heavily silted and hinders correct and safe construction practices. The collected water removed from the ponded area, either through gravity or pumping, must be spread through natural wooded buffers or removed to areas that are specifically designed to collect the maximum amount of sediment possible, like a cofferdam sedimentation basin. Avoid allowing the water to flow over disturbed
- For guidance on dewatering controls, consult the Maine Erosion and Sediment Control BMPs, published by the Maine Department of Environmental Protection.
 - 6. Non-stormwater discharges: Identify and prevent contamination by non-stormwater discharges. Where allowed non-stormwater discharges exist, they must be identified and steps should be taken to ensure the implementation of appropriate pollution prevention measures for the non-stormwater component(s) of the discharge. Authorized
 - non-stormwater discharges are:

Uncontaminated excavation dewatering

- Discharges from firefighting activities
- Fire hydrant flushings • Vehicle washwater if detergents are not used and washing is limited to the exterior of vehicles (engine, undercarriage, and transmission washing is prohibited
- Routine external building washdown, not including surface paint removal, that does not involve detergents • Pavement washwater (where spills/leaks of toxic or hazardous materials have not
- occurred, unless all spilled material had been removed) if detergents are not used • Uncontaminated air conditioning or compressor condensate
- Uncontaminated groundwater or spring water Foundation or footer drain—water where flows are not contaminated

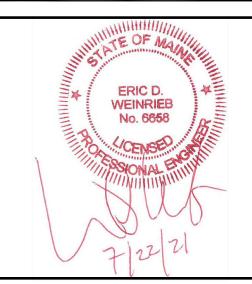
• Dust control runoff in accordance with permit conditions

- Potable water sources including waterline flushings
- 7. Unauthorized non-stormwater discharges: Identify and prevent contamination from discharges that is mixed with a source of non-stormwater, other than those discharges in compliance with 6. Unauthorized non-stormwater discharges are:
 - Wastewater from the washout or cleanout of concrete, stucco, paint, form release oils, curing compounds or other construction materials; • Fuels, oils, or other pollutants used in vehicle and equipment operations and
- Toxic or hazardous substances from a spill or other release.

• Soaps, solvents or detergents used in vehicle and equipment wash;

Allowable non-stormwater discharges cannot be authorized unless they are directly related to and originate from a construction site or dedicated support activity.

133 Court Street Portsmouth, NH 03801 (603) 433-2335 www.altus-eng.com



NOT FOR CONSTRUCTION

ISSUE DATE:

ISSUED FOR:

PLANNING BOARD

JULY 22, 2021

BY DATE

EBS 07/22/2

EBS

5116-SITE.dwg

REVISIONS NO. DESCRIPTION

O PLANNING BOARD

SCALE:

DRAWN BY:.

APPROVED BY: ___

DRAWING FILE: __

NOT TO SCALE

C-COAST PROPERTIES, LLC

8 BANKS ROCK YORK HARBOR, MAINE 03911

APPLICANT:

GOOD TO-GO c/o CAPE HOUSE

GOOD TO-GO SPECIALTY FOOD

EROSION AND

NOTES

MANAGEMENT, LLC 484 US ROUTE 1 KITTERY, MAINE 03904

PROJECT:

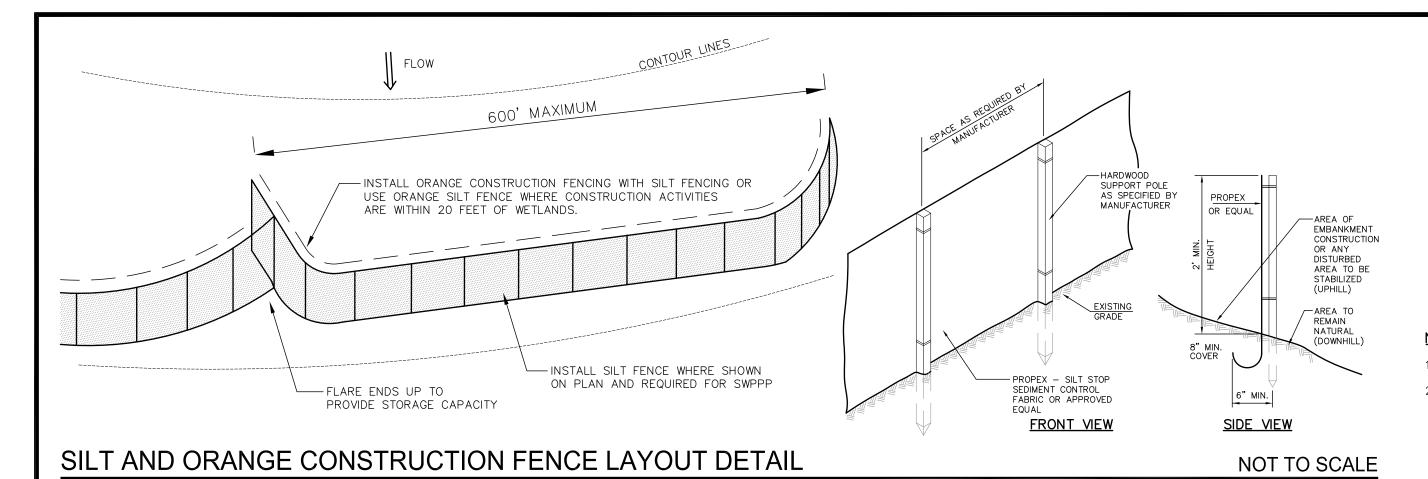
FACILITY

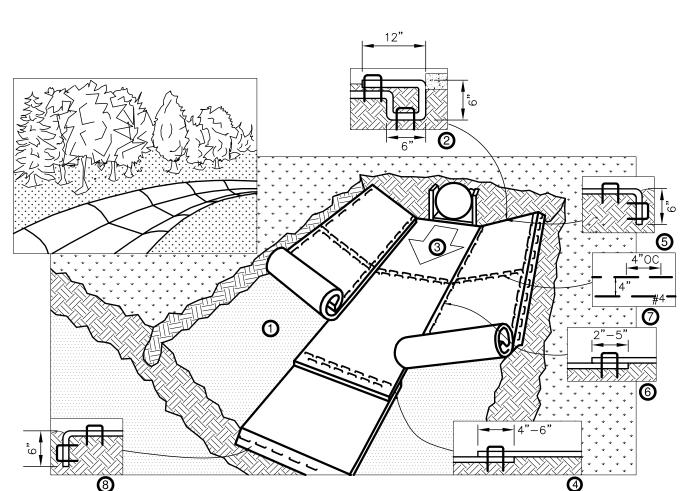
TAX MAP 67, LOT 1

524 U.S. ROUTE 1 KITTERY, MAINE

SEDIMENT CONTROL

SHEET NUMBER:





STAKE (TYP.); STAKE ON 10' LINEAR SPACING REBAR W/ORANGE SAFETY CAP MAY BE USED IN PAVED SURFACE ONLY FILTREXX® 12" SILT-SOXX^{IM}-WATER FLOW PROTECTED AREA TO BE \Longrightarrow WORK AREA PROTECTED WORK AREA - FILTREXX $^{ ext{(B)}}$ COMPOST SILT-SOXX IM <u>SECTION</u>

SILTSOXX MAY BY USED IN PLACE OF SILT FENCE OR OTHER SEDIMENT BARRIERS.

2. ALL MATERIAL TO MEET FILTREXX SPECIFICATIONS. 3. SILTSOXX COMPOST/SOIL/ROCK/SEED FILL MATERIAL SHALL BE ADJUSTED AS NECESSARY TO MEET THE REQUIREMENTS OF THE SPECIFIC APPLICATION.

4. ALL SEDIMENT TRAPPED BY SILTSOXX SHALL BE DISPOSED OF PROPERLY TUBULAR SEDIMENT BARRIER

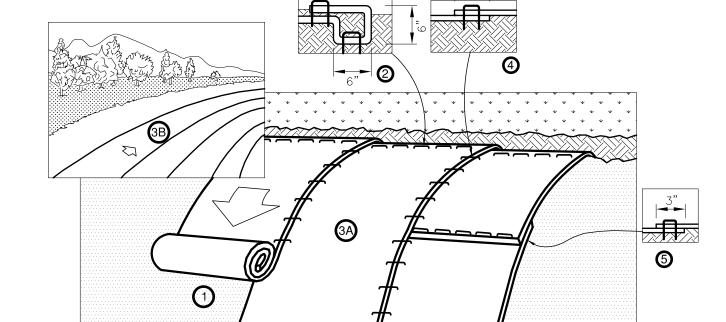
FERTILIZER, AND SEED.

IN THE STAPLE PATTERN GUIDE.

ON THE PREVIOUSLY INSTALLED BLANKET.

NOT TO SCALE

____ 2" x 2" WOODEN



1. PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING ANY NECESSARY APPLICATION OF LIME,

ANCHOR THE BLANKET WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN THE

COMPACTED SOIL AND FOLD REMAINING 12" PORTION OF BLANKET BACK OVER SEED AND COMPACTED SOIL. SECURE BLANKET OVER COMPACTED SOIL WITH A ROW OF STAPLES/STAKES

3. ROLL THE BLANKETS (A) DOWN OR (B) HORIZONTALLY ACROSS THE SLOPE. BLANKETS WILL

4. THE EDGES OF PARALLEL BLANKETS MUST BE STAPLED WITH APPROXIMATELY 2"-5" OVERLAP

5. CONSECUTIVE BLANKETS SPLICED DOWN THE SLOPE MUST BE PLACED END OVER END (SHINGLE

STAKE LENGTHS GREATER THAN 6" MAY BE NECESSARY TO PROPERLY SECURE THE BLANKETS.

SPACED APPROXIMATELY 12" APART ACROSS THE WIDTH OF THE BLANKET.

2. BEGIN AT THE TOP OF THE SLOPE BY ANCHORING THE BLANKET IN A 6" DEEP BY 6" WIDE TRENCH

WITH APPROXIMATELY 12" OF BLANKET EXTENDED BEYOND THE UP-SLOPE PORTION OF THE TRENCH.

BOTTOM OF THE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING. APPLY SEED TO

UNROLL WITH APPROPRIATE SIDE AGAINST THE SOIL SURFACE. ALL BLANKETS MUST BE SECURELY

FASTENED TO SOIL SURFACE BY PLACING STAPLES/STAKES IN APPROPRIATE LOCATIONS AS SHOWN

DEPENDING ON BLANKET TYPE. TO ENSURE PROPER SEAM ALIGNMENT, PLACE THE EDGE OF THE

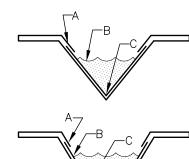
OVERLAPPING BLANKET (BLANKET BEING INSTALLED ON TOP) EVEN WITH THE COLORED SEAM STITCH

STYLE) WITH AN APPROXIMATE 3" OVERLAP. STAPLE THROUGH OVERLAPPED AREA, APPROXIMATELY 12"

APART ACROSS ENTIRE BLANKET WIDTH. NOTE: IN LOOSE SOIL CONDITIONS, THE USE OF STAPLE OR

<u>NOTES</u>

- . PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING ANY NECESSARY APPLICATION OF LIME, FERTILIZER, AND SEED.
- 2. BEGIN AT THE TOP OF THE CHANNEL BY ANCHORING THE BLANKET IN A 6" DEEP BY 6" WIDE TRENCH WITH APPROXIMATELY 12" OF BLANKET EXTENDED BEYOND THE UP-SLOPE PORTION OF THE TRENCH. ANCHOR THE BLANKET WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN THE BOTTOM OF THE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING. APPLY SEED TO COMPACTED SOIL AND FOLD REMAINING 12" PORTION OF BLANKET BACK OVER SEED AND COMPACTED SOIL. SECURE BLANKET OVER COMPACTED SOIL WITH A ROW OF STAPLES/STAKES SPACED APPROXIMATELY 12" APART ACROSS THE WIDTH OF THE BLANKET.
- 3. ROLL CENTER BLANKET IN DIRECTION OF WATER FLOW IN BOTTOM OF CHANNEL. BLANKETS WILL UNROLL WITH APPROPRIATE SIDE AGAINST THE SOIL SURFACE. ALL BLANKETS MUST BE SECURELY FASTENED TO SOIL SURFACE BY PLACING STAPLES/STAKES IN APPROPRIATE LOCATIONS AS SHOWN IN THE STAPLE PATTERN GUIDE.
- 4. PLACE CONSECUTIVE BLANKETS END OVER END (SHINGLE STYLE) WITH A 4"-6" OVERLAP. USE A DOUBLE ROW OF STAPLES STAGGERED 4" APART AND 4" ON CENTER TO SECURE BLANKETS.
- 5. FULL LENGTH EDGE OF BLANKETS AT TOP OF SIDE SLOPES MUST BE ANCHORED WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN A 6" DEEP BY 6" WIDE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING.
- 6. ADJACENT BLANKETS MUST BE OVERLAPPED APPROXIMATELY 2"-5" (DEPENDING ON BLANKET TYPE) AND STAPLED. TO INSURE PROPER SEAM ALIGNMENT, PLACE THE EDGE OF THE OVERLAPPING BLANKET (BLANKET BEING INSTALLED ON TOP) EVEN WITH THE COLORED SEAM STITCH ON THE BLANKET BEING OVERLAPPED.
- 7. IN HIGH FLOW CHANNEL APPLICATIONS, A STAPLE CHECK SLOT IS RECOMMENDED AT 30 TO 40 FOOT INTERVALS. USE A DOUBLE ROW OF STAPLES STAGGERED 4" APART AND 4" ON CENTER OVER ENTIRE WIDTH OF THE CHANNEL.
- 8. THE TERMINAL END OF THE BLANKETS MUST BE ANCHORED WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN A 6" DEEP BY 6" WIDE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING.



CRITICAL POINTS:

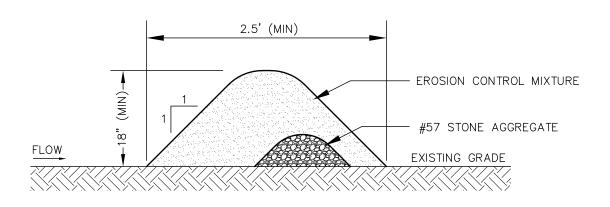
- . OVERLAPS AND SEAMS 3. PROJECTED WATER LINE
- C. CHANNEL BOTTOM/SIDE SLOPE VERTICES

EROSION CONTROL BLANKET - SWALE NOT TO SCALE

* HORIZONTAL STAPLE SPACING SHOULD BE ALTERED IF NECESSARY TO ALLOW STAPLES TO SECURE THE CRITICAL POINTS ALONG THE CHANNEL

** IN LOOSE SOIL CONDITIONS, THE USE OF STAPLE OR STAKE LENGTHS GREATER THAN 6" MAY BE NECESSARY TO PROPERLY ANCHOR THE

EROSION CONTROL BLANKET - SLOPE NOT TO SCALE



- 1. ORGANIC FILTER BERMS MAY BE UTILIZED IN LIEU OF SILT FENCE OR OTHER SEDIMENT BARRIERS.
- 2. THE EROSION CONTROL MIXTURE USED IN FILTER BERMS SHALL BE A WELL-GRADED MIX OF PARTICLE SIZES THAT MAY CONTAIN ROCKS LESS THAN 4" IN DIAMETER, STUMP GRINDINGS, SHREDDED OR COMPOSTED BARK, AND/OR ACCEPTABLE MANUFACTURED PRODUCTS AND SHALL BE FREE OF REFUSE, PHYSICAL CONTAMINANTS AND MATERIAL TOXIC TO PLANT GROWTH. EROSION CONTROL MIXTURE SHALL MEET THE FOLLOWING STANDARDS:
- a) THE ORGANIC CONTENT SHALL BE 80-100% OF DRY WEIGHT
- b) PARTICLE SIZE BY WEIGHT SHALL BE 100% PASSING A 6" SCREEN, AND 70-85%
- PASSING A 0.75" SCREEN. c) THE ORGANIC PORTION SHALL BE FIBROUS AND ELONGATED.
- d) LARGE PORTIONS OF SILTS, CLAYS, OR FINE SANDS SHALL NOT BE INCLUDED IN THE MIXTURE.
- e) SOLUBLE SALTS CONTENT SHALL BE >4.0mmhos/cm. f) THE pH SHALL BE BETWEEN 5.0 AND 8.0.
- 3. ORGANIC FILTER BERMS SHALL BE INSTALLED ALONG A RELATIVELY LEVEL CONTOUR. IT MAY BE NECESSARY TO CUT TALL GRASSES OR WOODY VEGETATION TO AVOID CREATING VOIDS AND BRIDGES THAT WOULD ENABLE FINES TO WASH UNDER THE BERM.
- 4. ON SLOPES LESS THAN 5%, OR AT THE BOTTOM OF SLOPES NO STEEPER THAN 3:1 AND UP TO 20 LONG, THE BERM SHALL BE A MINIMUM OF 12" HIGH (AS MEASURED ON THE UPHILL SIDE) AND A MINIMUM OF 36" WIDE. ON LONGER AND/OR STEEPER SLOPES, THE BERM SHALL BE TALLER AND WIDER TO ACCOMMODATE THE POTENTIAL FOR ADDITIONAL RUNOFF (MAXIMUM HEIGHT SHALL NOT
- 5. FROZEN GROUND, OUTCROPS OF BEDROCK, AND VERY ROOTED FORESTED AREAS PRESENT THE MOST PRACTICAL AND EFFECTIVE LOCATIONS FOR ORGANIC FILTER BERMS. OTHER BMP'S SHOULD BE USED AT LOW POINTS OF CONCENTRATED RUNOFF, BELOW CULVERT OUTLET APRONS, AROUND CATCH BASINS, AND AT THE BOTTOM OF STEEP PERIMETER SLOPES THAT HAVE A LARGE CONTRIBUTING
- 6. SEDIMENT SHALL BE REMOVED FROM BEHIND THE FILTER BERMS WHEN IT HAS ACCUMULATED TO ONE HALF THE ORIGINAL HEIGHT OF THE BERM.
- 7. ORGANIC FILTER BERMS MAY BE LEFT IN PLACE ONCE THE SITE IS STABILIZED PROVIDED ANY SEDIMENT DEPOSITS TRAPPED BY THEM ARE REMOVED AND DISPOSED OF PROPERLY.
- 8. FILTER BERMS ARE PROHIBITED AT THE BASE OF SLOPES STEEPER THAN 8% OR WHERE THERE IS FLOWING WATER WITHOUT THE SUPPORT OF ADDITIONAL MEASURES SUCH AS SILTFENCE.

ORGANIC FILTER BERM

NOT TO SCALE

- LIFTING STRAP DANDY BAG II OR STANDARD FABRIC APPROVED EQUAL OF ORANGE WOVEN MONOFILAMENT-DUMPING STRAP ALLOWS FOR EASY REMOVAL OF CONTENTS

INSTALLATION AND MAINTENANCE:

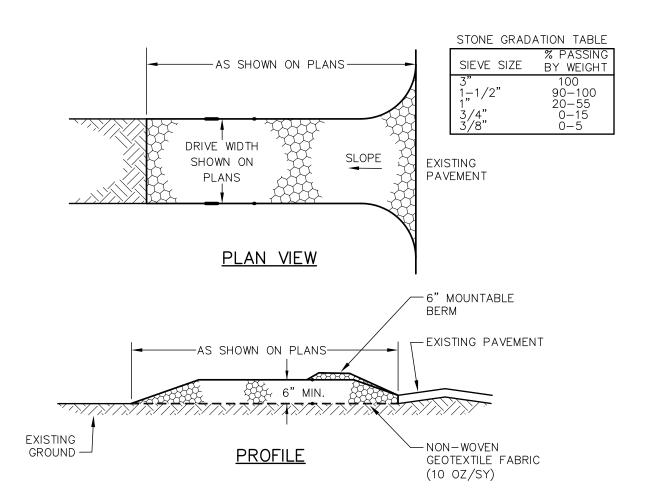
INSTALLATION: REMOVE THE GRATE FROM CATCH BASIN. IF USING OPTIONAL OIL ABSORBENTS; PLACE ABSORBENT PILLOW IN UNIT. STAND GRATE ON END. MOVE THE TOP LIFTING STRAPS OUT OF THE WAY AND PLACE THE GRATE INTO CATCH BASIN INSERT SO THE GRATE IS BELOW THE TOP STRAPS AND ABOVE THE LOWER STRAPS. HOLDING THE LIFTING DEVICES, INSERT THE GRATE INTO THE INLET.

MAINTENANCE: REMOVE ALL ACCUMULATED SEDIMENT AND DEBRIS FROM VICINITY OF THE UNIT AFTER EACH STORM EVENT. AFTER EACH STORM EVENT AND AT REGULAR INTERVALS, LOOK INTO THE CATCH BASIN INSERT. IF THE CONTAINMENT AREA IS MORE THAN 1/3 FULL OF SEDIMENT, THE UNIT MUST BE EMPTIED. TO EMPTY THE UNIT, LIFT THE UNIT OUT OF THE INLET USING THE LIFTING STRAPS AND REMOVE THE GRATE. IF USING OPTIONAL ABSORBENTS; REPLACE ABSORBENT WHEN NEAR SATURATION.

UNACCEPTABLE INLET PROTECTION METHOD:

A SIMPLE SHEET OF GEOTEXTILE UNDER THE GRATE IS NOT ACCEPTABLE

STORM DRAIN INLET PROTECTION

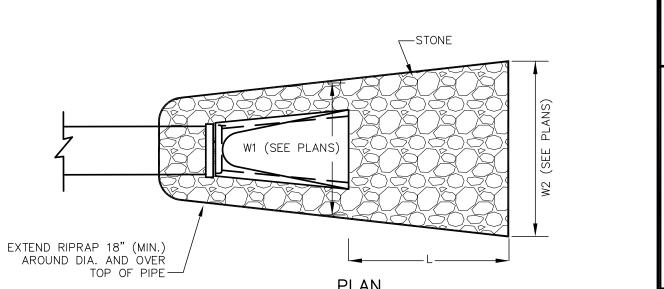


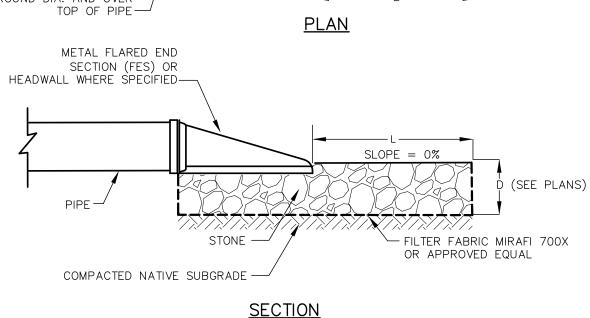
CONSTRUCTION SPECIFICATIONS

- 1. <u>STONE SIZE</u> NHDOT STANDARD STONE SIZE #4 SECTION 703 OF NHDOT STANDARD.
- 2. <u>LENGTH</u> DETAILED ON PLANS (50 FOOT MINIMUM).
- 3. <u>THICKNESS</u> SIX (6) INCHES (MINIMUM).
- 4. WIDTH FULL DRIVE WIDTH UNLESS OTHERWISE SPECIFIED.
- 5. <u>FILTER FABRIC</u> MIRAFI 600X OR EQUAL APPROVED BY ENGINEER
- SURFACE WATER CONTROL ALL SURFACE WATER THAT IS FLOWING TO OR DIVERTED TOWARD THE CONSTRUCTION ENTRANCE SHALL BE PIPED BENEATH THE ENTRANCE. IF PIPING IS IMPRACTICAL, A BERM WITH 5:1 SLOPES THAT CAN BE CROSSED BY VEHICLES MAY BE SUBSTITUTED FOR THE PIPE.
- MAINTENANCE THE ENTRANCE SHALL BE MAINTAINED IN A CONDITION WHICH WILL PREVENT RACKING OR FLOWING OF SEDIMENT ONTO PUBLIC RIGHTS-OF-WAY. THIS WILL REQUIRE PERIODIC TOP DRESSING WITH ADDITIONAL STONE OR ADDITIONAL LENGTH AS CONDITIONS DEMAND AND REPAIR AND/OR CLEANOUT OF ANY MEASURES USED TO TRAP SEDIMENT. ALL SEDIMENT SPILLED, DROPPED, WASHED OR TRACKED ONTO PUBLIC RIGHTS-OF-WAY MUST BE REMOVED IMMEDIATELY.
- WHEELS SHALL BE CLEANED TO REMOVE MUD PRIOR TO ENTRANCE ONTO PUBLIC RIGHTS-OF-WAY. WHEN WASHING IS REQUIRED, IT SHALL BE DONE ON AN AREA STABILIZED WITH STONE WHICH DRAINS INTO AN APPROVED SEDIMENT TRAPPING DEVICE.
- 9. STABILIZED CONSTRUCTION EXITS SHALL BE INSTALLED AT ALL ENTRANCES TO PUBLIC RIGHTS-OF-WAY, AT LOCATIONS SHOWN ON THE PLANS, AND/OR WHERE AS DIRECTED BY THE

STABILIZED CONSTRUCTION EXIT

NOT TO SCALE





MAINTENANCE

THE OUTLET PROTECTION SHOULD BE CHECKED AT LEAST ANNUALLY AND AFTER EVERY MAJOR STORM. IF THE RIPRAP HAS BEEN DISPLACED, UNDERMINED OR DAMAGED, IT SHOULD BE REPAIRED IMMEDIATELY. THE CHANNEL IMMEDIATELY BELOW THE OUTLET SHOULD BE CHECKED TO SEE THAT EROSION IS NOT OCCURRING. THE DOWNSTREAM CHANNEL SHOULD BE KEPT CLEAR OF OBSTRUCTIONS SUCH AS FALLEN TREES, DEBRIS, AND SEDIMENT THAT COULD CHANGE FLOW PATTERNS AND/OR TAILWATER DEPTHS ON THE PIPES. REPAIRS MUST BE CARRIED OUT IMMEDIATELY TO AVOID ADDITIONAL DAMAGE TO THE OUTLET PROTECTION APRON.

CONSTRUCTION SPECIFICATIONS

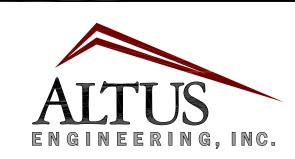
- 1. THE SUBGRADE FOR THE FILTER MATERIAL, GEOTEXTILE FABRIC, AND RIPRAP SHALL BE PREPARED TO THE LINES AND GRADES SHOWN ON THE PLANS.
- . THE ROCK OR GRAVEL USED FOR FILTER OR RIPRAP SHALL CONFORM TO THE SPECIFIED GRADATION. GEOTEXTILE FABRICS SHALL BE PROTECTED FROM PUNCTURE OR TEARING DURING THE PLACEMENT OF THE ROCK RIPRAP. DAMAGED AREAS IN THE FABRIC SHALL BE REPAIRED BY PLACING A PIECE OF FABRIC OVER THE

DAMAGED AREA OR BY COMPLETE REPLACEMENT OF THE FABRIC. ALL OVERLAPS REQUIRED FOR JOINING TWO

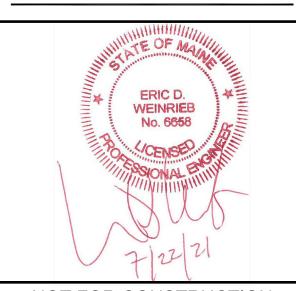
PIECES OF FABRIC SHALL BE A MINIMUM OF 12 INCHES. 4. STONE FOR THE RIP RAP MAY BE PLACED BY EQUIPMENT AND SHALL BE CONSTRUCTED TO THE FULL LAYER THICKNESS IN ONE OPERATION AND IN SUCH A MANNER AS TO PREVENT SEGREGATION OF THE STONE SIZES.

RIPRAP OUTLET PROTECTION

NOT TO SCALE



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<u>ISSUED FOR:</u>

ISSUE DATE:

JULY 22, 2021

<u>REVISIONS</u> NO. DESCRIPTION BY DATE D PLANNING BOARD EBS 07/22/2

PLANNING BOARD

DRAWN BY: APPROVED BY: 5116-SITE.dwg DRAWING FILE:

SCALE:

NOT TO SCALE

OWNER:

C-COAST PROPERTIES, LLC

8 BANKS ROCK YORK HARBOR, MAINE 0391

<u>APPLICANT:</u>

GOOD TO-GO c/o CAPE HOUSE MANAGEMENT, LLC

484 US ROUTE 1 KITTERY, MAINE 03904

<u>PROJECT:</u>

GOOD TO-GO SPECIALTY FOOD **FACILITY**

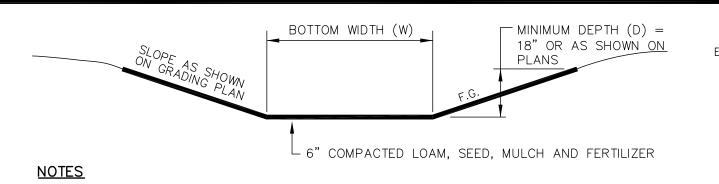
TAX MAP 67, LOT 1

524 U.S. ROUTE 1 KITTERY, MAINE

DETAILS

SHEET NUMBER:

NOT TO SCALE



- 1. THE FOUNDATION AREA OF THE SWALE SHALL BE CLEARED AND GRUBBED OF ALL TREES, BRUSH, STUMPS, AND OTHER OBJECTIONABLE MATERIAL.
- THE SWALE SHALL BE EXCAVATED OR SHAPED TO LINE, GRADE AND CROSS SECTION AS REQUIRED TO MEET THE DESIGN CRITERIA AND BE FREE OF IRREGULARITIES.
- 3. EARTH FILLS REQUIRED TO MEET SUBGRADE REQUIREMENTS BECAUSE OF OVER EXCAVATION OR TOPOGRAPHY SHALL BE COMPACTED TO THE SAME DENSITY AS THE SURROUNDING SOIL TO PREVENT UNEQUAL SETTLEMENT THAT COULD CAUSE DAMAGE TO THE COMPLETED SWALE.

4. VEGETATION SHALL BE ESTABLISHED IN THE SWALE OR AN EROSION CONTROL MATTING INSTALLED

- PRIOR TO DIRECTING STORMWATER TO IT. 5. MAINTENANCE OF THE VEGETATION IS EXTREMELY IMPORTANT IN ORDER TO PREVENT RILLING, EROSION, AND FAILURE OF THE SWALE. MOWING SHALL BE DONE FREQUENTLY ENOUGH TO CONTROL ENCROACHMENT OF WEEDS AND WOODY VEGETATION AND TO KEEP GRASSES IN A VIGOROUS CONDITION. THE VEGETATION SHALL NOT BE MOWED TOO CLOSELY SO AS TO REDUCE
- THE EROSION RESISTANCE IN THE SWALE. 6. THE SWALE SHOULD BE INSPECTED PERIODICALLY AND AFTER ANY STORM GREATER THAN 0.5" OF RAINFALL IN 24 HOURS TO DETERMINE ITS CONDITION. RILLS AND DAMAGED AREAS SHOULD BE PROMPTLY REPAIRED AND REVEGETATED AS NECESSARY TO PREVENT FURTHER DETERIORATION.

W (AS SHOWN ON PLAN)

1. CONSTRUCT RIP RAP LINED SWALE TO THE WIDTHS AND LENGTHS SHOWN ON THE PLAN.

2. THE SUBGRADE FOR THE GEOTEXTILE FABRIC AND RIPRAP SHALL BE PREPARED TO LINES AND

3. EROSION STONE USED FOR THE RIP RAP LINED SWALE SHALL MEET THE GRADATION SHOWN ON THE

OF THE EROSION STONE. DAMAGED AREAS IN THE FABRIC SHALL BE REPAIRED BY PLACING A PIECE

OVERLAPS REQUIRED FOR REPAIRS OR JOINING TWO PIECES OF FABRIC SHALL BE A MINIMUM OF 18

4. GEOTEXTILE FABRICS SHALL BE PROTECTED FROM PUNCTURE OR TEARING DURING THE PLACEMENT

OF FABRIC OVER THE DAMAGED AREA OR BY COMPLETE REPLACEMENT OF THE FABRIC. ALL

5. THE EROSION STONE MAY BE PLACED BY EQUIPMENT AND SHALL BE CONSTRUCTED TO THE FULL

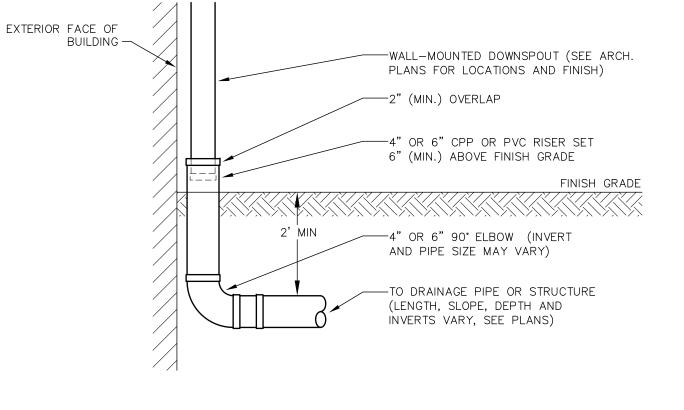
LAYER THICKNESS IN ONE OPERATION AND IN SUCH A MANNER AS TO PREVENT SEGREGATION OF

VEGETATED SWALE

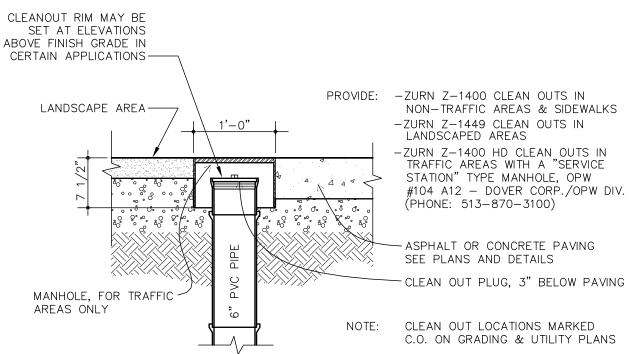
GRADES SHOWN ON THE PLANS.

OR AS SHOWN ON PLANS-

NOT TO SCALE



EXTERIOR ROOF DRAIN CONNECTION NOT TO SCALE



DIMENSIONS (2:1 SLOPE) (=PIPE DIA.+5") 5'-4" | 3'-0" | 1'-9" | 2'-0" | 4'-3" | 3'-9" | 3'-4"

END ELEVATION

ROUND SLOPE

SIDE ELEVATION

OF TOP STEEL

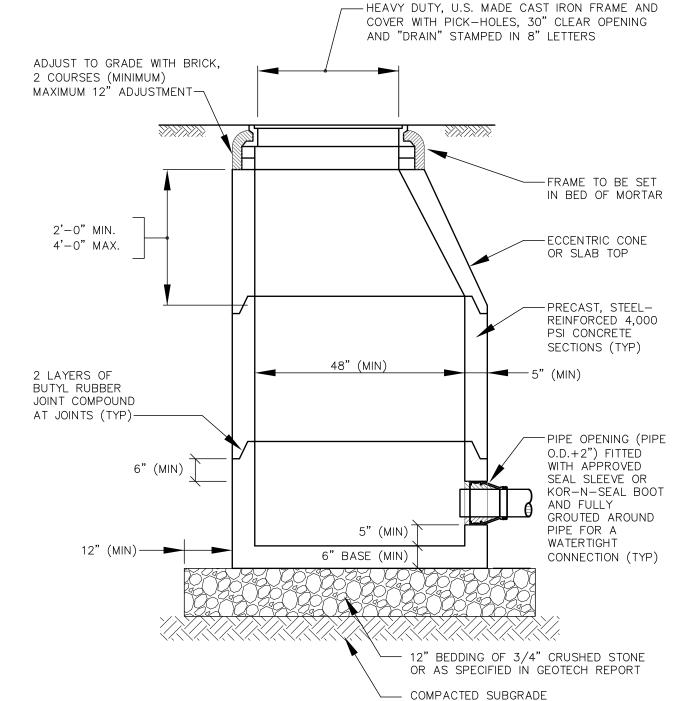
-4" WEEPHOLE IN

OUTLET HEADWALL (TYPx2)

HALF PLAN

OF BOTTOM STEEL

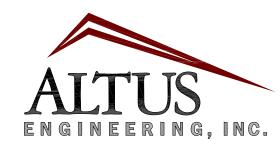
CONCRETE HEADWALL w/WINGWALLS NOT TO SCALE



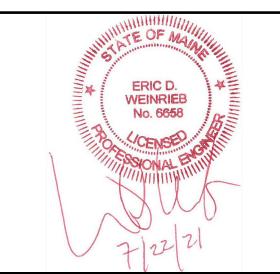
- 1. ALL SECTIONS SHALL BE CONCRETE CLASS AA (4000 psi). 2. CIRCUMFERENTIAL REINFORCEMENT SHALL BE 0.12 SQ.IN. PER LINEAR FT. IN ALL SECTIONS AND SHALL BE PLACED IN THE CENTER THIRD OF THE WALL. 3. THE TONGUE OR GROOVE OF THE JOINT SHALL CONTAIN ONE LINE OF
- CIRCUMFERENTIAL REINFORCEMENT EQUAL TO 0.12 SQ. IN. PER LINEAR FT. 4. RISERS OF 1', 2', 3' & 4' CAN BE USED TO REACH DESIRED DEPTH.
- 5. ALL MANHOLE STRUCTURES SHALL BE DESIGNED FOR H20 LOADING. 6. USE H-20 LOADING SLAB TOP SECTION IN LIEU OF ECCENTRIC TOP WHERE PIPE
- INVERT IS WITHIN 4 FT OF GRADE. 7. MANHOLE STEPS ARE NOT PERMITTED.

DRAIN MANHOLE DETAIL (DMH)

NOT TO SCALE



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ISSUED FOR:

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C-COAST PROPERTIES, LLC

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484 US ROUTE 1 KITTERY, MAINE 03904

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GOOD TO-GO SPECIALTY FOOD **FACILITY**

TAX MAP 67, LOT 1

524 U.S. ROUTE 1

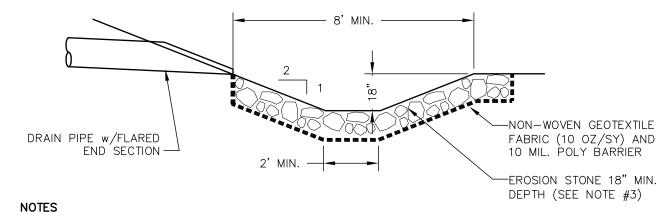
KITTERY, MAINE

TITLE:

DETAILS

SHEET NUMBER:

D-3



CONSTRUCT PLUNGE POOL TO THE WIDTHS AND LENGTHS SHOWN ON THE PLAN. THE SUBGRADE FOR THE GEOTEXTILE FABRIC AND RIPRAP SHALL BE PREPARED TO ACCOUNT FOR

THE EROSION STONE MAY BE PLACED BY EQUIPMENT AND SHALL BE CONSTRUCTED TO THE FULL

LAYER THICKNESS IN ONE OPERATION AND IN SUCH A MANNER AS TO PREVENT SEGREGATION OF

3. EROSION STONE USED FOR THE PLUNGE POOL SHALL MEET THE FOLLOWING GRADATION: PERCENT PASSING BY WEIGHT

90-100 4. GEOTEXTILE FABRICS SHALL BE PROTECTED FROM PUNCTURE OR TEARING DURING THE PLACEMENT OF THE EROSION STONE. DAMAGED AREAS IN THE FABRIC SHALL BE REPAIRED BY PLACING A PIECE OF FABRIC OVER THE DAMAGED AREA OR BY COMPLETE REPLACEMENT OF THE FABRIC. ALL OVERLAPS REQUIRED FOR REPAIRS OR JOINING TWO PIECES OF FABRIC SHALL BE A MINIMUM OF 18".

PLUNGE POOL

THE STONE SIZES.



THE STONE SIZES.

NOT TO SCALE

- NON-WOVEN GEOTEXTILE

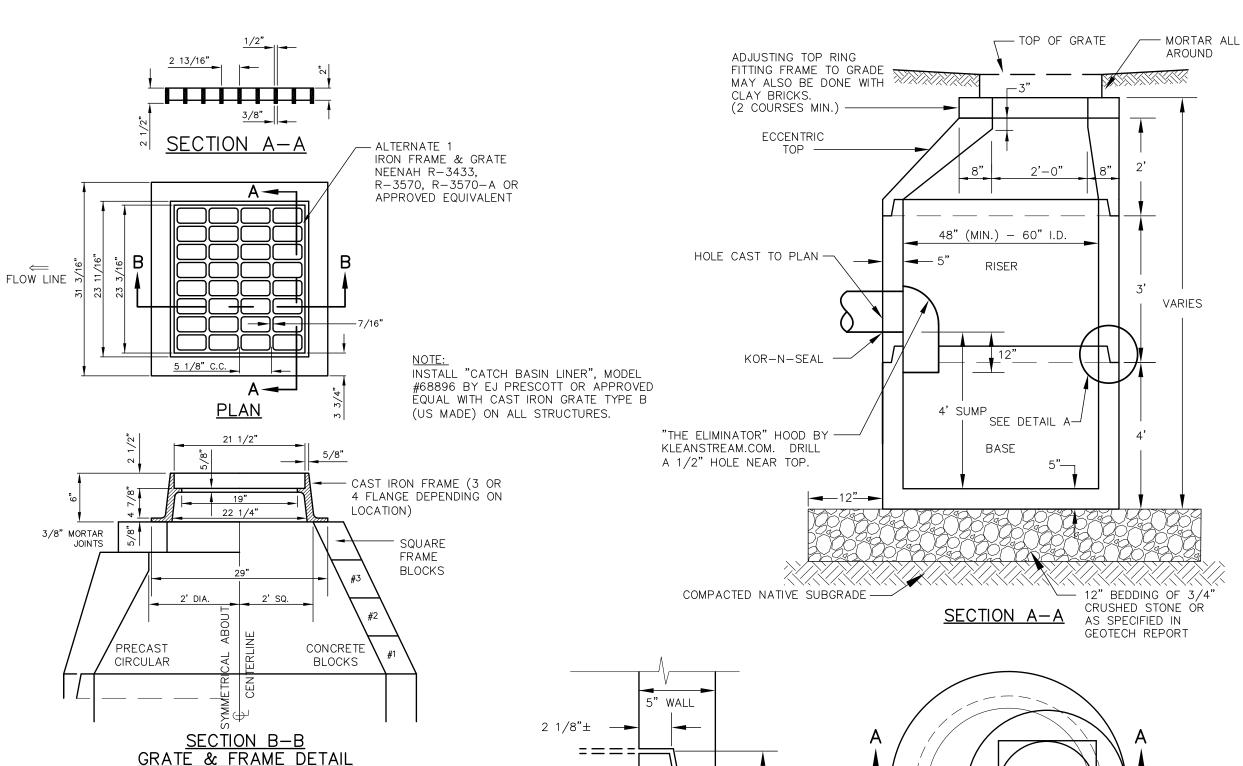
EROSION STONE, 18" MIN.

DEPTH (SEE NOTE 3 BELOW)

(10 OZ/SY)



NOT TO SCALE



-HEAVY DUTY CAST IRON GRATE -4" HEAVY DUTY CAST IRON FRAME -MORTAR ALL AROUND (NO BRICK) -6" THICK SLAB TOP -MODIFY FLANGE AS NECESSARY TO ACCOMMODATE PIPE 12" D.I. OUTLET PIPE SEAL OPENING w/NON-SHRINK GROUT -24" RISER SECTION -36" BASE SECTION 12" BEDDING OF 3/4" CRUSHED STONE OR AS SPECIFIED IN GEOTECH REPORT -COMPACTED NATIVE SUBGRADE

<u>NOTES</u>

1. STRUCTURE SHALL TO ACCOMMODATE HEAVY DUTY 24" SQ. C.I. FRAME AND GRATE.

- 2. "3' DIAMETER AREA DRAIN" AVAILABLE FROM PHOENIX PRECAST PRODUCTS (800-639-2199) OR APPROVED EQUAL.
- 3. CONCRETE: 4,000 PSI AFTER 28 DAYS
- 4. STRUCTURE SHALL BE STEEL REINFORCED MEET OR EXCEED H-20 LOADING.
- 5. SEAL ALL TONGUE AND GROOVE JOINTS W/BUTYL RUBBER JOINT COMPOUND.

3' I.D. LOW PROFILE CATCH BASIN

NOT TO SCALE

DEEP SUMP CATCH BASIN (CB)

1. ALL SECTIONS SHALL BE CONCRETE CLASS AA (4000 PSI).

THE STRUCTURES SHALL BE DESIGNED FOR H20 LOADING.

2. CIRCUMFERENTIAL REINFORCEMENT SHALL BE 0.12 SQ.IN. PER LINEAR FT. IN

3. THE TONGUE OR GROOVE OF THE JOINT SHALL CONTAIN ONE LINE OF

RISERS OF 1', 2', 3' & 4' CAN BE USED TO REACH DESIRED DEPTH.

6. USE H20 LOADING SLAB TOP SECTION IN LIEU OF ECCENTRIC TOP WHERE

ALL SECTIONS AND SHALL BE PLACED IN THE CENTER THIRD OF THE WALL.

CIRCUMFERENTIAL REINFORCEMENT EQUAL TO 0.12 SQ. IN. PER LINEAR FT.

PIPE INVERT IS WITHIN 4' OF FINISH GRADE. <u>DETAIL A</u> 7. FRAME AND GRATE DIMENSIONS ARE TYPICAL BUT MAY VARY BASED ON (TONGUE & GROOVE JOINT) <u>PLAN</u>

1 LAYER OF-

BUTYL

JOINT

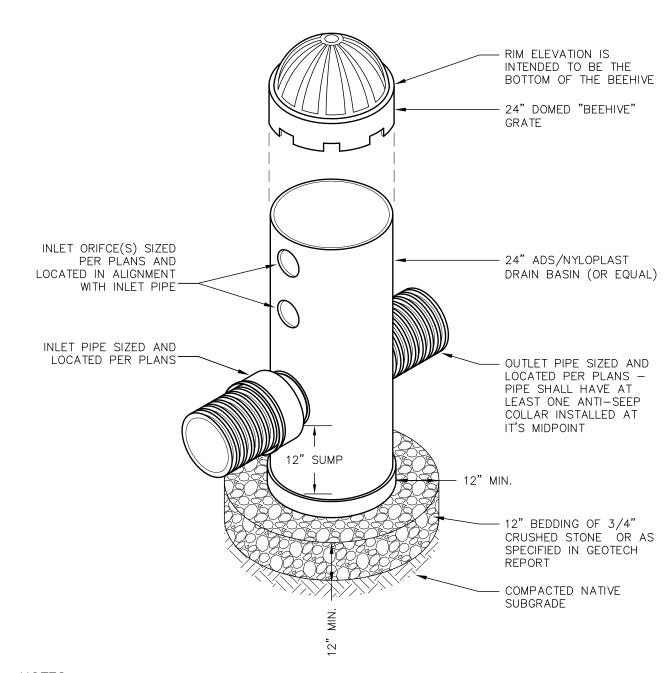
(TYP.)

RUBBER

COMPOUND

PRODUCT SELECTED OR EQUIVALENT APRROVED BY THE ENGINEER. NOT TO SCALE

⊸ 2 1/8"±

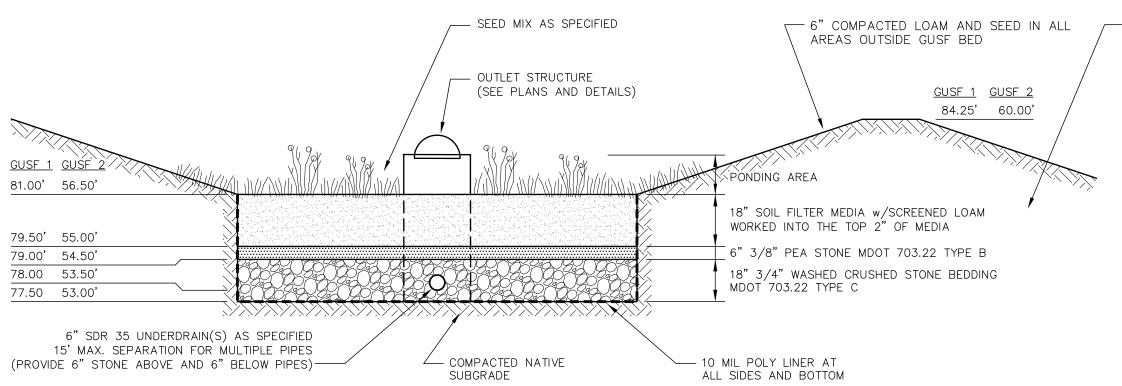


DIAMETER OF PIPE

2' MIN. PROJECTION

- 1. FRAMES AND GRATES SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05.
- 2. DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN AND DETAILS.
- 3. DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO ASTM D3212 FOR CORRUGATED HDPE, N-12HP AND PVC SEWER.
- 4. INLINE DRAIN TO BE PVC DIAMETER AS SPECIFIED AND AS MANUFACTURED BY
- ADS OR APPROVED EQUAL.

THE CONTRACTOR SHALL INSTALL THE DRAIN BASIN PER THE MANUFACTURER'S RECOMMENDATIONS AND AS SHOWN ON THE DRAWINGS.



SOIL, STONES MORE THAN 4" IN DIAMETER, AND OTHER OBJECTIONABLE MATERIAL INSTALLED IN CONTINUOUS COMPACTED 8" LIFTS (SEE GRADATION)

TYPE	LB/AC
CREEPING RED FESCUE	20
TALL FESCUE	20
BIRD'S FOOT TREFOIL	8
ANNUAL RYE	20
TOTAL	68

-TOP TRASH RACK (SEE

-3/4" STAINLESS STEEL

-36"Wx6"H INLET ORIFICE

CUT OR CAST IN PLACE

#4 REBAR & ANGLE IRON

RACK (OPENINGS 2"x2" MAX.) - SEE NOTES

-33"Wx5H" INLET ORIFICE

CUT OR CAST IN PLACE

-3/4" STAINLESS STEEL

-5'x5'x6"—THICK CONCRETE

BOLTS AND CLASP

ÖR PREFABRICATED TRASH

#4 REBAR & ANGLE IRON

OR PREFABRICATED TOP

(OPENINGS 2"x2" MAX.)

SEE NOTES -

6" UNDERDRAIN -

3" (MAX)

3/4" STONE _

- GRANITE CURB WEIR

AND FRONT TRASH RACKS

BOLTS AND CLASP

(TYPx4-MIN)

INV.: 58.35'

INV.: 57.30'

(TYPx2)

-INLET FOR 6"

UNDERDRAIN

INV.: 53.50'

FOOTING

(MAX)

-3/4" STAINLESS STEEL

(TYPx2-MIN EACH SIDE)

1. OUTLET STRUCTURE SHALL BE CONSTRUCTED OF STEEL REINFORCED CONCRETE FABRICATED ONSITE

FOOTING SHALL HAVE A CONTINUOUS KEYWAY INSTALLED AND REBAR CAST INTO IT THAT SHALL

EXTEND ABOVE THE SLAB A MINIMUM OF 8" FOR CONNECTION TO THE BOX AND ANY REINFORCING

2. CONCRETE FOOTING TO BE CONSTRUCTED INTEGRAL WITH BASE. IF CONSTRUCTED SEPARATELY,

4. ALL EXPOSED REBAR TO BE PAINTED WITH RUST-RESISTANT PAINT OR HOT-DIPPED GALVANIZED

5. PRE-FABRICATED TRASH RACKS ARE ACCEPTABLE UPON WRITTEN ACCEPTANCE BY THE ENGINEER.

7. NATIVE IN SITU SOILS UNDERLYING THE STRUCTURE'S STONE BASE PAD AND THE PAD ITSELF ARE

9. STAINLESS STEEL BOLTS FOR TRASH RACK TO BE INSTALLED WITH HILTI AND EPOXY OR CAST IN.

10. EXTERIOR TRASH RACK DIMENSIONS ARE APPROXIMATE. THE CONTRACTOR SHALL BE RESPONSIBLE

3. ALL JOINTS AND PIPE OPENINGS SHALL BE SEALED WATERTIGHT WITH MORTAR.

BOLTS AND CLASP

OR PRECAST TO EQUAL DIMENSIONS AND REINFORCING.

6. STRUCTURE IS TO BE BUILT TO WITHSTAND H20 LOADING.

TO BE COMPACTED PRIOR TO INSTALLING STRUCTURE...

8. ALL CONCRETE SHALL BE 4,000 PSI MINIMUM.

CONSTRUCTION SPECIFICATIONS

BERM GRANULAR FILL GRADATION		
Sieve size	Embankment Material % Passing sieve	
4 40 100 200	90-100% 50-80% 29-43% 15-30%	

18'x18"x6" GRANITE OR CONCRETE EROSION STOP SET AT MID POINT OF

- WEIR ALONG BERM CENTERLINE -
 - 1. CONSTRUCT EMERGENCY OVERFLOW WEIR TO THE WIDTHS AND LENGTHS SHOWN ON THE PLAN. 2. THE SUBGRADE FOR THE GEOTEXTILE FABRIC AND RIPRAP SHALL BE PREPARED TO LINES AND GRADES SHOWN ON THE PLANS.
 - 3. UNLESS OTHERWISE SPECIFIED OR DIRECTED, RIPRAP USED FOR THE EMERGENCY OVERFLOW WEIR SHALL MEET THE FOLLOWING GRADATION:

<u>SIZE</u> PERCENT PASSING BY WEIGHT 90-100

- 4. GEOTEXTILE FABRICS SHALL BE PROTECTED FROM PUNCTURE OR TEARING DURING THE PLACEMENT OF THE EROSION STONE. DAMAGED AREAS IN THE FABRIC SHALL BE REPAIRED BY PLACING A PIECE OF FABRIC OVER THE DAMAGED AREA OR BY COMPLETE REPLACEMENT OF THE FABRIC. ALL OVERLAPS REQUIRED FOR REPAIRS OR JOINING TWO PIECES OF FABRIC SHALL BE A MINIMUM OF 18 INCHES.
- 5. THE EROSION STONE MAY BE PLACED BY EQUIPMENT AND SHALL BE CONSTRUCTED TO THE FULL LAYER THICKNESS IN ONE OPERATION AND IN SUCH A MANNER AS TO PREVENT SEGREGATION OF THE STONE SIZES.

FOR PROVIDING TRASH RACKS THAT ALLOW FULL SCREENING PROTECTION TO EVERY INLET ORIFICE AND THE TOP OF THE STRUCTURE. THIS MAY REQUIRE CUSTOM FABRICATION AND/OR ALTERNATE METHODS TO CONNECT THE RACKS TO THE OUTLET STRUCTURE. **OUTLET STRUCTURE #1 OUTLET STRUCTURE #2** NOT TO SCALE NOT TO SCALE

- GRANULAR FILL MATERIAL FREE OF SOD, ROOTS, FROZEN

> • All the material used for the construction of the filter basin must be confirmed as suitable by the design engineer. Testing must be done by a certified laboratory to show that they are passing DEP specifications.

Testing and Submittals: The contractor shall identify the location of the source of each component of the soil filter media. All results of field and laboratory testing shall be submitted to the project engineer for confirmation. The contractor shall:

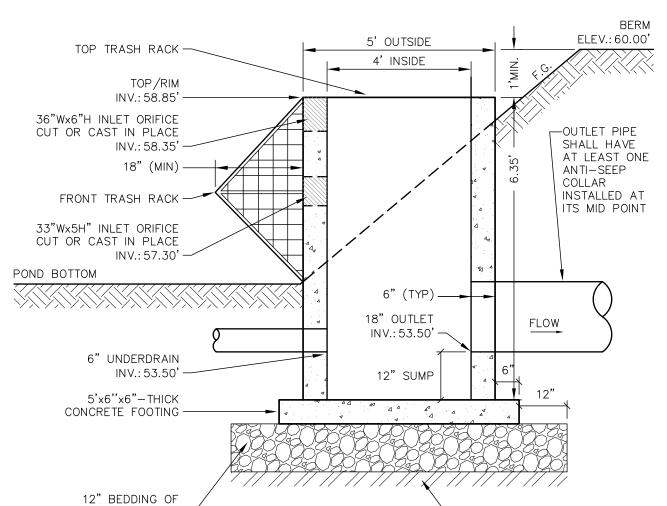
- Select samples for sampling of each type of material to be blended for the mixed filter media and samples of the underdrain bedding material. Samples must be a composite of three different locations (grabs) from the stockpile or pit face. Sample size required will be determined by the testing laboratory.
- Perform a sieve analysis conforming to ASTM C136 (Standard Test Method for Sieve Analysis of fine and Course Aggregates 1996A) on each type of the sample material. The resulting soil filter media mixture must have 8% to 12% by weight passing the #200 sieve, a clay content of less than 2% (determined hydrometer grain size analysis) and have 10% dry weight of organic matter.
- Perform a permeability test on the soil filter media mixture conforming to ASTM D2434 with the mixture compacted to 90-92% of maximum dry density based on ASTM D698. Alternative soil filter media source: MDEP approved filter mix is available from Shaw Brothers, Gorham, Maine at http://shawbrothers.com/

Outlet Discharge: Outflow of the filter basin underdrain is controlled with a ball valve within a three-piece valve box. Upon completion of the installation of the soil filter media and the establishment of 90% of grass cover over the filter media, the contractor shall flood the vegetated basin with 8" of clean water and adjust the outflow to obtain between 24 to 48 hour release time.

Maintenance: The basin shall be inspected semi-annually and following major storm events. debris and sediment buildup shall be removed from the forebay and basin as needed. any bare area or erosion rills shall be repaired with new filter media, seeded and mulched. Maintenance Agreement: Applicant or its representatives shall be responsibility for

- inspecting and maintaining any underdrained filter. • Inlets and Outlets: The inlets and outlets of the pond shall be checked to ensure that flow structures are not blocked by debris.
- Drainage: The filter shall drain within 24 to 48 hours following a one—inch storm or greater. If the system drains too fast, an orifice may need to be added on the underdrain outlet or may need to be modified if already present. Sediment Removal: Sediment and plant debris shall be removed from the
- pretreatment structure at least annually.
- Mowing: If mowing is desired, only hand—held string trimmers or push—mowers are allowed on the filter (no tractor) and the grass bed shall be mowed no more than 2 times per growing season to maintain grass heights of no less than 6 inches. • Fertilization: Fertilization of the underdrained filter area shall be avoided unless
- absolutely necessary to establish vegetation. • Harvesting and Weeding: Harvesting and pruning of excessive growth shall be done
- occasionally. weeding to control unwanted or invasive plants may also be necessary. • Grass Cover: Maintaining a healthy cover of grass will minimize clogging with fine sediments. If ponding exceeds 48 hours, the top of the filter bed shall be rototilled to reestablish the soil's filtration capacity.
- Soil Filter Replacement: The top several inches of the filter shall be replaced with fresh material if water is ponding for more than 72 hours, or the basin can be rototilled, seeded and mulched. Once the filter is mature, adding new material (a 1-inch to 2-inch cover of mature compost) can compensate for subsidence.

-6'x6'x6"-THICK CONCRETE FOOTING -18" OUTLET PIPE ·3/4" STAINLESS STEEL BOLTS AND CLASP (TYPx4-MIN)



BOTTOM WIDTH

PER PLAN

PER PLAN

EROSION STOP TOP SET AT INV. ELEV.

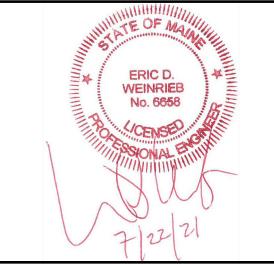
<u>PLAN</u>

FOOTING = 6'RISER = 5'

RACK = 4.5

133 Court Street Portsmouth, NH 03801

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PLANNING BOARD

ISSUE DATE:

BY DATE

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JULY 22, 2021 <u>REVISIONS</u>

NO. DESCRIPTION

D PLANNING BOARD

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DRAWING FILE:

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-COMPACTED NATIVE SUBGRADE

3 : 1

- NON-WOVEN GEOTEXTILE

-1'-DEEP RIPRAP ON BOTH SIDES OF

EROSION STOP (SEE NOTE 3 BELOW)

NOT TO SCALE

C-COAST PROPERTIES, LLC

8 BANKS ROCK YORK HARBOR, MAINE 03911

APPLICANT:

TOP OF

BERM

GOOD TO-GO c/o CAPE HOUSE MÁNAGEMENT, LLC

484 US ROUTE 1 KITTERY, MAINE 03904

PROJECT:

GOOD TO-GO SPECIALTY FOOD **FACILITY**

TAX MAP 67, LOT 1

524 U.S. ROUTE 1 KITTERY, MAINE

TITLE:

DETAILS

SHEET NUMBER:

TYPICAL GRASSED UNDERDRAINED SOIL FILTER (GUSF)

ANTI-SEEP COLLARS SHALL BE CLAY, CONCRETE, PLASTIC (AGRI-DRAIN), OR EQUAL APPROVED BY THE

ANTI-SEEP COLLAR SHALL

CONNECTION TO THE PIPE-

BE WATERPROOF AND HAVE A WATERTIGHT

ANTI-SEEP COLLAR

FILTER | MIXUTRE | SPECIFICATION

VOLUME

MEDIA BY

SAND

SIZE

1/2"

#50 #200

SOIL FILTER MEDIA

50-55% | MEDOT SPECICATION #703.01 FINE

TOPSOIL 20-30% SANDY LOAM TOPSOIL WITH MINIMAL CLAY

THE #200 SIEVE

MULCH | 20-30% | MODERATELY FINE, SHREDDED BARK OR

GRASSED UNDERDRAIN SOIL FILTER (GUSF) NOTES

least 2 lifts of 9 inches to prevent pockets of loose media.

MDOT 703.22 TYPE B | MDOT 703.22 TYPE C

75-100

50-100 15-80

0-15

0 - 5

in the plans and used on site.

installed but not backfilled,

PASSING #200 SIEVE

AGGREGATE FOR CONCRETE MODIFIED TO

CONTENT AND BETWEEN 20-70% PASSING

WOOD FIBER MULCH WITH LESS THAN 5%

90-100

0 - 75

0 - 25

The contractor will retain the services of a qualified professional to inspect the construction

stormwater management structures are constructed and stabilized, the qualified professional

completed. Accompanying the notification must be a log of the inspections giving the date

of each inspection, the time of each inspection, and the items inspected on each visit, and

include any testing data or sieve analysis data of every mineral soil and soil media specified

Construction Sequence: The soil filter media and vegetation must not be installed until the

structure, 90% vegetation cover, or other permanent stabilization unless the runoff from the

and stabilization of all stormwater management structures. If necessary, the qualified

professional shall interpret the pond's construction plan for the contractor. Once all

will notify the department in writing within 30 days to state that the pond has been

area that drains to the filter has been permanently stabilized with pavement or other

contributing drainage area is diverted around the filter until stabilization is completed.

Compaction of Soil Filter: Filter soil media and underdrain bedding material must be

Construction Oversight: Inspection by a professional engineer will occur at a minimum:

• After the filter media has been installed and seeded. Bio—retention cells must be

• After one year to inspect health of the vegetation and make corrections, and

compacted to between 90% and 92% standard proctor. The bed should be installed in at

• After the preliminary construction of the filter grades and once the underdrain pipes are

- After the drainage layer is constructed and prior to the installation of the filter media,

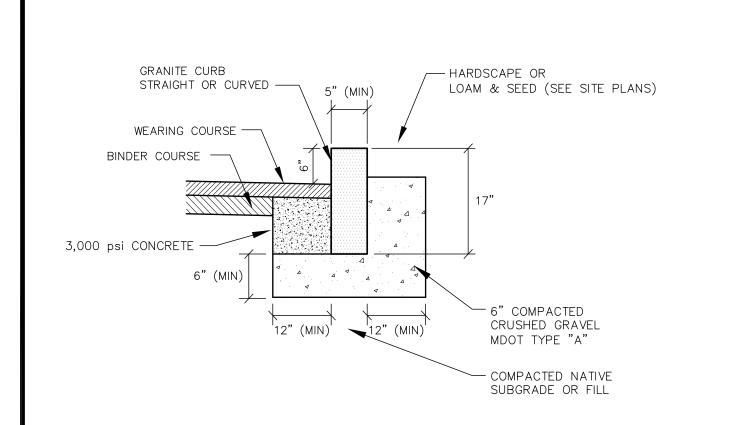
stabilized per the provided planting scheme and density for the canopy coverage of 30

SIEVE | % BY WEIGHT

HAVE 8-10% PASSING THE #200 SIEVE

RIPRAP SPILLWAY / OVERFLOW WEIR NOT TO SCALE

NOT TO SCALE



- 1. SEE PLANS FOR CURB LOCATION. 2. ADJOINING STONES SHALL HAVE THE SAME OR APPROXIMATELY THE SAME LENGTH.
- 3. MINIMUM LENGTH OF CURB STONES = 3
- 4. MAXIMUM LENGTH OF CURB STONES = 1 5. MAXIMUM LENGTH OF STRAIGHT CURB
- STONES LAID ON CURVES SEE CHART. 6. CURB ENDS TO ROUNDED AND BATTERED FACES TO BE CUT WHEN CALLED FOR

ON THE PLANS.

VERTICAL GRANITE CURB

WEARING COURSE -

BINDER COURSE -

3,000 psi CONCRETE

GRANITE CURB w/CHAMFERED EDGE

	21'	3'
	22'-28'	4'
	29'-35'	5'
	36'-42'	6'
0'	43'-49'	7'
	50'-56'	8'
)	57'-60'	9'
	OVER 60'	10'
	-	

RADIUS | MAX. LENGTH

- LOAM & SEED (SEE SITE PLANS) 6" UNLESS - GRANITE CURB OTHERWISE FINISH GRADE SPECIFIED SEE PAVEMENT CROSS SECTION -6" COMPACTED CRUSHED GRAVEL MDOT TYPE "A" 3,000 psi CONCRETE WITH CONCRETE BRICK SUPPORTS COMPACTED NATIVE SUBGRADE OR FILL

<u>NOTES</u>

- 1. SEE SITE PLAN FOR LIMITS OF CURBING
- 2. ADJOINING STONES OF STRAIGHT CURB LAID ON CURVES SHALL HAVE THE SAME OR APPROXIMATELY THE SAME LENGTH
- 3. MINIMUM LENGTH OF STRAIGHT CURB STONES = 18"
- 4. MAXIMUM LENGTH OF STRAIGHT CURB STONES = 8'
- CURVES -

5.	MAXIN	ИUМ	LENGTH	OF	STRAIGHT	CURB	STONES	LAID	ON	(
	SEE (CHAF	RT							

RADIUS FOR STONES WITH SQUARE JOINTS	MAXIMUM LENGTH
16'-28' 29'-41' 42'-55' 56'-68' 69'-82' 83'-96' 97'-110' OVER 110'	1'-6" 2' 3' 4' 5' 6' 7' 8'

6" BOLLARD WHERE SHOWN ─

SEE SITE PLAN

44 4 4 4

PITCH TO DRAIN 44

PER PLANS

4,000 psi CONCRETE PAD

(SEE CROSS SECTION)

⊸DOUBLE LEAF GATE ✓

PLAN - TYPICAL LAYOUT

DUMPSTER ENCLOSURE AND PAD

1/8-1/4" WIDE x 1" DEEP SAWCUT 16"-LONG 3/4" DIA.

DEFORMED DOWEL

AT 24" O.C. (ONE

END INSTALLED

SLEEVE-DO NOT

GREASE DOWELS)

SEALANT

1/4" TO 1/2"

PREMOLĎED

JOINT FILLER -

1" REVEAL WHERE

10"-THICK CONCRETE PAD-

REINFORCING AS SPECIFIED

BY STRUCTURAL ENGINEER

THICKENED HAUNCH

4,000 PSI WITH STEEL

AT EDGES

GROUND SLOPES AWAY

WITH PRE-FAB

ELEVATION

COMPACTED NATIVE SUBGRADE -

- 1x3 VERTICAL P.T. FACE BOARDS.

ATTACH WITH GALVANIZED NAILS.

GALVANIZED IRON PIPE

(3 PIPES PER 10' SECTION)

- 2x4 P.T. RAILS (TYP.)

10 SECTIONS (TYP.)

- DUMPSTER PAD

1/4" CHAMFER (TYP) -

FINISHED PAVEMENT GRADE

- BROOM FINISH

GALVANIZED IRON PIPE

2" DIA. LINE POST 2 1/2" DIA. CORNER POSTS—

EXISTING

SECTION A-A

- 1/4-1/2"-WIDE JOINT

EDGE

1/4" TO 1/2"

BUILDING OR OTHER / RIGID STRUCTURE (DOWEL SIDEWALK

TO BUILDING

ISOLATION JOINT

FOUNDATION AT BUILDING ENTRANCE

LOCATIONS ONLY)

EXPANSION/CONSTRUCTION JOINT

WITH 1/4" RADIUS TOOLED

PREMOLDED JOINT

FILLER AND SEALANT

GROUND

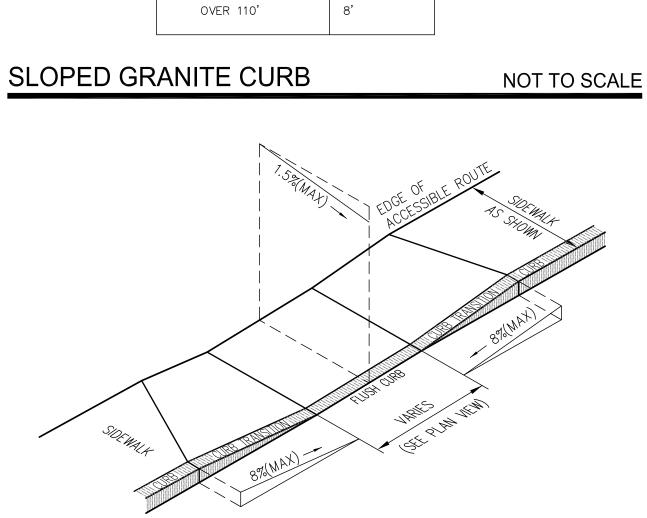
DIMENSIONS PER SITE PLANS

 \sim 6" \times 6" W. W. F. (1.4 \times 1.4)

12" BEDDING OF 3/4"

CRUSHED STONE

2% MAX. CROSS SLOPE



MOUNTABLE CURB

NOT TO SCALE

NOT TO SCALE

- PAVEMENT OR LANDSCAPING

AS SPECIFIED (PAVEMENT

TOWARDS THE GUTTER LINE

FOR TRUCK TURNING

AT 2% MIN.)

COMPACTED

CRUSHED RAVEL MDOT TYPE "A"

COMPACTED NATIVE SUBGRADE OR FILL

APRONS SHALL SLOPE

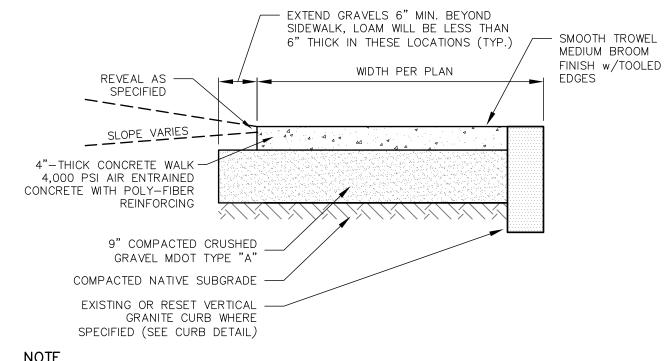
CURB RAMP (TYPE 'A')

NOT TO SCALE

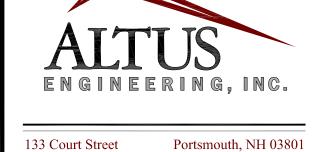
NOTES APPLICABLE TO ALL CURB RAMPS:

- 1. THE MAXIMUM ALLOWABLE CROSS SLOPE OF AN ACCESSIBLE ROUTE (SIDEWALK) AND CURB SHALL
- 2. THE MAXIMUM ALLOWABLE RUNNING SLOPE OF AN ACCESSIBLE ROUTE EXCLUDING CURB RAMPS SHALL BE 5%.
- 3. THE MAXIMUM ALLOWABLE RUNNING SLOPE OF AN ACCESSIBLE ROUTE (SIDEWALK) CURB RAMP SHALL BE 8.3% FOR A MAXIMUM ELEVATION CHANGE OF 6".
- 4. CURB TREATMENT VARIES, SEE PLANS FOR CURB TYPE.
- 5. BASE OF RAMP SHALL BE GRADED TO PREVENT THE PONDING OF WATER.
- 6. SEE CONCRETE SIDEWALK SECTION FOR RAMP CONSTRUCTION.
- 7. ALL CURB RAMPS SHALL BE CONSTRUCTED IN ACCORDANCE WITH AMERICANS WITH DISABILITIES ACT (ADA) AND ALL APPLICABLE CODES.
- 8. FLUSH CURB SECTIONS SHALL HAVE A MAXIMUM LIP REVEAL OF 1/4" WITH A BEVEL AT THE EDGE
- 9. EDGES OF SIDEWALK FOOTINGS ALONG FLUSH CURBS SHALL BE HAUNCHED SO AS TO EXTEND TO A MINIMUM DEPTH OF 1' BELOW FINISH GRADE.
- 10. NO RAMP SHALL BE LESS THAN 4' IN WIDTH.
- 11. CURB RAMPS SHALL HAVE A FLAT 2% MAX LANDING AT THE TOP AND BOTTOM OF THE RAMPS WHEN THERE IS A CHANGE IN DIRECTION.

CURB RAMP NOTES



1. JOINTS IN CONCRETE SIDEWALKS SHALL CONFORM TO THE TYPES AND LOCATIONS SHOWN IN THE HEAVY-DUTY CONCRETE PAVEMENT DETAIL



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┌6" MIN. LOAM & SEED

AT VEGETATED AREA

- 4000 PSI CONCRETE

SECTION B-B

— CONCRETE PAD

OR 1/8-1/4" WIDE x 1' DEEP GROOVE WITH 1/4" RADIUS TOOLED EDGES

(BOTH SAME DAY AS POUR) -

CONTROL/SAWCUT JOINT

- CONTROL/SAWCUT JOINT 6' O.C.

SMOOTH TROWEL

MEDIUM BROOM

FINISH w/TOOLED

- ISOLATION

JOINT AT

ASPHALT

PAVEMENT

BUILDING OR

EDGES

12" COMPACTED 3/4"

SPECIFIED IN

CRUSHED STONE OR AS

GEOTECHNICAL REPORT

(TYP), ALL JOINTS SHALL BE

RADIAL ON CURVES

<u>PLAN</u>

EXPANSION/CONSTRUCTION JOINT

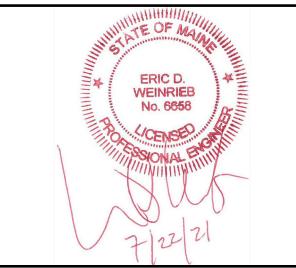
30' O.C. MAX. EACH WAY (TYP)

GAI VANIZED

BRACKET TO

CONCRETE FOOTING

HOLD PIPE-



NOT FOR CONSTRUCTION

ISSUED FOR:

PLANNING BOARD

ISSUE DATE:

JULY 22, 2021

<u>REVISIONS</u> BY DATE NO. DESCRIPTION O PLANNING BOARD EBS 07/22/2

EBS DRAWN BY: APPROVED BY:

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C-COAST PROPERTIES, LLC

8 BANKS ROCK YORK HARBOR, MAINE 03911

APPLICANT:

GOOD TO-GO c/o CAPE HOUSE MÁNAGEMENT, LLC

484 US ROUTE 1 KITTERY, MAINE 03904

PROJECT:

GOOD TO-GO SPECIALTY FOOD **FACILITY**

TAX MAP 67, LOT 1

524 U.S. ROUTE 1

KITTERY, MAINE

D-5

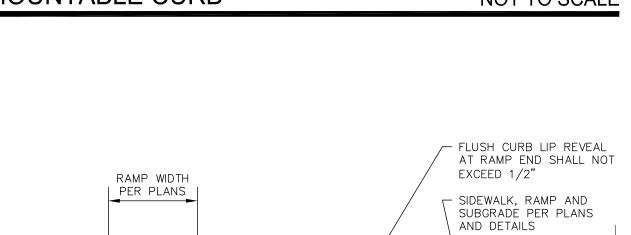
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EXTEND GRAVELS 12" MIN. BEYOND PAD

WIDTH PER PLAN

WHERE PAD ABUTS LANDSCAPE AREAS

COMPACTED NATIVE **SECTION** SUBGRADE **DETAILS** 1. PROJECT GEOTECHNICAL REPORT MAY REQUIRE A DIFFERENT PAVEMENT CROSS SECTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR READING AND FOLLOWING ALL RECOMMENDATIONS IN THE GEOTECHNICAL REPORT. IN THE EVENT THAT THE REPORT AND CIVIL PLANS DIFFER, THE MORE SHEET NUMBER: STRINGENT SPECIFICATION SHALL APPLY.



CONCRETE EDGE TO VERTICAL GRANITE CURB -EXTEND 1' (MIN) BELOW CURB TAPER TO MATCH VERTICAL GRANITE CURB TRANSITION CURB PER PER DIMENSIONS IN CURB RAMP DETAIL (TYP) -

PAVEMENT PER

FLUSH CURB AT RAMP DETAIL

NOT TO SCALE

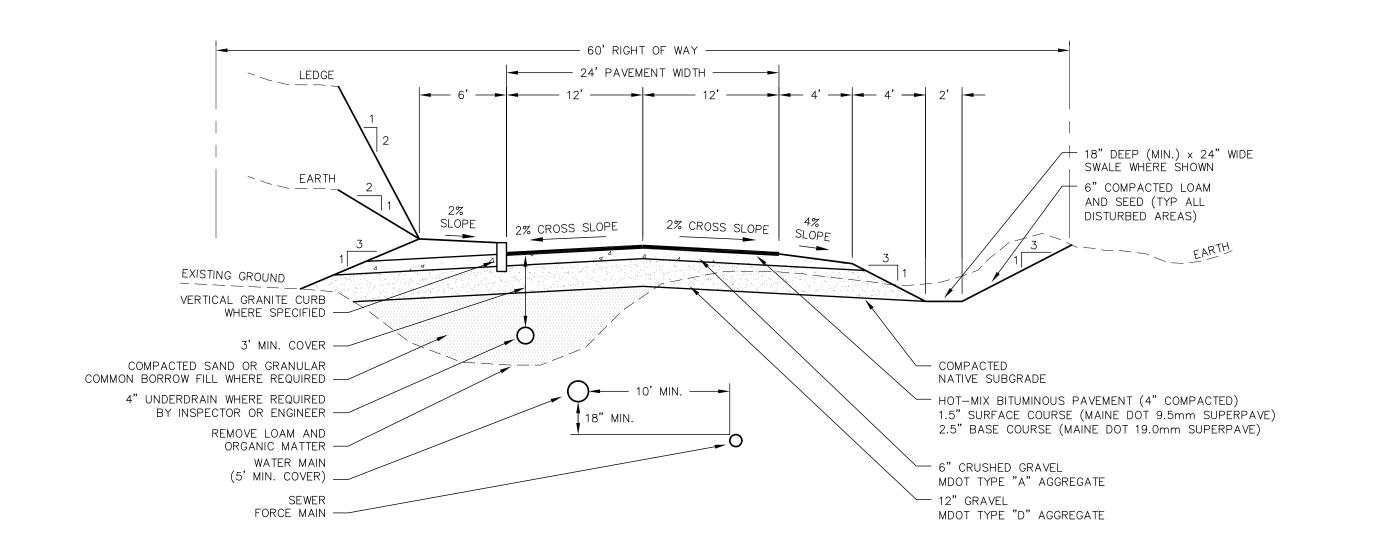
6"-WIDE (MIN) THICKENED

NOT TO SCALE

CONCRETE SIDEWALK

NOT TO SCALE

HEAVY-DUTY CONCRETE PAVEMENT



- 1. EACH GRAVEL BASE COURSE TO BE CONSTRUCTED AT THE PAVEMENT CROSS SLOPE.
- 2. REMOVE LEDGE 18" BELOW LOWEST WORK BEING INSTALLED.
- 3. REMOVE ALL LOAM, CLAY, MUCK, ORGANIC, YIELDING OR OTHERWISE UNSTABLE MATERIAL TO A MINIMUM OF 18" BELOW FINISHED GRADE. ADDITIONAL DEPTH MAY BE REQUIRED BY THE GEOTECHNICAL REPORT.
- 4. THE OVER-EXCAVATION OF UNSUITABLE MATERIAL BEYOND THAT SPECIFIED ABOVE, THE INSTALLATION OF UNDERDRAINAGE, AND/OR THE INSTALLATION OF GEOTEXTILE FABRIC SHALL BE PROVIDED UPON DETERMINATION OF THE INSPECTOR OR THE ENGINEER.
- 5. FILL BELOW PAVEMENT SUBGRADE SHALL BE SAND OR GRANULAR COMMON BORROW COMPACTED PER MDOT REQUIREMENTS.
- 6. SITEWORK CONTRACTOR SHALL COORDINATE GEOTECHNICAL ENGINEERING INSPECTIONS PRIOR TO PLACEING GRAVELS.
- 7. SUBGRADE SHALL BE FREE OF VOIDS THAT ALLOW MOVEMENT AND/OR SETTLEMENT OF MATERIALS.
- 8. SUBGRADE SHALL BE ROLLED WITH A MINIMUM OF SIX PASSES OF A 10-TON VIBRATORY COMPACTOR OPERATING AT PEAK RATED FREQUENCY OR BY OTHER MEANS APPROVED
- 9. BASE AND SUBBASE MATERIALS SHALL BE COMPACTED TO AT LEAST 95 PERCENT OF THEIR MAXIMUM DRY DENSITIES AS DETERMINED BY ASTM D-1557.
- 10. SUBGRADE SHALL BE PROOF-ROLLED WITH A FULLY LOADED DUMP TRUCK PRIOR TO PLACEMENT OF SELECT GRAVELS. PROOF-ROLLING SHALL BE WITNESSED AND APPROVED
- 11. BITUMINOUS PAVEMENT SHALL BE COMPACTED TO 90 TO 97 PERCENT OF ITS THEORETICAL MAXIMUM DENSITY AS DETERMINED BY ASTM D-2041.
- 12. TACK COAT SHALL BE APPLIED BETWEEN SUCCESSIVE LIFTS OF ASPHALT PAVEMENT.

FINISH GRADE PER PLANS -6" COMPACTED LOAM AND SEED (TYP) MDOT TYPE "A" AGGREGATE -6" CRUSHED GRAVEL -MDOT TYPE "D" AGGREGATE -12" GRAVEL

-HOT-MIX BITUMINOUS PAVEMENT (4" COMPACTED)

-2' MIN. (AREAS WITHOUT CURB) w/COMPACTED LOAM AND SEED

-COMPACTED NATIVE SUBGRADE

OR FILL WHERE REQUIRED

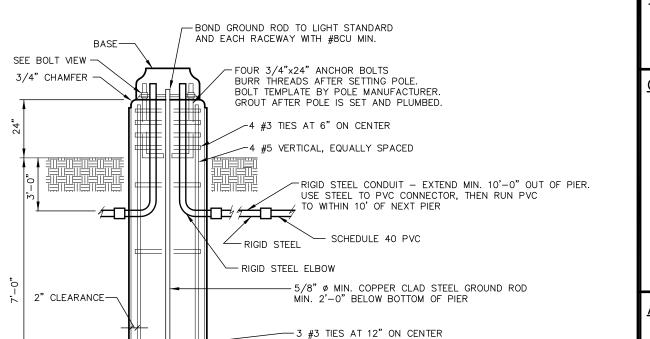
1.5" SURFACE COURSE (MAINE DOT 9.5mm SUPERPAVE) 2.5" BASE COURSE (MAINE DOT 19.0mm SUPERPAVE)

- 1. PROJECT GEOTECHNICAL REPORT MAY REQUIRE A DIFFERENT PAVEMENT CROSS SECTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR READING AND FOLLOWING ALL RECOMMENDATIONS IN THE GEOTECHNICAL REPORT. IN THE EVENT THAT THE REPORT AND CIVIL PLANS DIFFER, THE MORE STRINGENT SPECIFICATION SHALL APPLY.
- 2. ALL EXISTING FILL, BURIED ORGANIC MATTER, CLAY, LOAM, MUCK, AND/OR OTHER QUESTIONABLE MATERIAL SHALL BE REMOVED FROM BELOW ALL PAVEMENT, SHOULDERS AND UNDERGROUND PIPING/UTILITIES TO DEPTHS RECOMMENDED IN GEOTECHNICAL REPORT.
- 3. SUBGRADE SHALL BE PROOFROLLED A MINIMUM OF 6 PASSES WITH A 10-TON VIBRATORY COMPACTOR OPERATING AT PEAK RATED FREQUENCY OR BY MEANS APPROVED BY THE ENGINEER.
- 4. FILL BELOW PAVEMENT GRADES SHALL BE GRANULAR BORROW COMPACTED PER MDOT REQUIREMENTS.
- 5. SITEWORK CONTRACTOR SHALL COORDINATE GEOTECHNICAL ENGINEERING INSPECTIONS WITH THE CONSTRUCTION MANAGER PRIOR TO PLACING GRAVELS.
- 6. TACK COAT SHALL BE APPLIED BETWEEN SUCCESSIVE LIFTS OF ASPHALT.
- 7. THE BITUMINOUS PAVEMENT SHALL BE COMPACTED TO 92 TO 97 PERCENT OF ITS THEORETICAL MAXIMUM DENSITY AS DETERMINED BY ASTM D-2041. THE BASE AND SUBBASE MATERIALS SHOULD BE COMPACTED TO AT LEAST 95 PERCENT OF THEIR MAXIMUM DRY DENSITIES AS DETERMINED BY

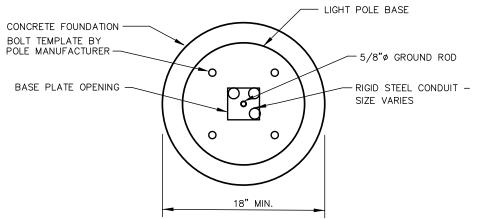
SITE PAVEMENT CROSS SECTION

SECTION

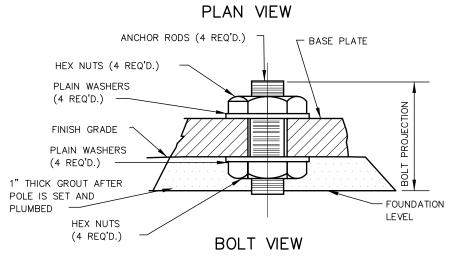
LIGHT POLE BASE DETAIL



CONCRETE TO BE 4000 PSI



3" CLEARANCE

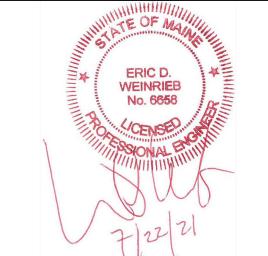


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133 Court Street (603) 433-2335

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C-COAST PROPERTIES, LLC

8 BANKS ROCK YORK HARBOR, MAINE 0391

<u>APPLICANT:</u>

GOOD TO-GO c/o CAPE HOUSE MANAGEMENT, LLC

484 US ROUTE 1 KITTERY, MAINE 03904

PROJECT:

GOOD TO-GO SPECIALTY FOOD **FACILITY**

TAX MAP 67, LOT 1

524 U.S. ROUTE 1 KITTERY, MAINE

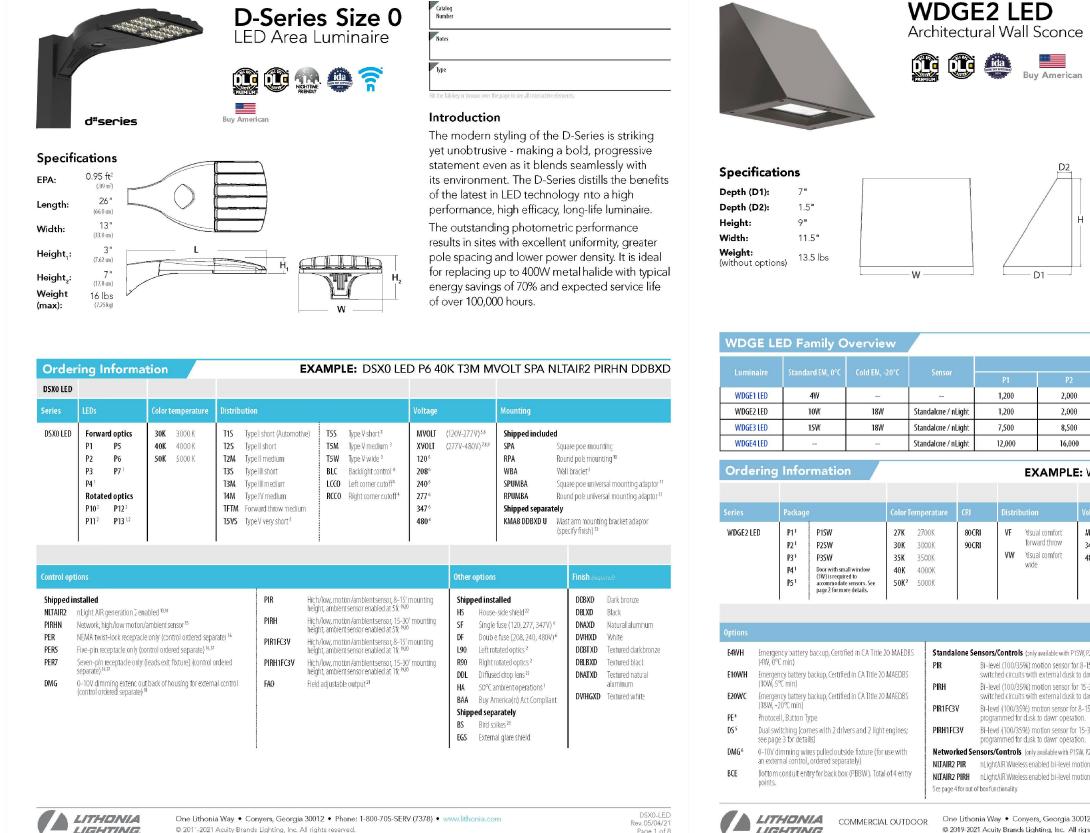
DETAILS

SHEET NUMBER:

D-6

TYPICAL ROADWAY CROSS SECTION

NOT TO SCALE



Introduction The WDGE LED family is designed to meet specifier's every wall-mounted lighting need in a widely accepted shape that blands with any architecture. The clean rectilinear design comes in four sizes with lumen packages ranging from 1,200 to 25,000 lumens, providing a true site-wide solution. Embedded with nLight® AIR wireless controls, the WDGE family provides additional energy savings and code compliance. WDGE2 delivers up to 6,000 lumens with a soft, non-pixelated light source, creating a visually comfortable environment. When combined with multiple integrated emergency battery backup options, including an 18W cold temperature option, the WDGE2 becomes the ideal wallmounted lighting solution for pedestrian scale applications in any environment 2,000 2,000 3,000 8,500 10,000 12,000 16,000 18,000 **EXAMPLE:** WDGE2 LED P3 40K 80CRI VF MVOLT SRM DDBXD AWS 3/8inch Architectural wall spacer VW Visual comfort bracket PBBW Surface-mounted back box (top, left ICW Indirect Canopy/Ceilin Washer bracket (dry/ right conduit entry). Use when there

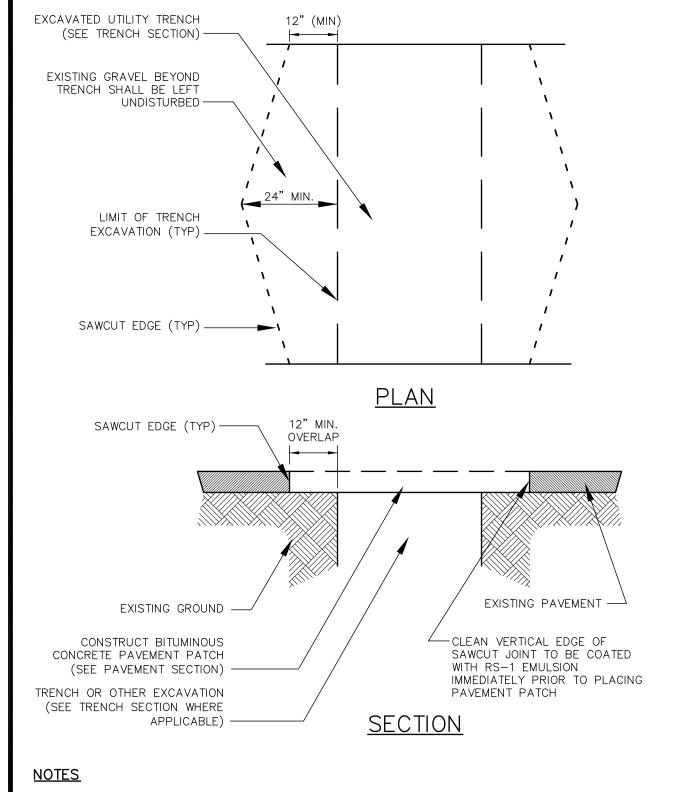
DDBXD Dark bronze Standalone Sensors/Controls (only available with P1SW, P2SW & P3SW) Bi-level (100/35%) motion sensor for 8-15' mounting heights. Intended for use on **DBLXD** Black switched circuits with external dusk to dawn switching. Bi-level (100/35%) motion sensor for 15-30' mounting heights. Intended for use on DWHXD White DSSXD Sandstone PIR1FC3V Bi-level (100/35%) motion sensor for 8-15' mounting heights with photocell pre-DDBTXD Textured dark bronze DBLBXD Textured black **PIRH1FC3V** Bi-level (100/35%) motion sensor for 15-30′ mounting heights with photocell preprogrammed for dusk to dawn operation. DNATXD Textured natural aluminum Networked Sensors/Controls (only available with P1SW, P2SW & P3SW) DWHGXD Textured white NITAIR2 PIR nLightAIR Wireless enabled bi-level motion/ambient sensor for 8-15' mounting heights. DSSTXD Textured sandstone NLTAIR2 PIRH nLightAIR Wireless enabled bi-level motion/ambient sensor for 15-30' mounting heights CCMMERCIAL OUTDOOR

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LIGHT FIXTURE CUT SHEETS

LIGHTING.

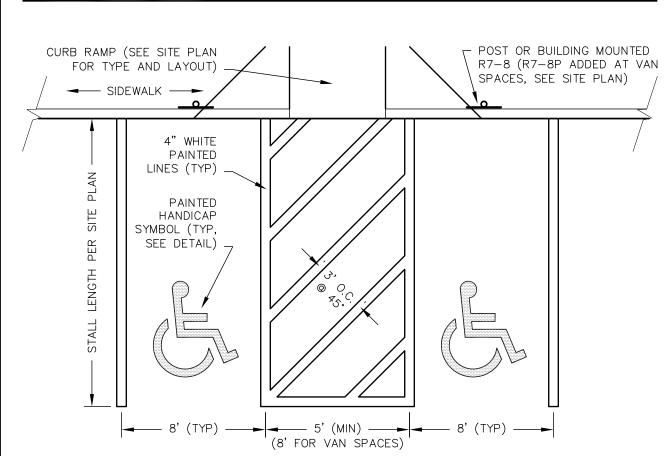
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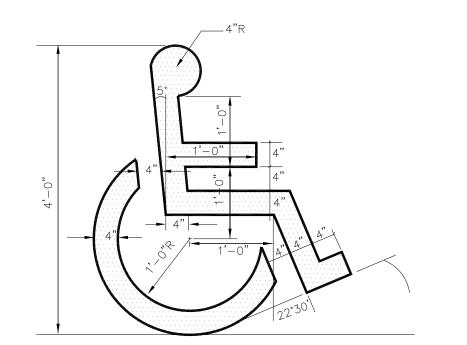
- 1. MACHINE CUT EXISTING PAVEMENT.
- 2. ALL TEMPORARY, DAMAGED OR DEFECTIVE PAVEMENT SHALL BE REMOVED PRIOR TO PLACEMENT OF PERMANENT TRENCH REPAIRS.
- 3. DIAMOND PATCHES, SHALL BE REQUIRED FOR ALL TRENCHES CROSSING ROADWAY. DIAMOND PATCHES SHALL MEET NHDOT REQUIREMENTS.

TYPICAL TRENCH PATCH

NOT TO SCALE



HANDICAP PARKING STALL LAYOUT NOT TO SCALE



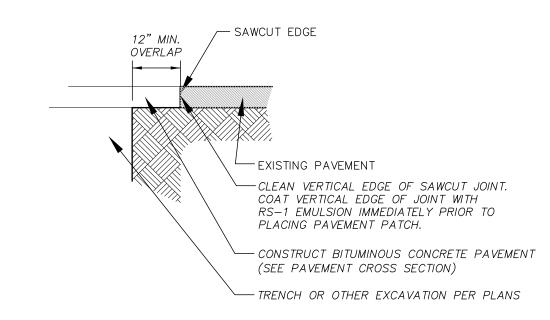
SYMBOL TO BE PAINTED IN ALL HANDICAPPED ACCESSIBLE SPACES IN WHITE PAINT (BLUE-

PAINTED SQUARE BACKGROUND OPTIONAL)

PAINTED HANDICAP SYMBOL

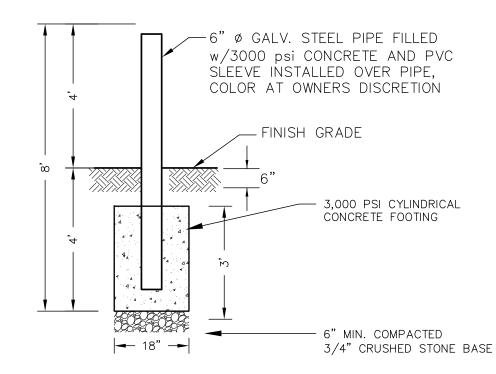
<u>NOTES</u>

NOT TO SCALE

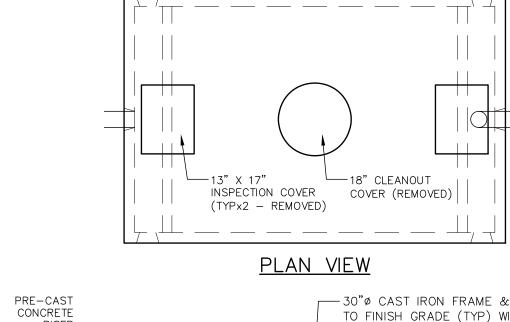


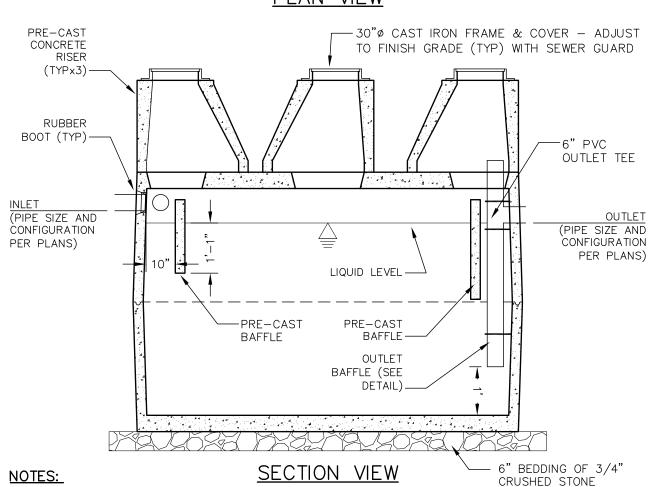
TYPICAL PAVEMENT SAWCUT

NOT TO SCALE



BOLLARD NOT TO SCALE

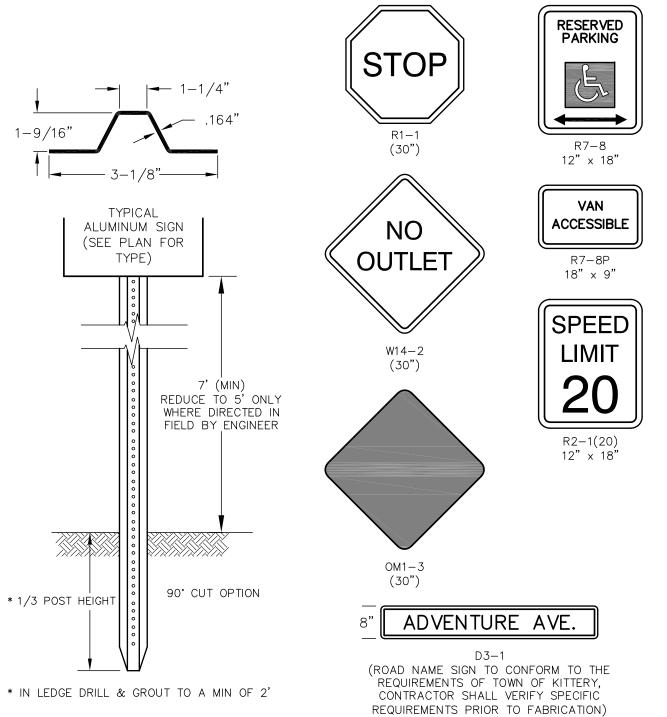




- TANK SHALL BE 4,000 PSI (MIN.) STEEL REINFORCED CONCRETE.
- KEYED TANK JOINTS SHALL BE SEALED WITH BUTYL RUBBER.
- TANK SHALL BE MANUFACTURED BY SHEA CONCRETE PRODUTS OR APPROVED EQUAL. TANK DIMENSIONS MAY VARY DEPENDING ON THE MANUFACTURER.
- 4. INLET AND OUTLET PIPE SIZES AND CONFIGURATION SHALL BE CONSTRUCTED PER THE PLANS.

1,500 GALLON GREASE TRAP

NOT TO SCALE



LENGTH: AS REQUIRED

WEIGHT PER LINEAR FOOT: 2.50 LBS (MIN.) HOLES: 3/8" DIAMETER, 1" C-C FULL LENGTH

STEEL: SHALL CONFORM TO ASTM A-499 (GRADE 60) OR ASTM A-576 (GRADE 1070 - 1080)

SIGN DETAILS

NOT TO SCALE

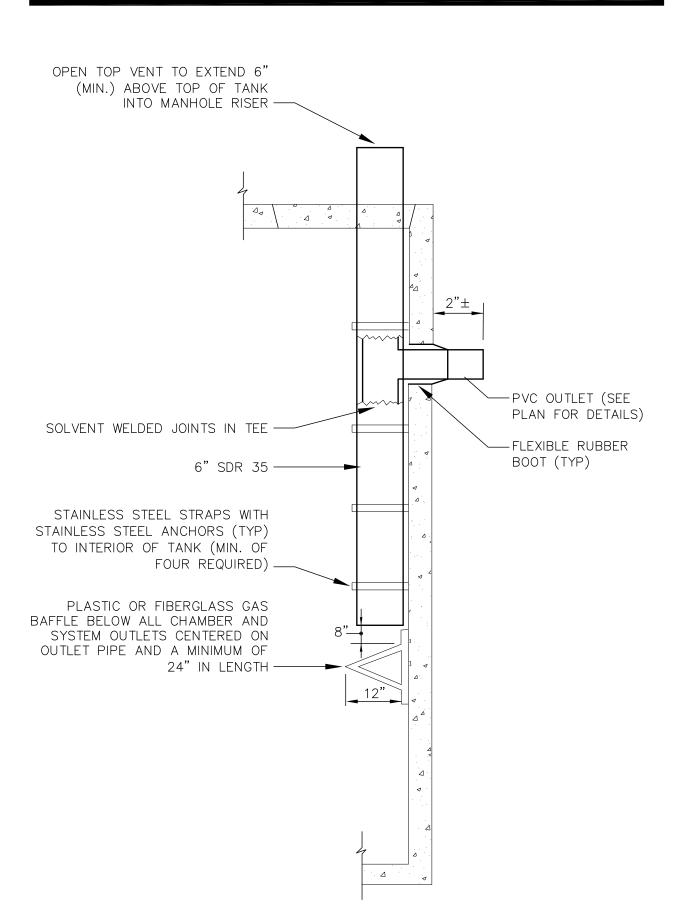
REQUIREMENTS OF AND BE INSTALLED

UNIFORM TRAFFIC CONTROL DEVICES,

AS INDICATED IN THE MANUAL ON

1. ALL SIGNS SHALL MEET THE

LATEST EDITION.



GREASE TRAP OUTLET BAFFLE DETAIL NOT TO SCALE

LEGEND - PROPERTY LINE - · - · - RIGHT OF WAY ----- EASEMENT BUILDING SETBACK — — WETLAND SETBACK ---- 250' VERNAL POOL SETBACK — — 250' SHORELAND PROTECTION OVERLAY ZONE STONEWALL — · · — · · — WETLAND BOUNDARY HISS SOIL BOUNDARY HISS SOIL DESIGNATION TESTPIT OR BORING LOCATION ---- EXISTING/PROPOSED GRAVEL VGC SGC EXISTING PAVEMENT/CURB PROPOSED PAVEMENT/VERTICAL OR SLOPED GRANITE CURB __________ SINGLE WHITE LINE/SINGLE YELLOW LINE/DOUBLE YELLOW LINE EXISTING/PROPOSED GUARDRAIL EXISTING/PROPOSED STOCKADE FENCE — — 60— — EXISTING CONTOUR —60---- PROPOSED CONTOUR/INTERMEDIATE CONTOUR

 $\times \frac{104.001}{100.008}$ PROPOSED SPOT GRADE/TOP & BOTTOM OF WALL OR CURB PROPOSED RETAINING WALL

-----W- * EXISTING WATER/CURB STOP/VALVE/HYDRANT —(S)— EXISTING SEWER/MANHOLE

— OHW——UGU— EXIST. OVERHEAD/UNDERGROUND UTILITIES/POLE

▶──W───W ROPOSED THRUST BLOCK/CURB STOP/VALVE/HYDRANT — PW —— F —— PROPOSED DOMESTIC/FIRE WATER SERVICE LINE ──S ---S- PROPOSED SEWER/MANHOLE/CLEANOUT

PROPOSED SEWER FORCEMAIN/AIR RELIEF VALVE ----- PROPOSED GAS OR PROPANE

-OHW- 🔪 PROPOSED OVERHEAD UTILITIES/UTILITY POLE —— PROPOSED UNDERGROUND ELECTRIC/PHONE/TV PROPOSED DRAINAGE (HARD PIPE)/CB/DCB/DMH/FES

======= PROPOSED DRAINAGE (PERFORATED PIPE)/CLEANOUT HDWL CORRUGATED PLASTIC PIPE/FLARED END SECTION/HEADWALL PROPOSED GROUND SLOPE/APPROX. GRADE/STONE CHECK DAM

■ ■ ■ ■ ■ ■ ■ ■ STABILIZED CONSTRUCTION EXIT PROPOSED LIMIT OF DISTURBANCE/TREE CLEARING

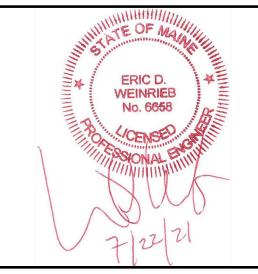
----- PROPOSED SAWCUT EXISTING TREE/DRIP LINE PROPOSED TREELINE

PARKING COUNT PER ROW/FOR TOTAL SITE 226 PROPOSED EROSION CONTROL BLANKET

PROPOSED RIPRAP

PROPOSED GRASSED UNDERDRAINED SOIL FILTER (GUSF)

133 Court Street Portsmouth, NH 03801 (603) 433-2335 www.altus-eng.com



NOT FOR CONSTRUCTION

ISSUED FOR:

ISSUE DATE:

PLANNING BOARD

JULY 22, 2021 <u>REVISIONS</u>

BY DATE NO. DESCRIPTION O PLANNING BOARD EBS 07/22/2

EBS DRAWN BY: APPROVED BY: 5116-SITE.dwg DRAWING FILE: _

SCALE: NOT TO SCALE

<u>OWNER:</u>

C-COAST PROPERTIES, LLC

8 BANKS ROCK YORK HARBOR, MAINE 03911

APPLICANT:

GOOD TO-GO c/o CAPE HOUSE MÁNAGEMENT, LLC

484 US ROUTE 1 KITTERY, MAINE 03904

PROJECT:

GOOD TO-GO SPECIALTY FOOD **FACILITY**

TAX MAP 67, LOT 1

524 U.S. ROUTE 1

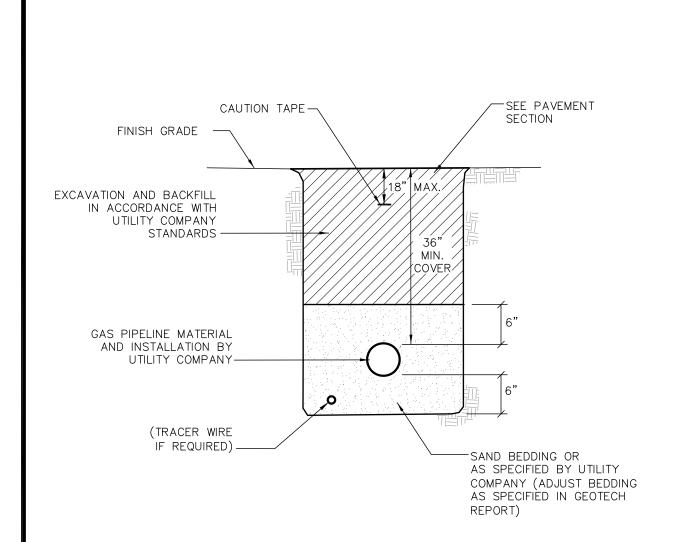
KITTERY, MAINE

TITLE:

DETAILS

SHEET NUMBER:

D-7



- 1. CONTRACTOR TO COORDINATE WITH UTILITY COMPANY AND PROVIDE ALL EXCAVATION, COMPACTION AND BACKFILL FOR PIPE INSTALLATION.
- 2. BACKFILL MATERIAL BELOW PAVED OR CONCRETE AREAS, BEDDING MATERIAL, AND SAND BLANKET SHALL BE COMPACTED TO NOT LESS THAN 95% OF AASHTO T 99, METHOD C. SUITABLE BACKFILL MATERIAL BELOW LOAM AREAS SHALL BE COMPACTED TO NOT LESS THAN 90% OF AASHTO T 99,

GAS TRENCH

NOT TO SCALE

SAND BLANKET/BARRIER

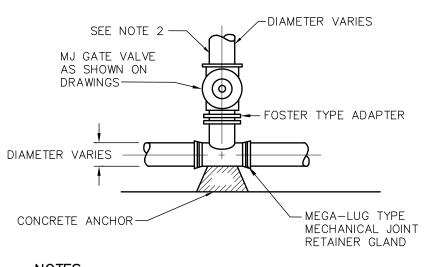
% FINER BY WEIGHT

90 - 100

0 - 15

SIEVE SIZE

200

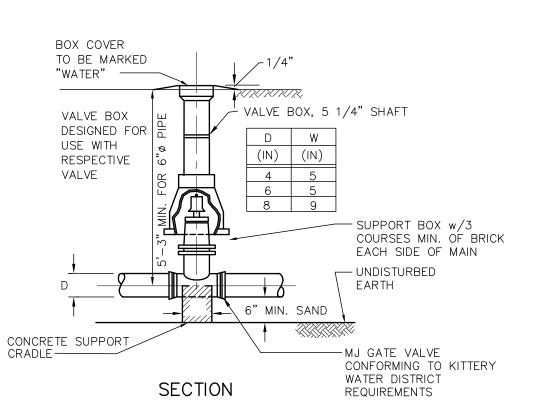


NOTES:

- 1. GATE VALVES MUST OPEN LEFT AND CONFORM TO ALL
- KITTERY WATER DISTRICT REQUIREMENTS. 2. BRANCH PIPING SHALL BE MECHANICALLY RESTRAINED AS

TEE & GATE VALVE ASSEMBLY DETAIL NOT TO SCALE

NOTED UNDER THRUST BLOCK DETAIL REQUIREMENTS.

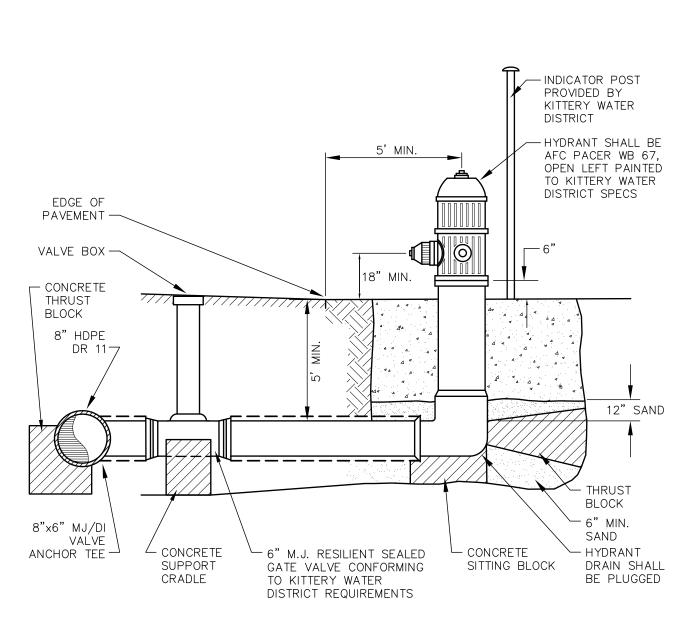


WATER VALVE DETAIL NOT TO SCALE

NON-PAVED AREA | PAVED AREA SEE ROADWAY CROSS-SECTION OR BUILDING PAD DETAILS MAGNETIC WARNING TAPE (12" ABOVE EA. CONDUIT) -SAND BLANKET/BARRIER SIEVE SIZE % FINER BY WEIGHT 1/2" 90 - 100 200 0 - 15 " CLEAR (MIN) 12" -CLEAN GRANULAR BACKFILL MATERIAL COMPACTED AS SPECIFIED 3'-7" (MIN) 51" MIN. UNDER SLAB CONDUIT SELECT SAND COMPACTED TO (AS REQUIRED) 95% STANDARD PROCTOR (ADJUST BEDDING AS SPECIFIED IN GEOTECH REPORT) <u>NOTES</u>

- 1. ALL CONDUIT IS TO BE SCHEDULE 40 PVC, ELECTRICAL GRADE, GRAY IN COLOR AND INSTALLED PER THE MANUFACTURER'S RECOMMENDATIONS. A 10-FOOT HORIZONTAL SECTION OF RIGID GALVANIZED STEEL CONDUIT WILL BE REQUIRED AT EACH SWEEP, UNLESS IN THE OPINION OF THE SERVICE PROVIDER DESIGNER, THE SWEEP-PVC JOINT IS NOT SUBJECT TO FAILURE DURING PULLING OF THE CABLE. ALL JOINTS ARE TO BE WATERTIGHT.
- 2. ALL 90 DEGREE SWEEPS WILL BE MADE WITH RIGID GALVANIZED STEEL WITH A MINIMUM RADIUS OF 36 INCHES FOR PRIMARY CABLES AND 24 INCHES FOR SECONDARY CABLES.
- 3. BACKFILL MAY BE MADE WITH EXCAVATED MATERIAL OR COMPARABLE, UNLESS MATERIAL IS DEEMED UNSUITABLE BY SERVICE PROVIDER. BACKFILL SHALL BE FREE OF FROZEN LUMPS, ROCKS, DEBRIS, AND RUBBISH. ORGANIC MATERIAL SHALL NOT BE USED AS BACKFILL. BACKFILL SHALL BE IN 6-INCH LAYERS AND THOROUGHLY COMPACTED.
- 4. A SUITABLE PULLING STRING, CAPABLE OF 300 POUNDS OF PULL, MUST BE INSTALLED IN THE CONDUIT BEFORE SERVICE PROVIDER IS NOTIFIED TO INSTALL CABLE. THE STRING SHOULD B BLOWN INTO THE CONDUIT AFTER THE RUN IS ASSEMBLED TO AVOID BONDING THE STRING TO THE CONDUIT. A MINIMUM OF TWENTY-FOUR (24") INCHES OF ROPE SLACK SHALL REMAIN AT THE END OF EACH DUCT. PULL ROPE SHALL BE INSTALLED IN ALL CONDUIT FOR FUTURE PULLS. PULL ROPE SHALL BE NYLON ROPE HAVING A MINIMUM TENSILE STRENGTH OF THREE HUNDRED (300#) LBS.
- 5. SERVICE PROVIDER SHALL BE GIVEN THE OPPORTUNITY TO INSPECT ALL CONDUIT PRIOR TO BACKFILL. THE CONTRACTOR IS RESPONSIBLE FOR ALL REPAIRS SHOULD SERVICE PROVIDER BE UNABLE TO INSTALL ITS CABLE IN A SUITABLE MANNER.
- 6. TYPICAL CONDUIT SIZES ARE 3-INCH FOR SINGLE PHASE PRIMARY AND SECONDARY VOLTAGE CABLES, 4-INCH FOR THREE PHASE SECONDARY, AND 5-INCH FOR THREE PHASE PRIMARY. HOWEVER, SERVICE PROVIDERS MAY REQUIRE DIFFERENT NUMBERS, TYPES AND SIZES OF CONDUIT THAN THOSE SHOWN HERE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFYING ALL CONDUIT SIZES, TYPES AND NUMBERS WITH EACH SERVICE PROVIDER PRIOR TO ORDERING THEM.
- 7. ROUTING OF CONDUIT, LOCATION OF MANHOLES, TRANSFORMERS, CABINETS, HANDHOLES, ETC., SHALL BE DETERMINED BY SERVICE PROVIDER DESIGN PERSONNEL. THE CONTRACTOR SHALL COORDINATE WITH ALL SERVICE PROVIDERS PRIOR TO THE INSTALLATION OF ANY CONDUIT.
- 8. ALL CONDUIT INSTALLATIONS MUST CONFORM TO THE CURRENT EDITION OF THE NATIONAL ELECTRIC SAFETY CODE, STATE AND LOCAL CODES AND ORDINANCES, AND WHERE APPLICABLE, THE NATIONAL ELECTRIC CODE. WHERE REQUIRED BY UTILITY PROVIDER, CONDUIT SHALL BE SUPPORTED IN PLACE USING PIPE STANCHIONS PLACED EVERY FIVE (5') FEET ALONG THE CONDUIT RUN.
- 9. UNDER A BUILDING SLAB THE CONDUIT SHALL BE ENCASED IN 8" OF CONCRETE ON ALL SIDES. 10.ALL CONDUIT TERMINATIONS SHALL BE CAPPED TO PREVENT DEBRIS FROM ENTERING CONDUIT.

ELECTRIC / COMMUNICATION TRENCH NOT TO SCALE



- 1. OPERATION OF HYDRANTS AND VALVES SHALL BE OPEN LEFT PER THE REQUIREMENTS OF THE KITTERY WATER DISTRICT.
- 2. ALL WORK SHALL CONFORM TO KITTERY WATER DISTRICT "WATER MAIN MATERIAL AND INSTALLATION SPECIFICATIONS, MARCH 2009". CONTRACTOR SHALL OBTAIN A COPY OF SAID SPECIFICATIONS AND MEET WITH THE KITTERY WATER DISTRICT PRIOR TO PURCHASING MATERIALS OR COMMENCING CONSTRUCTION.
- MECHANICAL JOINT FITTINGS ARE TO BE CLASS 350 AND HAVE ROMAC "GRIP RING" RETAINER GLANDS WITH CORTEN LOW ALLOY STEEL NUTS AND BOLTS OR MEGALUG RETAINER GLANDS.

FIRE HYDRANT NOT TO SCALE

STANDARD TRENCH NOTES

- ORDERED EXCAVATION OF UNSUITABLE MATERIAL BELOW GRADE: BACKFILL AS STATED IN THE TECHNICAL SPECIFICATIONS OR AS SHOWN ON THE DRAWING.
- BEDDING: SCREENED GRAVEL AND/OR CRUSHED STONE FREE FROM CLAY, LOAM, ORGANIC MATTER AND MEETING THE GRADATION SHOWN IN THE TRENCH DETAIL. WHERE ORDERED BY THE ENGINEER TO STABILIZE THE BASE, SCREENED GRAVEL OR CRUSHED STONE 1-1/2 INCH TO 1/2 INCH SHALL BE USED.
- 3. SAND BLANKET: CLEAN SAND FREE FROM ORGANIC MATTER MEETING THE GRADATION SHOWN IN THE TRENCH DETAIL. BLANKET MAY BE REPLACED WITH BEDDING MATERIAL FOR CAST-IRON, DUCTILE IRON, AND REINFORCED CONCRETE PIPE PROVIDED THAT NO STONE LARGER THAN 2" IS IN CONTACT WITH THE PIPE AND THE GEOTEXTILE IS RELOCATED ACCORDINGLY.
- 4. SUITABLE MATERIAL: IN ROADS, ROAD SHOULDERS, WALKWAYS AND TRAVELED WAYS, SUITABLE MATERIAL FOR TRENCH BACKFILL SHALL BE THE NATURAL MATERIAL EXCAVATED DURING THE COURSE OF CONSTRUCTION, BUT SHALL EXCLUDE DEBRIS, PIECES OF PAVEMENT, ORGANIC MATTER, TOP SOIL, ALL WET OR SOFT MUCK, PEAT, OR CLAY, ALL EXCAVATED LEDGE MATERIAL, ALL ROCKS OVER 6 INCHES IN LARGEST DIMENSION, AND ANY MATERIAL WHICH, AS DETERMINED BY THE ENGINEER, WILL NOT PROVIDE SUFFICIENT SUPPORT OR MAINTAIN THE COMPLETED CONSTRUCTION IN A STABLE CONDITION. IN CROSS COUNTRY CONSTRUCTION, SUITABLE MATERIAL SHALL BE AS DESCRIBED ABOVE, EXCEPT THAT THE ENGINEER MAY PERMIT THE USE OF TOP SOIL, LOAM, MUCK, OR PEAT, IF SATISFIED THAT THE COMPLETED CONSTRUCTION WILL BE ENTIRELY STABLE AND PROVIDED THAT EASY ACCESS TO THE SEWER FOR MAINTENANCE AND POSSIBLE RECONSTRUCTION WILL BE PRESERVED.
- 5. BASE COURSE AND PAVEMENT SHALL MEET THE REQUIREMENTS OF THE MAINE DEPARTMENT OF TRANSPORTATION'S LATEST EDITION OF THE STANDARD SPECIFICATIONS FOR HIGHWAYS AND BRIDGES - DIVISION 700.
- 6. SHEETING, IF REQUIRED: WHERE SHEETING IS PLACED ALONGSIDE THE PIPE AND EXTENDS BELOW MID-DIAMETER, IT SHALL BE CUT OFF AND LEFT IN PLACE TO AN ELEVATION 1 FOOT ABOVE THE TOP OF PIPE. WHERE SHEETING IS ORDERED BY THE ENGINEER TO BE LEFT IN PLACE, IT SHALL BE CUT OFF AT LEAST 3 FEET BELOW FINISHED GRADE, BUT NOT LESS THAT 1 FOOT ABOVE THE TOP OF THE PIPE.
- 7. W = MAXIMUM ALLOWABLE TRENCH WIDTH TO A PLANE 12 INCHES ABOVE THE PIPE. FOR PIPES 15 INCHES NOMINAL DIAMETER OR LESS, W SHALL BE NO MORE THAN 36 INCHES. FOR PIPES GREATER THAN 15 INCHES IN NOMINAL DIAMETER, W SHALL BE 24 INCHES PLUS PIPE OUTSIDE DIAMETER (O.D.) ALSO, W SHALL BE THE PAYMENT WIDTH FOR LEDGE EXCAVATION AND FOR ORDERED EXCAVATION BELOW GRADE.
- FOR CROSS COUNTRY CONSTRUCTION, BACKFILL, FILL AND/OR LOAM SHALL BE MOUNDED TO A HEIGHT OF 6 INCHES ABOVE THE ORIGINAL GROUND SURFACE.
- 9. CONCRETE FOR ENCASEMENT SHALL CONFORM TO THE MAINE DEPARTMENT OF PUBLIC WORKS AND HIGHWAYS STANDARD SPECIFICATION REQUIREMENTS FOR CLASS A (3000#) CONCRETE AS FOLLOWS:

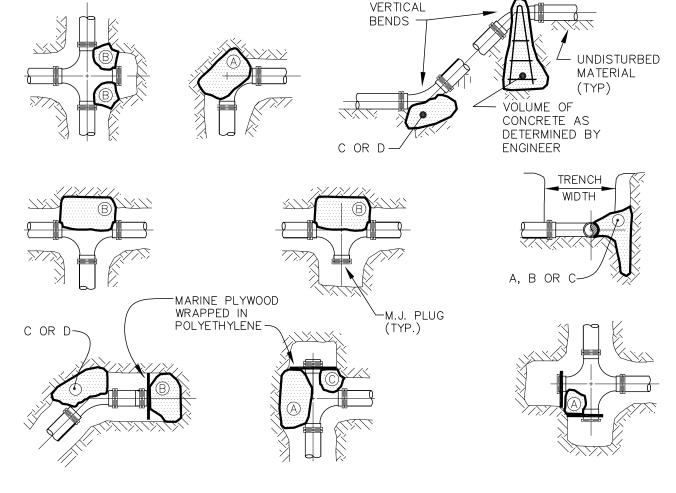
CEMENT: 6.0 BAGS PER CUBIC YARD WATER: 5.75 GALLONS PER BAG

CEMENT MAXIMUM SIZE OF AGGREGATE: 1 INCH CONCRETE ENCASEMENT IS NOT ALLOWED FOR PVC PIPE.

- 10. CONCRETE FULL ENCASEMENT: IF FULL ENCASEMENT IS UTILIZED, DEPTH OF CONCRETE BELOW PIPE SHALL BE 1/4 I.D. (4" MINIMUM). BLOCK SUPPORT SHALL BE SOLID CONCRETE BLOCKS.
- 11. MAINE DEPARTMENT OF ENVIRONMENTAL PROTECTION DESIGN STANDARDS REQUIRE TEN FEET (10') SEPARATION BETWEEN WATER AND SEWER. REFER TO TOWN'S STANDARD SPECIFICATIONS FOR METHODS OF PROTECTION IN AREAS THAT CANNOT MEET THESE REQUIREMENTS.

DRAINAGE AND SEWER TRENCH

NOT TO SCALE



NON-PAVED AREA |

LOAM AND SEED OR OTHER

SURFACE TREATMENT PER PLANS -

6" GRAVEL BORROW -

SUITABLE EXCAVATED

BACKFILL OR CLEAN GRANULAR BACKFILL

AS SPECIFIED -

SURFACE

THICKNESS) -

TAPE 24" BELOW

SAND BLANKET AS

SPECIFIED BELOW

WOOD SHEETING AS

A.O.S.=70 OR LESS -

UNDISTURBED SOIL ---

REQUIRED (3" MINIMUM

NON-WOVEN GEOTEXTILE

ARE IN TRENCH.

200

SAND BLANKET/BARRIER

% FINER BY WEIGHT

90 - 100

0 - 15

MATERIAL COMPACTED

"CAUTION - WARNING"

PAVED AREA

3'-0" (MIN) OR D+2

FOR SINGLE PIPE

(WHICHEVER IS GREATER)

1. BACKFILL MATERIAL BELOW PAVED OR CONCRETE AREAS, BEDDING MATERIAL, AND SAND BLANKET

SHALL BE COMPACTED TO NOT LESS THAN 95% OF AASHTO T 99, METHOD C. SUITABLE BACKFILL

MATERIAL BELOW LOAM AREAS SHALL BE COMPACTED TO NOT LESS THAN 90% OF AASHTO T 99,

2. INSULATE GRAVITY SEWER AND FORCEMAINS WHERE THERE IS LESS THAN 5'-0" OF COVER WITH 2"

3. MAINTAIN 12" MINIMUM HORIZONTAL SEPARATION AND WIDEN TRENCH ACCORDINGLY IF MULTIPLE PIPES

THICK CLOSED CELL RIGID BOARD INSULATION, 18" ON EACH SIDE OF PIPE.

SEE PAVEMENT SECTION

SEE PAVEMENT SECTION

SEE PAVEMENT SECTION

-SCREENED GRAVEL OR

BELOW PIPE IN ROCK

GEOTECH REPORT)

- ROCK SUBGRADE

(TEMPLATE)

SCREENED GRAVEL OR CRUSHED STONE BEDDING

3/4"

3/8"

#8

% PASSING BY WEIGHT

100

90 - 100

20 - 55

0 - 10

0 - 5

(ADJUST AS SPECIFIED IN

CRUSHED STONE BEDDING FOR

UP TO SPRINGLINE OF PIPE, 6"

BELOW PIPE IN EARTH AND 12"

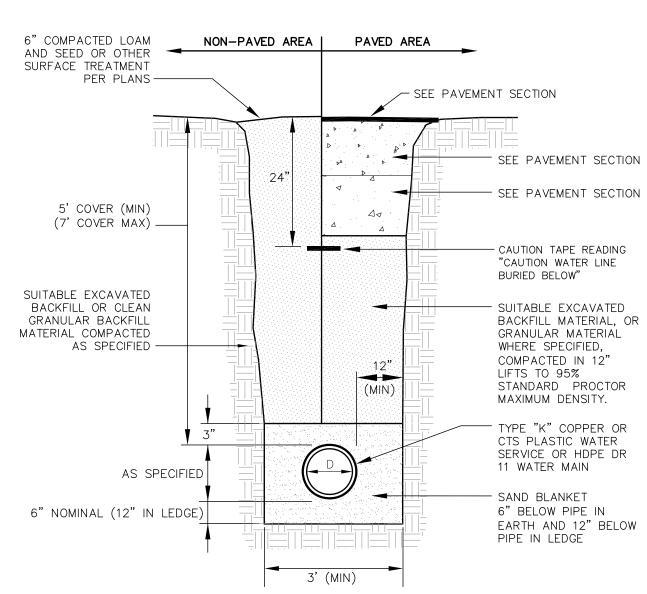
FULL WIDTH OF THE TRENCH

50 psi	SQUARE FEET OF CONCRETE THRUST BLOCKING BEARING ON UNDISTURBED MATERIAL					
-	REACTION		PIPE SIZE			
Ш	TYPE	4"	6"	8"	10"	12"
TEST PRESSURE	A 90° B 180° C 45° D 22-1/2° E 11-1/4°	0.89 0.65 0.48 0.25 0.13	2.19 1.55 1.19 0.60 0.30	3.82 2.78 2.12 1.06 0.54	11.14 8.38 6.02 3.08 1.54	17.24 12.00 9.32 4.74 2.38

- 1. POUR THRUST BLOCKS AGAINST UNDISTURBED MATERIAL. WHERE TRENCH WALL HAS BEEN DISTURBED, EXCAVATE LOOSE MATERIAL AND EXTEND THRUST BLOCK TO UNDISTURBED MATERIAL.
- 2. NO JOINTS SHALL BE COVERED WITH CONCRETE. POLYETHYLENE (6 MIL) SHALL BE PLACED AROUND FITTINGS PRIOR TO CONCRETE PLACEMENT.
- 3. ON BENDS AND TEES, EXTEND THRUST BLOCKS FULL LENGTH OF FITTING.

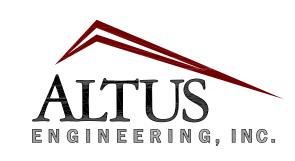
THRUST BLOCKING

4. PLACE BOARD IN FRONT OF ALL PLUGS BEFORE POURING THRUST BLOCKS. WHERE M.J. PIPE IS USED, M.J. PLUG WITH RETAINER GLAND MAY BE SUBSTITUTED FOR END BLOCKINGS.



SAND BLANKET/BARRIER		
SIEVE SIZE	% FINER BY WEIGHT	
1/2"	90 - 100	
200	0 - 15	

- 1. BACKFILL MATERIAL BELOW PAVED OR CONCRETE AREAS, BEDDING MATERIAL, AND SAND BLANKET SHALL BE COMPACTED TO NOT LESS THAN 95% OF AASHTO T 99, METHOD C. SUITABLE BACKFILL MATERIAL BELOW LOAM AREAS SHALL BE COMPACTED TO NOT LESS THAN 90% OF AASHTO T 99,
- 2. ALL TRENCHING AND BACKFILL SHALL CONFORM WITH THE STANDARDS OF THE KITTERY WATER DISTRICT.



Portsmouth, NH 03801

www.altus-eng.com

133 Court Street (603) 433-2335

ERIC D. WEINRIEB No. 6658

NOT FOR CONSTRUCTION

<u>ISSUED FOR:</u>

PLANNING BOARD

ISSUE DATE:

D PLANNING BOARD

JULY 22, 2021

<u>REVISIONS</u> NO. DESCRIPTION BY DATE

EBS 07/22/2

EBS DRAWN BY: APPROVED BY: 5116-SITE.dwg DRAWING FILE:

SCALE:

NOT TO SCALE

C-COAST PROPERTIES, LLC

8 BANKS ROCK YORK HARBOR, MAINE 0391

<u>APPLICANT:</u>

GOOD TO-GO c/o CAPE HOUSE MÁNAGEMENT, LLC

484 US ROUTE 1 KITTERY, MAINE 03904

PROJECT:

GOOD TO-GO SPECIALTY FOOD **FACILITY**

TAX MAP 67, LOT 1

524 U.S. ROUTE 1 KITTERY, MAINE

DETAILS

SHEET NUMBER:

D-8

WATER MAIN TRENCH NOT TO SCALE NOT TO SCALE

PLATE SHALL BE 5086 ALUMINUM.

1. STYLE "DT-HD" ACCESS HATCH, AS MANUFACTURED BY SYRACUSE CASTINGS, CICERO, NEW YORK (315-699-2601) OR APPROVED EQUAL.

2. MATERIAL SHALL BE 6061-T6 ALUMINUM FOR BARS, ANGLES, AND EXTRUSIONS. 1/4" DIAMOND

3. UNIT DESIGNED HEAVY DUTY, FOR H-20 WHEEL LOADS, WHERE NOT SUBJECT TO HIGH DENSITY TRAFFIC. FRAME AND BEARING PLATE MUST BE CAST INTO AND SUPPORTED BY CONCRETE DESIGNED

4. UNIT SUPPLIED WITH A HEAVY DUTY PNEU-SPRING, FOR EASE OF OPERATION WHEN OPENING COVER. COVER SHALL BE COUNTERBALANCED, SO ONE PERSON CAN EASILY OPEN THE HATCH DOOR.

5. FRAME SHALL BE OF EXTRUDED ALUMINUM WITH A CONTINUOUS 1-1/4" ANCHOR FLANGE. A DOVETAIL GROOVE SHALL BE EXTRUDED INTO THE SEAT OF THE FRAME FOR A 1/8" SILICONE GASKET.

6. EACH HATCH SHALL BE EQUIPPED WITH A STAINLESS STEEL HOLD OPEN ARM. DOOR SHALL LOCK OPEN IN THE 90 DEGREE POSITION. HOLD OPEN ARM SHALL BE FASTENED TO THE FRAME WITH A 1/2" GRADE 316 STAINLESS STEEL BOLT.

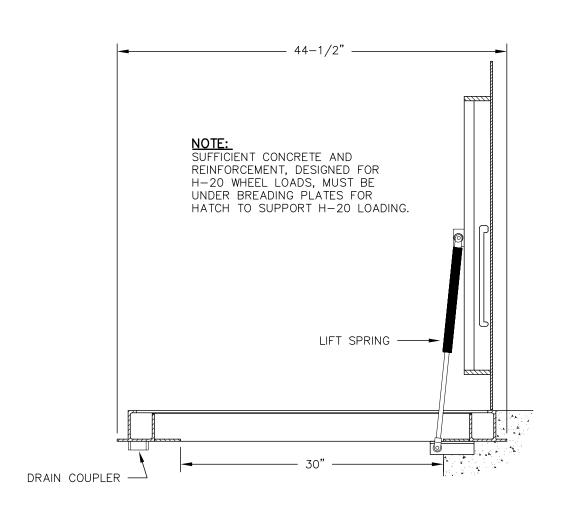
7. HINGES SHALL BE OF HEAVY DUTY DESIGN. MATERIAL SHALL BE GRADE 316 STAINLESS STEEL. EACH HINGE SHALL HAVE A GRADE 316 STAINLESS STEEL, 3/8" DIAMETER HINGE PIN. HINGE SHALL BE FASTENED TO THE CHANNEL FRAME AND DIAMOND PLATE WITH GRADE 316 STAINLESS STEEL BOLTS AND NY-LOCK NUTS.

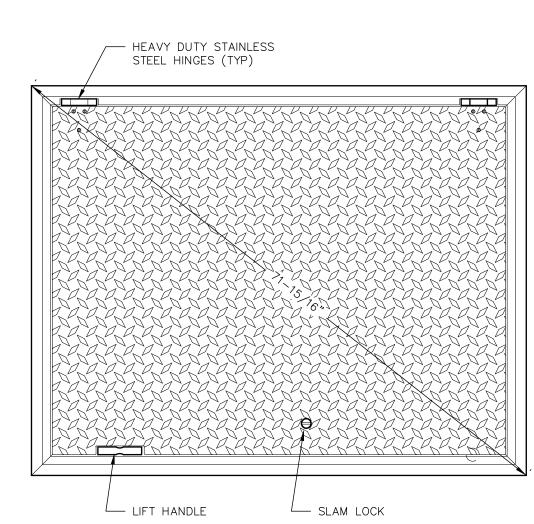
8. ALUMINUM SHALL BE SUPPLIED WITH MILL FINISH. EXTERIOR OF FRAME WHICH COMES IN CONTACT WITH CONCRETE SHALL HAVE ONE COAT BLACK PRIMER.

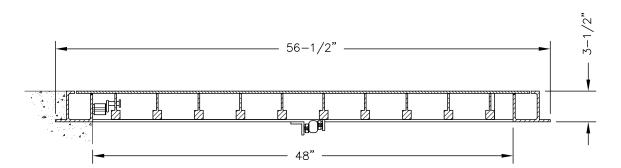
9. EACH HATCH SHALL BE SUPPLIED WITH A STAINLESS STEEL SLAM LOCK, WITH THE KEY WAY PROTECTED BY A THREADED ALUMINUM PLUG. THE PLUG SHALL BE FLUSH WITH THE TOP OF THE 1/4" DIAMOND PLATE. THE SLAM LOCK SHALL BE FASTENED WITH GRADE 316 STAINLESS STEEL BOLTS AND

10. EACH HATCH SHALL BE EQUIPPED WITH A STAINLESS STEEL LIFT HANDLE. LIFT HANDLE SHALL BE FLUSH WITH TOP OF 1/4" DIAMOND PLATE.

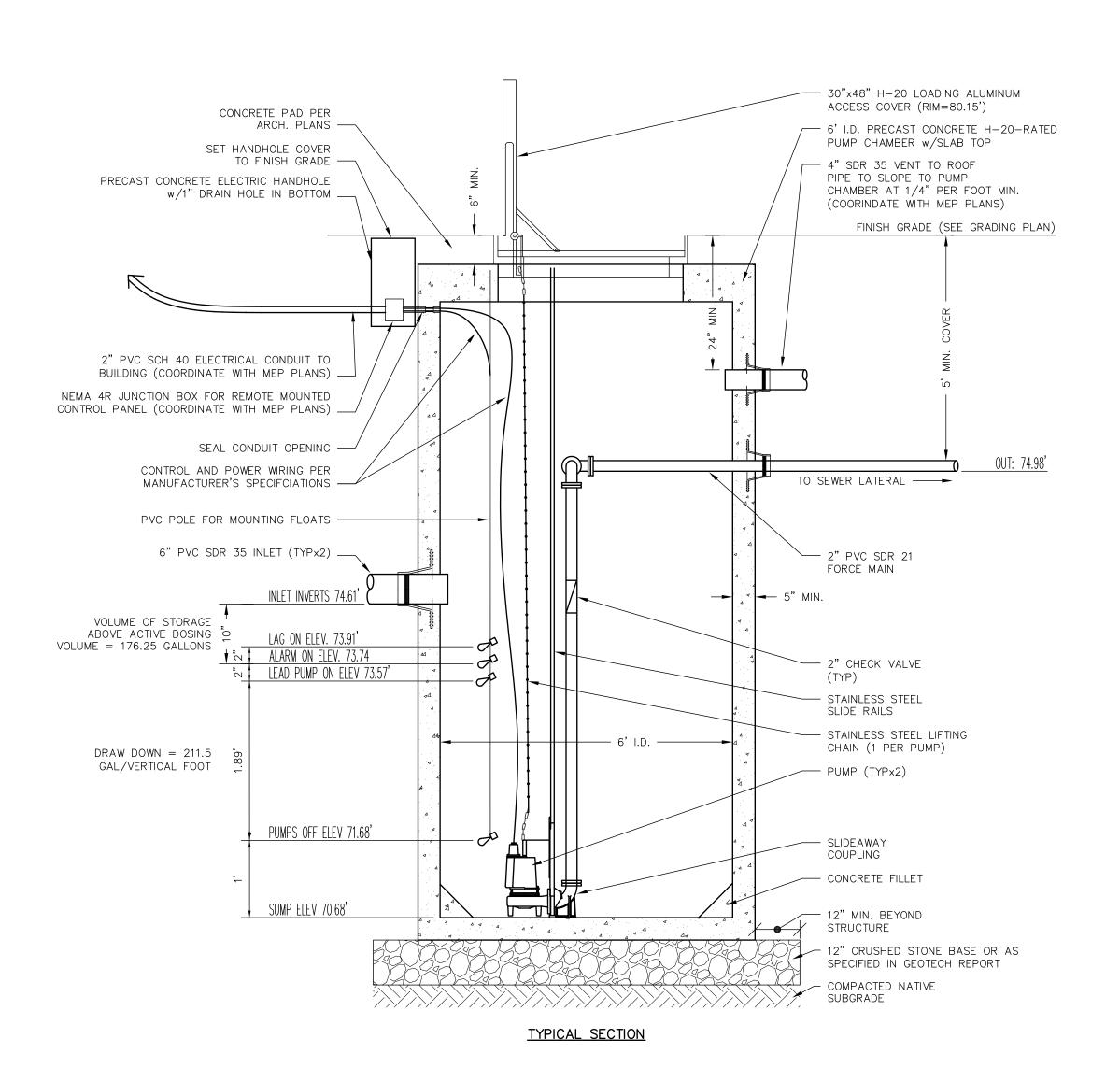
11. EACH "DT-HD" STYLE HATCH IS SUPPLIED WITH A 1-1/2" THREADED DRAIN COUPLER ON THE UNDERSIDE OF CHANNEL FRAME, FOR PIPE CONNECTION.

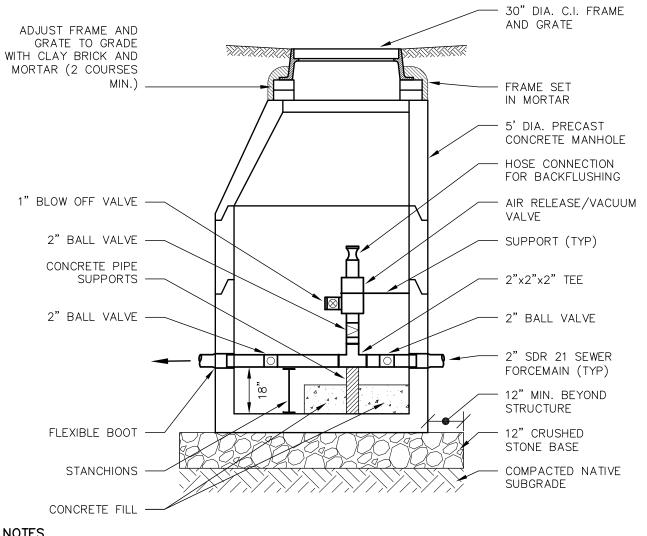






6" PVC SDR 35 INLET (SANITARY) - FLEXIBLE RUBBER BOOT KOR-N-SEAL OR EQUAL (TYP) FLOAT RACK 4" SDR 35 VENT TO - PUMP (TYPx2) BUILDING (COORDINATE w/MEP PLANS) - 30"x48" H-20 LOADING PRECAST CONCRETE ALUMINUM ACCESS COVER ELECTRIC HANDHOLE -ELECTRICAL CONDUIT AS REQUIRED -6" PVC SDR 35 INLET (FROM GREASE TRAP) FORCE MAIN





CONTRACTOR SHALL SUPPORT PIPING PER MANUFACTURERS REQUIREMENTS. ALL MANHOLE STRUCTURES, FRAMES AND GRATES SHALL BE DESIGNED FOR H20 LOADING. MANHOLE STEPS ARE NOT PERMITTED

SEWER AIR RELEASE MANHOLE

NOT TO SCALE

SEWER FLOW CALCULATIONS

AVERAGE DAILY FLOW CALCULATED FROM THE AVERAGE METERED WATER USE OVER A SIX MONTH PERIOD AT THE EXISTING 5,500 S.F. GOOD TO-GO FACILITY AT 484 U.S. ROUTE 1, KITTERY, MAINE:

13,978 CF / 154 DAYS = 90.77 CF/DAY (SUNDAYS EXCLUDED)

 $90.77 \text{ CF/DAY} \times 7.48 \text{ GAL/CF} = 679 \text{ GPD}$

679 GPD / 5,500 SF = 0.12 GPD/SF $0.12 \text{ GPD/SF} \times 20,000 \text{ SF} = 2,400 \text{ GPD DESIGN FLOW}$

PUMP STATION SPECIFICATIONS

Furnish and install pump station as shown on the plans. Station shall include, but not be limited to, a concrete pump chamber, pumps, slide rail assemblies, duplex controller, access covers discharge piping, fittings, valves, junction box, level sensors, alarms, electric service and level controls. All wiring shall be in compliance with local codes.

PUMP CHAMBER:

Pump chamber shall be an 6-foot inside diameter precast concrete pump chamber to the depth shown on the Drawings. Chamber shall be rated for H-20 loading.

The access covers shall be rigidly constructed to provide an H-20 rating with a 2'-6" X 4'-0" clear opening, maufactured by Syracuse Castings or approved equal. Cover shall be sealed with neoprene seal at openings and have hinges constructed of 316 stainless steel.

Pumps shall be supplied to operate at the following range of flow vs. TDH: Flow of 40 gpm with a total dynamic head of 34.2'. Provide pump motors with adequate horsepower to deliver flows at the TDH required to reach the receiving point, taking into account the manufacturer's rated efficiency. Motors shall be 200-240 volt, 3-phase, 60 Hz 3,450 rpm. Pumps shall be submersible non-clog sewage pumps with <u>2" discharges</u> as specified by the manufacturer and approved by the Engineer. Impellers shall have a diameter of <u>6.75" (172mm)</u>. Pumps shall be <u>Barnes 2SEV1092L (1 hp)</u> or approved equal. Provide discharge piping assembly for installation and removal of pump without entering wetwell with stainless steel lift—out rail system.

Duplex control to perform equal alternation of both pumps. Control to consist of two circuit breakers with through—door operating handle, two magnetic starters with ambient compensated quick—trip overloads in each line, discharge piping by manufacturer, duplex unit, running lights, lightening arrestor, door—mounted resets, hour meters, and door—mounted hand—off—automatic selector switches for each pump. Enclosure to include continuous hinge, neoprene gasket in cover and continuous seam weld. Controller shall be <u>Barnes Three Phase Duplex Alternating Versatrol Control Panel</u> or approved equal. The controls shall be NEMA 4x weathertight construction and mounted on the adjacent building. All conduit and wiring between the station junction boxes and control panel shall be included.

The slide rail assembly, mounting hardware, and lifting chain shall be AISI Type 316 stainless steel. Slide rails to be provided with AISI Type 316 stainless guide supports. Discharge coupling to be machined cast iron and support the pump four (4) inches above the floor.

The discharge pipe shall be two inch (2") diameter SDR 21 PVC pipe. All fittings shall be cemented or threaded. PVC ball check valves shall be provided with teflon seats. The working pressure of the check valves shall be 150 psi.

Four (4) liquid level control sensors shall be provided to control operation of the pumps and provide a high water alarm. The level control sensors shall be mounted on a PVC pipe. The controls shall be set at elevations shown on the plans and for a dosage rate of 400 gallons.

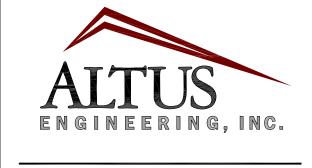
Alarm shall be exterior mounted audio and visual in a location as determined by the Owner.

Contractor shall provide a sign for identification.

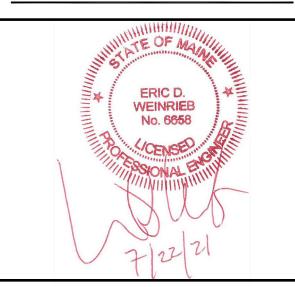
Design flow 2,400 GPD / 6 doses per day = 400 gallons per dose 400 gal / 40 gal/min = 10 minute run time

OWNER'S MAINTENANCE NOTES

1. PUMP CHAMBER TO BE PUMPED ANNUALLY BY A LICENSED SANITARY DISPOSAL CONTRACTOR.



133 Court Street Portsmouth, NH 03801 (603) 433-2335 www.altus-eng.com



NOT FOR CONSTRUCTION

ISSUED FOR:

ISSUE DATE:

PLANNING BOARD

JULY 22, 2021

EBS 07/22/2

<u>REVISIONS</u>

O PLANNING BOARD

NO. DESCRIPTION BY DATE

DRAWN BY:. APPROVED BY: ___ 5116-SITE.dwg DRAWING FILE: _

NOT TO SCALE

C-COAST PROPERTIES, LLC

8 BANKS ROCK YORK HARBOR, MAINE 03911

APPLICANT:

GOOD TO-GO c/o CAPE HOUSE MÁNAGEMENT, LLC

484 US ROUTE 1 KITTERY, MAINE 03904

PROJECT:

GOOD TO-GO SPECIALTY FOOD **FACILITY**

TAX MAP 67, LOT 1

524 U.S. ROUTE 1 KITTERY, MAINE

TITLE:

DETAILS

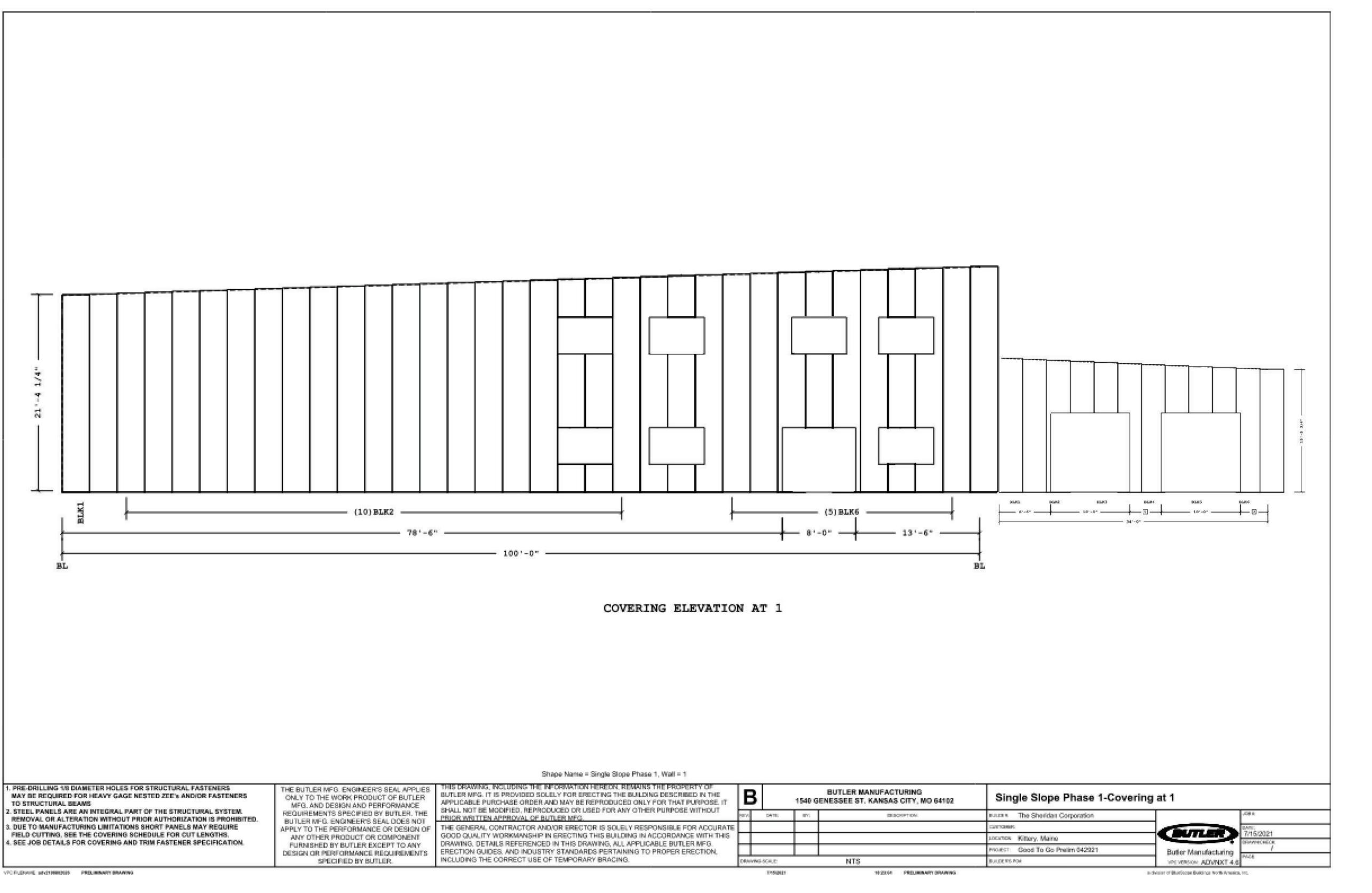
SHEET NUMBER:

NOT TO SCALE

D-9

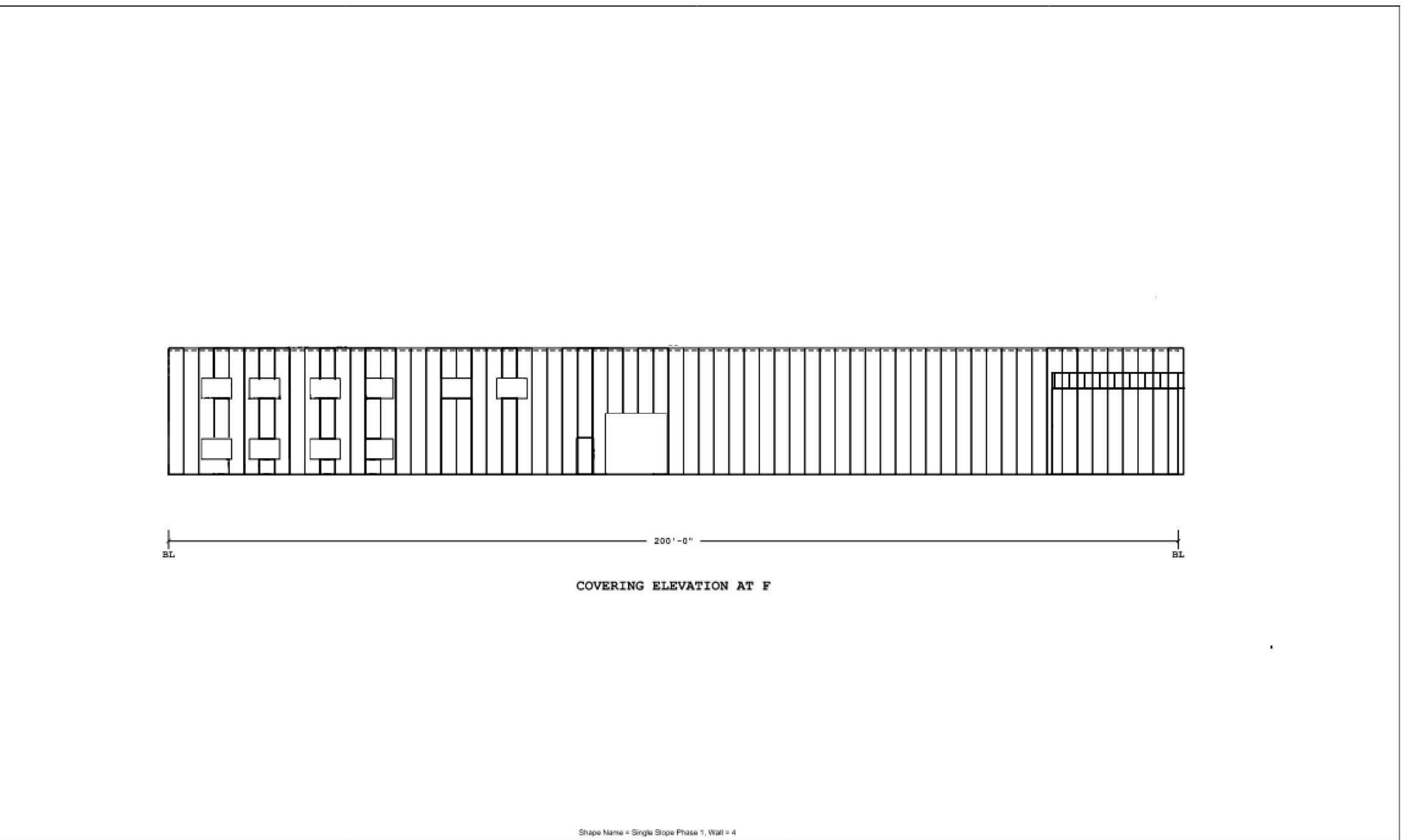
SINGLE LEAF H-20 ALUMINUM HATCH NOT TO SCALE

DUPLEX PUMP STATION



General Notes: Sheridan www.sheridaneerp.com FAIRFIELD PORTLAND MAINE Drawing Status: Engineering Designs For: Good To Go Kittery, Maine Sheet Title: **Butler Building** Front Elevation As Noted 07/12/2021

SK-2



Sheridan www.sheridancorp.com FAIRFIELD PORTLAND MAINE Drawing Status: Engineering Designs For: Good To Go Kittery, Maine Sheet Title: **Butler Building** Side Elevation As Noted 07/12/2021 SK-3

General Notes:

TO STRUCTURAL BEAMS

THE BUTLER MFG. ENGINEER'S SEAL APPLIES ONLY TO THE WORK PRODUCT OF BUTLER MFG, AND DESIGN AND PERFORMANCE REQUIREMENTS SPECIFIED BY BUTLER. THE BUTLER WEG, ENGINEER'S SEAL DOES NOT APPLY TO THE PERFORMANCE OR DESIGN OF ANY OTHER PRODUCT OR COMPONENT

FURNISHED BY BUTLER EXCEPT TO ANY

DESIGN OR PERFORMANCE REQUIREMENTS

SPECIFIED BY BUTLER.

THIS DRAWING, INCLUDING THE INFORMATION HEREON, REMAINS THE PROPERTY OF BUTLER MPG. IT IS PROVIDED SOLELY FOR ERECTING THE BUILDING DESCRIBED IN THE APPLICABLE PURCHASE ORDER AND MAY BE REPRODUCED ONLY FOR THAT PURPOSE. IT SHALL NOT BE MODIFIED, REPRODUCED OR USED FOR ANY OTHER PURPOSE WITHOUT PRIOR WRITTEN APPROVAL OF BUTLER MFG. THE GENERAL CONTRACTOR AND/OR ERECTOR IS SOLELY RESPONSIBLE FOR ACCURATE

GOOD QUALITY WORKMANSHIP IN ERECTING THIS BUILDING IN ACCORDANCE WITH THIS DRAWING, DETAILS REFERENCED IN THIS DRAWING, ALL APPLICABLE BUTLER MFG. ERECTION GUIDES, AND INDUSTRY STANDARDS PERTAINING TO PROPER ERECTION, INCLUDING THE CORRECT USE OF TEMPORARY BRACING.

BULLERS. The Sheridan Corporation DATE incation. Kittery, Maine. PROJECT: Good To Go Prelim 042921 BUILDER'S FOR DRAWWG-SCALE: NTS 19:2004 PRELIMINARY SPAANING

BUTLER MANUFACTURING

1540 GENESSEE ST. KANSAS CITY, MO 64102.

Single Slope Phase 1-Covering at F (BUTLER) Butter Manufacturing VPEVENSION ADVINCT 4.6

a division of Bluefoope Buildings North America, Inc.

VPC FLERWISE MINERARISES PRELIMINARY BRAWING

1. PRE-DRILLING 1/8 DIAMETER HOLES FOR STRUCTURAL FASTENERS

MAY BE REQUIRED FOR HEAVY GAGE NESTED ZEE'S AND/OR FASTENERS

2. STEEL PANELS ARE AN INTEGRAL PART OF THE STRUCTURAL SYSTEM.

3. DUE TO MANUFACTURING LIMITATIONS SHORT PANELS MAY REQUIRE

4. SEE JOB DETAILS FOR COVERING AND TRIM FASTENER SPECIFICATION.

FIELD CUTTING, SEE THE COVERING SCHEDULE FOR CUT LENGTHS.

REMOVAL OR ALTERATION WITHOUT PRIOR AUTHORIZATION IS PROHIBITED.

11/5/2011

В

TRAFFIC IMPACT STUDY PROPOSED FOOD MANUFACTURING FACILITY KITTERY, MAINE

July 22, 2021

Prepared For:

Altus Engineering, Inc. 133 Court Street Portsmouth, NH 03801

Prepared by:





INTRODUCTION

The purpose of this report is to summarize a traffic impact study performed by James W. Sewall Company (Sewall) for a proposed specialty food manufacturing facility, Good to Go, to be located off Route 1 in Kittery, Maine. The site location, on the easterly side of Route 1 is located is between Landmark Hill Lane and Parson's Lane, as shown on the map in Figure 1. The facility will be 20,000 square feet (S.F.) in size and will employ 30 persons. Access to the site will be provided by a single full-movement access drive to Route 1.

This report details the traffic analysis which determines the expected number of trips to be generated by the manufacturing facility and any off-site impacts on level of service or safety for the local Town of Kittery approval process.

It is understood that construction is expected to begin in fall of 2021 with completion and occupancy planned for summer 2022. Hence, 2022 was selected as the study year for traffic analysis puposes.

TRIP GENERATION ANALYSIS

The number of trips to be generated by the proposed manufacturing facility was estimated utilizing the latest Institute of Transportation Engineers (ITE) "Trip Generation, 10th edition". Land use code (LUC) 140 – Manufacturing was utilized on the basis of both 20,000 S.F. and 30 employees. The results are summarized below:

	ITE TRIP GENERATION				
<u>Time Period</u>	<u>S.F.</u>	<u>Employees</u>	<u>Average</u>		
Weekday	80	74	78		
AM Peak Hour – Adjacent Street	13	11	12		
Entering	10	8	9		
Exiting	3	3	3		
AM Peak Hour – Generator	16	13	15		
Entering	12	11	12		
Exiting	4	2	3		
PM Peak Hour – Adjacent Street	14	10	12		
Entering	4	4	4		
Exiting	10	6	8		
PM Peak Hour – Generator	16	14	15		
Entering	7	6	6		
Exiting	9	8	9		

The results were similar on both the square footage and employee bases so they were averaged together to best estimate trips. These results show that the proposed manufacturing facility is expected to generate 78 one-way trips (39 round-trips) on a daily basis. Twelve one-way trips are projected for the AM and PM peak hours of the adjacent street system. Fifteen one-way trips will be generated during the peak hours of the facility. This level of traffic would not be expected to have a significant impact off-site on traffic operations beyond the site drives.

However, to assess level of service to meet the requirements of the Kittery ordinances, traffic analysis was conducted for the site drive intersection to demonstrate level of service.

TRAFFIC VOLUMES

Turning movement/classification counts were conducted by Sewall during the weekday AM (7:00 – 9:00) and PM peak hour periods (3:00- 6:00) on June 3, 2021 at the intersection of Route 1 and Landmark Hill Lane to determine existing volumes and traffic patterns. The AM peak hour occurred from 8:00 to 9:00 while the PM peak hour occurred from 3:45 – 4:45. The counts were factored to 30th highest hour conditions using MaineDOT group mean factors. These volumes typically occur under peak summer conditions in July and August in Maine. The results are shown in Figure 2. The PM peak hour volumes are 40 % higher than the AM peak hour volumes. Given this and the similar site trip generation during both peak hours, the PM peak hour was selected as the analysis period, when the additional trips are expected to have the greatest impact.

Existing average annual daily traffic (AADT) data for the area was obtained from "Traffic Volume Counts, 2019 and 2014 Annual Reports", published by MaineDOT. This data is summarized in the following table:

	Average Annual Daily Traffic			fic
<u>Location Description</u>	<u>2010</u>	<u>2013</u>	<u>2016</u>	2019
Route 1, northeast of Cutts Road	11,340			10,550
Route 1, northeast of Haley Road	12,330	10,940	10,260	10,780
Route 1, southwest of Beechridge Road in York	11,450	9,370	9,490	9,440

As seen above, traffic volumes have generally been declining along this section of Route 1 over the period 2010 to 2019. As a result, a conservative ½ % annual traffic growth rate was utilized to project the 2021 volumes to base 2022 conditions.

The Town of Kittery Planner was contacted to determine if there are any other approved (but unbuilt) developments, expected to significantly impact future Route 1 volumes in the area, which should be considered in the traffic analysis. The only other development project identified is the Homestead Subdivision project, which is located on Route 1 opposite Lewis Road. The trips to be generated by this development were obtained from the Traffic Impact study prepared by Maine Traffic Resources (now Sewall) and dated 9/7/2018. Those other development volumes expected to be passing by the site during the PM peak hour are shown in Figure 3. The resulting 2022 No Build volumes, allowing for 1/2 % annual traffic growth and the Homestead Subdivision to be fully occupied, are shown in Figure 4.

The trip assignments for the manufacturing facility were assigned based upon the travel patterns recorded during the counts. The resulting trip assignments are shown in Figure 5. Based upon the trip assignments the facility is expected to have a minimal impact on off-site traffic operations. Generally, a project won't have an impact on traffic operations unless it generates in excess of twenty-five (25) lane hour trips. Based upon the trip assignments, the manufacturing facility will generate just four (4) lane hour trips during the PM peak hour analysis period. Given these trip assignments the study area would be limited to the site drive intersection but it was extended southerly through the intersection of Landmark Hill Lane to evaluate impact on nearby intersections. Lastly, the projected Build 2022 volumes are shown in Figure 6.

CAPACITY ANALYSIS

Traffic operations are evaluated in terms of level of service (LOS). Level of service is a qualitative measure that describes operations by letter designation. The levels range from A - very little delay to F - extreme delays. Level of service "D" is generally considered acceptable in urban locations while LOS "E" is generally considered the capacity of a facility and the minimum tolerable level. The level of service for unsignalized intersections is based upon average control delay per vehicle for each minor, opposed movement, as defined in the following table excerpted from the 2010 "Highway Capacity Manual":

Unsignalized Intersection Level of Service

<u>LOS</u>	<u>Delay Range</u>
Α	< = 10.0 seconds
В	> 10.0 and <= 15.0
С	> 15.0 and <= 25.0
D	> 25.0 and <= 35.0
E	> 35.0 and <= 50.0
F	> 50.0

UNSIGNALIZED INTERSECTION ANALYSIS

The level of service (LOS) was determined for the unsignalized study area intersection for existing 2021 and projected 2022 conditions using Synchro 10 and SimTraffic. The results are provided in the appendix and are summarized in the following tables:

	Route 1 & Landmark Hill Lane			
	PM Peak Hour Level of Service			
	Existing	No Build	Build	
Approach/Movement	<u>2021</u>	<u>2022</u>	<u>2022</u>	
Westbound Landmark Hill Lane	A (6.5)	A (8.1)	A (9.3)	
Northbound Route 1	A (1.2)	A (1.2)	A (1.3)	
Southbound Route 1	A (0.3)	A (0.3)	A (0.4)	
Overall Intersection	A (0.8)	A (0.9)	A (1.0)	

As seen above, Landmark Hill Lane currently operates at a good LOS "A" during the PM peak hour with no significant delay. The same LOS is expected in 2022 allowing for ½ % annual traffic growth and the Homestead Subdivision project. Lastly under projected build volumes, with the Good to Go facility fully occupied, it will continue to operate at LOS "A" with no capacity concerns. The increase in delay from No Build to Build conditions is negligible at 0.10 second demonstrating the minimal impact of the project on traffic operations off-site.

	Route 1 & Site Drive PM Peak Hour Level of Service		
	Build		
Approach/Movement	<u>2022</u>		
Westbound Site Drive	A (6.5)		
Northbound Route 1	A (0.3)		
Southbound Route 1	A (0.8)		
Overall Intersection	A (0.6)		

As seen above, there are also no capacity concerns at the unsignalized site drive intersection, which will also function at a very good LOS "A" in 2022 under full Build volumes.

SAFETY ANAYSIS ACCIDENT REVIEW

The Maine Department of Transportation uses two criteria to determine high crash locations (HCLs). The first is the critical rate factor (CRF), which is a measure of the accident rate. A CRF greater than one indicates a location which has a higher than expected crash rate. The expected rate is calculated as a statewide average of similar facilities.

The second criterion, which must also be met, is based upon the number of accidents that occur at a particular location. Eight or more accidents must occur over the three-year study period for the location to be considered a high crash location.

The MaineDOT Map Viewer was reviewed for high crash locations in the vicinity of the site for the most recent 3-year period (2018 – 2020). There are no high crash locations along Route 1 from Cutts Road in Kittery northerly to the intersection of Beech Ridge Road and Southside Road in York. As a result, no additional accident review or evaluation is necessary.

DRIVEWAY SIGHT DISTANCE

One of the most important safety factors to consider for a project is sight distance from the access drives. This sight distance is measured ten feet back from the edge of travel way at a driver's eye height of 3.5 feet to an object height of 4.25 feet. Sewall recommends a minimum sight distance of 450 feet for the posted 45 mile per hour speed limit on this segment of Route 1. The Kittery ordinance also requires 450' of sight distance while MaineDOT Entrance Rules require a lesser 425'.

Sewall field checked the sight distances from the proposed drive location and found it exceeds 500' to the left (south) and was approximately 450' to the right (north). Altus Engineering prepared a sight distance analysis, shown on their Highway Access Plan provided in this study, which confirms that the sight distance to the right exceeds 450'. Hence, sight distance will be adequate to provide for safe access. It is important that no signage or landscaping be located in the driveway sight triangle which could obscure or limit the driveway sight distances in the future.

SUMMARY AND RECOMMENDATIONS

The proposed specialty food manufacturing facility is expected to generate between 12 and 15 one-way trips during peak hours. Based upon both trip generation results and the peak hour volumes, the weekday PM peak hour of the adjacent street was selected as the analysis period. Also based upon the trip assignments, the study area for capacity purposes was defined as extending from the site drive through the intersection of Landmark Hill Lane to evaluate off-site impact.

In terms of capacity, the unsignalized intersection of Landmark Hill Lane currently operates at a good level of service "A" during the weekday PM peak hour. Under projected Build volumes the LOS will remain at this level with no capacity concerns. The site drive is also expected to operate at LOS "A", again showing no capacity concerns.

In terms of safety, there are no high crash locations within an extended study area so no further accident review or evaluation is necessary. Sight distances from the proposed site drive exceed the recommended standard providing for safe access. It is important that no signage or landscaping be located in the sight triangle which could obstruct driveway sight distance in the future.

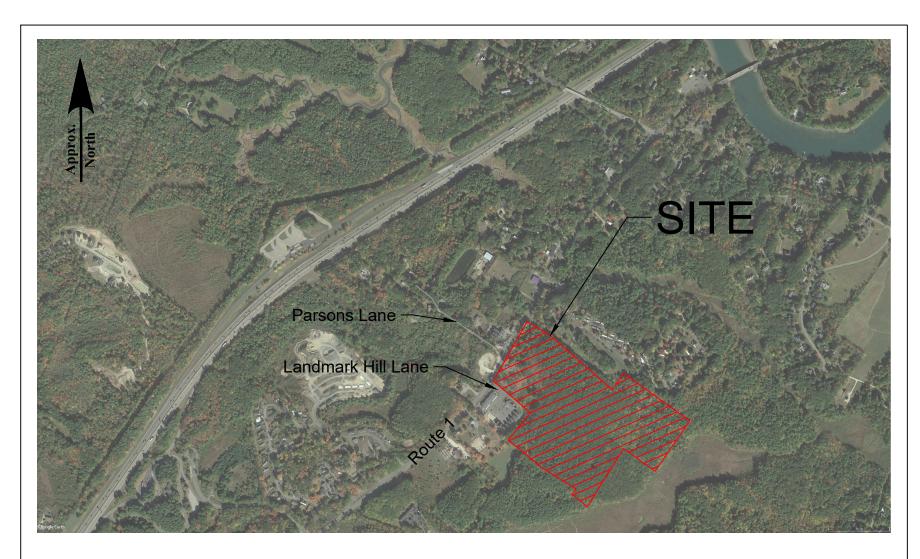


Figure 1
Site Location Map
Kittery Food Manufacturing
Kittery, Maine





-- AM Peak Hour (--) PM Peak Hour AM Peak Hour: 8:00 - 9:00 PM Peak Hour: 3:45 - 4:45

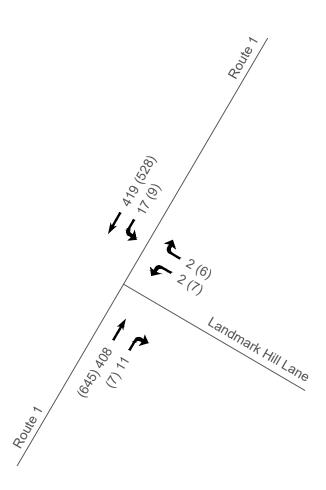


Figure 2

Existing 2021 Volumes
Kittery Food Manufacturing
Kittery, Maine







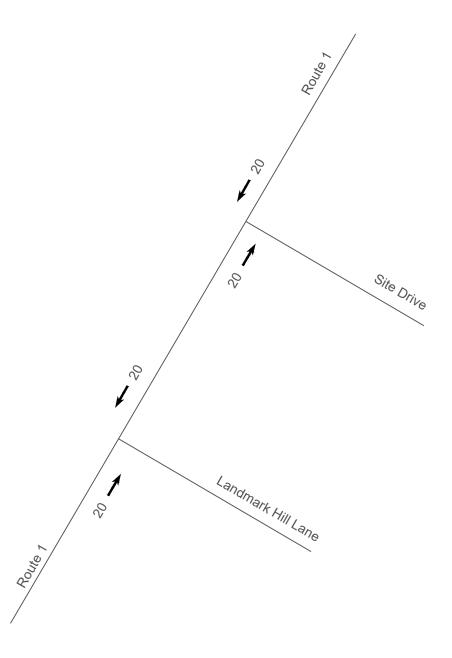


Figure 3

Other Developments PM Peak Hour
Kittery Food Manufacturing
Kittery, Maine







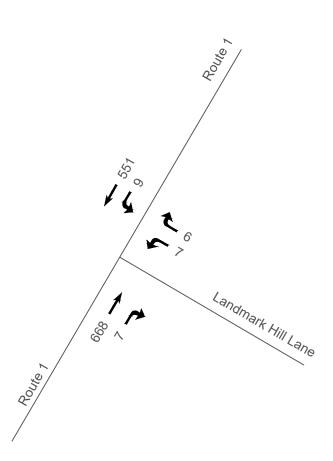


Figure 4

PM No Build 2022 Volumes
Kittery Food Manufacturing
Kittery, Maine







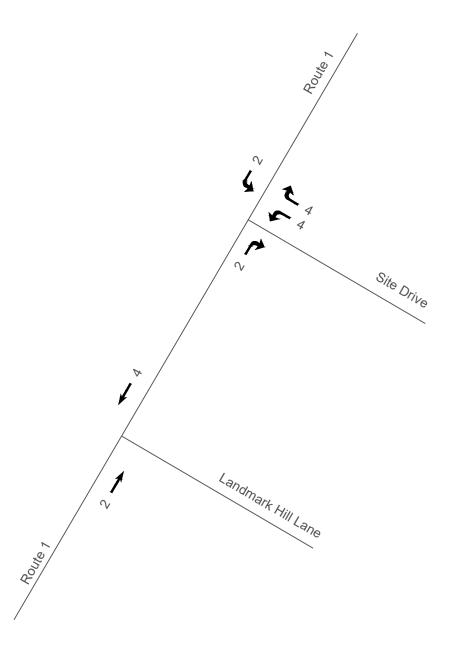


Figure 5

Trip Assignments PM Peak Hour
Kittery Food Manufacturing
Kittery, Maine







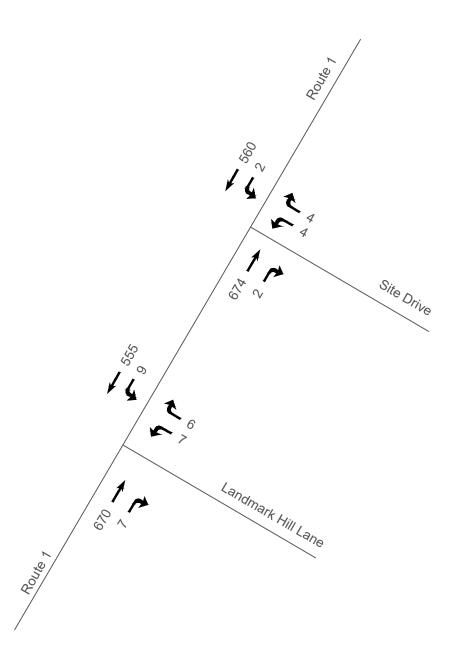


Figure 6

PM Build 2022 Volumes
Kittery Food Manufacturing
Kittery, Maine



APPENDIX

Turning Movement Counts

Capacity Analysis

Highway Access Plan

40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill Road File Name: KitteryLandmarkHill1AM2021

TOWN: Kittery, ME Site Code : 00000000 COUNTER: WD Start Date : 6/3/2021

WEATHER: Sun/clouds Page No : 1

Groups Printed- Passenger Vehicles - Light Trucks - Heavy Trucks

	Route 1						Lan	dmar	k Hill				Route	1			Lan	dmar	k Hill		
		So	uthbo	und			W	estbo	und			No	rthbo	und			Ea	stbo	und		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
07:00 AM	0	52	0	0	52	0	0	0	0	0	0	48	0	0	48	0	0	0	0	0	100
07:15 AM	0	55	0	0	55	0	0	0	1	1	0	50	0	0	50	0	0	0	0	0	106
07:30 AM	0	67	3	0	70	0	0	0	0	0	6	70	0	0	76	0	0	0	0	0	146
07:45 AM	0	75	4	0	79	0	0	0	1	1	8	59	0	0	67	0	0	0	0	0	147
Total	0	249	7	0	256	0	0	0	2	2	14	227	0	0	241	0	0	0	0	0	499
08:00 AM	0	70	4	0	74	1	0	0	0	1	5	82	0	0	87	0	0	0	0	0	162
08:15 AM	0	76	4	0	80	0	0	0	0	0	1	78	0	0	79	0	0	0	0	0	159
08:30 AM	0	96	3	0	99	1	0	1	0	2	2	85	0	0	87	0	0	0	0	0	188
08:45 AM	0	93	6	0	99	0	0	1	0	1	3	81	0	0	84	0	0	0	0	0	184
Total	0	335	17	0	352	2	0	2	0	4	11	326	0	0	337	0	0	0	0	0	693
Grand Total	0	584	24	0	608	2	0	2	2	6	25	553	0	0	578	0	0	0	0	0	1192
Apprch %	0	96.1	3.9	0		33.3	0	33.3	33.3		4.3	95.7	0	0		0	0	0	0		
Total %	0	49	2	0	51	0.2	0	0.2	0.2	0.5	2.1	46.4	0	0	48.5	0	0	0	0	0	
Passenger Vehicles																					
% Passenger Vehicles	0	95.2	100	0	95.4	100	0	100	100	100	96	91.5	0	0	91.7	0	0	0	0	0	93.6
Light Trucks																					
% Light Trucks	0	4.5	0	0_	4.3	0	0	0	0	0	0	6.5	0	0	6.2	0	0	0	0	0	5.2
Heavy Trucks	0	2	0	0	2	0	0	0	0	0	1	11	0	0	12	0	0	0	0	0	14
% Heavy Trucks																					

40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill Road File Name: KitteryLandmarkHill1AM2021

TOWN: Kittery, ME

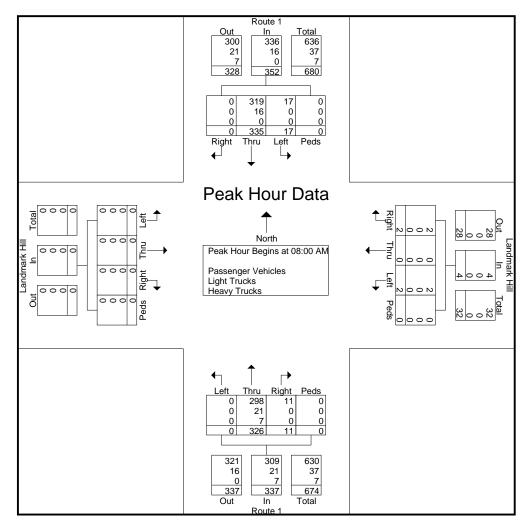
COUNTER: WD

Site Code : 00000000

Start Date : 6/3/2021

WEATHER: Sun/clouds Page No : 2

			Route					dmar					Route	-				dmar			
		<u>So</u>	<u>uthbo</u>	und			W	estbo	und			No	rthbo	und			Ea	astbo	und		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour A	nalysi	s From	07:00	AM to	08:45	AM - F	Peak 1	of 1													
Peak Hour fo	or Enti	re Inte	rsectio	n Begi	ns at 0	8:00 A	M														
08:00 AM	0	70	4	0	74	1	0	0	0	1	5	82	0	0	87	0	0	0	0	0	162
08:15 AM	0	76	4	0	80	0	0	0	0	0	1	78	0	0	79	0	0	0	0	0	159
08:30 AM	0	96	3	0	99	1	0	1	0	2	2	85	0	0	87	0	0	0	0	0	188
08:45 AM	0	93	6	0	99	0	0	1	0	1	3	81	0	0	84	0	0	0	0	0	184
Total Volume	0	335	17	0	352	2	0	2	0	4	11	326	0	0	337	0	0	0	0	0	693
% App. Total	0	95.2	4.8	0		50	0	50	0		3.3	96.7	0	0		0	0	0	0		
PHF	.000	.872	.708	.000	.889	.500	.000	.500	.000	.500	.550	.959	.000	.000	.968	.000	.000	.000	.000	.000	.922
Passenger Vehicles																					
% Passenger Vehicles	0	95.2	100	0	95.5	100	0	100	0	100	100	91.4	0	0	91.7	0	0	0	0	0	93.7
Light Trucks																					
% Light Trucks	0	4.8	0	0	4.5	0	0	0	0	0	0	6.4	0	0	6.2	0	0	0	0	0	5.3
Heavy Trucks	0	0	0	0	0	0	0	0	0	0	0	7	0	0	7	0	0	0	0	0	7
% Heavy Trucks																					1



40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill Road File Name: KitteryLandmarkHill1AM2021

TOWN: Kittery, ME

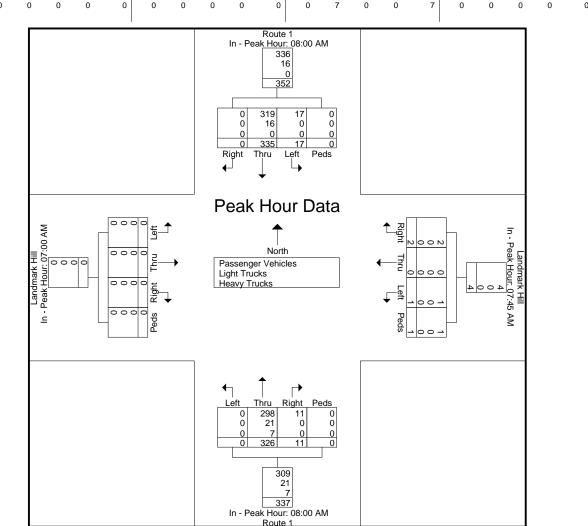
COUNTER: WD

Site Code : 00000000

Start Date : 6/3/2021

WEATHER: Sun/clouds Page No : 3

			Route	-				dmar estbo	k Hill			-	Route	-				dmar			
Start Time	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left		App. Total	Int. Tota
Peak Hour A									i eus	App. Total	IXIGIII	IIIIu	LCIT	i eus	App. I otal	Kigiit	IIIIu	LCIT	i eus	App. Total	Int. Tota
Peak Hour fo	,					/ (IVI - I	can i	OI I													
1 Cak Hour K	08:00 AM		<u> </u>	Jegins	at.	07:45 AM					08:00 AM					07:00 AM]
+0 mins.	08.00 AIV	70	4	0	74	07.45 AN	0	٥	1	1	5	82	0	0	87	07.00 AIV	0	0	0	0	
+15 mins.	0	76	4	0	80	1	0	0	0	1	1	78	0	0	79	Ö	0	0	0	0	
+30 mins.	0	96	3	0	99		0	0	0	Ö	2	85	0	0	87	0	0	0	0	0	
+45 mins.	0	93	6	0	99	1	0	1	0	2	3	81	0	0	84	0	0	0	0	0	
Total Volume	0	335	17	0	352	2	0	1	1	4	11	326	0	0	337	0	0	0	0	0	
% App. Total	o o	95.2	4.8	0	332	50	0	25	25	7	3.3	96.7	0	0	337	0	0	0	0	U	
PHF	.000	.872	.708	.000	.889	.500	.000	.250	.250	.500	.550	.959	.000	.000	.968	.000	.000	.000	.000	.000	-
Passenger Vehicles	.000	.012	.,, 00	.000	.000	.000	.000	.200	.200	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
3	0	95.	100	0	95.5	100	0	100	100	100	100	91.	0	0	91.7	0	0	0	0	0	
% Passenger Vehicles	0	2	100	U	95.5	100	U	100	100	100	100	4	U	U	91.7	0	U	U	U	U	
Light Trucks	0	16	0	0	16	0	0	0	0	0	0	21	0	0	21	0	0	0	0	0	
% Light Trucks	0	4.8	0	0	4.5	0	0	0	0	0	0	6.4	0	0	6.2	0	0	0	0	0	
Heavy Trucks	0	0	0	0	0	0	0	0	0	0	0	7	0	0	7	0	0	0	0	0	
% Heavy Trucks																					



40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill File Name: KitteryLandmarkHill1PM2021

TOWN: Kittery, ME Site Code : 00000000 COUNTER: WD Start Date : 6/3/2021

WEATHER: Sun/clouds Page No : 1

Groups Printed- Passenger Vehicles - Light Trucks - Heavy Trucks

	Route 1 Landmark Hill								1011101	_		Route	1	,							
		So	uthbo	und			W	estbo	und			No	rthbo	und			Ea	stbo	und		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
03:00 PM	0	103	0	0	103	0	0	0	0	0	7	126	0	0	133	0	0	0	0	0	236
03:15 PM	0	95	4	0	99	2	0	1	0	3	3	115	0	0	118	0	0	0	0	0	220
03:30 PM	0	94	4	0	98	3	0	2	0	5	5	134	0	0	139	0	0	0	0	0	242
03:45 PM	0	87	2	0	89	1	0	2	0	3	3	120	0	0	123	0	0	0	0	0	215
Total	0	379	10	0	389	6	0	5	0	11	18	495	0	0	513	0	0	0	0	0	913
	1					ı					1					ı					I.
04:00 PM	0	103	0	0	103	4	0	2	0	6	2	116	0	0	118	0	0	0	0	0	227
04:15 PM	0	102	3	0	105	0	0	2	1	3	0	145	0	0	145	0	0	0	0	0	253
04:30 PM	0	130	4	0	134	1	0	1	0	2	2	135	0	0	137	0	0	0	0	0	273
04:45 PM	0	96	1	0	97	3	0	0	0	3	0	110	0	0	110	0	0	0	0	0	210
Total	0	431	8	0	439	8	0	5	1	14	4	506	0	0	510	0	0	0	0	0	963
			_	_			_	_	_	_			_	_			_	_	_	_	
05:00 PM	0	85	3	0	88	3	0	0	0	3	1	101	0	0	102	0	0	0	0	0	193
05:15 PM	0	106	0	0	106	1	0	0	0	1	3	105	0	0	108	0	0	0	0	0	215
05:30 PM	0	70	2	0	72	0	0	0	0	0	3	102	0	0	105	0	0	0	0	0	177
05:45 PM	0	81	0	0	81	2	0	0	0	2	3	121	0	0	124	0	0	0	0	0	207
Total	0	342	5	0	347	6	0	0	0	6	10	429	0	0	439	0	0	0	0	0	792
				_			_						_	_			_	_	_	_	
Grand Total	0	1152	23	0	1175	20	0	10	1	31	32	1430	0	0	1462	0	0	0	0	0	2668
Apprch %	0	98	2	0		64.5	0	32.3	3.2		2.2	97.8	0	0		0	0	0	0		
Total %	0	43.2	0.9	0	44	0.7	0	0.4	0	1.2	1.2	53.6	0	0	54.8	0	0	0	0	0	
Passenger Vehicles	_	1135										1397									
% Passenger Vehicles	0	98.5	100	0	98.6	100	0	100	100	100	93.8	97.7	0	0	97.6	0	0	0	0	0	98.1
Light Trucks	_		_	_			_	_	_	_		_	_	_			_	_	_	_	
% Light Trucks	0	1_	0	0	1	0	0	0	0	0	6.2	2	0	0	2.1	0	0	0	0	0	1.6
Heavy Trucks	0	5	0	0	5	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	9
% Heavy Trucks																					

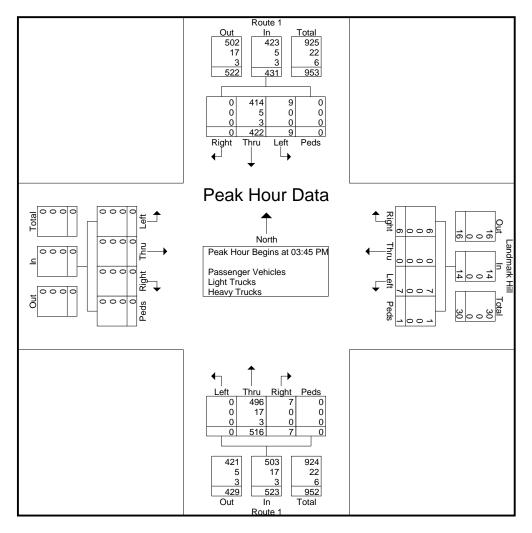
40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill File Name: KitteryLandmarkHill1PM2021

TOWN: Kittery, ME Site Code : 00000000 COUNTER: WD Start Date : 6/3/2021

WEATHER: Sun/clouds Page No : 2

			Route					dmar					Route								
		So	uthbo	und			We	estbo	und			No	rthbo	und			Ea	astbo	und		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour A	nalysi	s From	n 03:00	PM to	05:45	PM - F	Peak 1	of 1													
Peak Hour fo	or Enti	re Inte	rsectio	n Beg	ins at 0	3:45 P	M														
03:45 PM	0	87	2	0	89	1	0	2	0	3	3	120	0	0	123	0	0	0	0	0	215
04:00 PM	0	103	0	0	103	4	0	2	0	6	2	116	0	0	118	0	0	0	0	0	227
04:15 PM	0	102	3	0	105	0	0	2	1	3	0	145	0	0	145	0	0	0	0	0	253
04:30 PM	0	130	4	0	134	1	0	1	0	2	2	135	0	0	137	0	0	0	0	0	273
Total Volume	0	422	9	0	431	6	0	7	1	14	7	516	0	0	523	0	0	0	0	0	968
% App. Total	0	97.9	2.1	0		42.9	0	50	7.1		1.3	98.7	0	0		0	0	0	0		
PHF	.000	.812	.563	.000	.804	.375	.000	.875	.250	.583	.583	.890	.000	.000	.902	.000	.000	.000	.000	.000	.886
Passenger Vehicles																					
% Passenger Vehicles	0	98.1	100	0	98.1	100	0	100	100	100	100	96.1	0	0	96.2	0	0	0	0	0	97.1
Light Trucks																					
% Light Trucks	0	1.2	0	0	1.2	0	0	0	0	0	0	3.3	0	0	3.3	0	0	0	0	0	2.3
Heavy Trucks	0	3	0	0	3	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	6
% Heavy Trucks																					1



40 Forest Falls Drive Yarmouth, ME 04096

TITLE: Route 1 and Landmark Hill File Name: KitteryLandmarkHill1PM2021

TOWN: Kittery, ME

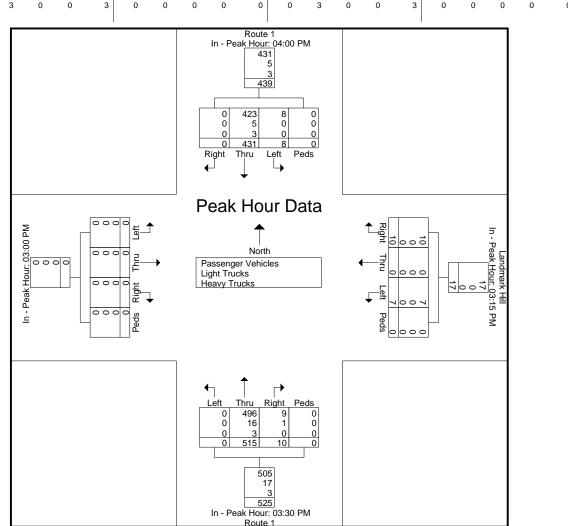
COUNTER: WD

Site Code : 00000000

Start Date : 6/3/2021

WEATHER: Sun/clouds Page No : 3

		_	Route	-				dmar					Route	-							
		So	uthbo	und			W	estbo	und			No	rthbo	und			Ea	astbo	und		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Tot
Peak Hour A	nalysi	s From	n 03:00	PM to	05:45	PM - F	Peak 1	of 1													
Peak Hour fo	or Eac	h Appr	oach E	Begins	at:																
	04:00 PM	1				03:15 PM					03:30 PM	1				03:00 PM	1				
+0 mins.	0	103	0	0	103	2	0	1	0	3	5	134	0	0	139	0	0	0	0	0	
+15 mins.	0	102	3	0	105	3	0	2	0	5	3	120	0	0	123	0	0	0	0	0	
+30 mins.	0	130	4	0	134	1	0	2	0	3	2	116	0	0	118	0	0	0	0	0	
+45 mins.	0	96	1_	0	97	4	0	2	0	6	0	145	0	0	145	0	0	0	0	0	
Total Volume	0	431	8	0	439	10	0	7	0	17	10	515	0	0	525	0	0	0	0	0	
% App. Total	0	98.2	1.8	0		58.8	0	41.2	0		1.9	98.1	0	0		0	0	0	0		
PHF	.000	.829	.500	.000	.819	.625	.000	.875	.000	.708	.500	.888	.000	.000	.905	.000	.000	.000	.000	.000	
Passenger Vehicles																					
% Passenger Vehicles	0	98. 1	100	0	98.2	100	0	100	0	100	90	96. 3	0	0	96.2	0	0	0	0	0	
Light Trucks	0	5	0	0	5	0	0	0	0	0	1	16	0	0	17	0	0	0	0	0	
% Light Trucks	0	1.2	0	0	1.1	0	0	0	0	0	10	3.1	0	0	3.2	0	0	0	0	0	
Heavy Trucks	0	3	0	0	3	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	
% Heavy Trucks																					



Summary of All Intervals

Run Number	1	2	3	4	5	Avg	
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	
End Time	8:00	8:00	8:00	8:00	8:00	8:00	
Total Time (min)	70	70	70	70	70	70	
Time Recorded (min)	60	60	60	60	60	60	
# of Intervals	2	2	2	2	2	2	
# of Recorded Intervals	1	1	1	1	1	1	
Vehs Entered	1198	1172	1164	1155	1258	1190	
Vehs Exited	1193	1166	1157	1145	1259	1185	
Starting Vehs	14	9	11	11	14	12	
Ending Vehs	19	15	18	21	13	17	
Travel Distance (mi)	637	623	619	609	673	632	
Travel Time (hr)	15.3	15.0	14.8	14.7	16.3	15.2	
Total Delay (hr)	1.0	0.9	0.9	0.9	1.0	0.9	
Total Stops	19	11	17	16	22	17	
Fuel Used (gal)	17.0	16.4	16.5	16.2	17.8	16.8	

Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10

Volumes adjusted by Growth Factors.

No data recorded this interval.

Interval #1 Information Recording

Start Time	7:00							
End Time	8:00							
Total Time (min)	60							
Volumes adjusted by Growth Factors.								

Run Number	1	2	3	4	5	Avg	
Vehs Entered	1198	1172	1164	1155	1258	1190	
Vehs Exited	1193	1166	1157	1145	1259	1185	
Starting Vehs	14	9	11	11	14	12	
Ending Vehs	19	15	18	21	13	17	
Travel Distance (mi)	637	623	619	609	673	632	
Travel Time (hr)	15.3	15.0	14.8	14.7	16.3	15.2	
Total Delay (hr)	1.0	0.9	0.9	0.9	1.0	0.9	
Total Stops	19	11	17	16	22	17	
Fuel Used (gal)	17.0	16.4	16.5	16.2	17.8	16.8	

3: Route 1 & Landmark Hill Lane Performance by lane

Lane	WB	NB	SB	All	
Movements Served	LR	TR	LT		
Denied Del/Veh (s)				0.3	
Total Del/Veh (s)	6.5	1.2	0.3	8.0	

Intersection: 3: Route 1 & Landmark Hill Lane

WB	NB	SB
LR	TR	LT
35	6	44
9	0	5
33	4	24
546	1435	172
	LR 35 9 33	LR TR 35 6 9 0 33 4

Summary of All Intervals

Run Number	1	2	3	4	5	Avg	
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	
End Time	8:00	8:00	8:00	8:00	8:00	8:00	
Total Time (min)	70	70	70	70	70	70	
Time Recorded (min)	60	60	60	60	60	60	
# of Intervals	2	2	2	2	2	2	
# of Recorded Intervals	1	1	1	1	1	1	
Vehs Entered	1341	1317	1240	1209	1203	1263	
Vehs Exited	1347	1302	1242	1197	1197	1257	
Starting Vehs	22	8	20	9	11	14	
Ending Vehs	16	23	18	21	17	19	
Travel Distance (mi)	708	688	651	630	631	662	
Travel Time (hr)	17.1	16.8	15.6	15.2	15.1	16.0	
Total Delay (hr)	1.1	1.2	1.0	1.0	0.9	1.0	
Total Stops	18	16	20	18	18	18	
Fuel Used (gal)	18.7	18.4	17.5	16.7	16.8	17.6	

Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Values a sellusted by Ossuth F	1

Volumes adjusted by Growth Factors.

No data recorded this interval.

Interval #1 Information Recording

Start Time	7:00				
End Time	8:00				
Total Time (min)	60				
Volumes adjusted by Growth Factors.					

Run Number	1	2	3	4	5	Avg	
Vehs Entered	1341	1317	1240	1209	1203	1263	
Vehs Exited	1347	1302	1242	1197	1197	1257	
Starting Vehs	22	8	20	9	11	14	
Ending Vehs	16	23	18	21	17	19	
Travel Distance (mi)	708	688	651	630	631	662	
Travel Time (hr)	17.1	16.8	15.6	15.2	15.1	16.0	
Total Delay (hr)	1.1	1.2	1.0	1.0	0.9	1.0	
Total Stops	18	16	20	18	18	18	
Fuel Used (gal)	18.7	18.4	17.5	16.7	16.8	17.6	

3: Route 1 & Landmark Hill Lane Performance by lane

Lane	WB	NB	SB	All	
Movements Served	LR	TR	LT		
Denied Del/Veh (s)				0.3	
Total Del/Veh (s)	8.1	1.2	0.3	0.9	

Intersection: 3: Route 1 & Landmark Hill Lane

Movement	WB	NB	SB
Directions Served	LR	TR	LT
Maximum Queue (ft)	40	11	59
Average Queue (ft)	10	0	5
95th Queue (ft)	34	8	28
Link Distance (ft)	546	1435	171
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Summary of All Intervals

Run Number	1	2	3	4	5	Avg	
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	
End Time	8:00	8:00	8:00	8:00	8:00	8:00	
Total Time (min)	70	70	70	70	70	70	
Time Recorded (min)	60	60	60	60	60	60	
# of Intervals	2	2	2	2	2	2	
# of Recorded Intervals	1	1	1	1	1	1	
Vehs Entered	1185	1273	1232	1245	1291	1246	
Vehs Exited	1186	1276	1229	1240	1283	1242	
Starting Vehs	15	17	14	12	10	13	
Ending Vehs	14	14	17	17	18	15	
Travel Distance (mi)	632	680	659	664	689	665	
Travel Time (hr)	15.2	16.6	15.9	16.1	16.7	16.1	
Total Delay (hr)	1.0	1.2	1.0	1.1	1.2	1.1	
Total Stops	30	36	25	27	28	29	
Fuel Used (gal)	17.0	18.3	17.5	17.8	18.4	17.8	

Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10

Volumes adjusted by Growth Factors.

No data recorded this interval.

Interval #1 Information Recording

Start Time	7:00				
End Time	8:00				
Total Time (min)	60				
Volumes adjusted by Growth Factors.					

Run Number	1	2	3	4	5	Avg	
Vehs Entered	1185	1273	1232	1245	1291	1246	
Vehs Exited	1186	1276	1229	1240	1283	1242	
Starting Vehs	15	17	14	12	10	13	
Ending Vehs	14	14	17	17	18	15	
Travel Distance (mi)	632	680	659	664	689	665	
Travel Time (hr)	15.2	16.6	15.9	16.1	16.7	16.1	
Total Delay (hr)	1.0	1.2	1.0	1.1	1.2	1.1	
Total Stops	30	36	25	27	28	29	
Fuel Used (gal)	17.0	18.3	17.5	17.8	18.4	17.8	

3: Route 1 & Landmark Hill Lane Performance by lane

Lane	WB	NB	SB	All
Movements Served	LR	TR	LT	
Denied Del/Veh (s)				0.3
Total Del/Veh (s)	9.3	1.3	0.4	1.0

4: Route 1 & Site Drive Performance by lane

Lane	WB	NB	SB	All
Movements Served	LR	TR	LT	
Denied Del/Veh (s)				0.2
Total Del/Veh (s)	6.5	0.3	8.0	0.6

Total Network Performance

Denied Del/Veh (s) 0.5
Total Del/Veh (s) 2.7

Intersection: 3: Route 1 & Landmark Hill Lane

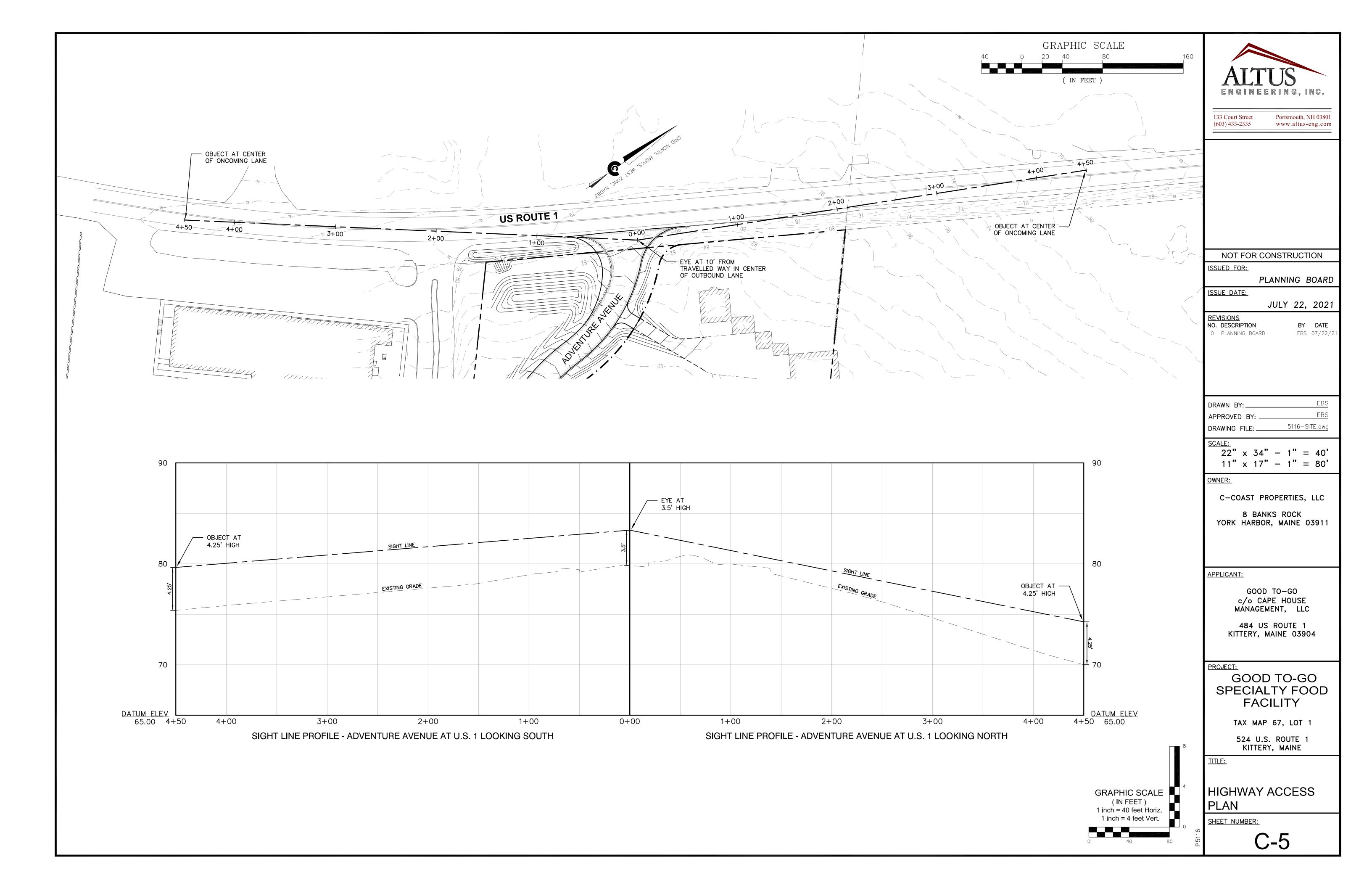
Movement	WB	SB
Directions Served	LR	LT
Maximum Queue (ft)	35	74
Average Queue (ft)	13	6
95th Queue (ft)	37	34
Link Distance (ft)	546	171
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 4: Route 1 & Site Drive

Movement	WB	SB
Directions Served	LR	LT
Maximum Queue (ft)	31	25
Average Queue (ft)	8	1
95th Queue (ft)	29	11
Link Distance (ft)	416	1133
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Network Summary

Network wide Queuing Penalty: 0



DRAINAGE ANALYSIS

FOR

Site Development for Good To-Go

524 U.S. Route 1 Kittery, Maine

Tax Map 67, Lot 1

July 22, 2021

Prepared For:

Good To-Go c/o Cape House Management, LLC

484 U.S. Route 1 Kittery, Maine 03904

Prepared By:

ALTUS ENGINEERING, INC.

133 Court Street Portsmouth, NH 03801 Phone: (603) 433-2335



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Pre-Development Watershed Plan Post-Development Watershed Plan



Section 1

Narrative



PROJECT DESCRIPTION

Good To-Go, a Kittery-based specialty food company focused on outdoor activities, is proposing to develop a commercial lot located at 524 U.S. Route 1 in Kittery, Maine. The 23.89 acre property is identified as Assessor's Map 47, Lot 201 and is located in the Mixed Use (MU) district. The site is primarily wooded and undeveloped save for an existing residence with several outbuildings, a woods road and several side trails.

The proposed project will construct a new public road to access a commercial specialty food facility with a 20,000 sf building serviced by municipal water and sewer, a paved parking area and new stormwater treatment measures. These measures will include two grassed underdrained soil filters. Pretreatment will be provided by catch basins with deep sumps and grease hoods.

The stormwater management system proposed for the site will reduce peak flows and treat runoff from 100% of the site's impervious areas and 75.2% of the linear access roadway prior to leaving the site.

Site Soils

A Class A High Intensity Soils Survey (HISS) was conducted on the site which indicated that the soils are generally poor with low rates of infiltration, relatively high water tables and numerous areas of shallow ledge. These soils fall into the following primary classifications:

BrB - Brayton, Hydrologic Soil Group (HSG) D

DxB – Dixfield, HSG D

LTB – Lyman Tunbridge Complex, HSG C

LTC – Lyman Tunbridge Complex, HSG C

LTD – Lyman Tunbridge Complex, HSG C

LTE – Lyman Tunbridge Complex, HSG C

NiB – Nicholville, HSG D

ScB – Scantic, HSG D

WhB – Whately, HSG D

WmB – Waumbek, HSG D

WsB – Westbury, HSG D

For the purposes of this analysis, offsite watershed areas beyond the limit of the HISS were classified using the USDA's NRCS Web Soil Survey.

Pre-Development (Existing Conditions)

The Pre-Development Watershed Plan (Sheet WS-1) reflects the current conditions of the site which include the existing building and parking areas. The current site can be divided into two (2) subcatchments which discharge to the west to a culvert under Route 1 at Point of Analysis (POA) #1 (HydroCAD Link 100L) and south to the property boundary at Point of Analysis #2 (HydroCAD Link 200L).

Post-Development (Proposed Conditions)

The proposed project will construct a new building, drainage system and associated site improvements.

As shown on the attached Post-Development Watershed Plan (Sheet WS-2), the site was divided into fifteen (15) subcatchment areas in the post-development conditions. The same points of analysis that were used in the Pre-Development model (POA #'s 1 and 2) were used for comparison of the Pre- and Post-development conditions.

CALCULATION METHODS

The drainage study was completed using the USDA SCS TR-20 Method within the HydroCAD Stormwater Modeling System. Reservoir routing was performed with the Dynamic Storage Indication method with automated calculation of tailwater conditions. A Type III 24-hour rainfall distribution was utilized in analyzing the data for the 2, 10 and 25 year - 24-hour storm events using rainfall data provided by Maine DEP. Infiltration rates through biofilter media were set at 2.41 in/hr with a phase-in depth of 0.01'.

Disclaimer

Altus Engineering, Inc. notes that stormwater modeling is limited in its capacity to precisely predict peak rates of runoff and flood elevations. Results should not be considered to represent actual storm events due to the number of variables and assumptions involved in the modeling effort. Surface roughness coefficients (n), entrance loss coefficients (ke), velocity factors (kv) and times of concentration (Tc) are based on subjective field observations and engineering judgment using available data. For design purposes, curve numbers (Cn) describe the average conditions. However, curve numbers will vary from storm to storm depending on the antecedent runoff conditions (ARC) including saturation and frozen ground. Also, higher water elevations than predicted by modeling could occur if drainage channels, closed drain systems or culverts are not maintained and/or become blocked by debris before and/or during a storm event as this will impact flow capacity of the structures. Structures should be re-evaluated if future changes occur within relevant drainage areas in order to assess any required design modifications.

Drainage Analysis

A complete summary of the drainage model is included in the appendix of this report. The following table compares pre- and post-development peak rates at the Point of Analysis identified on the plans for the 2, 10 and 25-year storm events:

Stormwater Modeling Summary
Peak Q (cfs) for Type III 24-Hour Storm Events

	2-Yr Storm	10-Yr Storm	25-Yr Storm
	(3.30 inch)	(4.90 inch)	(6.20 inch)
POA #1 (US 1 Culvert)			
Pre	2.74	5.55	6.75
Post	2.26	4.59	6.61
Change	-0.48	-0.96	-0.14
POA #2 (South Property Line)			
Pre	9.33	20.19	29.85
Post	9.24	19.31	29.79
Change	-0.09	-0.88	-0.06

As the above table demonstrates, the proposed peak rates of runoff will be decreased from the existing conditions for all analyzed storm events.

CONCLUSION

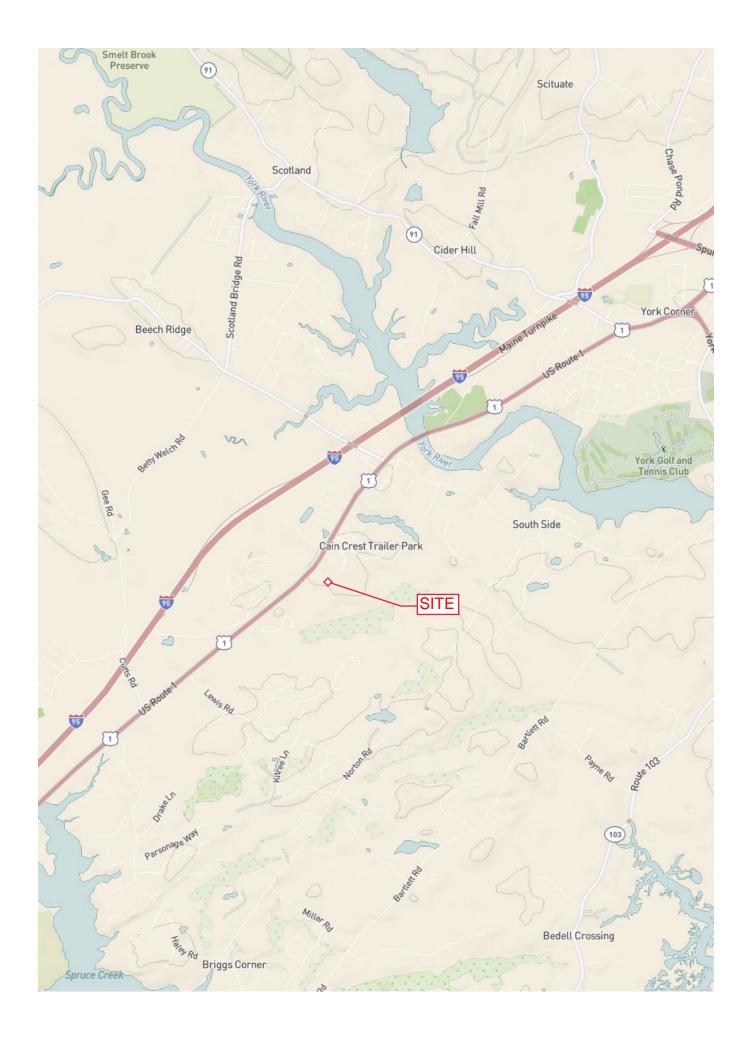
This proposed roadway and site development off U.S Route 1 in Kittery, ME will have minimal adverse effect on abutting properties and infrastructure as a result of stormwater runoff or siltation. Post-construction peak rates of runoff from the site will be lower than the existing conditions for all analyzed storm events. The new stormwater management system will also provide appropriate treatment to runoff from 100% of the proposed impervious surfaces from the site and 75.2% of the access road. Appropriate steps will be taken to properly mitigate erosion and sedimentation through the use of temporary and permanent Best Management Practices for sediment and erosion control, including deep sump catch basins with grease hoods and two grassed underdrained soil filters designed in accordance with the MDEP Stormwater Best Practices Manual.

Section 2

Aerial Photo and USGS Map





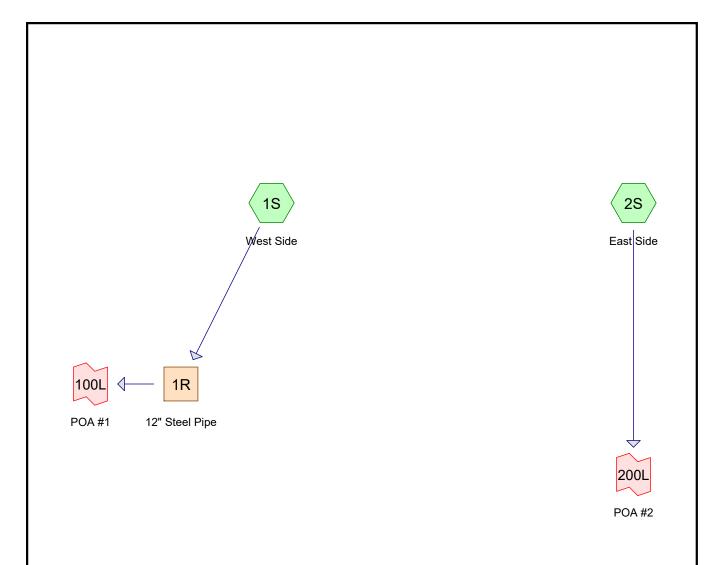


Section 3

Drainage Calculations

Pre-Development 2-Year, 24-Hour Summary 10-Year, 24-Hour Complete 25-Year, 24-Hour Summary





PRE-DEVELOPMENT









Routing Diagram for 5116-Pre-061721
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Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: West Side Runoff Area = 86,228 sf 2.71% Impervious Runoff Depth > 1.28"

Flow Length=611' Tc=7.7 min CN=77 Runoff=2.74 cfs 0.211 af

Subcatchment 2S: East Side Runoff Area=609,713 sf 2.66% Impervious Runoff Depth>1.09"

Flow Length=1,208' Tc=32.9 min CN=74 Runoff=9.33 cfs 1.276 af

Reach 1R: 12" Steel Pipe Avg. Flow Depth=0.45' Max Vel=8.00 fps Inflow=2.74 cfs 0.211 af

12.0" Round Pipe n=0.012 L=45.0' S=0.0291 '/' Capacity=6.59 cfs Outflow=2.74 cfs 0.211 af

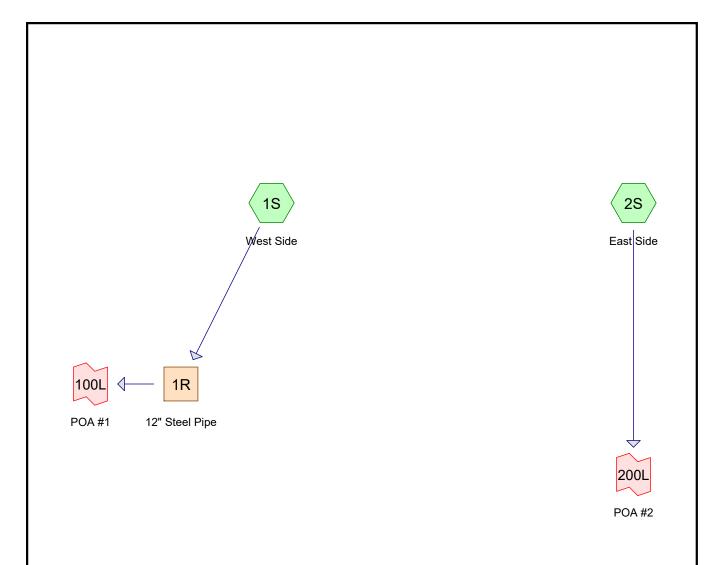
Link 100L: POA #1 Inflow=2.74 cfs 0.211 af

Primary=2.74 cfs 0.211 af

Link 200L: POA #2 Inflow=9.33 cfs 1.276 af

Primary=9.33 cfs 1.276 af

Total Runoff Area = 15.977 ac Runoff Volume = 1.488 af Average Runoff Depth = 1.12" 97.34% Pervious = 15.551 ac 2.66% Impervious = 0.426 ac



PRE-DEVELOPMENT









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Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: West Side Runoff Area = 86,228 sf 2.71% Impervious Runoff Depth > 2.54"

Flow Length=611' Tc=7.7 min CN=77 Runoff=5.55 cfs 0.418 af

Subcatchment 2S: East Side Runoff Area=609,713 sf 2.66% Impervious Runoff Depth>2.27"

Flow Length=1,208' Tc=32.9 min CN=74 Runoff=20.19 cfs 2.645 af

Reach 1R: 12" Steel Pipe Avg. Flow Depth=0.70' Max Vel=9.40 fps Inflow=5.55 cfs 0.418 af

12.0" Round Pipe n=0.012 L=45.0' S=0.0291 '/' Capacity=6.59 cfs Outflow=5.55 cfs 0.418 af

Link 100L: POA #1 Inflow=5.55 cfs 0.418 af

Primary=5.55 cfs 0.418 af

Link 200L: POA #2 Inflow=20.19 cfs 2.645 af

Primary=20.19 cfs 2.645 af

Total Runoff Area = 15.977 ac Runoff Volume = 3.063 af Average Runoff Depth = 2.30" 97.34% Pervious = 15.551 ac 2.66% Impervious = 0.426 ac

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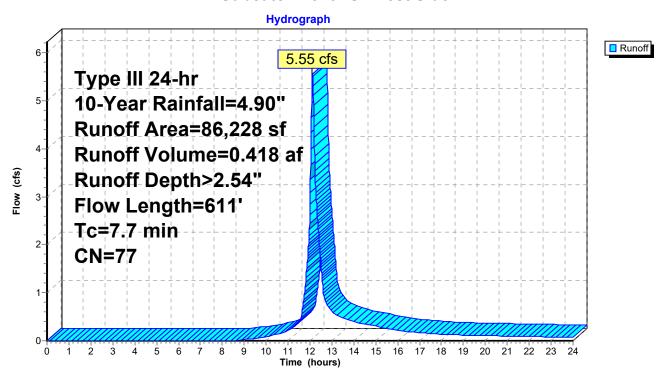
Summary for Subcatchment 1S: West Side

Runoff = 5.55 cfs @ 12.11 hrs, Volume= 0.418 af, Depth> 2.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Ar	ea (sf)	CN	Description				
*		1,015	98	Impervious Existing Pavement				
*		1,318	98	Impervious Existing Building				
		1,648		Gravel surfa				
		3,325		Gravel surfa	ace, HSG C			
		1,629		Dirt roads, I				
	2	27,302				ood, HSG D		
		2,700		Woods, Go				
		22,240				ood, HSG C		
		25,051		Woods, Go	od, HSG C			
		86,228		Weighted A	0			
	8	83,895		97.29% Pei				
		2,333		2.71% Impe	ervious Area	a		
_	_		01			D 1.00		
	ГС	Length	Slope			Description		
<u>(mi</u>		(feet)	(ft/ft)		(cfs)			
3	.9	54	0.0579	0.23		Sheet Flow,		
	_	400	0.0044	0.45		Grass: Short n= 0.150 P2= 3.30"		
1	.5	192	0.0941	2.15		Shallow Concentrated Flow,		
0	_	07	0.0226	2.05		Short Grass Pasture Kv= 7.0 fps		
U	.5	97	0.0336	2.95		Shallow Concentrated Flow,		
0	.3	80	0.0750	4.41		Unpaved Kv= 16.1 fps Shallow Concentrated Flow,		
U	.5	00	0.0730	4.41		Unpaved Kv= 16.1 fps		
0	.2	16	0.0060	1.57		Shallow Concentrated Flow,		
U		10	0.0000	1.07		Paved Kv= 20.3 fps		
1	.3	172	0.0214	2.19		Shallow Concentrated Flow,		
•	. •	· · -	3.0-1			Grassed Waterway Kv= 15.0 fps		
7	.7	611	Total			, 1		

Subcatchment 1S: West Side



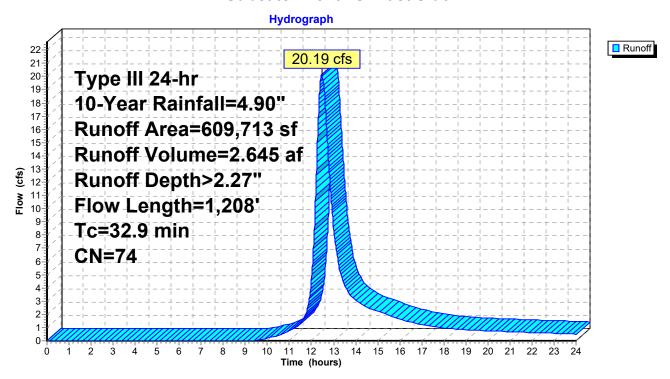
Summary for Subcatchment 2S: East Side

Runoff = 20.19 cfs @ 12.47 hrs, Volume= 2.645 af, Depth> 2.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Α	rea (sf)	CN [Description						
*		11,834	98 I	98 Impervious Existing Pavement						
*		4,369		mpervious						
		1,161		Dirt roads, I		ŭ				
		4,839	87 [Dirt roads, I	HSG C					
		51,144	80 >	>75% Gras	s cover, Go	ood, HSG D				
	1	93,586	77 \	Noods, Go	od, HSG D					
		22,432	74 >	>75% Gras	s cover, Go	ood, HSG C				
	3	20,348	70 \	Noods, Go	od, HSG C					
		09,713	74 \	Weighted A	verage					
	5	93,510	-	97.34% Per						
		16,203	2	2.66% Impe	ervious Area	a				
	_		01			B				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	8.8	83	0.1231	0.16		Sheet Flow,				
	4.4	404	0.0000	4 4 4		Woods: Light underbrush n= 0.400 P2= 3.30"				
	1.4	121	0.0826	1.44		Shallow Concentrated Flow,				
	7.1	301	0.0199	0.71		Woodland Kv= 5.0 fps				
	7.1	301	0.0199	0.71		Shallow Concentrated Flow, Woodland Kv= 5.0 fps				
	7.8	223	0.0090	0.47		Shallow Concentrated Flow,				
	7.0	223	0.0090	0.47		Woodland Kv= 5.0 fps				
	1.6	77	0.0250	0.79		Shallow Concentrated Flow,				
	1.0	, ,	0.0200	0.73		Woodland Kv= 5.0 fps				
	1.1	98	0.0816	1.43		Shallow Concentrated Flow,				
	•••	00	3.0010	1.10		Woodland Kv= 5.0 fps				
	5.1	305	0.0393	0.99		Shallow Concentrated Flow,				
			3.22 30	2.30		Woodland Kv= 5.0 fps				
	32.9	1,208	Total			·				

Subcatchment 2S: East Side



Summary for Reach 1R: 12" Steel Pipe

Inflow Area = 1.980 ac, 2.71% Impervious, Inflow Depth > 2.54" for 10-Year event

Inflow = 5.55 cfs @ 12.11 hrs, Volume= 0.418 af

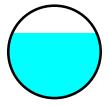
Outflow = 5.55 cfs @ 12.11 hrs, Volume= 0.418 af, Atten= 0%, Lag= 0.1 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

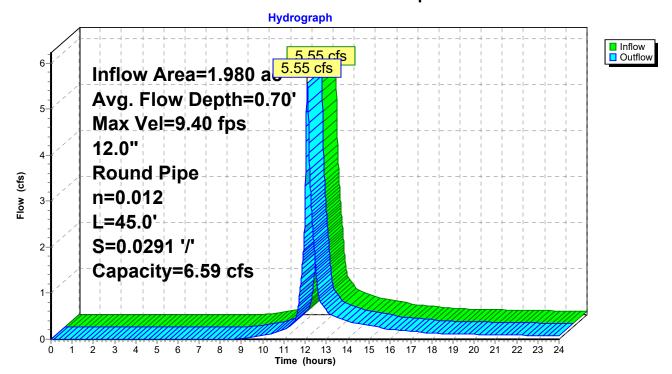
Max. Velocity= 9.40 fps, Min. Travel Time= 0.1 min Avg. Velocity = 3.68 fps, Avg. Travel Time= 0.2 min

Peak Storage= 27 cf @ 12.11 hrs Average Depth at Peak Storage= 0.70' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 6.59 cfs

12.0" Round Pipe n= 0.012 Length= 45.0' Slope= 0.0291 '/' Inlet Invert= 76.08', Outlet Invert= 74.77'



Reach 1R: 12" Steel Pipe



Summary for Link 100L: POA #1

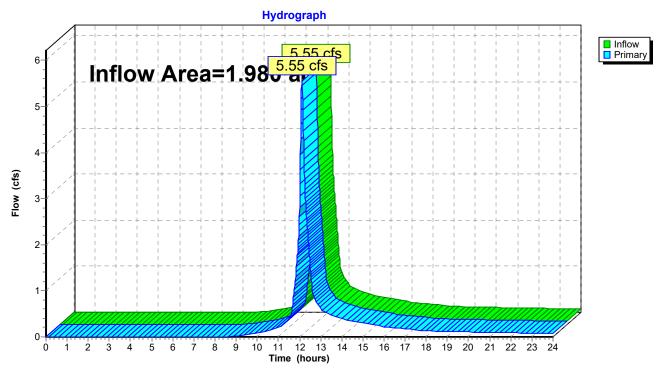
Inflow Area = 1.980 ac, 2.71% Impervious, Inflow Depth > 2.54" for 10-Year event

Inflow = 5.55 cfs @ 12.11 hrs, Volume= 0.418 af

Primary = 5.55 cfs @ 12.11 hrs, Volume= 0.418 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 100L: POA #1



Summary for Link 200L: POA #2

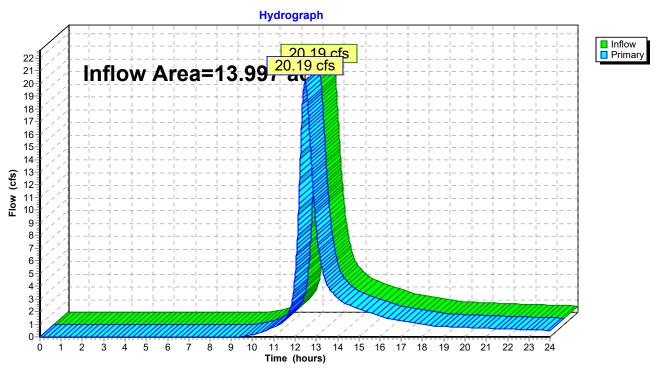
Inflow Area = 13.997 ac, 2.66% Impervious, Inflow Depth > 2.27" for 10-Year event

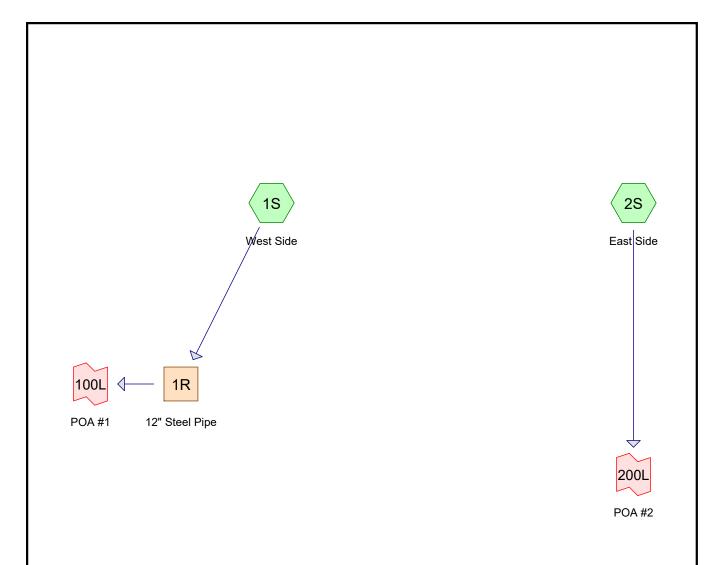
Inflow = 20.19 cfs @ 12.47 hrs, Volume= 2.645 af

Primary = 20.19 cfs @ 12.47 hrs, Volume= 2.645 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 200L: POA #2





PRE-DEVELOPMENT









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Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: West Side Runoff Area=86,228 sf 2.71% Impervious Runoff Depth>3.65"

Flow Length=611' Tc=7.7 min CN=77 Runoff=7.99 cfs 0.602 af

Subcatchment 2S: East Side Runoff Area=609,713 sf 2.66% Impervious Runoff Depth>3.33"

Flow Length=1,208' Tc=32.9 min CN=74 Runoff=29.85 cfs 3.885 af

Reach 1R: 12" Steel Pipe Avg. Flow Depth=1.00' Max Vel=9.55 fps Inflow=7.99 cfs 0.602 af

12.0" Round Pipe n=0.012 L=45.0' S=0.0291 '/' Capacity=6.59 cfs Outflow=6.75 cfs 0.602 af

Link 100L: POA #1 Inflow=6.75 cfs 0.602 af

Primary=6.75 cfs 0.602 af

Link 200L: POA #2 Inflow=29.85 cfs 3.885 af

Primary=29.85 cfs 3.885 af

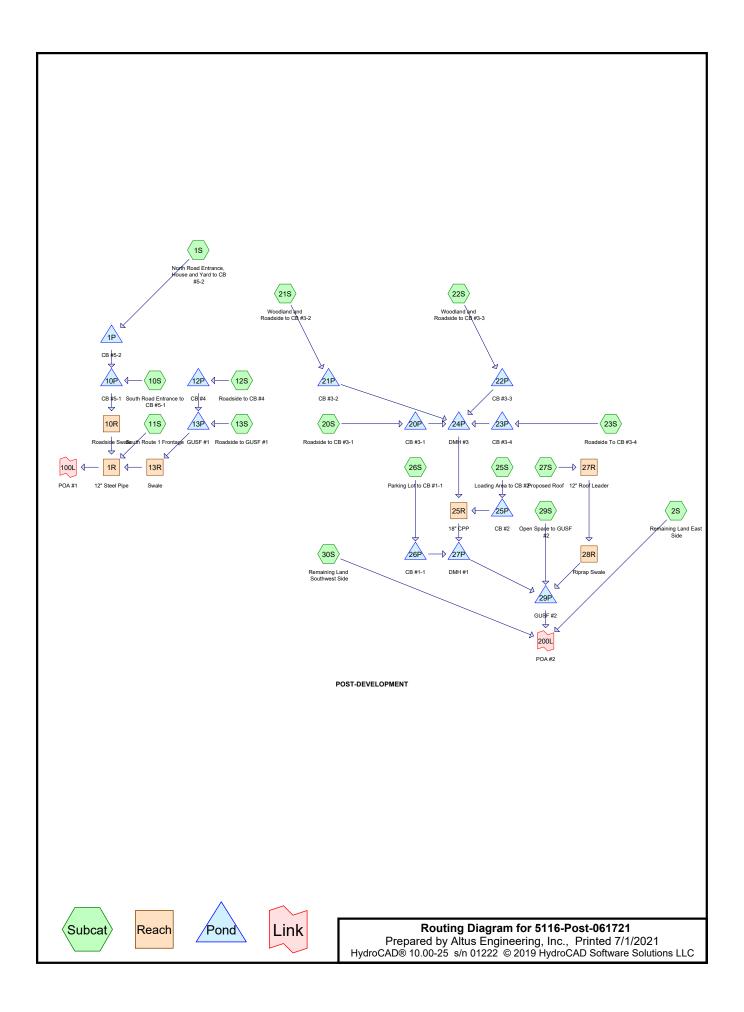
Total Runoff Area = 15.977 ac Runoff Volume = 4.487 af Average Runoff Depth = 3.37" 97.34% Pervious = 15.551 ac 2.66% Impervious = 0.426 ac

Section 4

Drainage Calculations

Post-Development 2-Year, 24-Hour Summary 10-Year, 24-Hour Complete 25-Year, 24-Hour Summary





Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: North Road Entrance, Runoff Area=51,236 sf 8.13% Impervious Runoff Depth=1.28" Flow Length=432' Tc=6.3 min CN=77 Runoff=1.71 cfs 0.126 af

Subcatchment 2S: Remaining Land East Runoff Area=279,061 sf 0.00% Impervious Runoff Depth=1.05" Flow Length=1,208' Tc=32.9 min CN=73 Runoff=4.01 cfs 0.559 af

Subcatchment 10S: South Road Entrance to Runoff Area=3,377 sf 82.44% Impervious Runoff Depth=2.74" Flow Length=139' Tc=6.0 min CN=95 Runoff=0.24 cfs 0.018 af

Subcatchment 11S: South Route 1 Frontage Runoff Area=6,211 sf 0.00% Impervious Runoff Depth=1.48" Flow Length=166' Tc=6.0 min CN=80 Runoff=0.25 cfs 0.018 af

Subcatchment 12S: Roadside to CB #4 Runoff Area=9,746 sf 23.27% Impervious Runoff Depth=1.55" Flow Length=282' Tc=9.6 min CN=81 Runoff=0.36 cfs 0.029 af

Subcatchment 13S: Roadside to GUSF #1 Runoff Area=13,602 sf 16.81% Impervious Runoff Depth=1.55" Flow Length=264' Tc=6.0 min CN=81 Runoff=0.56 cfs 0.040 af

Subcatchment 20S: Roadside to CB #3-1 Runoff Area=11,105 sf 40.77% Impervious Runoff Depth=2.00" Flow Length=390' Tc=6.0 min CN=87 Runoff=0.60 cfs 0.043 af

Subcatchment 21S: Woodland and

Runoff Area=40,322 sf 6.67% Impervious Runoff Depth=1.28"
Flow Length=338' Tc=6.5 min CN=77 Runoff=1.34 cfs 0.099 af

Subcatchment 22S: Woodland and

Runoff Area=53,034 sf 6.79% Impervious Runoff Depth=1.10"

Flow Length=408' Tc=16.0 min CN=74 Runoff=1.10 cfs 0.112 af

Subcatchment 23S: Roadside To CB #3-4 Runoff Area=8,495 sf 25.20% Impervious Runoff Depth=1.48" Flow Length=150' Tc=6.0 min CN=80 Runoff=0.34 cfs 0.024 af

Subcatchment 25S: Loading Area to CB #2 Runoff Area=4,411 sf 100.00% Impervious Runoff Depth=3.07" Flow Length=137' Tc=6.0 min CN=98 Runoff=0.32 cfs 0.026 af

Subcatchment 26S: Parking Lot to CB #1-1 Runoff Area=18,776 sf 85.85% Impervious Runoff Depth=2.74" Flow Length=332' Tc=6.0 min CN=95 Runoff=1.31 cfs 0.099 af

Subcatchment 27S: Proposed Roof

Runoff Area=20,000 sf 100.00% Impervious Runoff Depth=3.07"

Tc=6.0 min CN=98 Runoff=1.47 cfs 0.117 af

Subcatchment 29S: Open Space to GUSF #2 Runoff Area=90,054 sf 0.00% Impervious Runoff Depth=1.10" Flow Length=457' Tc=6.0 min CN=74 Runoff=2.55 cfs 0.190 af

Subcatchment 30S: Remaining Land

Runoff Area=86,511 sf 18.73% Impervious Runoff Depth=1.55"
Flow Length=760' Tc=12.0 min CN=81 Runoff=2.94 cfs 0.256 af

Reach 1R: 12" Steel PipeAvg. Flow Depth=0.40' Max Vel=7.60 fps Inflow=2.26 cfs 0.230 af 12.0" Round Pipe n=0.012 L=45.0' S=0.0291 '/' Capacity=6.59 cfs Outflow=2.26 cfs 0.230 af

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Reach 10R: Roadside Swale	Avg. Flow Depth=0.33' Max Vel=1.96 fps Inflow=1.94 cfs 0.144 af n=0.030 L=98.0' S=0.0104 '/' Capacity=17.99 cfs Outflow=1.93 cfs 0.144 af
Reach 13R: Swale	Avg. Flow Depth=0.08' Max Vel=1.72 fps Inflow=0.29 cfs 0.069 af n=0.030 L=41.0' S=0.0395 '/' Capacity=28.58 cfs Outflow=0.29 cfs 0.069 af
Reach 25R: 18" CPP 18.0" Round Pipe	Avg. Flow Depth=0.47' Max Vel=6.80 fps Inflow=3.27 cfs 0.304 af n=0.012 L=83.0' S=0.0175 '/' Capacity=15.04 cfs Outflow=3.27 cfs 0.304 af
Reach 27R: 12" Roof Leader 12.0" Round Pipe	Avg. Flow Depth=0.43' Max Vel=4.57 fps Inflow=1.47 cfs 0.117 af n=0.012 L=300.0' S=0.0100 '/' Capacity=3.86 cfs Outflow=1.45 cfs 0.117 af
Reach 28R: Riprap Swale	Avg. Flow Depth=0.21' Max Vel=2.82 fps Inflow=1.45 cfs 0.117 af n=0.069 L=108.0' S=0.1759 '/' Capacity=26.22 cfs Outflow=1.45 cfs 0.117 af
Pond 1P: CB #5-2	Peak Elev=78.48' Storage=12 cf Inflow=1.71 cfs 0.126 af 12.0" Round Culvert n=0.012 L=52.0' S=0.0050 '/' Outflow=1.71 cfs 0.126 af
Pond 10P: CB #5-1	Peak Elev=78.13' Storage=12 cf Inflow=1.94 cfs 0.144 af 12.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=1.94 cfs 0.144 af
Pond 12P: CB #4	Peak Elev=82.47' Storage=16 cf Inflow=0.36 cfs 0.029 af 12.0" Round Culvert n=0.120 L=50.0' S=0.0050 '/' Outflow=0.35 cfs 0.029 af
Pond 13P: GUSF #1	Peak Elev=82.34' Storage=1,664 cf Inflow=0.88 cfs 0.069 af Outflow=0.29 cfs 0.069 af
Pond 20P: CB #3-1	Peak Elev=76.93' Storage=7 cf Inflow=0.60 cfs 0.043 af 15.0" Round Culvert n=0.012 L=8.0' S=0.0100 '/' Outflow=0.59 cfs 0.043 af
Pond 21P: CB #3-2	Peak Elev=84.26' Storage=8 cf Inflow=1.34 cfs 0.099 af 12.0" Round Culvert n=0.012 L=142.0' S=0.0500 '/' Outflow=1.34 cfs 0.099 af
Pond 22P: CB #3-3	Peak Elev=79.54' Storage=7 cf Inflow=1.10 cfs 0.112 af 12.0" Round Culvert n=0.012 L=68.0' S=0.0360 '/' Outflow=1.10 cfs 0.112 af
Pond 23P: CB #3-4	Peak Elev=77.29' Storage=4 cf Inflow=0.34 cfs 0.024 af 12.0" Round Culvert n=0.012 L=45.0' S=0.0100 '/' Outflow=0.33 cfs 0.024 af
Pond 24P: DMH #3	Peak Elev=76.86' Storage=16 cf Inflow=2.96 cfs 0.278 af 18.0" Round Culvert n=0.012 L=177.0' S=0.0175 '/' Outflow=2.96 cfs 0.278 af
Pond 25P: CB #2	Peak Elev=73.84' Storage=4 cf Inflow=0.32 cfs 0.026 af 12.0" Round Culvert n=0.012 L=36.0' S=0.0100 '/' Outflow=0.32 cfs 0.026 af
Pond 26P: CB #1-1	Peak Elev=72.81' Storage=9 cf Inflow=1.31 cfs 0.099 af 12.0" Round Culvert n=0.012 L=13.0' S=0.0100 '/' Outflow=1.31 cfs 0.099 af
Pond 27P: DMH #1	Peak Elev=72.47' Storage=14 cf Inflow=4.53 cfs 0.402 af 18.0" Round Culvert n=0.012 L=50.0' S=0.0100 '/' Outflow=4.53 cfs 0.402 af
Pond 29P: GUSF #2	Peak Elev=57.96' Storage=17,547 cf Inflow=8.52 cfs 0.710 af Outflow=3.81 cfs 0.667 af

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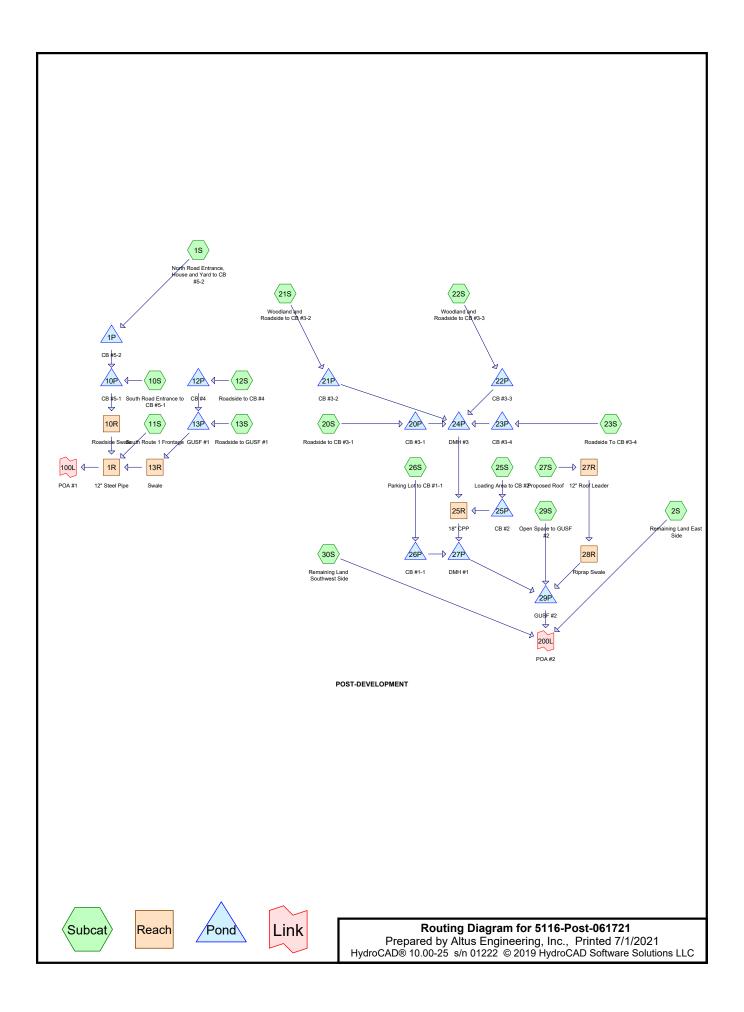
Link 100L: POA #1 Inflow=2.26 cfs 0.230 af

Primary=2.26 cfs 0.230 af

Link 200L: POA #2 Inflow=9.24 cfs 1.482 af

Primary=9.24 cfs 1.482 af

Total Runoff Area = 15.977 ac Runoff Volume = 1.755 af Average Runoff Depth = 1.32" 88.33% Pervious = 14.113 ac 11.67% Impervious = 1.864 ac



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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: North Road Entrance, Runoff Area=51,236 sf 8.13% Impervious Runoff Depth=2.54" Flow Length=432' Tc=6.3 min CN=77 Runoff=3.47 cfs 0.249 af

Subcatchment 2S: Remaining Land East Runoff Area=279,061 sf 0.00% Impervious Runoff Depth=2.20" Flow Length=1,208' Tc=32.9 min CN=73 Runoff=8.88 cfs 1.176 af

Subcatchment 10S: South Road Entrance to Runoff Area=3,377 sf 82.44% Impervious Runoff Depth=4.32" Flow Length=139' Tc=6.0 min CN=95 Runoff=0.36 cfs 0.028 af

Subcatchment 11S: South Route 1 Frontage Runoff Area=6,211 sf 0.00% Impervious Runoff Depth=2.81" Flow Length=166' Tc=6.0 min CN=80 Runoff=0.47 cfs 0.033 af

Subcatchment 12S: Roadside to CB #4 Runoff Area=9,746 sf 23.27% Impervious Runoff Depth=2.90" Flow Length=282' Tc=9.6 min CN=81 Runoff=0.67 cfs 0.054 af

Subcatchment 13S: Roadside to GUSF #1 Runoff Area=13,602 sf 16.81% Impervious Runoff Depth=2.90" Flow Length=264' Tc=6.0 min CN=81 Runoff=1.06 cfs 0.075 af

Subcatchment 20S: Roadside to CB #3-1 Runoff Area=11,105 sf 40.77% Impervious Runoff Depth=3.47" Flow Length=390' Tc=6.0 min CN=87 Runoff=1.02 cfs 0.074 af

Subcatchment 21S: Woodland and

Runoff Area=40,322 sf 6.67% Impervious Runoff Depth=2.54"
Flow Length=338' Tc=6.5 min CN=77 Runoff=2.71 cfs 0.196 af

Subcatchment 22S: Woodland and

Runoff Area=53,034 sf 6.79% Impervious Runoff Depth=2.28"
Flow Length=408' Tc=16.0 min CN=74 Runoff=2.39 cfs 0.232 af

Subcatchment 23S: Roadside To CB #3-4 Runoff Area=8,495 sf 25.20% Impervious Runoff Depth=2.81" Flow Length=150' Tc=6.0 min CN=80 Runoff=0.64 cfs 0.046 af

Subcatchment 25S: Loading Area to CB #2 Runoff Area=4,411 sf 100.00% Impervious Runoff Depth=4.66" Flow Length=137' Tc=6.0 min CN=98 Runoff=0.49 cfs 0.039 af

Subcatchment 26S: Parking Lot to CB #1-1 Runoff Area=18,776 sf 85.85% Impervious Runoff Depth=4.32" Flow Length=332' Tc=6.0 min CN=95 Runoff=2.01 cfs 0.155 af

Subcatchment 27S: Proposed Roof

Runoff Area=20,000 sf 100.00% Impervious Runoff Depth=4.66"

Tc=6.0 min CN=98 Runoff=2.20 cfs 0.178 af

Subcatchment 29S: Open Space to GUSF #2 Runoff Area=90,054 sf 0.00% Impervious Runoff Depth=2.28" Flow Length=457' Tc=6.0 min CN=74 Runoff=5.51 cfs 0.394 af

Subcatchment 30S: Remaining LandRunoff Area=86,511 sf 18.73% Impervious Runoff Depth=2.90"
Flow Length=760' Tc=12.0 min CN=81 Runoff=5.54 cfs 0.479 af

Reach 1R: 12" Steel PipeAvg. Flow Depth=0.62' Max Vel=9.07 fps Inflow=4.59 cfs 0.439 af 12.0" Round Pipe n=0.012 L=45.0' S=0.0291 '/' Capacity=6.59 cfs Outflow=4.59 cfs 0.439 af

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Reach 10R: Roadside Swale	Avg. Flow Depth=0.47' Max Vel=2.37 fps Inflow=3.78 cfs 0.277 af n=0.030 L=98.0' S=0.0104 '/' Capacity=17.99 cfs Outflow=3.76 cfs 0.277 af
Reach 13R: Swale	Avg. Flow Depth=0.12' Max Vel=2.26 fps Inflow=0.63 cfs 0.129 af n=0.030 L=41.0' S=0.0395 '/' Capacity=28.58 cfs Outflow=0.63 cfs 0.129 af
Reach 25R: 18" CPP 18.0" Round Pipe	Avg. Flow Depth=0.69' Max Vel=8.18 fps Inflow=6.43 cfs 0.586 af n=0.012 L=83.0' S=0.0175 '/' Capacity=15.04 cfs Outflow=6.43 cfs 0.586 af
Reach 27R: 12" Roof Leader 12.0" Round Pipe	Avg. Flow Depth=0.54' Max Vel=5.06 fps Inflow=2.20 cfs 0.178 af n=0.012 L=300.0' S=0.0100 '/' Capacity=3.86 cfs Outflow=2.17 cfs 0.178 af
Reach 28R: Riprap Swale	Avg. Flow Depth=0.27' Max Vel=3.21 fps Inflow=2.17 cfs 0.178 af n=0.069 L=108.0' S=0.1759 '/' Capacity=26.22 cfs Outflow=2.17 cfs 0.178 af
Pond 1P: CB #5-2	Peak Elev=79.68' Storage=26 cf Inflow=3.47 cfs 0.249 af 12.0" Round Culvert n=0.012 L=52.0' S=0.0050 '/' Outflow=3.43 cfs 0.249 af
Pond 10P: CB #5-1	Peak Elev=78.83' Storage=20 cf Inflow=3.77 cfs 0.277 af 12.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=3.78 cfs 0.277 af
Pond 12P: CB #4	Peak Elev=84.16' Storage=38 cf Inflow=0.67 cfs 0.054 af 12.0" Round Culvert n=0.120 L=50.0' S=0.0050 '/' Outflow=0.65 cfs 0.054 af
Pond 13P: GUSF #1	Peak Elev=82.99' Storage=2,543 cf Inflow=1.63 cfs 0.129 af Outflow=0.63 cfs 0.129 af
Pond 20P: CB #3-1	Peak Elev=77.34' Storage=12 cf Inflow=1.02 cfs 0.074 af 15.0" Round Culvert n=0.012 L=8.0' S=0.0100 '/' Outflow=1.01 cfs 0.074 af
Pond 21P: CB #3-2	Peak Elev=84.66' Storage=13 cf Inflow=2.71 cfs 0.196 af 12.0" Round Culvert n=0.012 L=142.0' S=0.0500 '/' Outflow=2.71 cfs 0.196 af
Pond 22P: CB #3-3	Peak Elev=79.89' Storage=12 cf Inflow=2.39 cfs 0.232 af 12.0" Round Culvert n=0.012 L=68.0' S=0.0360 '/' Outflow=2.39 cfs 0.232 af
Pond 23P: CB #3-4	Peak Elev=77.52' Storage=7 cf Inflow=0.64 cfs 0.046 af 12.0" Round Culvert n=0.012 L=45.0' S=0.0100 '/' Outflow=0.64 cfs 0.046 af
Pond 24P: DMH #3	Peak Elev=77.30' Storage=25 cf Inflow=5.97 cfs 0.547 af 18.0" Round Culvert n=0.012 L=177.0' S=0.0175 '/' Outflow=5.97 cfs 0.547 af
Pond 25P: CB #2	Peak Elev=73.94' Storage=5 cf Inflow=0.49 cfs 0.039 af 12.0" Round Culvert n=0.012 L=36.0' S=0.0100 '/' Outflow=0.48 cfs 0.039 af
Pond 26P: CB #1-1	Peak Elev=73.37' Storage=16 cf Inflow=2.01 cfs 0.155 af 12.0" Round Culvert n=0.012 L=13.0' S=0.0100 '/' Outflow=1.98 cfs 0.155 af
Pond 27P: DMH #1	Peak Elev=73.12' Storage=22 cf Inflow=8.36 cfs 0.742 af 18.0" Round Culvert n=0.012 L=50.0' S=0.0100 '/' Outflow=8.36 cfs 0.742 af
Pond 29P: GUSF #2	Peak Elev=58.66' Storage=24,031 cf Inflow=16.00 cfs 1.314 af Outflow=7.85 cfs 1.270 af

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Link 100L: POA #1 Inflow=4.59 cfs 0.439 af

Primary=4.59 cfs 0.439 af

Link 200L: POA #2 Inflow=19.31 cfs 2.926 af

Primary=19.31 cfs 2.926 af

Total Runoff Area = 15.977 ac Runoff Volume = 3.408 af Average Runoff Depth = 2.56" 88.33% Pervious = 14.113 ac 11.67% Impervious = 1.864 ac

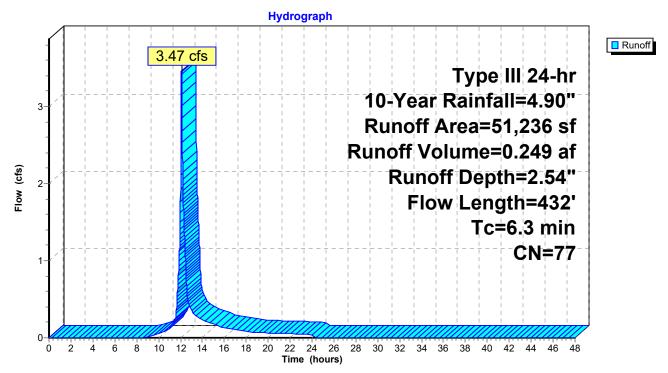
Summary for Subcatchment 1S: North Road Entrance, House and Yard to CB #5-2

Runoff = 3.47 cfs @ 12.09 hrs, Volume= 0.249 af, Depth= 2.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

_	Α	rea (sf)	CN [Description				
*		741	98 I	Impervious Existing Pavement				
*		1,318	98 I	Impervious Existing Building				
*		2,105	98 I	mpervious	Proposed	Pavement		
		333	96 (Gravel surfa	ace, HSG [
		3,755			ace, HSG (
		1,629		Dirt roads, I				
		7,139				ood, HSG D		
		818			od, HSG D			
		14,145				ood, HSG C		
_		19,253			od, HSG C			
		51,236		Veighted A				
		47,072	-	-	vious Area			
		4,164	3	3.13% Impe	ervious Are	a		
	_		01					
	Tc	Length	Slope			Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	3.9	54	0.0579	0.23		Sheet Flow,		
	4 -	400	0.0044	0.45		Grass: Short n= 0.150 P2= 3.30"		
	1.5	192	0.0941	2.15		Shallow Concentrated Flow,		
	0.5	07	0.0006	2.05		Short Grass Pasture Kv= 7.0 fps		
	0.5	97	0.0336	2.95		Shallow Concentrated Flow,		
	0.3	80	0.0750	4.41		Unpaved Kv= 16.1 fps		
	0.3	00	0.0750	4.41		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps		
	0.1	9	0.0075	1.76		Shallow Concentrated Flow,		
	0.1	9	0.0075	1.70		Paved Kv= 20.3 fps		
_	6.3	432	Total			1 ανοα 11ν- 20.0 τρο		
	0.5	432	Total					

Subcatchment 1S: North Road Entrance, House and Yard to CB #5-2



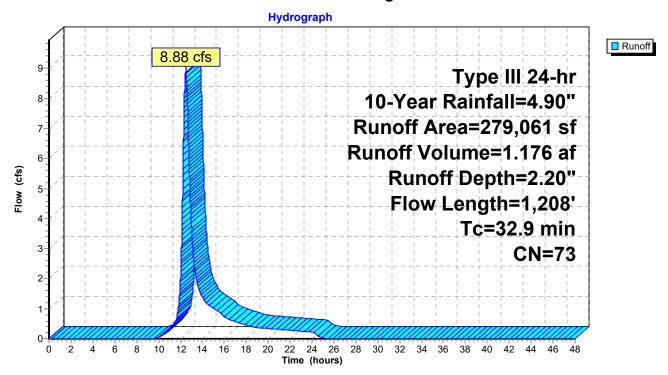
Summary for Subcatchment 2S: Remaining Land East Side

Runoff = 8.88 cfs @ 12.47 hrs, Volume= 1.176 af, Depth= 2.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Area (sf)	CN D	escription					
	1,161	89 E	Dirt roads, HSG D					
	2,559	87 D	irt roads, l					
	2,459	80 >	75% Gras	s cover, Go	ood, HSG D			
	93,993	77 V	Voods, Go	od, HSG D				
	3,899	74 >	75% Gras	s cover, Go	ood, HSG C			
	174,990	70 V	Voods, Go	od, HSG C				
	279,061	73 V	Veighted A	verage				
	279,061	1	00.00% Pe	ervious Are	a			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
8.8	83	0.1231	0.16		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 3.30"			
1.4	121	0.0826	1.44		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
7.1	301	0.0199	0.71		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
7.8	223	0.0090	0.47		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
1.6	77	0.0250	0.79		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
1.1	98	0.0816	1.43		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
5.1	305	0.0393	0.99		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
32.9	1,208	Total						

Subcatchment 2S: Remaining Land East Side



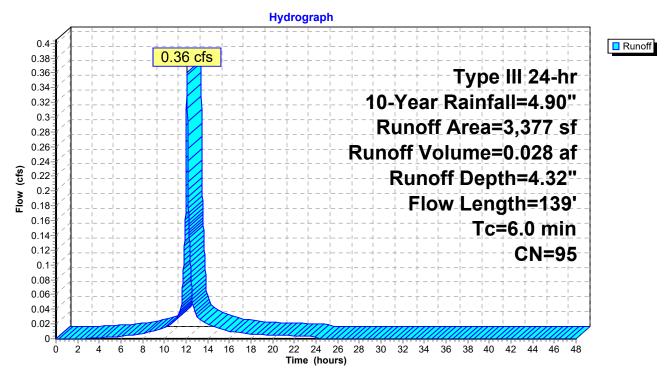
Summary for Subcatchment 10S: South Road Entrance to CB #5-1

Runoff = 0.36 cfs @ 12.08 hrs, Volume= 0.028 af, Depth= 4.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Area (sf) CN Description										
*		129	98 lı	98 Impervious Existing Pavement							
*		2,655	98 lı	1							
		593	80 >	·							
		3,377	95 V	95 Weighted Average							
		593			vious Area						
		2,784	8	2.44% Imp	ervious Ar	ea					
	_,. • . •										
	Tc	Length	Slope	Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·					
	0.4	50	0.0801	2.12		Sheet Flow,					
						Smooth surfaces n= 0.011 P2= 3.30"					
	0.1	34	0.0783	5.68		Shallow Concentrated Flow,					
						Paved Kv= 20.3 fps					
	0.1	37	0.0543	4.73		Shallow Concentrated Flow,					
						Paved Kv= 20.3 fps					
	0.1	18	0.0444	4.28		Shallow Concentrated Flow,					
						Paved Kv= 20.3 fps					
	0.7	139	Total, I	ncreased t	o minimum	Tc = 6.0 min					

Subcatchment 10S: South Road Entrance to CB #5-1



Summary for Subcatchment 11S: South Route 1 Frontage

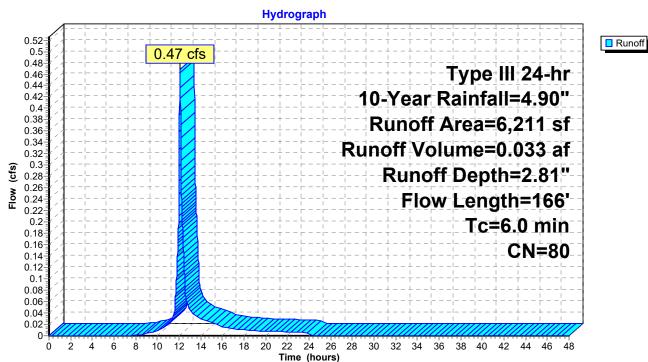
Runoff = 0.47 cfs @ 12.09 hrs, Volume= 0.033 af, Depth= 2.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Α	rea (sf)	CN	I Description							
		5,206		30 >75% Grass cover, Good, HSG D							
		1,005	77	Woods, Good, HSG D							
		6,211	80	80 Weighted Average							
		6,211		100.00% P	ervious Are	a					
	Tc	Length	Slope	Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	3.4	50	0.0660	0.24		Sheet Flow,					
						Grass: Short n= 0.150 P2= 3.30"					
	0.6	98	0.1326	2.55		Shallow Concentrated Flow,					
						Short Grass Pasture Kv= 7.0 fps					
	0.2	18	0.0142	1.79		Shallow Concentrated Flow,					
_						Grassed Waterway Kv= 15.0 fps					
	4.2	166	Total	Incresed t	a minimum	To = 6.0 min					

4.2 166 Total, Increased to minimum Tc = 6.0 min

Subcatchment 11S: South Route 1 Frontage



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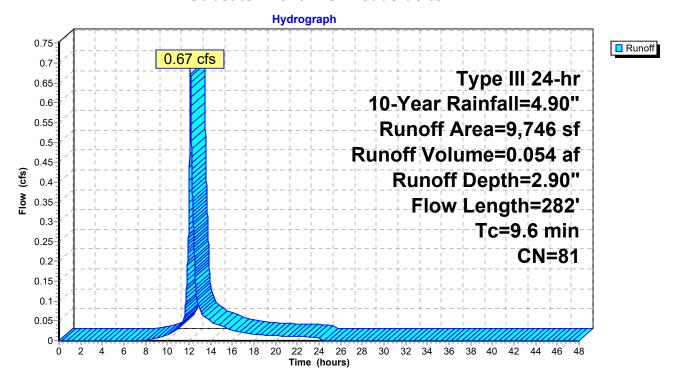
Summary for Subcatchment 12S: Roadside to CB #4

Runoff = 0.67 cfs @ 12.13 hrs, Volume= 0.054 af, Depth= 2.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Area (sf) CN Description						
*	2,268	98 Ir	npervious	Proposed F	Pavement		
	1,740	80 >	75% Grass	s cover, Go	ood, HSG D		
	1,668	77 V	Voods, Go	od, HSG D			
	3,711	74 >	75% Grass	s cover, Go	ood, HSG C		
	359	70 V	Voods, Go	od, HSG C			
	9,746	81 V	Veighted A	verage			
	7,478	7	6.73% Per	vious Area			
	2,268	2	3.27% Imp	ervious Are	ea		
To	•	Slope	Velocity	Capacity	Description		
(min) (feet)	(ft/ft)	(ft/sec)	(cfs)			
7.9	41	0.0399	0.09		Sheet Flow,		
					Woods: Light underbrush n= 0.400 P2= 3.30"		
0.9	9 61	0.0492	1.11		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
0.3	37	0.0849	2.04		Shallow Concentrated Flow,		
		0.0400	4.40		Short Grass Pasture Kv= 7.0 fps		
0.1	11	0.0400	1.40		Shallow Concentrated Flow,		
0.4	100	0.0044	5.00		Short Grass Pasture Kv= 7.0 fps		
0.4	132	0.0614	5.03		Shallow Concentrated Flow,		
					Paved Kv= 20.3 fps		
9.6	3 282	Total					

Subcatchment 12S: Roadside to CB #4



Summary for Subcatchment 13S: Roadside to GUSF #1

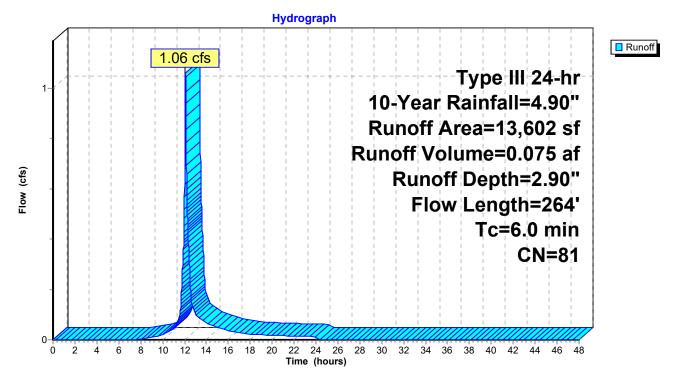
Runoff = 1.06 cfs @ 12.09 hrs, Volume= 0.075 af, Depth= 2.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

Area (sf)	CN E	Description							
2,286	98 l	mpervious	Proposed F	Pavement					
7,996		·							
33									
2,443	74 >	75% Gras	s cover, Go	ood, HSG C					
844	70 V	Voods, Go	od, HSG C						
13,602	81 V	Veighted A	verage						
11,316	8	3.19% Per	vious Area						
2,286	1	6.81% Imp	ervious Ar	ea					
		_							
Length	Slope	Velocity	Capacity	Description					
(feet)	(ft/ft)	(ft/sec)	(cfs)						
12	0.0200	0.91		Sheet Flow,					
				Smooth surfaces n= 0.011 P2= 3.30"					
8	0.3333	4.04		Shallow Concentrated Flow,					
				Short Grass Pasture Kv= 7.0 fps					
63	0.0159	1.89		Shallow Concentrated Flow,					
				Grassed Waterway Kv= 15.0 fps					
57	0.0351	2.81		Shallow Concentrated Flow,					
				Grassed Waterway Kv= 15.0 fps					
82	0.0610	3.70		Shallow Concentrated Flow,					
40	0.0050	4.00		Grassed Waterway Kv= 15.0 fps					
42	0.0952	4.63		Shallow Concentrated Flow,					
				Grassed Waterway Kv= 15.0 fps					
	2,286 7,996 33 2,443 844 13,602 11,316 2,286 Length (feet) 12 8 63 57	2,286 98 I 7,996 80 2 33 77 V 2,443 74 2 844 70 V 13,602 81 V 11,316 8 2,286 1 Length Slope (feet) (ft/ft) 12 0.0200 8 0.3333 63 0.0159 57 0.0351 82 0.0610 42 0.0952	2,286 98 Impervious 7,996 80 >75% Gras 33 77 Woods, Go 2,443 74 >75% Gras 844 70 Woods, Go 13,602 81 Weighted A 11,316 83.19% Per 2,286 16.81% Imp Length (feet) Slope Velocity (ft/sec) 12 0.0200 0.91 8 0.3333 4.04 63 0.0159 1.89 57 0.0351 2.81 82 0.0610 3.70 42 0.0952 4.63	2,286 98 Impervious Proposed I 7,996 80 >75% Grass cover, Go 33 77 Woods, Good, HSG D 2,443 74 >75% Grass cover, Go 844 70 Woods, Good, HSG C 13,602 81 Weighted Average 11,316 83.19% Pervious Area 2,286 16.81% Impervious Ar Length Slope Velocity Capacity (feet) (ft/ft) (ft/sec) (cfs) 12 0.0200 0.91 8 0.3333 4.04 63 0.0159 1.89 57 0.0351 2.81 82 0.0610 3.70 42 0.0952 4.63					

^{1.7 264} Total, Increased to minimum Tc = 6.0 min

Subcatchment 13S: Roadside to GUSF #1



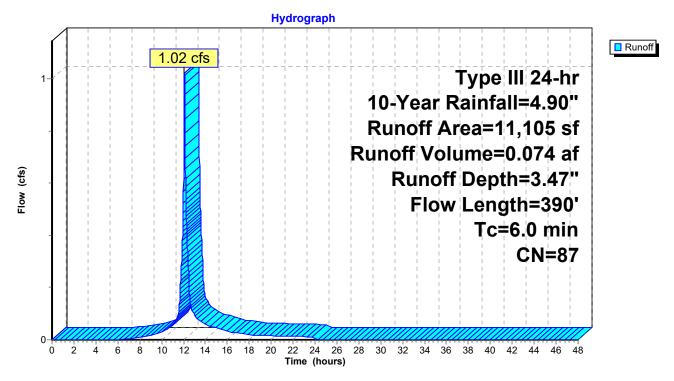
Summary for Subcatchment 20S: Roadside to CB #3-1

Runoff = 1.02 cfs @ 12.09 hrs, Volume= 0.074 af, Depth= 3.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Ar	rea (sf)	CN [Description						
*		4,527	98 I	98 Impervious Proposed Pavement						
		6,371	80 >	75% Gras	s cover, Go	ood, HSG D				
		207	74 >	75% Gras	s cover, Go	ood, HSG C				
		11,105	87 ١	Veighted A	verage					
		6,578	5	59.23% Per	vious Area					
		4,527	4	10.77% Imp	ervious Ar	ea				
				•						
Т	С	Length	Slope	Velocity	Capacity	Description				
(mir	า)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
0.	.2	12	0.0200	0.91		Sheet Flow,				
						Smooth surfaces n= 0.011 P2= 3.30"				
0.	.0	8	0.3333	4.04		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
0.	.6	63	0.0159	1.89		Shallow Concentrated Flow,				
						Grassed Waterway Kv= 15.0 fps				
1.	.5	257	0.0350	2.81		Shallow Concentrated Flow,				
						Grassed Waterway Kv= 15.0 fps				
0.	.2	50	0.0650	3.82		Shallow Concentrated Flow,				
						Grassed Waterway Kv= 15.0 fps				
2.	.5	390	Total,	ncreased t	o minimum	Tc = 6.0 min				

Subcatchment 20S: Roadside to CB #3-1



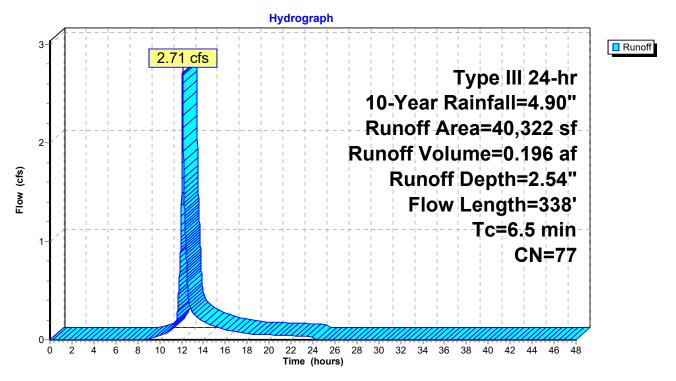
Summary for Subcatchment 21S: Woodland and Roadside to CB #3-2

Runoff = 2.71 cfs @ 12.10 hrs, Volume= 0.196 af, Depth= 2.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Д	rea (sf)	CN I	Description								
*		2,690	98 I	mpervious	mpervious Proposed Pavement							
		304	87 I	Dirt roads, I	HSĠ C							
		14,485	80 >	>75% Gras	s cover, Go	ood, HSG D						
		873	77 \	Noods, Good, HSG D								
		15,967				ood, HSG C						
		6,003	70 \	Noods, Go	od, HSG C							
		40,322	77 \	Veighted A	verage							
		37,632	(93.33% Per	rvious Area							
		2,690	(6.67% Impe	ervious Area	a						
	_				_							
_	Тс	Length	Slope		Capacity	Description						
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	3.9	50	0.0493	0.22		Sheet Flow,						
						Grass: Short n= 0.150 P2= 3.30"						
	2.1	180	0.0402	1.40		Shallow Concentrated Flow,						
						Short Grass Pasture Kv= 7.0 fps						
	0.1	11	0.0402	1.40		Shallow Concentrated Flow,						
						Short Grass Pasture Kv= 7.0 fps						
	0.4	97	0.0341	3.75		Shallow Concentrated Flow,						
						Paved Kv= 20.3 fps						
	6.5	338	Total									

Subcatchment 21S: Woodland and Roadside to CB #3-2



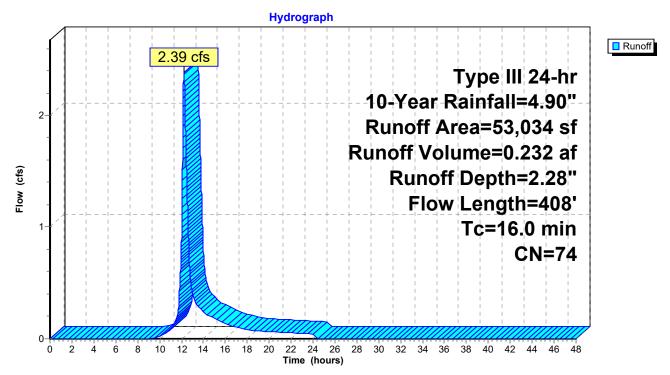
Summary for Subcatchment 22S: Woodland and Roadside to CB #3-3

Runoff = 2.39 cfs @ 12.22 hrs, Volume= 0.232 af, Depth= 2.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

A	rea (sf)	CN E	Description						
*	3,603	98 lı	B Impervious Proposed Pavement						
	1,976	87 E	Dirt roads, HSG C						
	3,978	80 >	75% Gras	s cover, Go	ood, HSG D				
	442	77 V	Voods, Go	od, HSG D					
	8,850	74 >	75% Gras	s cover, Go	ood, HSG C				
	34,185	70 V	Voods, Go	od, HSG C					
	53,034	74 V	Veighted A	verage					
	49,431		•	vious Area					
	3,603	6	.79% Impe	ervious Area	a				
	,		•						
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
12.4	50	0.0191	0.07		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 3.30"				
1.9	185	0.1017	1.59		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
0.4	52	0.0769	1.94		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
0.7	44	0.0471	1.09		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
0.1	8	0.0350	1.31		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
0.5	69	0.0140	2.40		Shallow Concentrated Flow,				
					Paved Kv= 20.3 fps				
16.0	408	Total							

Subcatchment 22S: Woodland and Roadside to CB #3-3



Summary for Subcatchment 23S: Roadside To CB #3-4

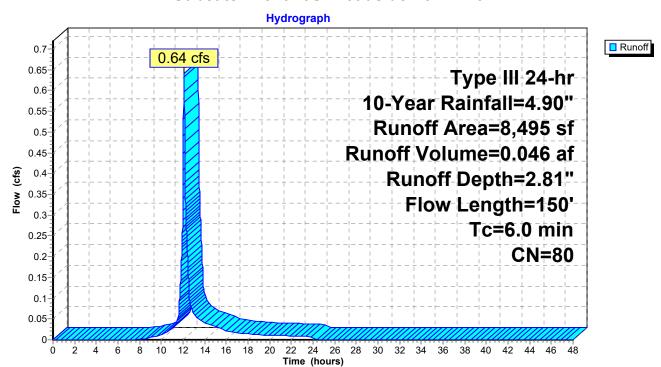
Runoff = 0.64 cfs @ 12.09 hrs, Volume= 0.046 af, Depth= 2.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

_	Α	rea (sf)	CN E	Description							
*		2,141	98 I	Impervoius Proposed Pavement							
		224	80 >	75% Grass cover, Good, HSG D							
		6,130	74 >	75% Gras	s cover, Go	ood, HSG C					
		8,495	80 V	Weighted Average							
		6,354	7	'4.80% Per	vious Area						
		2,141	2	5.20% Imp	ervious Ar	ea					
	Тс	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	0.2	14	0.0200	0.94		Sheet Flow,					
						Smooth surfaces n= 0.011 P2= 3.30"					
	0.0	4	0.0400	1.40		Shallow Concentrated Flow,					
						Short Grass Pasture Kv= 7.0 fps					
	0.0	5	0.3333	4.04		Shallow Concentrated Flow,					
						Short Grass Pasture Kv= 7.0 fps					
	0.9	127	0.0222	2.23		Shallow Concentrated Flow,					
						Grassed Waterway Kv= 15.0 fps					

1.1 150 Total, Increased to minimum Tc = 6.0 min

Subcatchment 23S: Roadside To CB #3-4



Summary for Subcatchment 25S: Loading Area to CB #2

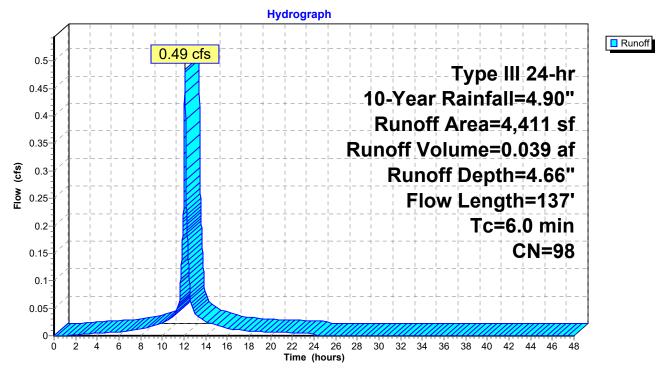
Runoff = 0.49 cfs @ 12.08 hrs, Volume= 0.039 af, Depth= 4.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Α	rea (sf)	CN E	escription			
*	4,411 98 Impervious Proposed Pavement						
	4,411 100.00% Impervious A					ırea	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	0.5	44	0.0316	1.42		Sheet Flow,	
	0.1	24	0.0238	3.13		Smooth surfaces n= 0.011 P2= 3.30" Shallow Concentrated Flow, Paved Kv= 20.3 fps	
	0.3	60	0.0200	2.87		Shallow Concentrated Flow,	
_	0.1	9	0.0040	1.28		Paved Kv= 20.3 fps Shallow Concentrated Flow, Paved Kv= 20.3 fps	
	1.0	127	Total I	naraaad t	a minimum	To = 6.0 min	

1.0 137 Total, Increased to minimum Tc = 6.0 min

Subcatchment 25S: Loading Area to CB #2



Summary for Subcatchment 26S: Parking Lot to CB #1-1

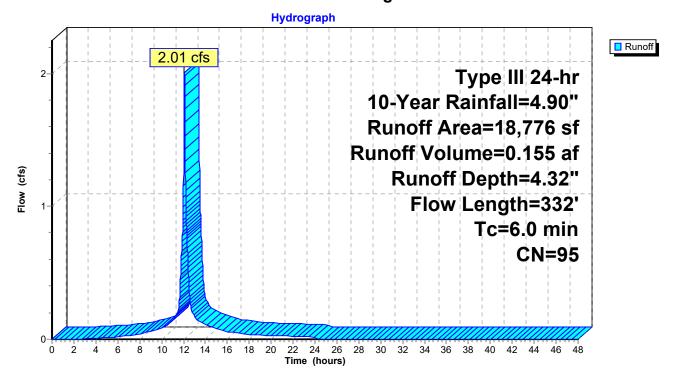
Runoff = 2.01 cfs @ 12.08 hrs, Volume= 0.155 af, Depth= 4.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

_	Α	rea (sf)	CN D	CN Description						
*		16,120	98 Ir	98 Impervious Proposed Pavement						
		2,295	80 >	75% Gras	s cover, Go	ood, HSG D				
		361	74 >	75% Gras	s cover, Go	ood, HSG C				
	18,776 95 Weighted Average									
		2,656	1	4.15% Per	vious Area					
		16,120	8	5.85% Imp	ervious Ar	ea				
	Tc	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	0.5	50	0.0444	1.67		Sheet Flow,				
						Smooth surfaces n= 0.011 P2= 3.30"				
	0.2	48	0.0334	3.71		Shallow Concentrated Flow,				
						Paved Kv= 20.3 fps				
	1.4	234	0.0200	2.87		Shallow Concentrated Flow,				
_						Paved Kv= 20.3 fps				
	2.1	332	Total, I	ncreased t	o minimum	Tc = 6.0 min				

Total, moreaced to minimum 10 0.0 min

Subcatchment 26S: Parking Lot to CB #1-1



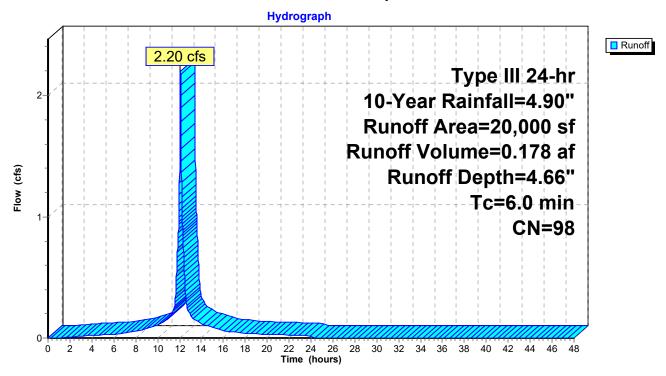
Summary for Subcatchment 27S: Proposed Roof

Runoff = 2.20 cfs @ 12.08 hrs, Volume= 0.178 af, Depth= 4.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

_	A	rea (sf)	CN [Description							
*		20,000	98 I	mpervious Proposed Roof							
	20,000 100.00% Impervious Are					rea					
	Тс	Length	Slope	Velocity	Capacity	Description					
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	6.0					Direct Entry,					

Subcatchment 27S: Proposed Roof



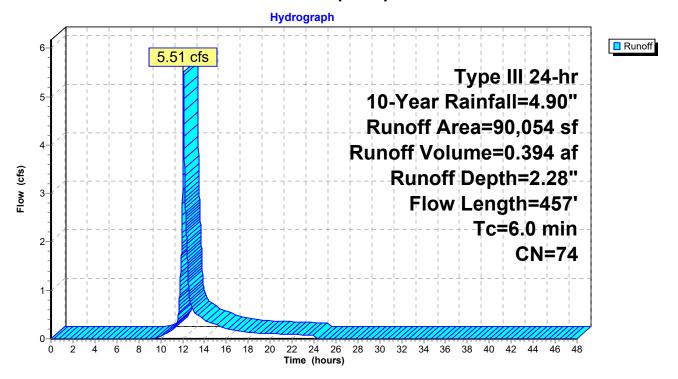
Summary for Subcatchment 29S: Open Space to GUSF #2

Runoff = 5.51 cfs @ 12.09 hrs, Volume= 0.394 af, Depth= 2.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Ar	ea (sf)	CN E	escription			
13,841 80 >75% Grass cover, Good, HSG D							
	•	18,593	77 V	Voods, Go	od, HSG D		
		31,340			,	ood, HSG C	
		26,280	70 V	Voods, Go	od, HSG C		
	Ć	90,054		Veighted A			
	Ć	90,054	1	00.00% Pe	ervious Are	a	
	_		01			B 1.0	
	Tc .	Length	Slope	Velocity		Description	
(mi		(feet)	(ft/ft)	(ft/sec)	(cfs)		
1	1.5	16	0.0582	0.18		Sheet Flow,	
_		- 1 -				Grass: Short n= 0.150 P2= 3.30"	
3	3.5	319	0.0100	1.50		Shallow Concentrated Flow,	
		07	0.4000	- 44	10.01	Grassed Waterway Kv= 15.0 fps	
C).1	27	0.1290	5.44	13.61	Trap/Vee/Rect Channel Flow,	
						Bot.W=2.00' D=1.00' Z= 0.5 '/' Top.W=3.00'	
_		40	0.0000	0.00	00.05	n= 0.069 Riprap, 6-inch	
C).1	48	0.2800	8.02	20.05	Trap/Vee/Rect Channel Flow,	
						Bot.W=2.00' D=1.00' Z= 0.5 '/' Top.W=3.00'	
C	١. ٥	17	0.0050	4.67	11 60	n= 0.069 Riprap, 6-inch	
C).2	47	0.0950	4.67	11.68	Trap/Vee/Rect Channel Flow,	
						Bot.W=2.00' D=1.00' Z= 0.5 '/' Top.W=3.00' n= 0.069 Riprap, 6-inch	
		457				• • •	
5	5.4	457	i otal. I	ncreased t	o minimum	Tc = 6.0 min	

Subcatchment 29S: Open Space to GUSF #2



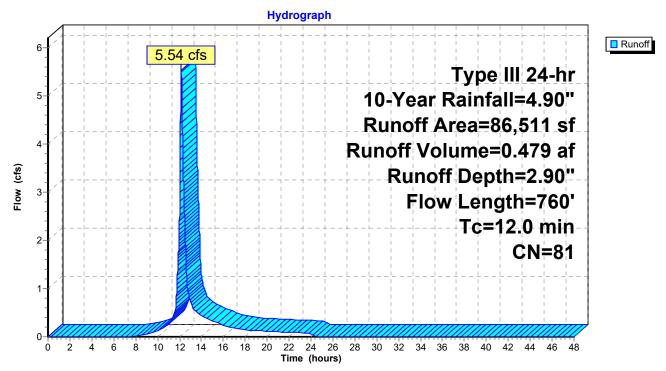
Summary for Subcatchment 30S: Remaining Land Southwest Side

Runoff = 5.54 cfs @ 12.17 hrs, Volume= 0.479 af, Depth= 2.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=4.90"

	Α	rea (sf)	CN E	escription						
*		11,834	98 lı	Impervious Existing Pavement						
*		4,369		Impervious Existing Roof						
		27,369	80 >	>75% Grass cover, Good, HSG D						
		35,628	77 V	Voods, Go	od, HSG D					
		1,815			ood, HSG C					
_		5,496	70 V	Voods, Go	od, HSG C					
		86,511	81 V	Veighted A	verage					
		70,308	8	1.27% Per	vious Area					
		16,203	1	8.73% Imp	pervious Are	ea				
	Тс	Length	Slope	Velocity		Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	3.8	31	0.0200	0.14		Sheet Flow,				
						Grass: Short n= 0.150 P2= 3.30"				
	0.1	15	0.0200	2.87		Shallow Concentrated Flow,				
	4.0	- 4		4.00		Paved Kv= 20.3 fps				
	1.2	74	0.0203	1.00		Shallow Concentrated Flow,				
	0.0	000	0.0005	0.00		Short Grass Pasture Kv= 7.0 fps				
	3.8	209	0.0335	0.92		Shallow Concentrated Flow,				
	1.4	207	0.0290	2.55		Woodland Kv= 5.0 fps				
	1.4	207	0.0290	2.55		Shallow Concentrated Flow,				
	0.3	75	0.0933	4.58		Grassed Waterway Kv= 15.0 fps Shallow Concentrated Flow,				
	0.5	13	0.0333	4.50		Grassed Waterway Kv= 15.0 fps				
	1.4	149	0.1208	1.74		Shallow Concentrated Flow,				
	17	173	5.1200	1.77		Woodland Kv= 5.0 fps				
_	12.0	760	Total			1100010110 111 010 190				
	12.0	, 00	ı Olai							

Subcatchment 30S: Remaining Land Southwest Side



5116-Post-061721

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Summary for Reach 1R: 12" Steel Pipe

Inflow Area = 1.932 ac, 13.66% Impervious, Inflow Depth = 2.73" for 10-Year event

Inflow = 4.59 cfs @ 12.11 hrs, Volume= 0.439 af

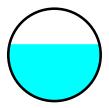
Outflow = 4.59 cfs @ 12.11 hrs, Volume= 0.439 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

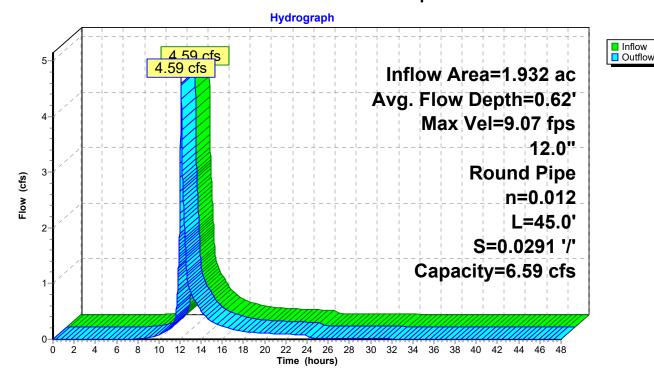
Max. Velocity= 9.07 fps, Min. Travel Time= 0.1 min Avg. Velocity = 2.07 fps, Avg. Travel Time= 0.4 min

Peak Storage= 23 cf @ 12.11 hrs Average Depth at Peak Storage= 0.62' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 6.59 cfs

12.0" Round Pipe n= 0.012 Length= 45.0' Slope= 0.0291 '/' Inlet Invert= 76.08', Outlet Invert= 74.77'



Reach 1R: 12" Steel Pipe



Summary for Reach 10R: Roadside Swale

Inflow Area = 1.254 ac, 12.72% Impervious, Inflow Depth = 2.65" for 10-Year event

Inflow = 3.78 cfs @ 12.09 hrs, Volume= 0.277 af

Outflow = 3.76 cfs (a) 12.11 hrs, Volume= 0.277 af, Atten= 0%, Lag= 1.1 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 2.37 fps, Min. Travel Time= 0.7 min Avg. Velocity = 0.63 fps, Avg. Travel Time= 2.6 min

Peak Storage= 156 cf @ 12.11 hrs Average Depth at Peak Storage= 0.47'

Bank-Full Depth= 1.00' Flow Area= 5.0 sf, Capacity= 17.99 cfs

2.00' x 1.00' deep channel, n= 0.030 Earth, grassed & winding

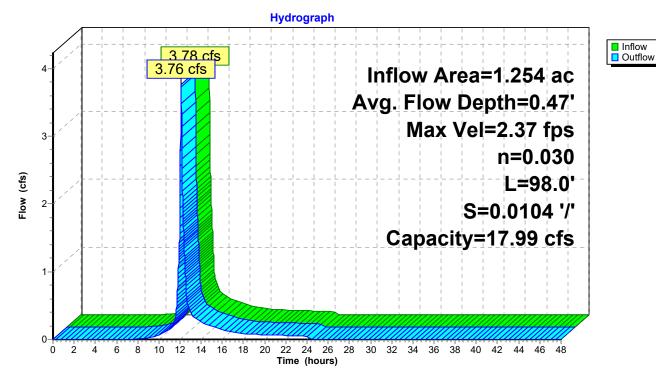
Side Slope Z-value= 3.0 '/' Top Width= 8.00'

Length= 98.0' Slope= 0.0104 '/'

Inlet Invert= 77.10', Outlet Invert= 76.08'



Reach 10R: Roadside Swale



Inflow
Outflow

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Summary for Reach 13R: Swale

Inflow Area = 0.536 ac, 19.50% Impervious, Inflow Depth > 2.89" for 10-Year event

Inflow = 0.63 cfs @ 12.41 hrs, Volume= 0.129 af

Outflow = 0.63 cfs @ 12.42 hrs, Volume= 0.129 af, Atten= 0%, Lag= 0.2 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 2.26 fps, Min. Travel Time= 0.3 min Avg. Velocity = 0.66 fps, Avg. Travel Time= 1.0 min

Peak Storage= 12 cf @ 12.42 hrs Average Depth at Peak Storage= 0.12'

Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 28.58 cfs

2.00' x 1.00' deep channel, n= 0.030 Earth, grassed & winding

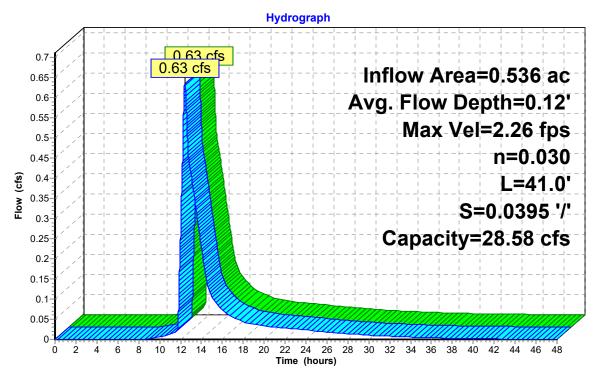
Side Slope Z-value= 2.0 '/' Top Width= 6.00'

Length= 41.0' Slope= 0.0395 '/'

Inlet Invert= 77.70', Outlet Invert= 76.08'



Reach 13R: Swale



Summary for Reach 25R: 18" CPP

Inflow Area = 2.694 ac, 14.80% Impervious, Inflow Depth = 2.61" for 10-Year event

Inflow = 6.43 cfs @ 12.11 hrs, Volume= 0.586 af

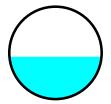
Outflow = 6.43 cfs (a) 12.11 hrs, Volume= 0.586 af, Atten= 0%, Lag= 0.1 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

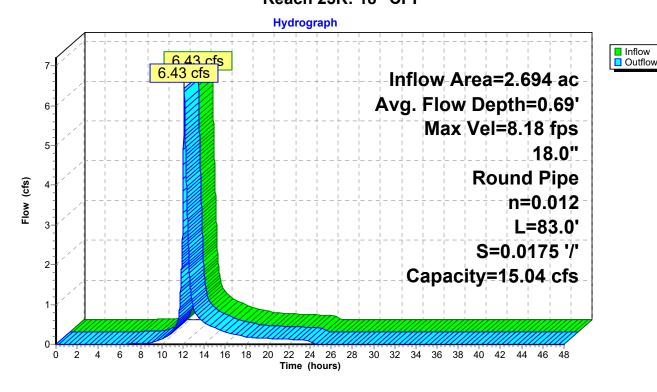
Max. Velocity= 8.18 fps, Min. Travel Time= 0.2 min Avg. Velocity = 2.49 fps, Avg. Travel Time= 0.6 min

Peak Storage= 65 cf @ 12.11 hrs Average Depth at Peak Storage= 0.69' Bank-Full Depth= 1.50' Flow Area= 1.8 sf, Capacity= 15.04 cfs

18.0" Round Pipe n= 0.012 Length= 83.0' Slope= 0.0175 '/' Inlet Invert= 72.95', Outlet Invert= 71.50'



Reach 25R: 18" CPP



Summary for Reach 27R: 12" Roof Leader

Inflow Area = 0.459 ac,100.00% Impervious, Inflow Depth = 4.66" for 10-Year event

Inflow = 2.20 cfs @ 12.08 hrs, Volume= 0.178 af

Outflow = 2.17 cfs @ 12.10 hrs, Volume= 0.178 af, Atten= 1%, Lag= 0.8 min

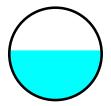
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 5.06 fps, Min. Travel Time= 1.0 min Avg. Velocity = 1.70 fps, Avg. Travel Time= 2.9 min

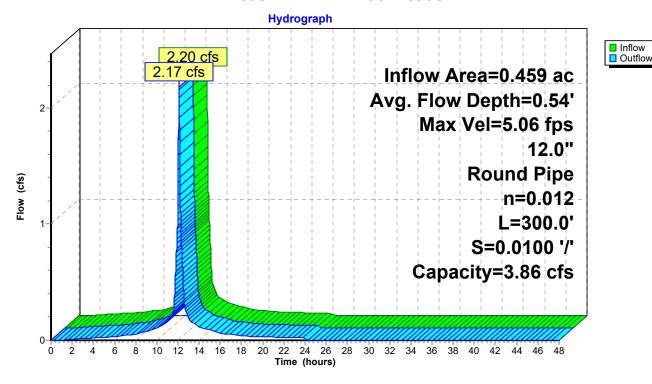
Peak Storage= 129 cf @ 12.10 hrs
Average Depth at Peak Storage= 0.54'

Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 3.86 cfs

12.0" Round Pipe n= 0.012 Length= 300.0' Slope= 0.0100 '/' Inlet Invert= 78.50', Outlet Invert= 75.50'



Reach 27R: 12" Roof Leader



Inflow
Outflow

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Summary for Reach 28R: Riprap Swale

Inflow Area = 0.459 ac,100.00% Impervious, Inflow Depth = 4.66" for 10-Year event

Inflow = 2.17 cfs @ 12.10 hrs, Volume= 0.178 af

Outflow = 2.17 cfs (a) 12.10 hrs, Volume= 0.178 af, Atten= 0%, Lag= 0.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 3.21 fps, Min. Travel Time= 0.6 min Avg. Velocity = 0.86 fps, Avg. Travel Time= 2.1 min

Peak Storage= 73 cf @ 12.10 hrs Average Depth at Peak Storage= 0.27'

Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 26.22 cfs

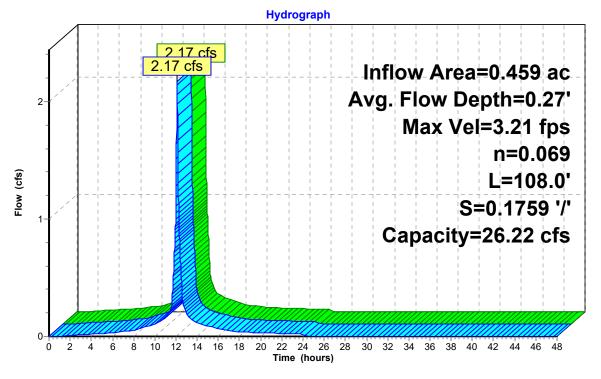
2.00' x 1.00' deep channel, n= 0.069 Riprap, 6-inch

Side Slope Z-value= 2.0 '/' Top Width= 6.00' Length= 108.0' Slope= 0.1759 '/'

Inlet Invert= 75.50', Outlet Invert= 56.50'



Reach 28R: Riprap Swale



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Summary for Pond 1P: CB #5-2

Inflow Area = 1.176 ac, 8.13% Impervious, Inflow Depth = 2.54" for 10-Year event

Inflow = 3.47 cfs @ 12.09 hrs, Volume= 0.249 af

Outflow = 3.43 cfs @ 12.11 hrs, Volume= 0.249 af, Atten= 1%, Lag= 0.9 min

Primary = 3.43 cfs @ 12.11 hrs, Volume= 0.249 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 79.68' @ 12.11 hrs Surf.Area= 228 sf Storage= 26 cf

Plug-Flow detention time= 0.2 min calculated for 0.249 af (100% of inflow)

Center-of-Mass det. time= 0.2 min (831.2 - 830.9)

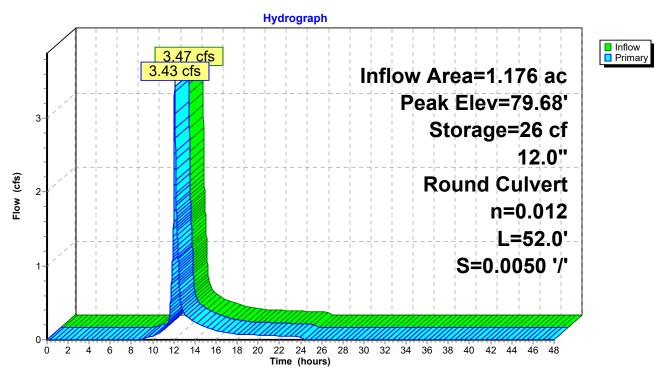
Volume	Invert	Avail.	.Storage	Storage	Description	
#1	77.56'		110 cf	Custon	n Stage Data (Pris	smatic)Listed below (Recalc)
Elevation (feet)		Area sq-ft)		:.Store c-feet)	Cum.Store (cubic-feet)	
77.56		13	(000)	0	0	
78.65 79.65		13 4		14 9	14 23	
79.80	,	I,155		87	110	

Device	Routing	Invert	Outlet Devices
#1	Primary	77 56'	12.0" Round Culvert

77.56' **12.0" Round Culvert**L= 52.0' CPP, square edge headwall, Ke= 0.500
Inlet / Outlet Invert= 77.56' / 77.30' S= 0.0050 '/' Cc= 0.900
n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=3.42 cfs @ 12.11 hrs HW=79.68' TW=78.83' (Dynamic Tailwater) 1=Culvert (Outlet Controls 3.42 cfs @ 4.35 fps)

Pond 1P: CB #5-2



5116-Post-061721

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Summary for Pond 10P: CB #5-1

Inflow Area = 1.254 ac, 12.72% Impervious, Inflow Depth = 2.65" for 10-Year event

3.77 cfs @ 12.11 hrs, Volume= Inflow 0.277 af

3.78 cfs @ 12.09 hrs, Volume= Outflow = 0.277 af, Atten= 0%, Lag= 0.0 min

3.78 cfs @ 12.09 hrs, Volume= Primary 0.277 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 78.83' @ 12.09 hrs Surf.Area= 8 sf Storage= 20 cf

Plug-Flow detention time= 0.2 min calculated for 0.277 af (100% of inflow)

Center-of-Mass det. time= 0.2 min (825.1 - 824.9)

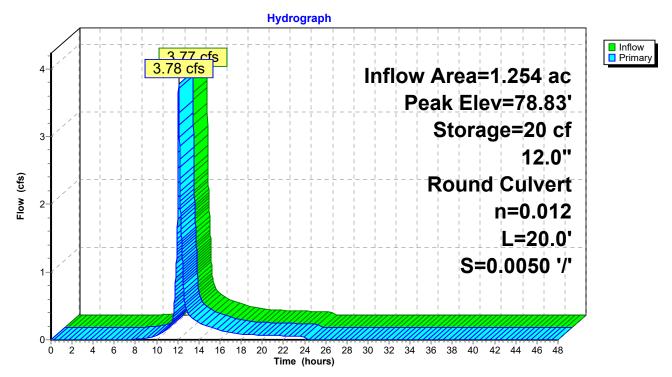
Volume	ln۱	vert Avail.	Avail.Storage		Storage Description			
#1	77.	.20'	65 cf	Custom S	Stage Data (P	rismatic)Listed below (Recalc)		
Elevatio		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)			
77.2	20	13		0	0			
78.3	30	13		14	14			
79.3	30	4		9	23			
79.5	50	416		42	65			
Device	Routing			et Devices				
#1	Drimon	, 77 ')(\' 4 7 0	" Daund (~lv.o.w+			

Primary 77.20' 12.0" Round Culvert #1

> L= 20.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 77.20' / 77.10' S= 0.0050 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=3.78 cfs @ 12.09 hrs HW=78.83' TW=77.57' (Dynamic Tailwater) 1=Culvert (Barrel Controls 3.78 cfs @ 4.81 fps)

Pond 10P: CB #5-1



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Summary for Pond 12P: CB #4

Inflow Area = 0.224 ac, 23.27% Impervious, Inflow Depth = 2.90" for 10-Year event

Inflow = 0.67 cfs @ 12.13 hrs, Volume= 0.054 af

Outflow = 0.65 cfs @ 12.15 hrs, Volume= 0.054 af, Atten= 3%, Lag= 1.0 min

Primary = 0.65 cfs @ 12.15 hrs, Volume= 0.054 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 84.16' @ 12.16 hrs Surf.Area= 13 sf Storage= 38 cf

Plug-Flow detention time= 4.4 min calculated for 0.054 af (100% of inflow)

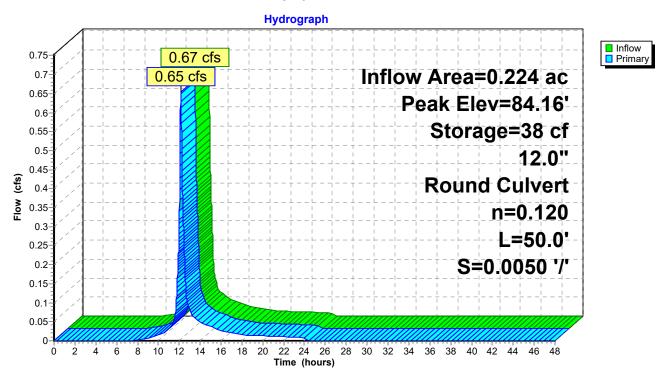
Center-of-Mass det. time= 4.3 min (827.6 - 823.3)

Volume	Inv	vert Avail.Storage		Storage Description			
#1	81.2	25'	51 cf	Custom S	Stage Data (P	rismatic)Listed below (Recalc)	
Elevation	on	Surf.Area	Inc.Store		Cum.Store		
(fee	et)	(sq-ft)	(cubic-feet)		(cubic-feet)		
81.2	25	13		0	0		
84.5	50	13	42		42		
85.5	50	4		9	51		
Device	Routing	Invert	Outle	et Devices			
#1	Primary	81.25'	12.0	" Round C	ulvert		
			L= 5	0.0' CPP,	square edge	headwall, Ke= 0.500	
			Inlat	/ Outlet Inv	ort- 21 25' / 2	21 00' S= 0 0050 '/' Cc= 0 000	

L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 81.25' / 81.00' S= 0.0050 '/' Cc= 0.900 n= 0.120, Flow Area= 0.79 sf

Primary OutFlow Max=0.65 cfs @ 12.15 hrs HW=84.14' TW=82.72' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.65 cfs @ 0.82 fps)

Pond 12P: CB #4



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Summary for Pond 13P: GUSF #1

Inflow Area = 0.536 ac, 19.50% Impervious, Inflow Depth = 2.90" for 10-Year event

1.63 cfs @ 12.10 hrs, Volume= Inflow 0.129 af

0.63 cfs @ 12.41 hrs, Volume= Outflow 0.129 af, Atten= 61%, Lag= 18.5 min

0.63 cfs @ 12.41 hrs, Volume= 0.129 af Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Starting Elev= 81.00' Surf.Area= 464 sf Storage= 601 cf

Peak Elev= 82.99' @ 12.41 hrs Surf.Area= 1,551 sf Storage= 2,543 cf (1,942 cf above start)

Flood Elev= 84.25' Surf.Area= 2,475 sf Storage= 5,079 cf (4,478 cf above start)

Plug-Flow detention time= 218.1 min calculated for 0.115 af (89% of inflow)

Center-of-Mass det. time= 136.5 min (959.6 - 823.1)

Volume	Invert Ava	il.Storage	Storage Description			
#1	77.50'	5,079 cf	Custom Stage Data (Prismatic)Listed below (Recalc)			
Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
77.50	464	0.0	0	0		
79.00	464	40.0	278	278		
79.50	464	40.0	93	371		
81.00	464	33.0	230	601		
81.80	850	100.0	526	1,126		
82.00	955	100.0	181	1,307		
83.00	1,559	100.0	1,257	2,564		
84.00	2,282	100.0	1,921	4,484		
84.25	2,475	100.0	595	5,079		

Device	Routing	Invert	Outlet Devices
#1	Primary	78.00'	12.0" Round Culvert
			L= 30.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 78.00' / 77.70' S= 0.0100 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf
#2	Device 1	78.00'	6.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	81.80'	4.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	82.83'	9.0" W x 5.0" H Vert. Orifice/Grate C= 0.600
#5	Device 1	83.25'	24.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#6	Device 2	81.00'	2.410 in/hr Exfiltration over Surface area above 81.00'
			Excluded Surface area = 464 sf Phase-In= 0.01'

Primary OutFlow Max=0.63 cfs @ 12.41 hrs HW=82.99' TW=77.82' (Dynamic Tailwater)

1=Culvert (Passes 0.63 cfs of 8.01 cfs potential flow)

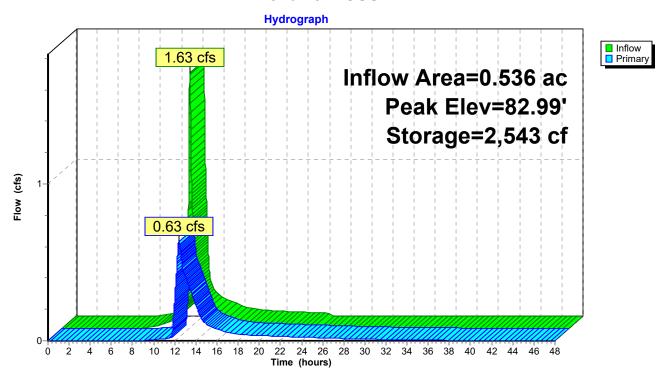
-2=Orifice/Grate (Passes 0.06 cfs of 2.06 cfs potential flow)
-6=Exfiltration (Exfiltration Controls 0.06 cfs)

-3=Orifice/Grate (Orifice Controls 0.42 cfs @ 4.86 fps)

-4=Orifice/Grate (Orifice Controls 0.15 cfs @ 1.27 fps)

-5=Orifice/Grate (Controls 0.00 cfs)

Pond 13P: GUSF #1



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Summary for Pond 20P: CB #3-1

Inflow Area = 0.255 ac, 40.77% Impervious, Inflow Depth = 3.47" for 10-Year event

1.02 cfs @ 12.09 hrs, Volume= Inflow 0.074 af

1.01 cfs @ 12.09 hrs, Volume= Outflow = 0.074 af, Atten= 1%, Lag= 0.1 min

1.01 cfs @ 12.09 hrs, Volume= Primary 0.074 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 77.34' @ 12.12 hrs Surf.Area= 13 sf Storage= 12 cf

Plug-Flow detention time= 0.6 min calculated for 0.074 af (100% of inflow)

Center-of-Mass det. time= 0.4 min (802.4 - 802.0)

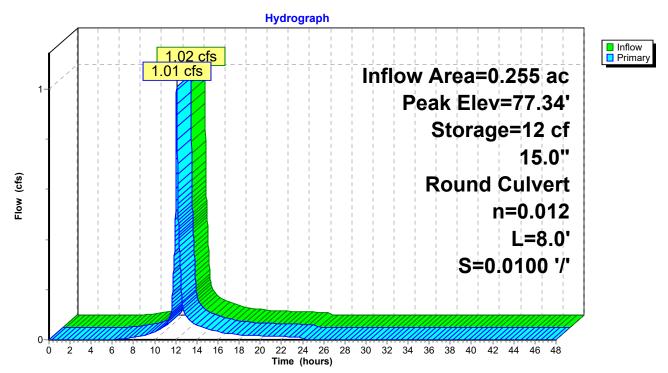
Volume	Inv	vert Avail.Storage		Storage [Storage Description		
#1	76.	38'	106 cf	Custom	Stage Data (Pi	rismatic)Listed below (Recalc)	
Elevation	on	Surf.Area		c.Store	Cum.Store		
(fee	et)	(sq-ft)	(cub	ic-feet)	(cubic-feet)		
76.38		13		0	0		
78.7	75	13		31	31		
79.7	75	4		9	39		
80.0	00	40		6	45		
80.7	71	131		61	106		
Device	Routing	Ir	vert Out	let Devices			
#1	Primary	76	3.38' 15.0	" Round	Culvert		

15.0" Round Culvert

L= 8.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 76.38' / 76.30' S= 0.0100 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=0.75 cfs @ 12.09 hrs HW=77.30' TW=77.27' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.75 cfs @ 1.07 fps)

Pond 20P: CB #3-1



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Summary for Pond 21P: CB #3-2

Inflow Area = 0.926 ac, 6.67% Impervious, Inflow Depth = 2.54" for 10-Year event

Inflow = 2.71 cfs @ 12.10 hrs, Volume= 0.196 af

Outflow = 2.71 cfs @ 12.10 hrs, Volume= 0.196 af, Atten= 0%, Lag= 0.1 min

Primary = 2.71 cfs @ 12.10 hrs, Volume= 0.196 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 84.66' @ 12.10 hrs Surf.Area= 13 sf Storage= 13 cf

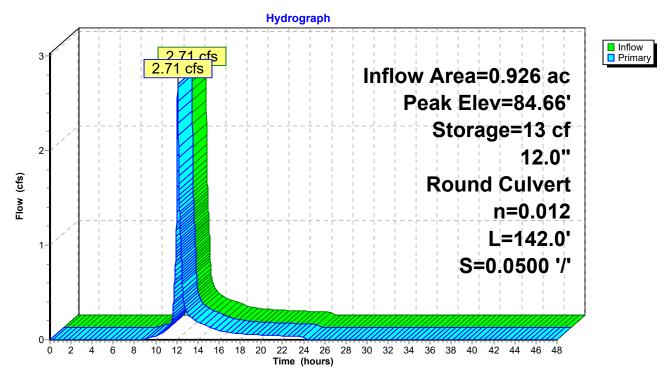
Plug-Flow detention time= 0.4 min calculated for 0.196 af (100% of inflow)

Center-of-Mass det. time= 0.2 min (831.3 - 831.1)

Volume	Inv	ert Avail.Sto	rage Storage	Description					
#1	83.6	65'	48 cf Custom	Stage Data (Pi	rismatic)Listed below (Recalc)				
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)					
83.6	35	13	0	0					
86.7	70	13	40	40					
87.7	70	4	9	48					
Device	Routing	Invert	Outlet Devices	S					
#1	Primary	83.65'	12.0" Round	12.0" Round Culvert					
	•		L= 142.0' CF	L= 142.0' CPP, square edge headwall, Ke= 0.500					
			Inlet / Outlet In	Inlet / Outlet Invert= 83.65' / 76.55' S= 0.0500 '/' Cc= 0.900					
		n= 0.012, Flow Area= 0.79 sf							

Primary OutFlow Max=2.70 cfs @ 12.10 hrs HW=84.66' TW=77.29' (Dynamic Tailwater) 1=Culvert (Inlet Controls 2.70 cfs @ 3.44 fps)

Pond 21P: CB #3-2



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Summary for Pond 22P: CB #3-3

Inflow Area = 1.217 ac, 6.79% Impervious, Inflow Depth = 2.28" for 10-Year event

2.39 cfs @ 12.22 hrs, Volume= Inflow 0.232 af

2.39 cfs @ 12.22 hrs, Volume= Outflow = 0.232 af, Atten= 0%, Lag= 0.0 min

Primary 2.39 cfs @ 12.22 hrs, Volume= 0.232 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 79.89' @ 12.22 hrs Surf.Area= 13 sf Storage= 12 cf

Plug-Flow detention time= 0.4 min calculated for 0.232 af (100% of inflow)

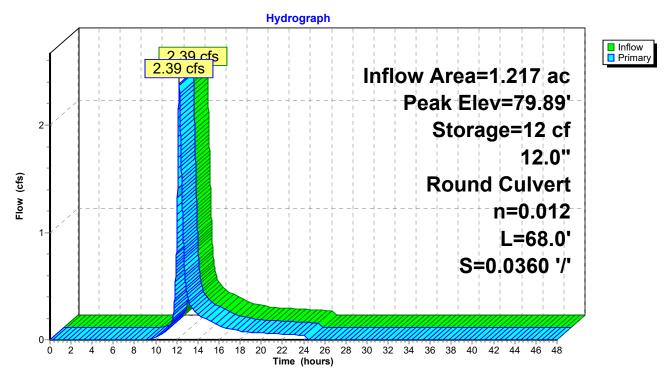
Center-of-Mass det. time= 0.2 min (847.9 - 847.7)

Volume	Inv	ert Avail.St	orage St	orage De	escription				
#1	79.	00'	48 cf Cι	stom St	tage Data (Pr	ismatic)Listed below (Recalc)			
Elevatio		Surf.Area (sq-ft)	Inc.Sto		Cum.Store (cubic-feet)				
			(cubic-le						
79.0)()	13		0	0				
82.0	00	13		39	39				
83.0	00	4		9	48				
Dovice	Douting	lavort	Outlet D	ovione.					
Device	Routing	Invert	Outlet D	evices					
#1	Primary	79.00		12.0" Round Culvert L= 68.0' CPP, square edge headwall, Ke= 0.500					

Inlet / Outlet Invert= 79.00' / 76.55' S= 0.0360 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=2.38 cfs @ 12.22 hrs HW=79.89' TW=77.13' (Dynamic Tailwater) 1=Culvert (Inlet Controls 2.38 cfs @ 3.22 fps)

Pond 22P: CB #3-3



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Summary for Pond 23P: CB #3-4

Inflow Area = 0.195 ac, 25.20% Impervious, Inflow Depth = 2.81" for 10-Year event

Inflow = 0.64 cfs @ 12.09 hrs, Volume= 0.046 af

Outflow = 0.64 cfs @ 12.09 hrs, Volume= 0.046 af, Atten= 1%, Lag= 0.1 min

Primary = 0.64 cfs @ 12.09 hrs, Volume= 0.046 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 77.52' @ 12.11 hrs Surf.Area= 13 sf Storage= 7 cf

Plug-Flow detention time= 0.5 min calculated for 0.046 af (100% of inflow)

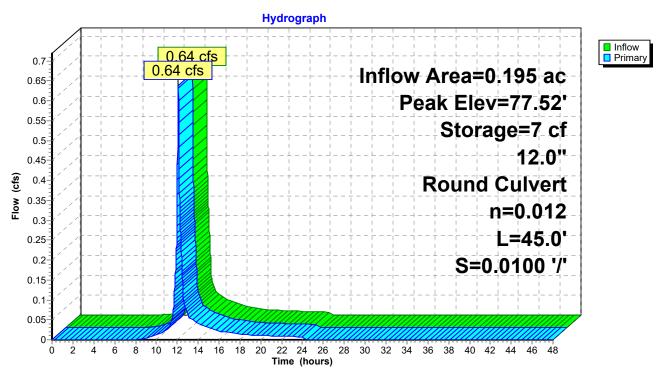
Center-of-Mass det. time= 0.5 min (823.2 - 822.7)

Volume	Inv	ert Avail.Sto	rage Stora	age Description	
#1	77.0	00' 1	33 cf Cust	om Stage Data (P	rismatic)Listed below (Recalc)
Elevatio (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	_	
77.0	0	13	0	0	
79.0	0	13	26	26	
80.0	0	4	9	35	
80.5	0	388	98	133	
Device	Routing	Invert	Outlet Dev	rices	
#1	Primary	77.00'		ind Culvert CPP. square edge l	headwall, Ke= 0.500

L= 45.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 77.00' / 76.55' S= 0.0100 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.61 cfs @ 12.09 hrs HW=77.51' TW=77.28' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.61 cfs @ 2.21 fps)

Pond 23P: CB #3-4



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Summary for Pond 24P: DMH #3

Inflow Area = 2.593 ac, 11.47% Impervious, Inflow Depth = 2.53" for 10-Year event

Inflow = 5.97 cfs @ 12.11 hrs, Volume= 0.547 af

Outflow = 5.97 cfs @ 12.11 hrs, Volume= 0.547 af, Atten= 0%, Lag= 0.0 min

Primary = $5.97 \text{ cfs } \bigcirc 0.547 \text{ af}$

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 77.30' @ 12.11 hrs Surf.Area= 20 sf Storage= 25 cf

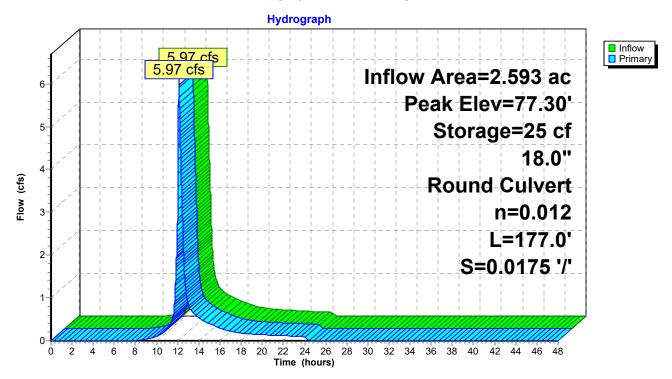
Plug-Flow detention time= 0.2 min calculated for 0.547 af (100% of inflow)

Center-of-Mass det. time= 0.2 min (834.0 - 833.8)

Volume	Inv	ert Avail.Sto	rage Storage	Description					
#1	76.0	05' 1	03 cf Custom	Stage Data (Pi	rismatic)Listed below (Recalc)				
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)					
76.0)5	20	0	0					
80.6	30	20	91	91					
81.6	60	4	12	103					
Device	Routing	Invert	Outlet Device	S					
#1	Primary	76.05'	18.0" Round	l Culvert					
			L= 177.0' CF	L= 177.0' CPP, square edge headwall, Ke= 0.500					
Inlet / Outlet Invert= 76.05' / 72.95' S= 0.0175 '/' Cc= 0.900									
			n= 0.012, Flo	ow Area= 1.77 sf					

Primary OutFlow Max=5.97 cfs @ 12.11 hrs HW=77.30' TW=73.63' (Dynamic Tailwater) 1=Culvert (Inlet Controls 5.97 cfs @ 3.80 fps)

Pond 24P: DMH #3



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Summary for Pond 25P: CB #2

Inflow Area = 0.101 ac,100.00% Impervious, Inflow Depth = 4.66" for 10-Year event

Inflow = 0.49 cfs @ 12.08 hrs, Volume= 0.039 af

Outflow = 0.48 cfs @ 12.08 hrs, Volume= 0.039 af, Atten= 0%, Lag= 0.1 min

Primary = 0.48 cfs @ 12.08 hrs, Volume= 0.039 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 73.94' @ 12.10 hrs Surf.Area= 13 sf Storage= 5 cf

Plug-Flow detention time= 0.8 min calculated for 0.039 af (100% of inflow)

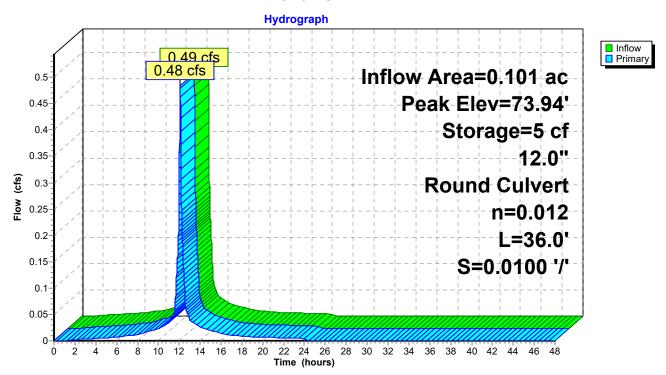
Center-of-Mass det. time= 0.6 min (749.0 - 748.4)

Volume	ln۱	ert Avail.St	orage Stora	ge Description					
#1	73.	56'	56 cf Custo	om Stage Data (Pi	rismatic)Listed below (Recalc)				
Elevation (fee	et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)					
73.56		13	0	0					
77.2	25	13	48	48					
78.2	25	4	9	56					
Device	Routing	Invert	Outlet Devi	ces					
#1	Primary	73.56'	L= 36.0' C	12.0" Round Culvert L= 36.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 73.56' / 73.20' S= 0.0100 '/' Cc= 0.900					

n= 0.012, Flow Area= 0.79 sf 7 cfs @ 12.08 hrs HW=73.94' TW=73.62' (Dynamic Tailwater)

Primary OutFlow Max=0.47 cfs @ 12.08 hrs HW=73.94' TW=73.62' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.47 cfs @ 2.55 fps)

Pond 25P: CB #2



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Summary for Pond 26P: CB #1-1

Inflow Area = 0.431 ac, 85.85% Impervious, Inflow Depth = 4.32" for 10-Year event

Inflow = 2.01 cfs @ 12.08 hrs, Volume= 0.155 af

Outflow = 1.98 cfs @ 12.09 hrs, Volume= 0.155 af, Atten= 1%, Lag= 0.1 min

Primary = 1.98 cfs @ 12.09 hrs, Volume= 0.155 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 73.37' @ 12.11 hrs Surf.Area= 13 sf Storage= 16 cf

Plug-Flow detention time= 0.5 min calculated for 0.155 af (100% of inflow)

Center-of-Mass det. time= 0.3 min (769.1 - 768.8)

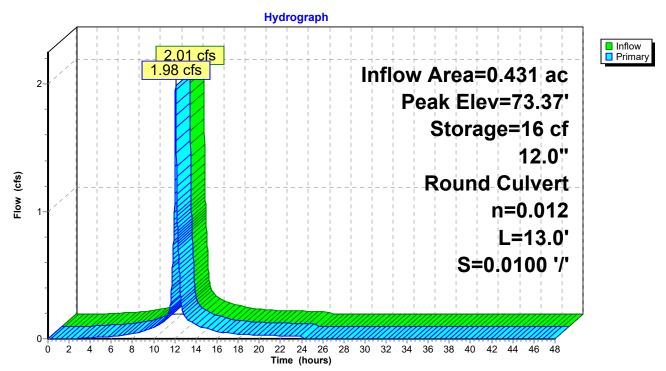
Volume	Inv	ert Avail.Sto	orage	Storage D	escription	
#1	72.	13'	66 cf	Custom S	tage Data (Pr	rismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)	Inc. (cubic	Store -feet)	Cum.Store (cubic-feet)	
72.1	13	13		0	0	
74.6	35	13		33	33	
75.6	35	4		9	41	
76.0	00	136		24	66	
Device	Routing	Invert	Outle	t Devices		
#1	Primary	72.13'		Round C		

L= 13.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 72.13' / 72.00' S= 0.0100 '/' Cc= 0.900

n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=1.80 cfs @ 12.09 hrs HW=73.30' TW=73.08' (Dynamic Tailwater) 1=Culvert (Inlet Controls 1.80 cfs @ 2.29 fps)

Pond 26P: CB #1-1



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Summary for Pond 27P: DMH #1

Inflow Area = 3.125 ac, 24.60% Impervious, Inflow Depth = 2.85" for 10-Year event

Inflow = 8.36 cfs @ 12.10 hrs, Volume= 0.742 af

Outflow = 8.36 cfs @ 12.10 hrs, Volume= 0.742 af, Atten= 0%, Lag= 0.1 min

Primary = 8.36 cfs @ 12.10 hrs, Volume= 0.742 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Peak Elev= 73.12' @ 12.10 hrs Surf.Area= 13 sf Storage= 22 cf

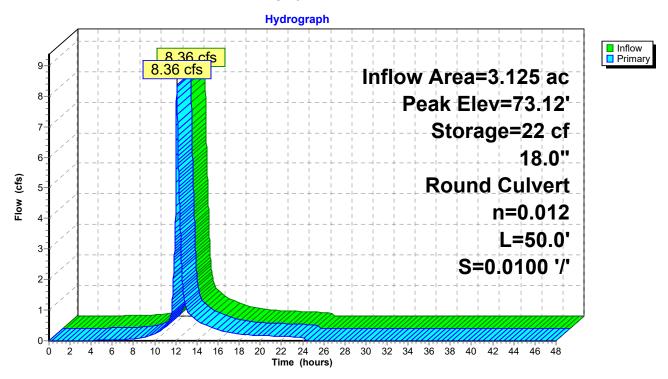
Plug-Flow detention time= 0.1 min calculated for 0.741 af (100% of inflow)

Center-of-Mass det. time= 0.1 min (816.3 - 816.1)

Volume	In	vert Avail.Sto	orage Storag	je Description						
#1	71	.40'	56 cf Custo	m Stage Data (P	rismatic)Listed below (Recalc)					
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)						
71.4	40	13	0	0						
75.05		13	47	47						
76.0	05	4	9	56						
Device	Routing	g Invert	Outlet Device	ces						
#1	Primary	/ 71.40'	18.0" Rour	18.0" Round Culvert						
			L= 50.0' C	L= 50.0' CPP, square edge headwall, Ke= 0.500						
			Inlet / Outle	Inlet / Outlet Invert= 71.40' / 70.90' S= 0.0100 '/' Cc= 0.900						
	n= 0.012, Flow Area= 1.77 sf									

Primary OutFlow Max=8.35 cfs @ 12.10 hrs HW=73.11' TW=58.29' (Dynamic Tailwater) 1=Culvert (Inlet Controls 8.35 cfs @ 4.73 fps)

Pond 27P: DMH #1



Printed 7/1/2021

Summary for Pond 29P: GUSF #2

Inflow Area = 5.652 ac, 21.73% Impervious, Inflow Depth = 2.79" for 10-Year event

Inflow = 16.00 cfs @ 12.10 hrs, Volume= 1.314 af

Outflow = 7.85 cfs @ 12.34 hrs, Volume= 1.270 af, Atten= 51%, Lag= 14.4 min

Primary = 7.85 cfs @ 12.34 hrs, Volume= 1.270 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Starting Elev= 56.50' Surf.Area= 5,832 sf Storage= 7,395 cf

Peak Elev= 58.66' @ 12.34 hrs Surf.Area= 9,986 sf Storage= 24,031 cf (16,636 cf above start)

Flood Elev= 60.00' Surf.Area= 13,062 sf Storage= 39,412 cf (32,017 cf above start)

Plug-Flow detention time= 225.4 min calculated for 1.100 af (84% of inflow)

Center-of-Mass det. time= 121.5 min (935.6 - 814.1)

Volume	Inve	rt Ava	il.Storag	ge Storage Description					
#1	53.00)'	39,412	cf Custom Stage Data (Prismatic)Listed below (Recalc)					
- 14:		D	17.51.	Les Oters Oters					
Elevation		Surf.Area	Voids	Inc.Store Cum.Store					
(fee		(sq-ft)	(%)	(cubic-feet) (cubic-feet)					
53.0		5,682	0.0	0 0					
54.5		5,682	40.0	3,409 3,409					
55.0		5,682	40.0	1,136 4,546					
56.5		5,832	33.0	2,850 7,395					
57.0		6,496	100.0	3,082 10,477					
57.2		6,886	100.0	1,673 12,150					
57.3		6,974	100.0	346 12,497					
57.3		7,061	100.0	351 12,847					
57.5		7,354	100.0	1,081 13,929					
58.0		8,503	100.0	3,964 17,893					
59.0		10,737	100.0	9,620 27,513					
60.0	00	13,062	100.0	11,900 39,412					
Device	Routing	In	vert O	Outlet Devices					
#1	Primary	53	3.50' 1 8	8.0" Round Culvert					
	•		L:	.= 25.0' CPP, square edge headwall, Ke= 0.500					
				nlet / Outlet Invert= 53.50' / 53.25' S= 0.0100 '/' Cc= 0.900					
				= 0.012, Flow Area= 1.77 sf					
#2	Device 1	53	3.50' 6 .	6.0" Vert. Orifice/Grate C= 0.600					
#3	Device 1	57	'.30' 3 :	3.0" W x 5.0" H Vert. Orifice/Grate C= 0.600					
#4	Device 1	58	3.35' 3 0	36.0" W x 6.0" H Vert. Orifice/Grate C= 0.600					
#5	Device 1	58	.85' 4 8	48.0" x 48.0" Horiz. Orifice/Grate C= 0.600					
				imited to weir flow at low heads					
#6	Device 2	56	5.50' 2 .	0' 2.410 in/hr Exfiltration over Surface area above 56.50'					
			E:	Excluded Surface area = 5,832 sf Phase-In= 0.01'					
#7	Primary	59		.0' long x 6.0' breadth Broad-Crested Rectangular Weir					
	•		Н	lead (feet)	2.00				
				2.50 3.00 3.50 4.00 4.50 5.00 5.50					
			_	(=)					

Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65

2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83

Primary OutFlow Max=7.85 cfs @ 12.34 hrs HW=58.66' TW=0.00' (Dynamic Tailwater)

1=Culvert (Passes 7.85 cfs of 17.88 cfs potential flow)

2=Orifice/Grate (Passes 0.23 cfs of 2.10 cfs potential flow)

6=Exfiltration (Exfiltration Controls 0.23 cfs)

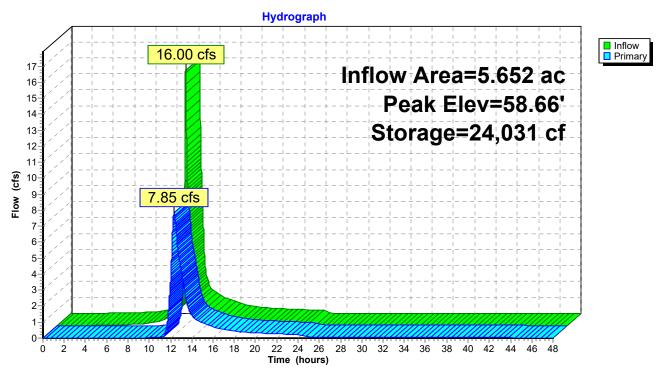
3=Orifice/Grate (Orifice Controls 5.92 cfs @ 5.17 fps)

4=Orifice/Grate (Orifice Controls 1.69 cfs @ 1.80 fps)

5=Orifice/Grate (Controls 0.00 cfs)

7=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 29P: GUSF #2



Summary for Link 100L: POA #1

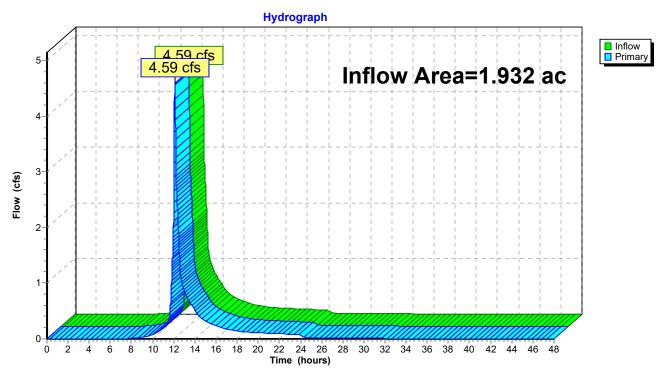
Inflow Area = 1.932 ac, 13.66% Impervious, Inflow Depth = 2.73" for 10-Year event

Inflow = 4.59 cfs @ 12.11 hrs, Volume= 0.439 af

Primary = 4.59 cfs @ 12.11 hrs, Volume= 0.439 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Link 100L: POA #1



Summary for Link 200L: POA #2

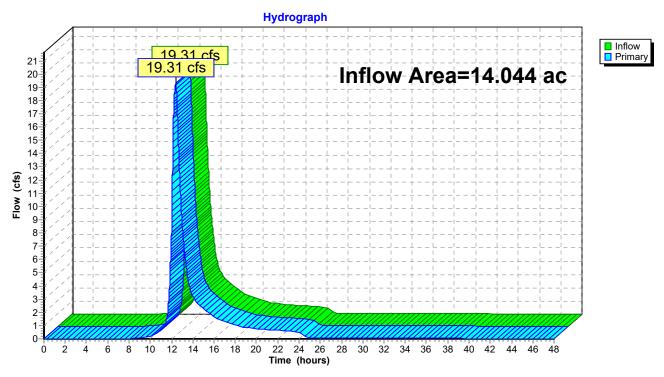
Inflow Area = 14.044 ac, 11.39% Impervious, Inflow Depth > 2.50" for 10-Year event

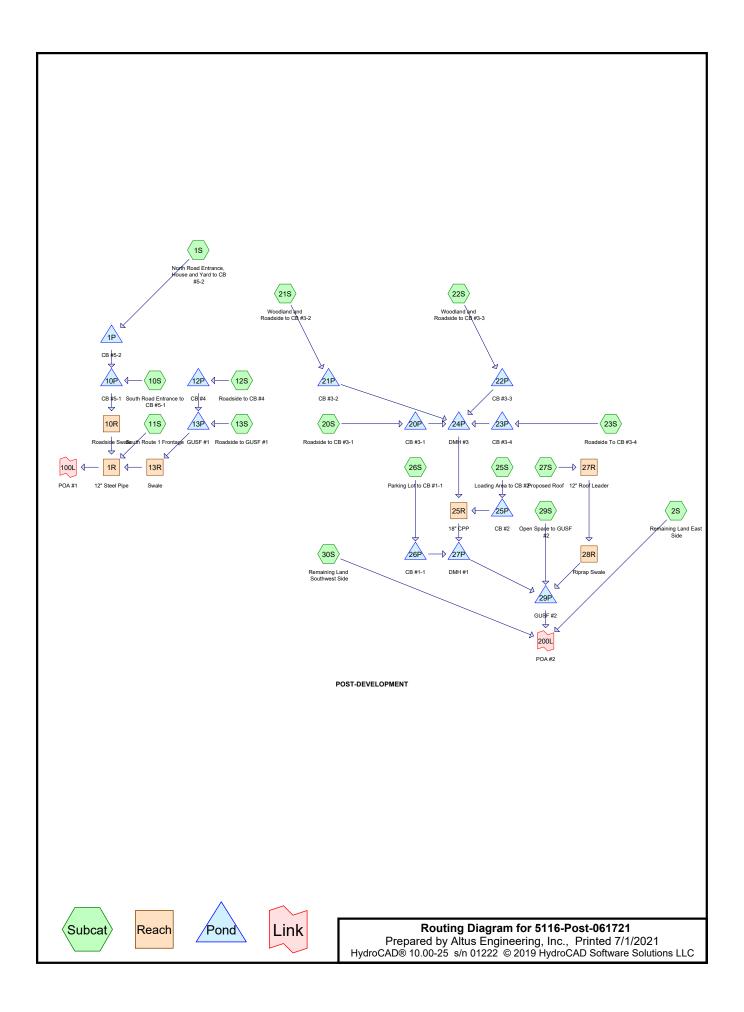
Inflow = 19.31 cfs @ 12.39 hrs, Volume= 2.926 af

Primary = 19.31 cfs @ 12.39 hrs, Volume= 2.926 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Link 200L: POA #2





Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: North Road Entrance, Runoff Area=51,236 sf 8.13% Impervious Runoff Depth=3.65" Flow Length=432' Tc=6.3 min CN=77 Runoff=4.99 cfs 0.358 af

Subcatchment 2S: Remaining Land East Runoff Area=279,061 sf 0.00% Impervious Runoff Depth=3.26" Flow Length=1,208' Tc=32.9 min CN=73 Runoff=13.25 cfs 1.738 af

Subcatchment 10S: South Road Entrance to Runoff Area=3,377 sf 82.44% Impervious Runoff Depth=5.61" Flow Length=139' Tc=6.0 min CN=95 Runoff=0.46 cfs 0.036 af

Subcatchment 11S: South Route 1 Frontage Runoff Area=6,211 sf 0.00% Impervious Runoff Depth=3.96" Flow Length=166' Tc=6.0 min CN=80 Runoff=0.66 cfs 0.047 af

Subcatchment 12S: Roadside to CB #4 Runoff Area=9,746 sf 23.27% Impervious Runoff Depth=4.07" Flow Length=282' Tc=9.6 min CN=81 Runoff=0.94 cfs 0.076 af

Subcatchment 13S: Roadside to GUSF #1 Runoff Area=13,602 sf 16.81% Impervious Runoff Depth=4.07" Flow Length=264' Tc=6.0 min CN=81 Runoff=1.48 cfs 0.106 af

Subcatchment 20S: Roadside to CB #3-1 Runoff Area=11,105 sf 40.77% Impervious Runoff Depth=4.71" Flow Length=390' Tc=6.0 min CN=87 Runoff=1.36 cfs 0.100 af

Subcatchment 21S: Woodland and

Runoff Area=40,322 sf 6.67% Impervious Runoff Depth=3.65"
Flow Length=338' Tc=6.5 min CN=77 Runoff=3.89 cfs 0.282 af

Subcatchment 22S: Woodland and

Runoff Area=53,034 sf 6.79% Impervious Runoff Depth=3.35"
Flow Length=408' Tc=16.0 min CN=74 Runoff=3.53 cfs 0.340 af

Subcatchment 23S: Roadside To CB #3-4 Runoff Area=8,495 sf 25.20% Impervious Runoff Depth=3.96" Flow Length=150' Tc=6.0 min CN=80 Runoff=0.90 cfs 0.064 af

Subcatchment 25S: Loading Area to CB #2 Runoff Area=4,411 sf 100.00% Impervious Runoff Depth=5.96" Flow Length=137' Tc=6.0 min CN=98 Runoff=0.62 cfs 0.050 af

Subcatchment 26S: Parking Lot to CB #1-1 Runoff Area=18,776 sf 85.85% Impervious Runoff Depth=5.61" Flow Length=332' Tc=6.0 min CN=95 Runoff=2.57 cfs 0.202 af

Subcatchment 27S: Proposed Roof

Runoff Area=20,000 sf 100.00% Impervious Runoff Depth=5.96"

Tc=6.0 min CN=98 Runoff=2.79 cfs 0.228 af

Subcatchment 29S: Open Space to GUSF #2 Runoff Area=90,054 sf 0.00% Impervious Runoff Depth=3.35" Flow Length=457' Tc=6.0 min CN=74 Runoff=8.13 cfs 0.578 af

Subcatchment 30S: Remaining Land

Runoff Area=86,511 sf 18.73% Impervious Runoff Depth=4.07"

Flow Length=760' Tc=12.0 min CN=81 Runoff=7.73 cfs 0.673 af

Reach 1R: 12" Steel PipeAvg. Flow Depth=0.82' Max Vel=9.56 fps Inflow=6.59 cfs 0.623 af 12.0" Round Pipe n=0.012 L=45.0' S=0.0291 '/' Capacity=6.59 cfs Outflow=6.61 cfs 0.623 af

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Reach 10R: Roadside Swale	Avg. Flow Depth=0.56' Max Vel=2.61 fps Inflow=5.74 cfs 0.394 af n=0.030 L=98.0' S=0.0104 '/' Capacity=17.99 cfs Outflow=5.39 cfs 0.394 af
Reach 13R: Swale	Avg. Flow Depth=0.18' Max Vel=2.80 fps Inflow=1.19 cfs 0.181 af n=0.030 L=41.0' S=0.0395 '/' Capacity=28.58 cfs Outflow=1.19 cfs 0.181 af
Reach 25R: 18" CPP 18.0" Round Pipe	Avg. Flow Depth=0.85' Max Vel=8.93 fps Inflow=9.17 cfs 0.837 af n=0.012 L=83.0' S=0.0175 '/' Capacity=15.04 cfs Outflow=9.16 cfs 0.837 af
Reach 27R: 12" Roof Leader 12.0" Round Pipe	Avg. Flow Depth=0.63' Max Vel=5.34 fps Inflow=2.79 cfs 0.228 af n=0.012 L=300.0' S=0.0100 '/' Capacity=3.86 cfs Outflow=2.76 cfs 0.228 af
Reach 28R: Riprap Swale	Avg. Flow Depth=0.31' Max Vel=3.46 fps Inflow=2.76 cfs 0.228 af n=0.069 L=108.0' S=0.1759 '/' Capacity=26.22 cfs Outflow=2.75 cfs 0.228 af
Pond 1P: CB #5-2	Peak Elev=82.27' Storage=110 cf Inflow=4.99 cfs 0.358 af 12.0" Round Culvert n=0.012 L=52.0' S=0.0050 '/' Outflow=5.69 cfs 0.358 af
Pond 10P: CB #5-1	Peak Elev=80.00' Storage=65 cf Inflow=6.15 cfs 0.394 af 12.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=5.74 cfs 0.394 af
Pond 12P: CB #4	Peak Elev=86.23' Storage=51 cf Inflow=0.94 cfs 0.076 af 12.0" Round Culvert n=0.120 L=50.0' S=0.0050 '/' Outflow=0.97 cfs 0.076 af
Pond 13P: GUSF #1	Peak Elev=83.25' Storage=2,968 cf Inflow=2.34 cfs 0.182 af Outflow=1.19 cfs 0.181 af
Pond 20P: CB #3-1	Peak Elev=77.86' Storage=19 cf Inflow=1.36 cfs 0.100 af 15.0" Round Culvert n=0.012 L=8.0' S=0.0100 '/' Outflow=1.34 cfs 0.100 af
Pond 21P: CB #3-2	Peak Elev=85.21' Storage=20 cf Inflow=3.89 cfs 0.282 af 12.0" Round Culvert n=0.012 L=142.0' S=0.0500 '/' Outflow=3.89 cfs 0.282 af
Pond 22P: CB #3-3	Peak Elev=80.37' Storage=18 cf Inflow=3.53 cfs 0.340 af 12.0" Round Culvert n=0.012 L=68.0' S=0.0360 '/' Outflow=3.53 cfs 0.340 af
Pond 23P: CB #3-4	Peak Elev=77.90' Storage=12 cf Inflow=0.90 cfs 0.064 af 12.0" Round Culvert n=0.012 L=45.0' S=0.0100 '/' Outflow=0.88 cfs 0.064 af
Pond 24P: DMH #3	Peak Elev=77.82' Storage=35 cf Inflow=8.58 cfs 0.787 af 18.0" Round Culvert n=0.012 L=177.0' S=0.0175 '/' Outflow=8.58 cfs 0.787 af
Pond 25P: CB #2	Peak Elev=74.04' Storage=6 cf Inflow=0.62 cfs 0.050 af 12.0" Round Culvert n=0.012 L=36.0' S=0.0100 '/' Outflow=0.61 cfs 0.050 af
Pond 26P: CB #1-1	Peak Elev=74.43' Storage=30 cf Inflow=2.57 cfs 0.202 af 12.0" Round Culvert n=0.012 L=13.0' S=0.0100 '/' Outflow=2.53 cfs 0.202 af
Pond 27P: DMH #1	Peak Elev=74.01' Storage=34 cf Inflow=11.62 cfs 1.038 af 18.0" Round Culvert n=0.012 L=50.0' S=0.0100 '/' Outflow=11.62 cfs 1.038 af
Pond 29P: GUSF #2	Peak Elev=58.98' Storage=27,340 cf Inflow=22.42 cfs 1.844 af Outflow=13.92 cfs 1.801 af

5116-Post-061721

Type III 24-hr 25-Year Rainfall=6.20"

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Link 100L: POA #1 Inflow=6.61 cfs 0.623 af

Primary=6.61 cfs 0.623 af

Link 200L: POA #2 Inflow=29.79 cfs 4.212 af

Primary=29.79 cfs 4.212 af

Total Runoff Area = 15.977 ac Runoff Volume = 4.878 af Average Runoff Depth = 3.66" 88.33% Pervious = 14.113 ac 11.67% Impervious = 1.864 ac

Section 5

Precipitation Table



APPENDIX H. 24-hour duration rainfalls for various return periods

COUNTY	Storm Type	1-YR	2- YR	5- YR	10- YR	25- YR	50- YR	100- YR	500- YR
ANDROSCOGGIN	III	2.5	3.0	3.7	4.3	5.4	6.4	7.6	11.1
AROOSTOOK C	II	1.9	2.3	2.8	3.2	3.9	4.6	5.3	7.6
(Presque Isle Area) AROOSTOOK N									
(Fort Kent Area)	II	1.9	2.2	2.7	3.1	3.7	4.3	5.0	7.0
AROOSTOOK S	II	2.1	2.5	3.0	3.4	4.1	4.7	5.4	7.5
(Houlton Area)	11	2.1	2.3	3.0	3.4	4.1	4.7	J. 4	1.5
CUMBERLAND	777	2.5	2.0	2.7	4.2	<i>5</i> 1	()	7.5	10.0
NW (Bridgton Area)	III	2.5	3.0	3.7	4.3	5.4	6.3	7.5	10.9
CUMBERLAND									
SE	III	2.6	3.1	3.9	4.6	5.8	6.9	8.1	12.1
(N Windham Area)		• •		• •			4.0		
FRANKLIN	II III	2.0 2.5	2.4 2.9	2.9	3.4 4.2	4.2 5.2	4.9	5.7 7.2	8.2
HANCOCK KENNEBEC	III	2.3	2.9	3.6 3.5	4.2	5.2 5.2	6.1 6.1	7.2	10.5 10.6
KNOX	III	2.6	3.2	3.9	4.6	5.7	6.7	7.2	11.5
LINCOLN	III	2.5	3.1	3.8	4.5	5.5	6.5	7.6	11.1
OXFORD E	II^1	2.3	2.7	3.3	3.9	4.8	5.7	6.7	9.7
(Rumford Area)		2.3	2.,	5.5	3.7	1.0	3.7	0.7	<i>7.1</i>
OXFORD W (Gilead Area)	II	2.2	2.7	3.4	4.0	4.9	5.8	6.9	10.1
PENOBSCOT N									
(Millinocket Area)	II	2.2	2.6	3.2	3.8	4.7	5.6	6.5	9.5
PENOBSCOT S	II	2.3	2.7	3.4	3.9	4.9	5.7	6.7	9.7
(Hudson Area)	11	2.3	2.7	5.4	3.7	7.7	5.7	0.7	7.1
PISCATAQUIS N (Chesuncook Area)	II	2.0	2.4	2.9	3.4	4.2	5.0	5.8	8.5
PISCATAQUIS S					• •	4.0			400
(Monson Area)	II	2.2	2.7	3.3	3.9	4.8	5.7	6.8	10.0
SAGADAHOC	III	2.6	3.2	3.9	4.6	5.7	6.7	7.8	11.4
SOMERSET N	II	2.0	2.3	2.8	3.3	4.0	4.7	5.4	7.8
(Pittston Farm Area) SOMERSET S									
(Solon Area)	II	2.3	2.7	3.4	3.9	4.9	5.7	6.7	9.8
WALDO	III	2.4	2.9	3.6	4.2	5.2	6.1	7.2	10.5
WASHINGTON	III	2.5	2.8	3.4	3.9	4.8	5.5	6.4	9.0
YORK	III	2.6	3.3	4.1	4.9	6.2	7.3	8.7	13.2

¹ Use Type III rainfall for the towns of Brownfield, Buckfield, Denmark, Hartford, Hebron, Hiram, Oxford, and Porter.

Source: Data extracted by the Maine Department of Environmental Protection from the Northeast Regional Climate Center website (http://precip.eas.cornell.edu), Extreme Precipitation Tables. Data from this website was obtained from the National Oceanic and Atmospheric Administration's Regional Climate Center Program.

June 2014

Section 6

Class A High Intensity Soil Survey Test Pit Logs



Michael Cuomo, Soil Scientist

6 York Pond Road, York, Maine 03909 207 363 4532 mcuomosoil@gmail.com

Class A

High Intensity Soil Survey Report

Tax map 67, Lot 1
US Route One
Kittery, Maine

prepared for:

Altus Engineering
133 Court Street
Portsmouth, NH 03801

Michael Chomo

17 May 2021

This report is in reference to this +/32 acre property at 514 US Route One in Kittery, Maine. In May of 2021 a class 'A' High Intensity Soil Survey of this property was completed in compliance with the standards created by the Maine Association of Professional Soil Scientists. The purpose of this soil investigation is to assist in planning a commercial development served by municipal water and sewer service. This report will explain the methods, limitations, and results of this work.

A high intensity soil survey is comprised of two components: a soil map and this report. The soil map is made by traversing the property and observing the soil at locations thought to be representative of the landform. Because soil is highly variable, it is not possible to represent every soil variation on the map. The map is a simplified two-dimensional interpretation of the complex three dimensional soil-landscape relationship. Class A standards allow for inclusions of soils other than those named in the map unit label, so long as no inclusion limiting for the proposed land use is greater than one-eighth acre in size. Boundaries between different soils are shown as lines on the soil map, but may be diffuse transition zones.

Soil names were selected using best fit with soils already researched in detail and found to occur extensively in Maine by the United States Department of Agriculture's Natural Resource Conservation Service. The map unit design and the interpretations of soil properties in this report are specific to this site and were selected considering the proposed use. Therefore, the interpretations and limitations described in this report may be insufficient for other uses. For example, soil suitability for on-site wastewater disposal was ignored in map unit design.

This soil map is based on 22 test pits dug with an excavator and two hand dug soil observations. The data for these is attached at the rear of this report, and their locations are shown on the base map. Other shallow soil observations were previously made to determine the edge of the wetland soils, but the data and locations of these were not recorded.

Hydrologic soil groups were assigned using the "HSG Triangle" developed by the University of Rhode Island.

The soil map is presented on a base plan: a two foot contour interval topographic and boundary survey with wetland flag locations prepared by Altus Engineering.

Eight different soils were mapped on the property and are described below.

Brayton (BrB)

Drainage class: poorly drained.

Parent material: basal till or loose till.

Texture range: stony fine sandy loam.

Description: see soil observation B.

Landscape position: lowland.

Landform: ground moraine.

Slope range: 0 to 8%.

Permeability: moderate in the upper layers and slow in the lower layers.

Bedrock class: moderately deep to deep.

Hydrologic soil group: D.

Saturated hydraulic conductivity: 0.0 to 0.6 in/hr in the most restrictive horizons.

Flood hazard: water ponds at the surface seasonally.

Inclusions: on this site Brayton map units represents poorly drained basal till soils which have variable bedrock depth.

Use and management: Land uses are limited by wetness close to the surface for prolonged periods of time during an average year. These are wetland soils and may not be drained or filled without permits.

Dixfield (DxB)

Drainage class: moderately well drained.

Parent material: basal till.

Texture range: stony fine sandy loam.

Description: see test pit one.

Landscape position: upland.

Landform: gently rolling.

Slope range: 0 to 8%.

Permeability: moderate in the upper layers and slow in the lower layers.

Bedrock class: very deep.

Hydrologic group: D.

Flood hazard: none.

Inclusions: test pit 5 has some horizons which are more sandy; Test pit 21 is an inclusion of the similar Marlow soil.

Use and management: land uses are slightly limited by the presence of basal till, which causes the ground water to perch after rain events and snow melt. This limitation can be overcome by appropriate grading and drainage.

Lyman-Tunbridge (LT)

Drainage class: somewhat excessively well and well drained.

Parent material: loose glacial till.

Texture range: stony fine sandy loam.

Description: Lyman is described in test pit 3 and Tunbridge in test pit 9.

Landscape position: upland.

Landform: gently rolling to steep.

Slope range: 0 to greater than 25%.

Permeability: moderately rapid.

Bedrock class: shallow and moderately deep.

Hydrologic soil group: the predominant HSG is C.

Saturated hydraulic conductivity: 0.1 to 14 in/hr in the most restrictive horizon.

Flood hazard: none.

Inclusions: This soil map unit represents upland soils with variable bedrock depth. Inclusions are the very shallow Abram soils in test pit 8; test pit 6, which has basal till over moderately deep bedrock; and few bedrock outcroppings at the surface.

Use and management: land uses are limited by bedrock 0 to 40 inches from the soil surface, which can be overcome by blasting and filling.

Nicholville (NiB)

Drainage class: somewhat poorly and moderately well drained. Parent material: lacustrine and shallow marine sediments.

Texture range: very fine sandy loam in the upper part over silt loam in the lower part.

Description: test pits 12 and 14.

Landscape position: lowland.

Landform: gently rolling to nearly level plains.

Slope range: 0 to 8%.

Permeability: moderate in the upper part and slow in the lower part.

Bedrock class: very deep.

Hydrologic group: D.

Flood hazard: none.

Inclusions: Nicholville is typically a moderately well drained soil, but on this site the name includes the extensive somewhat poorly drained variant.

Use and management: Land uses are limited by seasonal wetness close to the surface. These are not wetland soils and may be drained or filled to overcome this limitation. The Nicholville soils are highly erosive and have low bearing strength when wet.

Scantic (ScB)

Drainage class: poorly drained.

Parent material: marine.

Texture range: silt loam over silty clay loam.

Description: see test pit 16.

Landscape position: wetland.

Landform: glacial deltas, bays.

Slope range: 0 to 8%.

Permeability: slow in the upper layers and very slow in the lower layers.

Bedrock class: very deep.

Hydrologic group: D.

Flood hazard: water ponds at the surface seasonally.

Inclusions: none noted.

Use and management: Land uses are limited by frequent saturation to the surface and fine texture of the soil which makes it difficult to work in when wet. These are wetlands soils and may be not be drained or filled without permits.

Waumbek (WmB)

Drainage class: moderately well drained.

Parent material: loose glacial till.

Texture range: stony fine sandy loam over gravelly sand.

Description: see test pit 20.

Landscape position: upland.

Landform: sideslopes.

Slope range: 0 to 8%.

Permeability: moderately rapid in the upper layers and rapid in the lower layers.

Bedrock class: very deep.

Hydrologic group: D.

Flood hazard: none.

Inclusions: none noted.

Use and management: land uses are slightly limited by the presence of brief duration ground water within 2 feet of the surface. This limitation can be overcome by appropriate grading and drainage.

Westbury (WsB)

Drainage class: somewhat poorly drained.

Parent material: basal till and loose till.

Texture range: fine sandy loam to loamy sand.

Description: see test pit 4.

Landscape position: lowland.

Landform: nearly level.

Slope range: 0 to 8%.

Permeability: moderate in the upper layers and slow to rapid in

the lower layers.

Bedrock class: moderately deep to deep.

Hydrologic group: D.

Flood hazard: water will pond at the surface briefly after significant rainstorms or snow melt.

Inclusions: Though typically deep to bedrock, on this site the Westbury soils have significant area which is moderately deep to bedrock.

Use and management: land uses are limited by seasonal wetness close to the surface. These are not wetland soils and may be drained or filled to overcome this limitation.

Whately (WhB)

Drainage class: very poorly drained.

Parent material: glacial lacustrine or aeolian.

Texture range: very fine sandy loam to sand.

Description: see soil observation A.

Landscape position: wetland.

Landform: deltas, bays.

Slope range: 0 to 8%.

Permeability: moderately rapid in the upper layers and very slow in the lower layers.

Bedrock class: very deep.

Hydrologic soil group: D.

Saturated hydraulic conductivity: 0.6 to 20 in/hr.

Flood hazard: water ponds at the surface frequently.

Inclusions: none noted.

Use and management: Land uses are limited by near constant saturation to the surface and low bearing strength. These are regulated wetlands and may be not be drained or filled without permits.

Conclusion

The soils on this site are similar to those encountered elsewhere in York County. The limitations that the non-wetland soils present can be overcome by:

- 1) identifying the soils and their limitations, as has been done in this report;
- 2) engineering and designing measures such as construction sequencing, material specifications, drainage structures, grading, blasting, and erosion/sediment control in response to the limitations identified; and
- 3) implementing the designed measures properly.

The Brayton, Scantic, and Whately soils are regulated wetlands. No filling is allowed without permits. Proper erosion and sediment techniques must be employed to protect the wetlands during construction.

THIS LEGEND MUST APPEAR ON THE PLAN WHICH CONTAINS THE SOIL MAP.

High Intensity Soil Map Legend

```
BrB Brayton, 0-8% slopes*

DxB Dixfield, 0-8% slopes

LTB Lyman Tunbridge complex, 0-8% slopes

LTC Lyman Tunbridge complex, 8-15% slopes

LTD Lyman Tunbridge complex, 15-25% slopes

LTE Lyman Tunbridge complex, +25% slopes

NiB Nicholville, 0-8% slopes

ScB Scantic, 0-8% slopes

WmB Waumbek, 0-8% slopes

WhB Whately, 0-8% slopes*

WsB Westbury, 0-8% slopes
```

This soil survey complies with Class A standards as defined by the Maine Association of Professional Soil Scientists. See report dated 17 May 2021, for complete description of methods, soils, and results.

Michael Cuomo
Maine Soil Scientist #211

^{*} These are wetland soils.

Michael Cuomo, Soil Scientist

6 York Pond Road, York, Maine 03909 207 363 4532 mcuomosoil@gmail.com

TEST PIT DATA

Client: Altus Engineering

Location: 514 US Route One, Kittery

Date: 10 May 2021

Test Pit Number: 1

Description Depth 2"

Leaf litter.

Dark brown (10YR 3/3) fine sandy loam, granular, friable. 0 - 9''Dark yellowish brown (10YR 4/6) fine sandy loam, blocky, 9-24"

friable.

Light olive brown (2.5Y 5/4) fine sandy loam, blocky, friable, 24-35"

redox.

Dark olive brown (2.5Y 3/3) stony fine sandy loam, massive, 35-48"

firm, redox.

Dixfield Soil Name:

24" Depth to Seasonal High Water Table: 48"

Depth to Bedrock:

Test Pit Number: 2

Description Depth

1" Leaf litter.

Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 0-8"

Dark yellowish brown (10YR 4/6) stony fine sandy loam, blocky, 8-20"

friable.

Soil Name: Tunbridge

Depth to Seasonal High Water Table: none

Depth to Bedrock:

Test Pit Number: 3

Description Depth

2" Leaf litter.

Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 0-8"

20"

Dark yellowish brown (10YR 4/6) stony fine sandy loam, blocky, 8-18"

friable.

Lyman Soil Name: Depth to Seasonal High Water Table: none

Depth to Bedrock: 18"

Test Pit Number: 4

Description Depth

2" Leaf litter.

0-8" Dark grayish brown (2.5Y 4/2) fine sandy loam, granular,

friable.

Dark yellowish brown (10YR 4/6) fine sandy loam, blocky, 8-16"

friable, redox.

Light yellowish brown (2.5Y 6/4) fine sandy loam, blocky, firm, 16-24"

redox.

Westbury variant Soil Name:

8" Depth to Seasonal High Water Table:

24" Depth to Bedrock:

Test Pit Number: 5 Description Depth 1" Leaf litter. Yellowish brown (10YR 5/4) fine sandy loam, blocky, friable. 0-22" Dark yellowish brown (10YR 4/6) gravelly loamy sand, blocky, 22-32" friable, redox. Dark olive brown (2.5Y 3/3) gravelly sand, loose, massive, 32-44" Light olive brown (2.5Y 5/4) stony fine sandy loam, massive, 44-56" firm, redox. Dixfield Soil Name: Depth to Seasonal High Water Table: 22" 56" Depth to Bedrock: Test Pit Number: 6 Depth Description Leaf litter. Dark brown (10YR 3/3) fine sandy loam, granular, friable. 0-10" 10-24" Dark yellowish brown (10YR 4/6) fine sandy loam, blocky, friable. Light yellowish brown (2.5Y 6/4) stony fine sandy loam, massive, 24-38" firm, redox. Tunbridge variant Soil Name: 24" Depth to Seasonal High Water Table: Depth to Bedrock: 38" Test Pit Number: 7 Depth Description 1" Leaf litter. 0 - 7"Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. Yellowish brown (10YR 5/6) stony fine sandy loam, blocky, 7-18" friable. Lyman Soil Name: Depth to Seasonal High Water Table: none Depth to Bedrock: 18" Test Pit Number: 8 Depth Description 2" Leaf litter. Very dark gray (10YR 3/1) stony fine sandy loam, granular, 0-3" friable. Soil Name: Abram Depth to Seasonal High Water Table: none 3" Depth to Bedrock: Test Pit Number: 9 Description Depth 2" Leaf litter.

Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 0-6"

Yellowish brown (10YR 5/6) stony fine sandy loam, blocky, 6-27"

friable.

Tunbridge Soil Name:

Depth to Seasonal High Water Table: none 27"

Depth to Bedrock:

Test Pit Number: 10 Description Depth 2" Leaf litter. 0-6" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. Soil Name: Abram Depth to Seasonal High Water Table: none Depth to Bedrock: 6" Test Pit Number: 11 Description Depth 2" Leaf litter. 0 - 7''Dark brown (10YR 3/3) silt loam, granular, friable. 7-10" Light yellowish brown (2.5Y 6/4) silt loam, blocky, friable, redox. Pale olive (5Y 6/3) silt loam, massive, friable, redox. 10-28" 29-44" Light yellowish brown (2.5Y 6/4) fine sandy loam, massive, firm, redox. 44-96" Olive brown (2.5Y 4/4) sand, massive, loose, with strata of firm silt, redox. Soil Name: Westbury variant Depth to Seasonal High Water Table: Depth to Bedrock: none Test Pit Number: 12 Depth Description 1" Leaf litter. 0 - 7"Dark brown (10YR 3/3) silt loam, granular, friable. 7-11" Yellowish brown (10YR 5/6) silt loam, blocky, friable. 11-28" Light yellowish brown (2.5Y 6/4) silt loam, blocky, friable, redox. 28-64" Olive brown (2.5Y 4/4) sand, massive, loose, redox. 64-96" Olive brown (2.5Y 4/4) silt loam, massive, firm, redox. Soil Name: Nicholville variant Depth to Seasonal High Water Table: 11" Depth to Bedrock: none Test Pit Number: 13 Depth Description Leaf litter. 0-10" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 10-24" Strong brown (7.5YR 4/6) stony fine sandy loam, blocky, friable. Light yellowish brown (2.5Y 6/4) stony fine sandy loam, blocky, 24-32" firm, redox. Soil Name: Tunbridge variant Depth to Seasonal High Water Table: 24" Depth to Bedrock: 32" Test Pit Number: 14 Depth Description 2" Leaf litter. 0-6" Brown (10YR 4/3) fine sandy loam, granular, friable. 6-17" Yellowish brown (10YR 5/6) fine sandy loam, blocky, friable, redox. Olive brown (2.5Y 4/4) sand, massive, loose, redox. 17-24" 24-52" Light olive brown (2.5Y 5/4) stratified fine sand and silt, massive, firm, redox.

Soil Name: Nicholville

Depth to Seasonal High Water Table: 17" Depth to Bedrock: none

Test Pit Number: 15

Description

1" Leaf litter.

0-6" Brown (10YR 4/3) stony fine sandy loam, granular, friable.

Dark yellowish brown (10YR 5/6) stony fine sandy loam, blocky, 6-12"

friable.

12-18" Light yellowish brown (2.5Y 6/4) stony fine sandy loam, blocky,

friable.

Soil Name: Lyman Depth to Seasonal High Water Table: none 18"

Depth to Bedrock:

Test Pit Number: 16

Depth Description

Leaf litter. 0 - 7"Very dark gray (2.5Y 3/1) silt loam, granular, friable, redox.

7-13" Light gray (2.5Y 7/1) silt loam, blocky, friable, redox.

13-22" Olive brown (2.5Y 4/4) silt loam, blocky, firm, redox.

22-50" Olive (5Y 5/4) silty clay loam, massive, firm, redox.

Soil Name:

1"

Scantic

Depth to Seasonal High Water Table:

surface

Depth to Bedrock:

none

Test Pit Number: 17

Depth Description

2" Leaf litter.

0-5" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.

5-12" Strong brown (7.5YR 4/6) stony fine sandy loam, blocky, friable.

Soil Name:

Lyman Depth to Seasonal High Water Table: none Depth to Bedrock: 12"

Test Pit Number: 18

Depth Description

1" Leaf litter.

0 - 5Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.

5-17" Yellowish brown (10YR 5/4) fine sandy loam, blocky, friable.

Light olive brown (2.5Y 5/4) stony fine sandy loam, blocky, 17-24"

friable, redox.

24-54" Light yellowish brown (2.5Y 6/4) sand, massive, loose, redox.

Soil Name:

Waumbek

Depth to Seasonal High Water Table:

17"

Depth to Bedrock:

none

Test Pit Number: 19

Depth Description

0" Leaf litter.

0-8" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.

8-28" Dark yellowish brown (10YR 4/4) stony fine sandy loam, blocky,

friable.

Soil Name: Tunbridge

Depth to Seasonal High Water Table: none

Depth to Bedrock: 28" Test Pit Number: 20

Depth Description

0" Leaf litter.

0 - 10Dark brown (10YR 3/3) fine sandy loam, granular, friable.

10-28" Dark yellowish brown (10YR 4/4) fine sandy loam, blocky,

friable.

28-46" Light yellowish brown (2.5Y 6/4) gravelly loamy sand, massive,

28"

friable, redox.

Waumbek Soil Name:

Depth to Seasonal High Water Table:

Depth to Bedrock: 46"

Test Pit Number: 21

Depth Description

0" Leaf litter.

0-10" Very dark brown (10YR 3/3) stony fine sandy loam, granular,

friable.

10-28" Dark yellowish brown (10YR 4/6) stony fine sandy loam, blocky,

friable.

28-66" Light olive brown (2.5Y 5/4) stony fine sandy loam, massive,

firm, redox.

Soil Name: Marlow

Depth to Seasonal High Water Table: 28"

66" Depth to Bedrock:

Test Pit Number: 22

Depth Description

0" Leaf litter.

0-6" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.

6-12" Yellowish brown (10YR 5/6) stony fine sandy loam, blocky,

friable.

Soil Name: Lyman

Depth to Seasonal High Water Table: none 12"

Depth to Bedrock:

Soil Observation: A

Depth 3" Leaf litter.
0-10" Black (10YR2/1)

0-10" Black (10YR2/1) mucky peat, massive, friable, redox.

10-20" Gray (2.5Y 5/1) loamy fine sand, massive, friable, redox. 20-28" Olive gray (5Y 5/2) very fine sandy loam, massive, friable,

redox.

28-36" Gray (2.5Y 5/1) fine sand, massive, friable, redox.

36-42" Olive brown (2.5Y 4/4) very fine sandy loam, massive, firm,

redox.

Soil Name:

Whately

Depth to Seasonal High Water Table:

surface

Depth to Bedrock:

none

Soil Observation: B

<u>Depth</u> <u>Description</u> 4" Leaf litter.

0-8" Very dark gray (2.5Y 3/1) stony fine sandy loam, massive,

friable, redox.

8-14" Dark gray (2.5Y 4/1) stony fine sandy loam, massive, friable,

redox.

14-28" Light yellowish brown (2.5Y 6/3) stony fine sandy loam, massive,

friable, redox.

Soil Name: Brayton variant

Depth to Seasonal High Water Table: surface Depth to Bedrock: 28"

Section 7

NRCS Soils Report

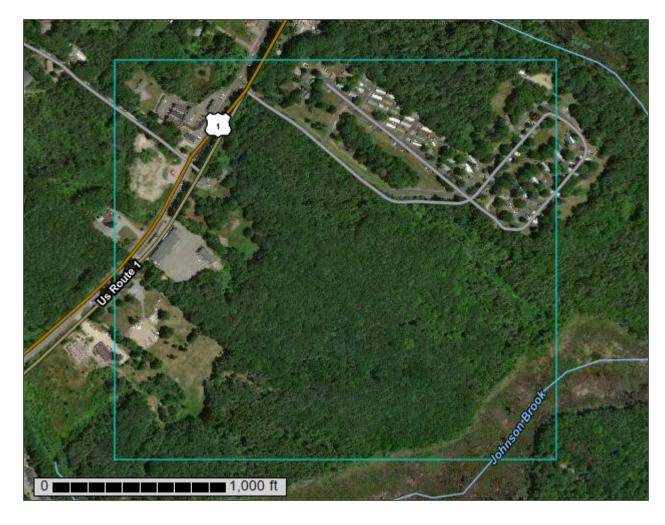




NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for York County, Maine



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Special Line Features Streams and Canals Very Stony Spot Stony Spot Spoil Area Wet Spot Other Nater Features W 8 ◁ Soil Map Unit Polygons Area of Interest (AOI) Soil Map Unit Points Soil Map Unit Lines Special Point Features Area of Interest (AOI) Blowout 9 Soils

- **Borrow Pit**
 - Clay Spot
- Closed Depression **Gravel Pit**

Interstate Highways

Rails

ŧ

Fransportation

Major Roads Local Roads

US Routes

- **Gravelly Spot**
- Lava Flow Landfill
- Marsh or swamp

Aerial Photography

3ackground

- Mine or Quarry
- Miscellaneous Water Perennial Water
 - Rock Outcrop
- Saline Spot Sandy Spot
- Severely Eroded Spot
- Sinkhole
- Slide or Slip
- Sodic Spot

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

contrasting soils that could have been shown at a more detailed Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of

Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Version 19, May 29, 2020 Soil Survey Area: York County, Maine Survey Area Data: Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Dec 31, 2009—Sep 9, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
Bm	Biddeford mucky peat, 0 to 3 percent slopes	11.1	8.2%
BrB	Brayton and Westbury fine sandy loams, 0 to 8 percent slopes	3.6	2.7%
BuB	Buxton silt loam, 3 to 8 percent slopes	1.2	0.9%
HeC	Hermon sandy loam, 8 to 15 percent slopes	21.2	15.7%
LnB	Lyman loam, 3 to 8 percent slopes, rocky	10.5	7.8%
LnC	Lyman loam, 8 to 15 percent slopes, rocky	20.0	14.8%
LnD	Lyman loam, 15 to 25 percent slopes, rocky	1.1	0.8%
LyC	Lyman-Rock outcrop complex, 8 to 15 percent slopes	1.2	0.9%
LyE	Lyman-Rock outcrop complex, 15 to 80 percent slopes	8.3	6.2%
MrB	Marlow fine sandy loam, 3 to 8 percent slopes	16.4	12.1%
MrC2	Marlow fine sandy loam, 8 to 15 percent slopes	4.7	3.5%
PeB	Peru fine sandy loam, 3 to 8 percent slopes	11.0	8.2%
Sa	Saco mucky silt loam	0.0	0.0%
Sc	Scantic silt loam, 0 to 3 percent slopes	25.0	18.5%
Totals for Area of Interest		135.1	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class.

Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The

pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

York County, Maine

Bm—Biddeford mucky peat, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2t0jn Elevation: 10 to 1,200 feet

Mean annual precipitation: 33 to 60 inches Mean annual air temperature: 39 to 45 degrees F

Frost-free period: 90 to 160 days

Farmland classification: Not prime farmland

Map Unit Composition

Biddeford and similar soils: 82 percent

Minor components: 18 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Biddeford

Setting

Landform: Marine terraces, river valleys

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip

Down-slope shape: Concave

Across-slope shape: Concave, linear

Parent material: Organic material over glaciomarine deposits

Typical profile

Oe - 0 to 12 inches: mucky peat Eg - 12 to 16 inches: silt loam Bg - 16 to 45 inches: silty clay Cg - 45 to 65 inches: clay

Properties and qualities

Slope: 0 to 3 percent

Surface area covered with cobbles, stones or boulders: 0.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 0 inches

Frequency of flooding: None Frequency of ponding: Frequent

Available water capacity: High (about 11.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: D

Ecological site: F144BY002ME - Marine Terrace Depression

Hydric soil rating: Yes

Minor Components

Scantic

Percent of map unit: 9 percent

Landform: Marine terraces, river valleys Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf

Down-slope shape: Linear Across-slope shape: Linear

Ecological site: F144BY001ME - Marine Terrace Flat

Hydric soil rating: Yes

Wonsqueak

Percent of map unit: 6 percent

Landform: Marine terraces, river valleys

Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Swanville

Percent of map unit: 2 percent

Landform: Lake plains, marine terraces Landform position (three-dimensional): Talf

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

Lamoine

Percent of map unit: 1 percent

Landform: Marine terraces, river valleys

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Rise

Down-slope shape: Linear Across-slope shape: Convex

Hydric soil rating: No

BrB—Brayton and Westbury fine sandy loams, 0 to 8 percent slopes

Map Unit Setting

National map unit symbol: 9k52 Elevation: 10 to 2,500 feet

Mean annual precipitation: 34 to 48 inches Mean annual air temperature: 37 to 46 degrees F

Frost-free period: 90 to 160 days

Farmland classification: Not prime farmland

Map Unit Composition

Brayton and similar soils: 70 percent Westbury and similar soils: 25 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Brayton

Setting

Landform: Till plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Coarse-loamy lodgment till derived from mica schist and/or

coarse-loamy lodgment till derived from gneiss

Typical profile

H1 - 0 to 8 inches: fine sandy loam H2 - 8 to 14 inches: fine sandy loam H3 - 14 to 65 inches: fine sandy loam

Properties and qualities

Slope: 0 to 8 percent

Depth to restrictive feature: 10 to 20 inches to densic material

Drainage class: Poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.60 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 3.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: D Hydric soil rating: Yes

Description of Westbury

Setting

Landform: Till plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Coarse-loamy lodgment till derived from granite and gneiss

Typical profile

H1 - 0 to 4 inches: fine sandy loam
H2 - 4 to 23 inches: fine sandy loam
H3 - 23 to 36 inches: fine sandy loam
H4 - 36 to 65 inches: sandy loam

Properties and qualities

Slope: 0 to 8 percent

Depth to restrictive feature: 13 to 24 inches to densic material

Drainage class: Somewhat poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: About 7 to 18 inches

Frequency of flooding: None

Frequency of ponding: None

Available water capacity: Very low (about 2.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: D Hydric soil rating: No

Minor Components

Skerry

Percent of map unit: 3 percent

Landform: Till plains

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Peru

Percent of map unit: 1 percent

Landform: Till plains

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Westbury, slopes >8%

Percent of map unit: 1 percent

Landform: Till plains

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

BuB—Buxton silt loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 9k54

Elevation: 10 to 900 feet

Mean annual precipitation: 34 to 48 inches Mean annual air temperature: 43 to 46 degrees F

Frost-free period: 90 to 160 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Buxton and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Buxton

Setting

Landform: Coastal plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Glaciolacustrine deposits derived from siltstone and/or fine-silty

marine deposits

Typical profile

H1 - 0 to 7 inches: silt loam H2 - 7 to 19 inches: silt loam H3 - 19 to 37 inches: silty clay H4 - 37 to 65 inches: silty clay

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: About 7 to 18 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: High (about 9.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: D Hydric soil rating: No

Minor Components

Scantic

Percent of map unit: 5 percent Landform: Coastal plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: Yes

Buxton mod well drained

Percent of map unit: 5 percent Landform: Coastal plains

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

Biddeford

Percent of map unit: 2 percent Landform: Coastal plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

Scio

Percent of map unit: 1 percent Landform: Coastal plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

Buxton, slopes >8%

Percent of map unit: 1 percent Landform: Coastal plains

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

Buxton, 0.1 to 3% stone cover

Percent of map unit: 1 percent Landform: Coastal plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

HeC—Hermon sandy loam, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2w9r9

Elevation: 0 to 980 feet

Mean annual precipitation: 31 to 65 inches Mean annual air temperature: 36 to 52 degrees F

Frost-free period: 90 to 160 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Hermon and similar soils: 90 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hermon

Setting

Landform: Hills, mountains

Landform position (two-dimensional): Backslope, summit, shoulder

Landform position (three-dimensional): Mountainbase, mountainflank, side slope,

nose slope, interfluve

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Sandy and gravelly supraglacial meltout till derived from granite

and gneiss

Typical profile

Ap - 0 to 9 inches: sandy loam

Bs1 - 9 to 16 inches: very gravelly sandy loam
Bs2 - 16 to 32 inches: extremely gravelly loamy sand
C - 32 to 65 inches: very gravelly coarse sand

Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(1.42 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: A Hydric soil rating: No

Minor Components

Monadnock

Percent of map unit: 4 percent Landform: Hills, mountains

Landform position (two-dimensional): Backslope, summit, shoulder

Landform position (three-dimensional): Mountainflank, mountainbase, side slope,

nose slope, interfluve Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Peru

Percent of map unit: 4 percent Landform: Mountains, hills

Landform position (two-dimensional): Footslope, backslope

Landform position (three-dimensional): Mountainflank, mountainbase, side slope,

nose slope, interfluve

Microfeatures of landform position: Open depressions, closed depressions, closed depressions, open depressions

Down-slope shape: Convex, concave Across-slope shape: Linear, concave

Hydric soil rating: No

Tunbridge

Percent of map unit: 1 percent Landform: Mountains, hills

Landform position (two-dimensional): Backslope, summit, shoulder

Landform position (three-dimensional): Mountainbase, mountainflank, side slope,

nose slope, interfluve Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Brayton

Percent of map unit: 1 percent Landform: Mountains, hills

Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Mountainflank, mountainbase, side slope,

nose slope, interfluve

Across-slope shape: Concave

Microfeatures of landform position: Closed depressions, open depressions, closed

depressions, open depressions Down-slope shape: Concave

Hydric soil rating: Yes

LnB—Lyman loam, 3 to 8 percent slopes, rocky

Map Unit Setting

National map unit symbol: 2trq7

Elevation: 0 to 520 feet

Mean annual precipitation: 36 to 65 inches
Mean annual air temperature: 36 to 52 degrees F

Frost-free period: 60 to 160 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Lyman, rocky, and similar soils: 86 percent

Minor components: 14 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Lyman, Rocky

Setting

Landform: Mountains, hills

Landform position (two-dimensional): Shoulder, summit, backslope

Landform position (three-dimensional): Mountaintop, mountainbase, crest, side

slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy supraglacial till derived from granite and gneiss and/or loamy supraglacial till derived from phyllite and/or loamy supraglacial till derived from mica schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loam

E - 3 to 5 inches: fine sandy loam

Bhs - 5 to 7 inches: loam Bs1 - 7 to 11 inches: loam

Bs2 - 11 to 18 inches: channery loam

R - 18 to 28 inches: bedrock

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 11 to 24 inches to lithic bedrock

Drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00

to 14.03 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: D Hydric soil rating: No

Minor Components

Tunbridge, rocky

Percent of map unit: 6 percent Landform: Hills, mountains

Landform position (two-dimensional): Backslope, summit, shoulder

Landform position (three-dimensional): Mountaintop, mountainbase, side slope,

crest

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No.

Hydric soil rating: No

Skerry, rocky

Percent of map unit: 5 percent Landform: Hills. mountains

Landform position (two-dimensional): Footslope, backslope

Landform position (three-dimensional): Mountaintop, mountainbase, crest, side

slope

Microfeatures of landform position: Closed depressions, closed depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: No

Hermon, rocky

Percent of map unit: 2 percent Landform: Hills, mountains

Landform position (two-dimensional): Backslope, summit, shoulder

Landform position (three-dimensional): Mountaintop, mountainbase, side slope,

crest

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Brayton, rocky

Percent of map unit: 1 percent Landform: Hills, mountains

Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Mountaintop, mountainbase, crest, side

slope

Microfeatures of landform position: Closed depressions, closed depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

LnC—Lyman loam, 8 to 15 percent slopes, rocky

Map Unit Setting

National map unit symbol: 2trq9

Elevation: 0 to 690 feet

Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F

Frost-free period: 60 to 160 days

Farmland classification: Not prime farmland

Map Unit Composition

Lyman, rocky, and similar soils: 86 percent

Minor components: 14 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Lyman, Rocky

Settina

Landform: Hills, mountains

Landform position (two-dimensional): Shoulder, summit, backslope Landform position (three-dimensional): Mountaintop, mountainbase,

mountainflank, crest, side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy supraglacial till derived from granite and gneiss and/or loamy supraglacial till derived from phyllite and/or loamy supraglacial till derived from mica schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loam

E - 3 to 5 inches: fine sandy loam

Bhs - 5 to 7 inches: loam

Bs1 - 7 to 11 inches: loam

Bs2 - 11 to 18 inches: channery loam

R - 18 to 28 inches: bedrock

Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: 11 to 24 inches to lithic bedrock

Drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00

to 14.03 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: D Hydric soil rating: No

Minor Components

Tunbridge, rocky

Percent of map unit: 6 percent Landform: Mountains, hills

Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Mountaintop, mountainbase,

mountainflank, side slope, crest

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

Skerry, rocky

Percent of map unit: 5 percent Landform: Hills, mountains

Landform position (two-dimensional): Footslope, backslope

Landform position (three-dimensional): Mountaintop, mountainbase,

mountainflank, crest, side slope

Microfeatures of landform position: Closed depressions, closed depressions, open

depressions, open depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: No

Hermon, rocky

Percent of map unit: 2 percent Landform: Hills, mountains

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Mountaintop, mountainbase,

mountainflank, side slope, crest

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

Brayton, rocky

Percent of map unit: 1 percent

Landform: Hills, mountains

Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Mountaintop, mountainbase,

mountainflank, crest, side slope

Microfeatures of landform position: Open depressions, open depressions, closed

depressions, closed depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

LnD—Lyman loam, 15 to 25 percent slopes, rocky

Map Unit Setting

National map unit symbol: 2trqd

Elevation: 0 to 850 feet

Mean annual precipitation: 36 to 65 inches
Mean annual air temperature: 36 to 52 degrees F

Frost-free period: 60 to 160 days

Farmland classification: Not prime farmland

Map Unit Composition

Lyman, rocky, and similar soils: 92 percent

Minor components: 8 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Lyman, Rocky

Setting

Landform: Hills, mountains

Landform position (two-dimensional): Shoulder, summit, backslope

Landform position (three-dimensional): Mountaintop, mountainflank, crest, side

slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy supraglacial till derived from granite and gneiss and/or loamy supraglacial till derived from phyllite and/or loamy supraglacial till

derived from mica schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loam

E - 3 to 5 inches: fine sandy loam

Bhs - 5 to 7 inches: loam Bs1 - 7 to 11 inches: loam

Bs2 - 11 to 18 inches: channery loam

R - 18 to 28 inches: bedrock

Properties and qualities

Slope: 15 to 25 percent

Depth to restrictive feature: 11 to 24 inches to lithic bedrock

Drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00

to 14.03 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: D Hydric soil rating: No

Minor Components

Tunbridge, rocky

Percent of map unit: 3 percent Landform: Hills, mountains

Landform position (two-dimensional): Backslope, summit, shoulder

Landform position (three-dimensional): Mountaintop, mountainflank, side slope,

crest

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Hermon, rocky

Percent of map unit: 2 percent Landform: Hills, mountains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Mountainflank, mountaintop, side slope,

crest

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Skerry, rocky

Percent of map unit: 2 percent Landform: Mountains, hills

Landform position (two-dimensional): Backslope, footslope

 $\textit{Landform position (three-dimensional):} \ \textit{Mountaintop, mountainflank, crest, side}$

slope

Microfeatures of landform position: Open depressions, open depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: No

Brayton, rocky

Percent of map unit: 1 percent Landform: Hills. mountains

Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Mountaintop, mountainflank, side slope,

Microfeatures of landform position: Open depressions, open depressions

Down-slope shape: Concave
Across-slope shape: Concave

Hydric soil rating: Yes

LyC—Lyman-Rock outcrop complex, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2trqj

Elevation: 0 to 790 feet

Mean annual precipitation: 36 to 65 inches
Mean annual air temperature: 36 to 52 degrees F

Frost-free period: 60 to 160 days

Farmland classification: Not prime farmland

Map Unit Composition

Lyman, very stony, and similar soils: 62 percent

Rock outcrop: 25 percent Minor components: 13 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Lyman, Very Stony

Setting

Landform: Hills, mountains

Landform position (two-dimensional): Shoulder, summit, backslope

Landform position (three-dimensional): Mountaintop, mountainbase, crest, side

slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy supraglacial till derived from granite and gneiss and/or loamy supraglacial till derived from phyllite and/or loamy supraglacial till derived from mica schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loam

E - 3 to 5 inches: fine sandy loam

Bhs - 5 to 7 inches: loam Bs1 - 7 to 11 inches: loam

Bs2 - 11 to 18 inches: channery loam

R - 18 to 28 inches: bedrock

Properties and qualities

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.5 percent

Depth to restrictive feature: 11 to 24 inches to lithic bedrock

Drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00

to 14.03 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D Hydric soil rating: No

Description of Rock Outcrop

Setting

Landform: Hills, mountains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Mountaintop, mountainbase, crest, side

slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Igneous and metamorphic rock

Typical profile

R - 0 to 10 inches: bedrock

Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: 0 inches to lithic bedrock

Capacity of the most limiting layer to transmit water (Ksat): Very low to very high

(0.00 to 14.17 in/hr)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: Unranked

Minor Components

Skerry, very stony

Percent of map unit: 4 percent Landform: Hills, mountains

Landform position (two-dimensional): Backslope, footslope

Landform position (three-dimensional): Mountaintop, mountainbase, crest, side

lana

slope

Microfeatures of landform position: Closed depressions, closed depressions, open

depressions, open depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: No

Hermon, very stony

Percent of map unit: 4 percent Landform: Mountains, hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Mountaintop, mountainbase, side slope,

crest

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

Tunbridge, very stony

Percent of map unit: 3 percent

Landform: Mountains, hills

Landform position (two-dimensional): Backslope, summit, shoulder

Landform position (three-dimensional): Mountaintop, mountainbase, side slope,

crest

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

Brayton, very stony

Percent of map unit: 2 percent Landform: Hills, mountains

Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Mountaintop, mountainbase, crest, side

slope

Microfeatures of landform position: Closed depressions, closed depressions, open

depressions, open depressions Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

LyE—Lyman-Rock outcrop complex, 15 to 80 percent slopes

Map Unit Setting

National map unit symbol: 2trqp

Elevation: 0 to 980 feet

Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F

Frost-free period: 60 to 160 days

Farmland classification: Not prime farmland

Map Unit Composition

Lyman, very stony, and similar soils: 60 percent

Rock outcrop: 30 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Lyman, Very Stony

Setting

Landform: Mountains, hills

Landform position (two-dimensional): Shoulder, summit, backslope

Landform position (three-dimensional): Mountaintop, mountainflank, crest, side

slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy supraglacial till derived from granite and gneiss and/or loamy supraglacial till derived from phyllite and/or loamy supraglacial till

derived from mica schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loam

E - 3 to 5 inches: fine sandy loam

Bhs - 5 to 7 inches: loam Bs1 - 7 to 11 inches: loam

Bs2 - 11 to 18 inches: channery loam

R - 18 to 28 inches: bedrock

Properties and qualities

Slope: 15 to 80 percent

Surface area covered with cobbles, stones or boulders: 1.5 percent

Depth to restrictive feature: 11 to 24 inches to lithic bedrock

Drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00

to 14.03 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D Hydric soil rating: No

Description of Rock Outcrop

Setting

Landform: Hills, mountains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Mountaintop, mountainflank, crest, side

slope, free face

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Igneous and metamorphic rock

Typical profile

R - 0 to 10 inches: bedrock

Properties and qualities

Slope: 15 to 80 percent

Depth to restrictive feature: 0 inches to lithic bedrock

Capacity of the most limiting layer to transmit water (Ksat): Very low to very high

(0.00 to 14.17 in/hr)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: Unranked

Minor Components

Tunbridge, very stony

Percent of map unit: 4 percent Landform: Hills, mountains

Landform position (two-dimensional): Backslope, summit, shoulder

Landform position (three-dimensional): Mountaintop, mountainflank, side slope, crest

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

Hermon, very stony

Percent of map unit: 3 percent Landform: Mountains, hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Mountaintop, mountainflank, side slope,

crest

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Skerry, very stony

Percent of map unit: 2 percent Landform: Mountains, hills

Landform position (two-dimensional): Backslope, footslope

Landform position (three-dimensional): Mountaintop, mountainflank, crest, side

slope

Microfeatures of landform position: Open depressions, open depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: No

Brayton, very stony

Percent of map unit: 1 percent Landform: Hills, mountains

Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Mountaintop, mountainflank, crest, side

slope

Microfeatures of landform position: Open depressions, open depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

MrB—Marlow fine sandy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2ty5d

Elevation: 0 to 690 feet

Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F

Frost-free period: 90 to 160 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Marlow and similar soils: 87 percent Minor components: 13 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Marlow

Setting

Landform: Mountains, hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Mountainbase, side slope, nose slope,

interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy lodgment till derived from granite and/or loamy lodgment till derived from mica schist and/or loamy lodgment till derived from phyllite

Typical profile

Ap - 0 to 4 inches: fine sandy loam E - 4 to 6 inches: fine sandy loam Bs1 - 6 to 10 inches: fine sandy loam Bs2 - 10 to 15 inches: fine sandy loam Bs3 - 15 to 20 inches: fine sandy loam BC - 20 to 24 inches: fine sandy loam Cd - 24 to 65 inches: fine sandy loam

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 20 to 39 inches to densic material

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.01 to 1.42 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C Hydric soil rating: No

Minor Components

Peru

Percent of map unit: 6 percent Landform: Hills. mountains

Landform position (two-dimensional): Footslope, backslope

Landform position (three-dimensional): Mountainbase, side slope, nose slope,

interfluve

Microfeatures of landform position: Closed depressions, closed depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: No

Tunbridge

Percent of map unit: 4 percent Landform: Mountains, hills

Landform position (two-dimensional): Backslope, summit, shoulder

Landform position (three-dimensional): Mountainbase, side slope, nose slope,

interfluve

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Brayton

Percent of map unit: 2 percent Landform: Hills, mountains

Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Mountainbase, side slope, nose slope,

interfluve

Microfeatures of landform position: Closed depressions, closed depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Colonel

Percent of map unit: 1 percent Landform: Hills, mountains

Landform position (two-dimensional): Footslope

Landform position (three-dimensional): Mountainbase, side slope, nose slope,

interfluve

Microfeatures of landform position: Closed depressions, closed depressions

Down-slope shape: Linear Across-slope shape: Concave

Hydric soil rating: No

MrC2—Marlow fine sandy loam, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2ty5g

Elevation: 0 to 820 feet

Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F

Frost-free period: 90 to 160 days

Farmland classification: Not prime farmland

Map Unit Composition

Marlow and similar soils: 88 percent Minor components: 12 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Marlow

Setting

Landform: Hills, mountains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Mountainbase, mountainflank, side slope,

nose slope, interfluve

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Loamy lodgment till derived from granite and/or loamy lodgment till derived from mica schist and/or loamy lodgment till derived from phyllite

Typical profile

Ap - 0 to 4 inches: fine sandy loam E - 4 to 6 inches: fine sandy loam Bs1 - 6 to 10 inches: fine sandy loam Bs2 - 10 to 15 inches: fine sandy loam Bs3 - 15 to 20 inches: fine sandy loam BC - 20 to 24 inches: fine sandy loam Cd - 24 to 65 inches: fine sandy loam

Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: 20 to 39 inches to densic material

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.01 to 1.42 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: C Hydric soil rating: No

Minor Components

Tunbridge

Percent of map unit: 5 percent Landform: Hills, mountains

Landform position (two-dimensional): Backslope, summit, shoulder

Landform position (three-dimensional): Mountainbase, mountainflank, side slope,

nose slope, interfluve Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Peru

Percent of map unit: 5 percent Landform: Hills, mountains

Landform position (two-dimensional): Footslope, backslope

Landform position (three-dimensional): Mountainbase, mountainflank, side slope, nose slope, interfluve

Microfeatures of landform position: Closed depressions, closed depressions, open

depressions, open depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: No

Brayton

Percent of map unit: 2 percent Landform: Mountains, hills

Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Mountainbase, mountainflank, side slope,

nose slope, interfluve

Microfeatures of landform position: Open depressions, open depressions, closed

depressions, closed depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

PeB—Peru fine sandy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2ty5x

Elevation: 0 to 720 feet

Mean annual precipitation: 36 to 65 inches Mean annual air temperature: 36 to 52 degrees F

Frost-free period: 90 to 160 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Peru and similar soils: 88 percent Minor components: 12 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Peru

Setting

Landform: Hills, mountains

Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Mountainbase, interfluve

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Loamy lodgment till derived from granite and/or loamy lodgment till derived from mica schist and/or loamy lodgment till derived from phyllite

Typical profile

Ap - 0 to 6 inches: fine sandy loam Bhs - 6 to 8 inches: fine sandy loam Bs1 - 8 to 12 inches: fine sandy loam

Bs2 - 12 to 18 inches: fine sandy loam Bs3 - 18 to 21 inches: fine sandy loam BC - 21 to 24 inches: fine sandy loam Cd - 24 to 65 inches: sandy loam

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 20 to 39 inches to densic material

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.01 to 1.42 in/hr)

Depth to water table: About 16 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C/D Hydric soil rating: No

Minor Components

Brayton

Percent of map unit: 5 percent Landform: Hills, mountains

Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Mountainbase, interfluve

Microfeatures of landform position: Closed depressions, closed depressions

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

Sunapee

Percent of map unit: 3 percent Landform: Hills, mountains

Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Mountainbase, interfluve

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Marlow

Percent of map unit: 3 percent Landform: Hills, mountains

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Mountainbase, interfluve

Microfeatures of landform position: Rises, rises

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Colonel

Percent of map unit: 1 percent Landform: Hills, mountains

Landform position (two-dimensional): Footslope

Landform position (three-dimensional): Mountainbase, interfluve

Microfeatures of landform position: Closed depressions, closed depressions

Down-slope shape: Linear, concave Across-slope shape: Concave

Hydric soil rating: No

Sa—Saco mucky silt loam

Map Unit Setting

National map unit symbol: 9k6j Elevation: 10 to 2,000 feet

Mean annual precipitation: 34 to 48 inches Mean annual air temperature: 37 to 46 degrees F

Frost-free period: 80 to 160 days

Farmland classification: Not prime farmland

Map Unit Composition

Saco and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Saco

Setting

Landform: Flood plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Coarse-silty alluvium

Typical profile

H1 - 0 to 13 inches: mucky silt loam H2 - 13 to 24 inches: silt loam

H3 - 24 to 65 inches: very fine sandy loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 2.00 in/hr)

Depth to water table: About 0 to 6 inches Frequency of flooding: FrequentNone

Frequency of ponding: None

Available water capacity: Very high (about 16.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6w

Hydrologic Soil Group: B/D Hydric soil rating: Yes

Minor Components

Rumney

Percent of map unit: 8 percent

Landform: Flood plains

Landform position (two-dimensional): Summit Landform position (three-dimensional): Rise

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: Yes

Chocorua

Percent of map unit: 7 percent

Landform: Bogs Hydric soil rating: Yes

Sc—Scantic silt loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2slv3

Elevation: 10 to 900 feet

Mean annual precipitation: 33 to 60 inches Mean annual air temperature: 39 to 45 degrees F

Frost-free period: 90 to 160 days

Farmland classification: Not prime farmland

Map Unit Composition

Scantic and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Scantic

Setting

Landform: Marine terraces, river valleys Landform position (three-dimensional): Talf

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Glaciomarine deposits

Typical profile

Ap - 0 to 9 inches: silt loam

Bg1 - 9 to 16 inches: silty clay loam Bg2 - 16 to 29 inches: silty clay Cg - 29 to 65 inches: silty clay

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Moderate (about 6.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: D Hydric soil rating: Yes

Minor Components

Lamoine

Percent of map unit: 8 percent

Landform: River valleys, marine terraces

Landform position (three-dimensional): Riser, rise

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Biddeford

Percent of map unit: 3 percent

Landform: Marine terraces, river valleys

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip

Down-slope shape: Concave

Across-slope shape: Concave, linear

Ecological site: F144BY002ME - Marine Terrace Depression

Hydric soil rating: Yes

Buxton

Percent of map unit: 2 percent

Landform: Marine terraces, river valleys

Landform position (three-dimensional): Riser, rise

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Roundabout

Percent of map unit: 2 percent

Landform: River valleys, marine terraces

Landform position (three-dimensional): Tread, talf

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

Section 8

BMP Sizing Calculations Riprap Calculations



BMP Water Quality Volume (WQV) Calculations

BMP: Grassed Underdrained Soil Filter #1 (Pond 13P)

	Area (sf)	Ratio (in/sf)	WQV (cf)	
Impervious	4554	1	380 c	f
Landscape	8462	0.4	282 c	f
25% Pretreatme	ent Credit		-165 c	f
Total W	QV Required:		496 c	f
Available Storag	ge (cf):			
			c	f
Surface to Lowe	est Outlet:		525 c	f
Total Stora	age Provided:		525 c	f
	Su	irplus/Deficit:	29 c	f
Filter Area:		% Area Req.		
Impervious	4554	5%	228 s	f
Landscape	8462	2%	169 s	f
Total Filter A	rea Required:		397 s	f
Filter A	rea Provided:		464 s	f
	Su	rplus/Deficit:	67 s	f



BMP Water Quality Volume (WQV) Calculations

BMP: Grassed Underdrained Soil Filter #1 (Pond 13P)

	Area (sf)	Ratio (in/sf)	WQV (cf)	
Impervious	4554	1	380 c	f
Landscape	8462	0.4	282 c	f
25% Pretreatme	ent Credit		-165 c	f
Total W	QV Required:		496 c	f
Available Storag	ge (cf):			
			c	f
Surface to Lowe	est Outlet:		525 c	f
Total Stora	age Provided:		525 c	f
	Su	irplus/Deficit:	29 c	f
Filter Area:		% Area Req.		
Impervious	4554	5%	228 s	f
Landscape	8462	2%	169 s	f
Total Filter A	rea Required:		397 s	f
Filter A	rea Provided:		464 s	f
	Su	rplus/Deficit:	67 s	f



				LCULAT				
Location	: CB #5-1,	12" Culvert	(HydroCA	AD Pond #1	10P)			
Date:	6/29/2021	By:	EBS					
T		1 7	61.1.1					
La T	Apron Leng		Calculated					
Tw	Tailwater,	r Storm, CFS	0.5 3.78					
Q D50	Median Sto		Calculated					
D30 D	Depth of St		Calculated					
Do	Pipe Diame		1.00					
W1	Width @ St		Calculated					
W2	Width @ E		Calculated					
W	Width of C		2					
XX/1								
W1:	3(Do)=		2	Ft.				
	3(D0)-		3	11.	Wid	th @ C4arr4	2	174
					wia	th @ Start:	<u> </u>	Ft.
D.C.0	0.02(0)4/3			D.50	0.22	Ε.		
D50:	$0.02(Q)^{4/3}$			D50=	0.23	Ft.		
	Tw(Do)			or	2.8	In		
				or	2.0	111.		
					Median	Stone Size:	6	In.
					1v1culul	Stone Size.		1110
D:	2.25*D50				Denth	of Riprap:	14	In.
D.	2.23 D30				Бери	or Kiprap.	17	111.
La:	If Tw<= Do	/2:		Do/2=	0.5	Ft.		
		La=1.8Q/Do ^{3/2}	+ 7Do	Tw=	0.5	Ft.		
	and	W2=width of c						
		or						
		W2=3Do+La						
	If Tw>Do/2							
		La=3Q/Do ^{3/2} +						
		W2=width of c	hannel		_			
	and		ĺ	1	Length	of Apron:		Ft.
	and	or						
	and	or W2=3Do+0.4I	La			lth @ End:	2	Ft.
	and		∟a			Ith @ End:	2	Ft.
	and		La			Ith @ End:	2	Ft.
	and		a			Ith @ End:	2	Ft.
A 17T	and		a			Ith @ End:	2	Ft.

		<u>R</u>]	IPRAP CA	LCULATI	<u>IONS</u>			
Locatio	on: CB #4, 12	 ! Culvert (I	IvdroCAD	 Pond #12	D)			
Locatio	л. С Б # 4 , 12	Cuivert (1	IyuIUCAD	1 Ullu #12	· <i>)</i>			
Date:	12/31/2020	By:	EBS					
Date.	12/31/2020	By.	EDS					
La	Apron Leng	th. Ft.	Calculated					
Tw	Tailwater,		0.5					
Q		r Storm, CFS	0.65					
D50	Median Stor		Calculated					
D	Depth of Sto	one, In	Calculated					
Do	Pipe Diame		1.00					
W1	Width @ St		Calculated					
W2	Width @ E1		Calculated					
W	Width of C	hannel	2]				
W1:								
** 1.	3(Do)=		3	Ft.				
	3(50)		3	1	Wide	th @ Start:	2	Ft.
					vv iu	ın w start:	3	r t.
D50	0.02(0)4/3			D50	0.02	Ε.		
D50:	$0.02(Q)^{4/3}$			D50=	0.02	Ft.		
	Tw(Do)				0.3	In		
				or	0.3	111.		
					Modian	Stone Size:	6	In.
					Miculan	Stolle Size.	- 0	111.
D:	2.25*D50				Donth	of Riprap:	1/	In.
D:	2.23 D30				Deptii	or Kiprap.	14	111.
La:	If Tw<= Do	/2:		Do/2=	0.5	Ft		
_ _u.	11 IW \ DO	La=1.8Q/Do ^{3/2}	± 7D°	Tw=	0.5			
	and	W2=width of c		1 W=	0.3	I't.		
	anu	or	mannici					
		W2=3Do+La						
		2 230 24						
	If Tw>Do/2	:						
		La=3Q/Do ^{3/2} +	7Do					
	and	W2=width of c						
		or	·		Length	of Apron:	Q	Ft.
		W2=3Do+0.4L	а		WIC	lth @ End:		Ft.
		· -						
					i .	1		1
A T'	LIC	_						

				LCULATI				
Location	: GUSF #1	, 12" Culver	t (HydroC	AD Pond #	(13P)			
		_						
Date:	12/31/2020	By:	EBS					
La	Apron Leng	rth Et	Calculated					
Tw	Tailwater,		0.5					
Q		r Storm, CFS	0.63					
D50	Median Sto		Calculated					
D	Depth of St		Calculated					
Do	Pipe Diamo		1.00					
W1	Width @ St		Calculated					
W2	Width @ E1	nd, Ft	Calculated					
W	Width of C	hannel	2					
W1:								
** 1.	3(Do)=		3	Ft.				
	, ,				Widt	th @ Start:	3	Ft.
					,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			- **
	4/2							
D50:	$0.02(Q)^{4/3}$			D50=	0.02	Ft.		
	Tw(Do)				0.2			
				or	0.3	In.		
					Modian	Stone Size:	6	In.
					Mcuiaii	Stolle Size.	0	111.
D:	2.25*D50				Denth	of Riprap:	14	In.
<u>. </u>	2.23 230				Бери	оттартарт		
т	ICT C D	/2		D /2	0.5	Ε.		
La:	If Tw<= Do		- 7D	Do/2=	0.5			
	1	La=1.8Q/Do ^{3/2}		Tw=	0.5	Ft.		
	and	W2=width of c	nannei					
		or W2=3Do+La						
		** 2-3D0+La						
	If Tw>Do/2	!:						
		La=3Q/Do ^{3/2} +	· 7Do					
	and	W2=width of c						
		or			Length	of Apron:	Q	Ft.
		W2=3Do+0.4I	La		VV 10	lth @ End:	2	Ft.
	_	·						
				1				
						J. J.		
AIT	'IIS							

	T	<u>R</u>	IPRAP CA	LCULAT	<u>IONS</u>	1		I
Location:	Roof Lea	der - 12" Cu	lvert (Hyd	roCAD Re	each #27R)		
Date:	12/31/2020	By:	EBS					
La	Apron Leng		Calculated					
Tw	Tailwater,		0.5					
Q		r Storm, CFS	2.17					
D50 D	Median Stor Depth of Sto		Calculated Calculated					
	_							
Do W1	Pipe Diame Width @ St		1.00 Calculated					
W1 W2	Width @ Er		Calculated					
W	Width of C		2					
. * *	Width of C	namici	2					
W1:								
	3(Do)=		3	Ft.				
	, ,				Widt	th @ Start:	3	Ft.
					,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	2.1.2.1		
D50:	$0.02(Q)^{4/3}$			D50=	0.11	Ft		
	Tw(Do)			D30	0.11			
	1 "(100)			or	1.3	In.		
					Median	Stone Size:	6	In.
						474		_
D:	2.25*D50				Depth	of Riprap:	14	In.
Lo	If Tw<= Do	/2.		Do/2=	0.5	E ₄		
La:	11 1 W<= D0				0.5			
		La=1.8Q/Do ^{3/2}		Tw=	0.5	Ft.		
	and	W2=width of c	hannel					
		or W2=3Do+La						
	If Tw>Do/2	:						
		La=3Q/Do ^{3/2} +	7Do					
	and	W2=width of c	hannel					
		or			Length	of Apron:	11	Ft.
		W2=3Do+0.4L	a		WIC	lth @ End:		Ft.
				1	i i	i		1
^	1							
ΔIT	I IC							

				LCULATI				
Location	1: GUSF #2	, 18" Culver	t (HydroC	AD Pond #	29P)			,
Date:	12/31/2020	By:	EBS					
La	Apron Leng	th Et	Calculated					
Tw	Tailwater,		0.5					
Q		r Storm, CFS	7.85					
D50	Median Stor		Calculated					
D	Depth of St		Calculated					
Do	Pipe Diame		1.50					
W1	Width @ St		Calculated					
W2	Width @ E1	nd, Ft	Calculated					
W	Width of C	hannel	2					
W1:								
	3(Do)=		4.5	Ft.				
					Widt	th @ Start:	5	Ft.
D.50	0.02(0)4/3			D.50	0.41	Tr.		
D50:	$0.02(Q)^{4/3}$			D50=	0.41	Ft.		
	Tw(Do)				5.0	I.a		
				or	3.0	III.		
					Median	Stone Size:	6	In.
					1/1041411			
D:	2.25*D50				Depth	of Riprap:	14	In.
					_			
La:	If Tw<= Do	/2.		Do/2=	0.75	T/4		
La.	11 1 W \ - DC		+ 7D					
	and	La=1.8Q/Do ^{3/2} W2=width of c		Tw=	0.5	rt.		
	and		nannei					
		or W2=3Do+La						
		W 2-3D0 La						
	If Tw>Do/2	:						
		La=3Q/Do ^{3/2} +	7Do					
	and	W2=width of c						
		or			Length	of Apron:	10	Ft.
		W2=3Do+0.4L	.a		VV 10	lth @ End:	2	Ft.
	_	-						
ATA	TT TC							
\mathbf{A}								

Section 9

Stormwater Operations & Maintenance Plan



STORMWATER INSPECTION AND MAINTENANCE MANUAL

Good To-GoKittery Assessor's Map 67, Lot 1

OWNER AT TIME OF APPROVAL: Good To-Go c/o Cape House Management, LLC 484 U.S. Route 1 Kittery, Maine 03904

Proper inspection, maintenance, and repair are key elements in maintaining a successful stormwater management program on a developed property. Routine inspections ensure permit compliance and reduce the potential for deterioration of infrastructure or reduced water quality. The following responsible parties shall be in charge of managing the stormwater facilities:

RESPONSIBLE PARTIES:

Owner:	Good To-Go c/o	(207) 451-9060		
	Name	Company	Phone	
Inspection:	Good To-Go c/o	Cape House Management	(207) 451-9060	
	Name	Company	Phone	
Maintenance	e: <u>Good To-Go c/o</u>	Cape House Management	(207) 451-9060	
	Name	Company	Phone	

NOTES:

Inspection and maintenance responsibilities shall transfer to any future property owner(s).

This manual shall be updated as needed to reflect any changes related to any transfer of ownership and/or any delegation of inspection and maintenance responsibilities to any entity other than those listed above.



GRASSED UNDERDRAINED SOIL FILTERS

Underdrain soil filters control stormwater quality by capturing and retaining runoff and passing it through a filter bed comprised of a specific media. The basin shall be inspected semi-annually and following major storm events for evidence of erosion, clogging or of bypass conditions.

Maintenance

- *Drainage:* The filter should within 24 to 48 hours following a one-inch storm or greater. If the system drains too fast, adjust the outlet release valve opening to regulate the outflow.
- *Sediment Removal*: Sediment and plant debris should be removed from the pretreatment structure at least annually.
- *Mowing*: If mowing is desired, only hand-held string trimmers or push-mowers are allowed on the filter (no tractor) and the grass bed should be mowed no more than 2 times per growing season to maintain grass heights of no less than 6 inches.
- Fertilization: Fertilization of the underdrained filter area should be avoided unless absolutely necessary to establish vegetation.
- Weeding: Weeding to control unwanted or invasive plants if necessary.
- *Grass cover:* Maintaining a healthy cover of grass will minimize clogging with fine sediments. If ponding exceeds 48 hours, the top of the filter bed should be rototilled to reestablish the soil's filtration capacity.
- Soil Filter Replacement: The top several inches of the filter can be replaced with fresh material if water is ponding for more than 72 hours, or the basin can be rototilled, seeded and mulched. Once the filter is mature, adding new material (a 1-inch to 2-inch cover of mature compost) can compensate for subsidence.

CULVERTS AND DRAINAGE PIPES

Function – Culverts and drainage pipes convey stormwater away from buildings, walkways, and parking areas and to surface waters or closed drainage systems.

Maintenance

- Culverts and drainage pipes shall be inspected semi-annually, or more often as needed, for accumulation of debris and structural integrity. Leaves and other debris shall be removed from the inlet and outlet to insure the functionality of drainage structures. Debris shall be disposed of on site where it will not concentrate back at the drainage structures or at a solid waste disposal facility.
- Riprap Areas Culvert outlets and inlets shall be inspected during annual maintenance and operations for erosion and scour. If scour or erosion is identified, the owner shall take appropriate means to prevent further erosion.

DEEP SUMP CATCH BASINS

Function – Catch basins collect stormwater, primarily from paved surfaces and roofs. Stormwater from paved areas often contains sediment and contaminants. Catch basin sumps serve to trap sediment, trace metals, nutrients and debris. Hooded catch basins trap hydrocarbons and floating debris.

Maintenance

- Remove leaves and debris from structure grates on an as-needed basis.
- Sumps shall be inspected and cleaned annually and any removed sediment and debris shall be disposed of at a solid waste disposal facility.

LANDSCAPED AREAS - FERTILIZER MANAGEMENT

Function – Fertilizer management involves controlling the rate, timing and method of fertilizer application so that the nutrients are taken up by the plants thereby reducing the chance of polluting the surface and ground waters. Fertilizer management can be effective in reducing the amounts of phosphorus and nitrogen in runoff from landscaped areas, particularly lawns.

Maintenance

- Have the soil tested by your landscaper or local Soil Conservation Service for nutrient requirements and follow the recommendations.
- Do not apply fertilizer to frozen ground.
- Clean up any fertilizer spills.
- Do not allow fertilizer to be broadcast into water bodies.
- When fertilizing a lawn, water thoroughly, but do not create a situation where water runs off the surface of the lawn.

LANDSCAPED AREAS - LITTER CONTROL

Function – Landscaped areas tend to filter debris and contaminates that may block drainage systems and pollute the surface and ground waters.

Maintenance

- Litter Control and lawn maintenance involves removing litter such as trash, leaves, lawn clippings, pet wastes, oil and chemicals from streets, parking lots, and lawns before materials are transported into surface waters.
- Litter control shall be implemented as part of the grounds maintenance program.

VEGETATIVE SWALES

Function – Vegetative swales filter sediment from stormwater, promote infiltration, and the uptake of contaminates. They are designed to treat runoff and dispose of it safely into the natural drainage system.

Maintenance

- Timely maintenance is important to keep a swale in good working condition. Mowing of grassed swales shall be monthly to keep the vegetation in vigorous condition. The cut vegetation shall be removed to prevent the decaying organic litter from adding pollutants to the discharge from the swale.
- Fertilizing shall be bi-annual or as recommended from soil testing.
- Inspect swales following significant rainfall events.
- Woody vegetation shall not be allowed to become established in the swales or rock riprap outlet protection and if present shall be removed.
- Accumulated debris disrupts flow and leads to clogging and erosion. Remove debris and litter as necessary.
- Inspect for eroded areas. Determine cause of erosion and correct deficiency as required. Monitor repaired areas.

RIP RAP OUTLETS

Function – Rip rap outlets slow the velocity of runoff, minimizing erosion and maximizing the treatment capabilities of associated buffers. Vegetated buffers, either forested or meadow, slow runoff which promotes and reduces peak rates of runoff. The reduced velocities and the presence of vegetation encourage the filtration of sediment and the limited bio-uptake of nutrients.

Maintenance

- Inspect level spreaders and buffers at least annually for signs of erosion, sediment buildup, or vegetation loss.
- Inspect level for signs of condensed flows. Level spreader and rip rap shall be maintained to disperse flows evenly over level spreader.
- If a meadow buffer, provide periodic mowing as needed to maintain a healthy stand of herbaceous vegetation.
- If a forested buffer, then the buffer should be maintained in an undisturbed condition, unless erosion occurs.
- If erosion of the buffer (forested or meadow) occurs, eroded areas should be repaired and replanted with vegetation similar to the remaining buffer. Corrective action should include eliminating the source of the erosion problem and may require retrofit or reconstruction of the level spreader.
- Remove debris and accumulated sediment and dispose of properly.

GENERAL CLEAN UP

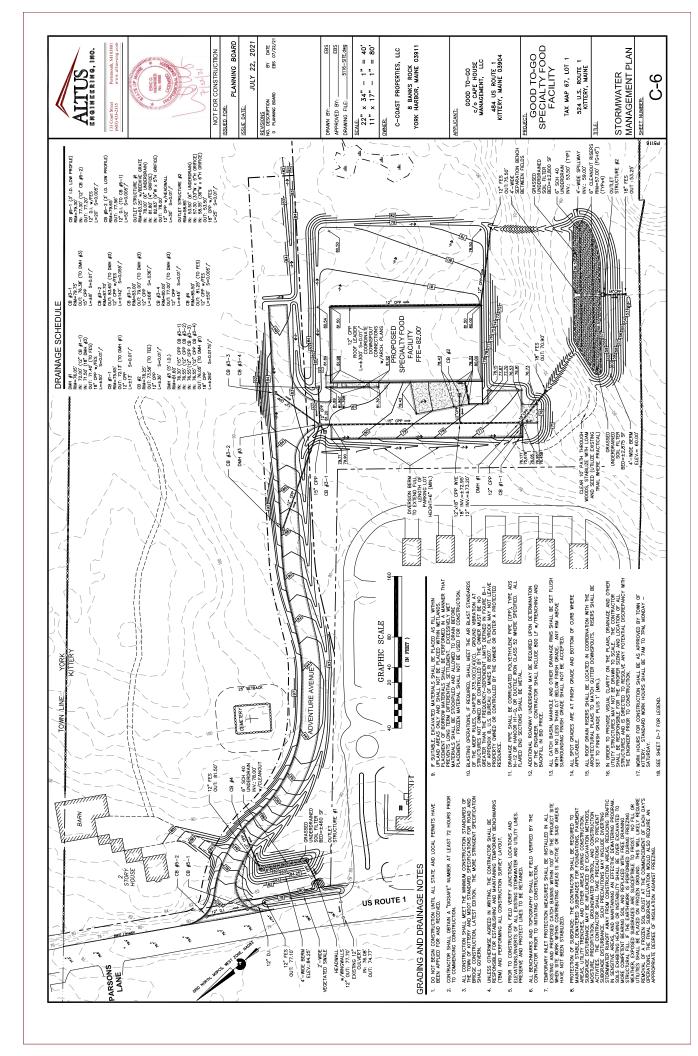
- Upon completion of the project, the contractor shall remove all temporary stormwater structures (i.e., temporary stone check dams, silt fence, temporary diversion swales, catch basin inlet filter, etc.). Any sediment deposits remaining in place after the silt fence or filter barrier is no longer required shall be dressed to conform to the existing grade, prepared, and seeded. Remove any sediment in catch basins and clean drain pipes that may have accumulated during construction.
- Once in operation, all paved areas of the site should be swept at least once annually at the end of winter/early spring prior to significant spring rains.

APPPENDIX

- A. Stormwater System Operations and Maintenance Report
- B. Site Grading and Drainage Plan

STORM WATER SYSTEM OPERATION AND MAINTENANCE REPORT

		Gen	eral Information	
Pro	oject Name			
Ow	ner			
Ins	pector's Name(s)			
	pector's Contact formation			
Dat	te of Inspection		Start Time:	End Time:
Tyl	pe of Inspection: Annual Report Post-storm	n event 🔲 Due	e to a discharge of significant amounts of sedin	ment
No	tes:			
<u> </u>			charges of Significant Amounts of Sedin	nent
	bject	Status	Notes	C.1 C.11
	lischarge of significant amounts of . te whether any are observed during		indicated by (but is not limited to) observation	ns of the following.
IVOI	e whether any are observed during	inis inspection:	Notes/ Action take	on·
1	Do the current site conditions ref	lect Yes	Ivoles/ Action take	м.
1	the attached site plan?	□No		
2	Is the site permanently stabilized			
	temporary erosion and sediment	□No		
	controls are removed, and stormy			
	discharges from construction acti	vity		
3	are eliminated? Is there evidence of the discharge	of U Yes		
3	significant amounts of sediment t			
	surface waters, or conveyance			
	systems leading to surface waters	?		
		•		
		Permit (Coverage and Plans	
#	BMP/Facility	Inspected	Corrective Action Needed and Notes	Date Corrected
	Grassed Underdrained Soil Filter			
	Catch Basins	□No □Yes		
	Catch Basins			
	Drainage Pipes	□Yes		
	8 1	□No		
	Riprap Aprons	□Yes		
		□No		
		□Yes		
		□No □Yes		
		□No		
		□Yes □No		



Section 10

Watershed Plans

Pre-Development Drainage Area Plan Post-Development Drainage Area Plan



