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ITEM 1 – 22 Shapleigh Road – Site Plan - Final Plan Review

Action: approve final plan or continue review Owner/applicant Fair Tide and acting agent Geoffrey R Aleva, PE of Civil Consultants propose to redevelop an existing commercial building with additions creating a footprint of 5,669sf, and to add a 6-unit residential building consisting of a 2,058sf building footprint, at real property located at 22 Shapleigh Road (Tax Map 15, Lot 64) in the Business-Local (B-LI) and Residential-Urban (R-U) Zones respectively.

Town of Kittery

Planning Board Meeting

April 27, 2023

PROJECT TRACKING

REQ' D	ACTION	COMMENTS	STATUS
NO	Sketch Plan Review	Reviewed by Planning Board during December 8, 2022 meeting	Accepted 12/8/22
YES	Preliminary Plan Review	Application submitted to KDPD 1.6.23	Approved
YES	Determination of Completeness/Acceptan ce	Preliminary site plan application accepted as complete during 1/26/23 meeting.	Complete
NO	Site Visit	Held February 6, 2023 and continued to February 21, 2023. Abutter notices sent by staff on January 30, 2023 and February 13, 2023.	Held
YES	Public Hearing	Opened during February 9, 2023 meeting and continued to February 23, 2023 meeting.	Held
YES	Final Plan Review and Decision	Submitted via online portal 4/6/23	Under review

Plan Review Notes reflect comments and recommendations regarding applicability of Town Land Use Development Code, and standard planning and development practices. Only the PB makes final decisions on code compliance and approves, approves with conditions or denies final plans. Prior to the signing of the approved Plan any Conditions of Approval related to the Findings of Fact along with waivers and variances (by the BOA) must be placed on the Final Plan and recorded at the York County Registry of Deeds. PLACE THE MAP AND LOT NUMBER IN 1/4" HIGH LETTERS As per Section 16.4.4.L -AT LOWER RIGHT BORDER OF ALL PLAN SHEETS. Grading/Construction Final Plan Required. - Grading or construction of roads, grading of land or lots, or construction of buildings is prohibited until the original copy of the approved final plan endorsed has been duly recorded in the York County registry of deeds when applicable.

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The project is located at the intersection of Shapleigh Road and Manson Avenue, the total lot area is 84,831sf (1.95-acres), and the property is divided into two zones the Business-Local (B-L1) Zone and the Residential Urban (R-U) Zone. The parcel is crossed by a wetland that is approximately 24,000sf (or less than 1 acre) and was delineated in 2021 and determined to be a forested wetland related to stormwater directed to the location from several culverts in the vicinity. An important note is that this proposal is subject to the recently approved (10/2022) revision in the (B-L1) zone for affordable housing. See: Microsoft Word - 2022.03.14 Title 16 Affordable Housing BL-1 (ecode360.com) The project is

proposing to utilize the 50ft zone extension provision indicated in §16.1.8.B.5. The proposed extension would place all building footprint area in the (B-L1) zone.

The proposed use of the renovated existing building to the north has the allowed uses of retail sales, a neighborhood grocery store as well as business and professional offices. This will be comprised of a collective of social service agencies knows as "Mainspring"; which will be home to Fair Tide's thrift store and administrative offices, Footprints Food Pantry, York Community Action and other programs that service the community.

The southern portion of the property is the location of the proposed new 6-unit residential building owned by Fair Tide and managed by York Housing. The required land area for each available unit will be 1500sf per unit, the available lot can easily support the density of the 6 multifamily units based on the land area $(6 \times 1500\text{sf}) < 54,000\text{sf})$.

The Planning Board voted 7-0 to approve the preliminary site plan application for this project during the February 23, 2023 meeting. Several additional details or plan notes were outstanding at that time, including stormwater facilities design and monitoring details, on-site traffic signage details, snow storage, and exterior lighting hours. The applicant provided updated plans and supporting information that addresses these items and satisfies the comments provided by the Town's peer review engineer.

Staff Review: Draft/ Preliminary Findings

Process (§16.7.10):

Any mixed-use project that contains residential and non-residential uses is classified as a **major site plan** per §16.7.5-A.2.c. Section 4402-6 of Maine Revised Statutes exempts division of structures from subdivision requirements where a project is subject to municipal site plan review (applicable to the 6-unit residential component of this project). Since Title 16 of Kittery's Town Code (KTC) classifies this project as a major site plan, subdivision review is not required and the provisions of KTC Chapter 16.7 General Development Requirements apply.

Major site plan applicants may choose to submit a **sketch plan** for a proposal but are not required to do so. The applicants submitted a sketch plan application for this project that was reviewed and accepted by the Planning Board on December 8, 2022. The packet for that meeting can be reviewed at: <u>Planning Board Meeting December 8th</u>, 2022 | Kittery ME.

Submittal and approval of a **preliminary site plan application is required** per §16.7.10-C. The applicant submitted a preliminary site plan application and supporting plans and materials via the Town's online portal on January 6, 2023. Staff reviewed the documents and the submittal checklists provided by the applicant and found the application to be generally complete. The Planning Board reviewed this application during the January 26, 2023 meeting and voted 7-0 to accept the application and find it complete. The January 26 meeting packet includes site plans, building elevations and renderings, a photometric lighting plan, a stormwater management plan, a warranty deed, and verification of water and sewer service availability, which can be reviewed at item 1 22 shapleigh rd.pdf (kitteryme.gov).

 The Board held a **site walk** at the subject property on February 6, 2023 and voted to continue it on February 21, 2023. The Board opened a **public hearing** during the February 9, 2023 meeting and voted to continue the hearing to the February 23, 2023 meeting. Third party peer review of plans for compliance

with stormwater and engineering requirements was requested from CMA Engineers; comments were received by Town staff on February 13, 2023. Their review memo is included in the packet for this meeting.

Following Planning Board approval of a preliminary site plan application, submittal and approval of a separate Final Site Plan application is required prior to construction.

Other permit(s) needed:

- Final site plan approval
- Road Excavation Permit/ Driveway Entrance Permit (Kittery Public Works)
- Building Permit
- Sewer Connection Permit; other utility permits?
- Sign permit

Land Use Zone Regulations Chapter 16.4

Multifamily Dwellings are permitted in B-L1 zoning district per 16.4.18- B. A variety of office and retail uses are also permitted.

16.4.18-D.1 Standards:

- a.3: one nonresidential use must be located on the first floor facing Shapleigh Rd. Staff and the Board determined this requirement to be met via the commercial uses proposed for the existing building.
- a.4.a unit density: 1,500 square feet of land area per dwelling unit required (complies)
- a.4.b-g: dimensional standards (setbacks, building height, lot coverage): complies
- a.4.h: stormwater: LID and BMPs required for all stormwater generated onsite. Stormwater
 Management Plan submitted by applicant. Applicant proposes to reduce impervious surfaces on the
 northern portion of the property while adding approx. 7,700 square feet of impervious surfaces on the
 southern portion of the property. Most stormwater runoff is proposed to flow to the on-site wetland,
 which drains southwest to public facilities located in the Shapleigh Rd right-of-way and south via a
 culvert which underlies abutting property.

Revised drainage plans were reviewed on the Board's behalf by a qualified peer review consultant (Jodie Bray Strickland, CMA Engineers), who determined that stormwater-related comments have been addressed by the updated plans.

- a.4.j: hours of operation and hours of exterior lighting are required to be limited. Final plans should be noted accordingly. Hours of operation were added to plans. Hours of exterior lighting are not specified.
- a.4.l: setback from streams & wetlands: 50 feet for buildings, 40 feet for 1-5 stall parking areas: commercial building and parking area existing. Reduction in nonconformity for parking/ driveway setback proposed. Proposed residential building and parking facilities comply with standard.

D.2 Parking:

- must be located in rear of building: new parking complies
- access: provided via existing sidewalk. Further connectivity infeasible due to wetland location
- screening required: provided see landscape plans. Trees, shrubs, and groundcovers provided per requirements.

117 D.3 Building Design:

- materials and details consistent in all facades
- peaked roof form proposed

121 D.4 Landscaping:

- 15% of property to be landscaped or in natural condition per landscape plan and existing wetland
- outdoor spaces required. Garden beds proposed near commercial building. **Usable outdoor space** limited near residential building. *Discussion item?*

D.7 Affordable Housing: 16.5.4 must be met. Recording of covenants required.

General Development Requirements Chapter 16.7 (Site Plans)

16.7.8 Waivers: Waiver request for residential parking submitted.

- 131 16.7.11 Standards and approval criteria:
- 132 A. Water and B. Sewer
 - Utilities are available to serve this development. Review by Town and District staff and peer review engineers pending. Verification of availability has been provided.

C & D. Stormwater:

• See above. Waiver request submitted for minimal increase in peak stormwater flows. Post-construction stormwater plan provided.

E. Traffic:

- Vehicular access to the existing/ proposed commercial building is from Manson Ave and Shapleigh Rd via existing driveways. Access to the proposed residential building will be from Shapleigh Rd via a new driveway. Vehicular connectivity between the commercial and residential portions of the site is infeasible due to the location of the on-site wetland. Driveway and paving plans were reviewed by CMA Engineers and by Kittery's Technical Review Committee members. Provision of sight distance information, vehicle turning diagrams, on-site signage, and updated drainage plans addressed remaining comments, which included:
 - o Sidewalk improvements must be concrete (no asphalt in ROW)
 - O Traffic and parking controls are needed within the site, including fire lane/ no parking markings in the residential driveway and one-way & do not enter signage for the angled-parking portion of the commercial driveway.
- Number and spacing of driveways comply with E.3 and E.4. Internal vehicular circulation complies with E.5.

F. Parking:

- 35 parking stalls proposed for commercial building, 6 parking stalls proposed for residential building. Waiver requested for reduction in residential parking requirements.
- A note was added to the site plan for snow storage but **Snow storage** areas are not shown on plans. Applicant should provide snow storage information during the meeting for planning board review. Compatibility with landscape plans should be assessed.

H. Lighting

Lighting plans provided showing pole-mounted exterior lighting in parking/ driveway areas and canopy lighting near building entries. All fixtures are cut-off and not more than 20 feet above ground.

Maximum illumination levels on-site and at property lines comply with standards.

I. Erosion Control:

- Erosion control plan provided. Erosion control measures required to be implemented and inspected during construction.
 - J. Water quality and Wastewater Pollution.
 - Town standards for sewer facility design and construction apply and to be inspected by PW and CEO. Surface water impacts to be reviewed and minimized via stormwater plans.
 - P. Technical and Financial Capacity.
 - The applicant and all contractors and consultants must demonstrate to the board's satisfaction the financial and technical capacity to construct the project in adherence to applicable standards.

16.7.12 Post-Approval

• Construction required to begin within 1 year of planning board approval. **Pre-construction meeting** with staff required prior to start of construction. Stormwater and erosion control inspection by qualified professional required during construction. Annual inspection of stormwater facilities required following project completion.

Discussion Items (Italicized above):

- time restrictions of exterior lighting
- Snow storage

Recommendation

Staff find that, with provision of additional information as noted above, this proposal complies with applicable standards and is likely to improve conditions related to existing paving and stormwater runoff while having minimal impacts on infrastructure, traffic, or nearby properties. Outstanding items may be resolved during final review of plans prior to recording. Staff recommend approval of this application with conditions requiring resolution of specific items. The Board may also choose to continue review to a future meeting and advise the applicant and staff of items requiring resolution.

Recommended Motions

Move to approve/deny/continue review of final site plan.

Owner/applicant Fair Tide and acting agent Geoffrey R Aleva, PE of Civil Consultants propose to redevelop an existing commercial building with proposed additions creating a footprint of 5,669sf, and to add a 6-unit residential building consisting of a 2,058sf building footprint, at real property located at 22 Shapleigh Road (Tax Map 15, Lot 64) in the Business-Local (B-LI) and Residential-Urban (R-U) Zoning Districts. Based on the plans and supporting information submitted to the Town through April 27, 2023, I move to approve/deny/continue review of the preliminary site plan application for this project.

Kittery Planning Board Findings of Fact For 22 Shapleigh Rd Site Plan Review



Note: This approval by the Planning Board constitutes an agreement between the Town and the Developer incorporating the Development plan and supporting documentation, the Findings of Fact, and all waivers and/or conditions approved and required by the Planning Board.

WHEREAS: Owner and applicant Fair Tide, and agent Geoffrey Aleva of Civil Consultants request final approval to redevelop an existing commercial building with additions creating a footprint of 5,669sf, and to construct a new 6-unit residential building consisting of a 2,058sf building footprint, at real property located at 22 Shapleigh Road (Tax Map 15, Lot 64) in the Business-Local (B-LI) and Residential-Urban (R-U) Zones

Hereinafter the "Development".

Pursuant to the Plan Review meetings conducted by the Planning Board as noted in the Plan Review Notes dated 4/27/23;

REQ'D	ACTION	COMMENTS	STATUS
NO	Sketch Plan	Reviewed by Planning Board during December 8, 2022 meeting	Accepted 12/8/22
YES	Site Visit	February 6 and February 21, 2023	HELD
YES	Completeness/Acceptance	January 26, 2023	ACCEPTED
YES	Public Hearing	February 9 and 23, 2023	HELD
YES	Preliminary Plan Approval	Approved February 23, 2023	APPROVED
YES	Final Plan Review and Decision	Final Site Plan Application submitted April 6, 2023	Pending

and pursuant to the Project Application and Plan and other documents considered to be a part of the approval by the Planning Board in this finding consist of the following and as noted in the Plan Review Notes dated 4/27/2023 (Hereinafter the "Plan").

1. 22 Shapleigh Rd site plans revised 4/5/23

NOW THEREFORE, based on the entire record before the Planning Board as and pursuant to the applicable standards in the Land Use and Development Code, the Planning Board makes the following factual findings as required by Section §16.7.10(5)(b) and as recorded below:

FINDINGS OF FACT

Action by the Board shall be based upon findings of fact which certify or waive compliance with all the required standards of this title, and which certify that the development satisfies the following requirements:

[1] Development Conforms to Local Ordinances.

Standard: The proposed development conforms to a duly adopted comprehensive plan as per adopted provisions in the Town Code, zoning ordinance, subdivision regulation or ordinance, development plan or land use plan, if any. In making this determination, the municipal reviewing authority may interpret these ordinances and plans.

Finding: The proposed development conforms to the applicable provisions of Kittery's town code, as summarized in the Planner's Review Notes that accompany these findings. The applicant requested waivers from applicable parking standards. Staff conclude that the parking requirements for affordable housing developments in the B-L1 zoning district are published incorrectly, the project complies with the adopted standards, and the planning board should approve the requested parking waiver accordingly.

Conclusion: This standard appears to be met.

Vote of _ in favor _ against _ abstaining

[2] Water Supply Sufficient.

Standard: The proposed development has sufficient water available for the reasonably foreseeable needs of the development.

Finding: The proposed use plans to connect to public water and has received a capacity letter from the Water District stating water supply is sufficient.

Conclusion: This standard appears to be met.

Vote of in favor against abstaining

[3] Sewage Disposal Adequate.

Standard: The proposed development will provide for adequate sewage waste disposal and will not cause an unreasonable burden on municipal services if they are utilized.

Finding: The proposed use plans to tie into existing sewer infrastructure and has received a capacity letter from the Sewer Department.

Conclusion: This standard appears to be met.

Vote of _in favor _against _ abstaining

[4] Stormwater Managed.

Standard: *The proposed development will provide for adequate stormwater management.*

Finding: Applicant proposes to reduce impervious surfaces on the northern portion of the property while adding approx. 7,700 square feet of impervious surfaces on the southern portion of the property. Most stormwater runoff is proposed to flow to the on-site wetland, which drains southwest to public facilities located in the Shapleigh Rd right-of-way and south via a culvert which underlies abutting property. The applicant requests a waiver from the board to authorize a minimal increase in stormwater runoff from the residential portion of the project into the wetland and buffer areas. The proposed increase in stormwater flows is not anticipated to significantly impact wetland or buffer areas or neighboring properties. Staff and the Town's peer review engineer recommend approving this waiver accordingly. The applicant has prepared a Post Construction Stormwater Management Plan.

Conclusion: This standard appears to be met.

Vote of _in favor _against _ abstaining

[5] Traffic Managed.

Standard: The proposed development will:

[a] Not cause unreasonable highway or public road congestion or unsafe conditions with respect to the use of the highways or public roads existing or proposed; and

[b] Provide adequate traffic circulation, both on-site and off-site.

Finding: The proposed development will not cause unreasonable congestion and unsafe conditions onto public ways and provides for adequate on-and off-site traffic circulation.

Conclusion: This standard appears to be met.

Vote of _in favor _against _ abstaining

[6] Parking and Loading.

Standard: Provisions have been made for safe internal vehicular circulation, loading and service areas, and parking associated with the proposed development.

Finding: The proposed development shows that internal vehicular circulation will be safe, with adequate loading and service areas are provided, and the number of parking spaces is sufficient based on the proposed regulated uses.

Conclusion: This standard appears to be met.

Vote of _in favor _against _ abstaining

[7] Utilities.

Standard: The size, type, and locations of all public utilities and private utilities to serve the proposed development will be installed per accepted engineering practices

Finding: The proposed development will utilize existing public utilities for the proposed use and will install lighting for the building and parking areas in accordance with Town regulations.

Conclusion: This standard appears to be met.

Vote of _ in favor _ against _ abstaining

[8] Erosion controlled.

Standard: The proposed development will not cause unreasonable soil erosion or a reduction in the land's capacity to hold water so that a dangerous or unhealthy condition results.

Finding: The proposed development will be required to provide erosion and sedimentation controls during construction. Maintenance of stormwater facilities and monitoring of sedimentation is also required in accordance with the Stormwater Management Plan.

Conclusion: This standard appears to be met.

Vote of in favor against abstaining

[9] Groundwater protected.

Standard: The proposed development will not, alone or in conjunction with existing activities, adversely affect the quality or quantity of groundwater.

Finding: This proposal is not anticipated to adversely affect the quality or quantity of groundwater.

Conclusion: This standard appears to be met.

Vote of _in favor _against _ abstaining

[10] Freshwater wetlands identified.

Standard: All freshwater wetlands within the project area have been identified on any maps submitted as part of the application, regardless of the size of these wetlands.

Finding: The plan identifies wetlands in the middle of the property. Improvements to the developed portion of the site are proposed to improve the runoff that flows into the wetland. New construction is located and designed to minimize disturbance to wetland and setback areas.

Conclusion: This standard appears to be met.

Vote of _in favor _against _ abstaining

[11] River, stream or brook identified.

Standard: Any river, stream or brook within or abutting the proposed project area has been identified on any maps submitted as part of the application. For purposes of this section, "river, stream or brook" has the same meaning as in 38 M.R.S. § 480-B, subsection 9. Municipal solid waste disposal available. The proposed development will not cause an unreasonable burden on the municipality's ability to dispose of solid waste, if municipal services are to be used.

Finding: It appears that a stream does not exist in or abutting the property within 75 feet.

Conclusion: This standard appears to be met.

Vote of _in favor _against _ abstaining

[12] Water body quality and shoreline protected.

Standard: Whenever situated entirely or partially within 250 feet of any wetland, the proposed development will not adversely affect the quality of that body of water or unreasonably affect the shoreline of that body of water. Flood areas identified and development conditioned. All flood-prone areas within the project area have been identified on maps submitted as part of the application. Water and air pollution minimized. The proposed development will not result in undue water or air pollution. In making this determination, the following must be considered:

- [a] Elevation of the land above sea level and its relation to the floodplains;
- [b] Nature of soils and subsoils and their ability to adequately support waste disposal;
- [c] Slope of the land and its effect on effluents;
- [d] Availability of streams for disposal of effluents;
- [e] Applicable state and local health and water resource rules and regulations; and
- [f] Safe transportation, disposal and storage of hazardous materials.

Finding: It appears that the proposed development will not adversely affect the quality of any water or wetland body.

Conclusion: This standard appears to be met.

Vote of in favor against abstaining

[13] Aesthetic, cultural and natural values protected.

Standard: The proposed development will not have an undue adverse effect on the scenic or natural beauty of the area, aesthetics, historic sites, significant wildlife habitat identified by the Department of Inland Fisheries and Wildlife or the municipality, or rare and irreplaceable natural areas, or any public rights for physical or visual access to the shoreline.

Finding: The proposed development is not anticipated to have an undue adverse effect on the scenic or natural beauty of the area, aesthetics, known historic sites, or significant wildlife habitat.

Conclusion: This standard appears to be met.

Vote of _ in favor _ against _ abstaining

[14] Environmental considerations.

Standard: The proposed development will not result in undue levels of lighting, noise, vibrations, smoke, heat, glare, fumes, dust, toxic matter, odors, or electromagnetic interference.

Finding: The proposed development is not anticipated to result in any undue levels of lighting, noise, vibrations, or other nuisance impacts on nearby areas.

Conclusion: This standard appears to be met.

Vote of _ in favor _ against _ abstaining

[15] Utilization of the site.

Standard: The proposed development does reflect the natural capabilities of the site to support development.

Finding: The proposed development is designed in a manner that respects the natural capabilities of the lot.

Conclusion: This standard appears to be met.

Vote of _in favor _against _ abstaining

[16] Developer financially and technically capable.

Standard: Developer is financially and technically capable to meet the standards of this section.

Finding: It appears the developer is financially and technically capable to effectuate the project. Provision of a performance guarantee and escrow funds for development inspections are required prior to start of construction.

Conclusion: This standard appears to be met.

Vote of _ in favor _ against _ abstaining

NOW THEREFORE the Kittery Planning Board adopts each of the foregoing Findings of Fact and based on these Findings determines the proposed Development will have no significant detrimental impact, and the Kittery Planning Board hereby grants final approval for the Development at the above referenced property, including any waivers granted or conditions as noted.

Waivers:

1. Waiver from 16.7.11.F.4.d – Parking standards. Amendments were adopted for B-L and B-L1 zoning standards to encourage affordable housing. Reduced off-street parking requirements (1 stall per unit) for affordable housing were published for B-L but omitted for B-L1. Staff believe

this omission was in error. The applicant requests a waiver from parking standards which would authorize the project to comply with the requirements applicable to affordable housing projects in B-L zoning districts.

2. Waiver from 16.7.11.C.4.a. – Stormwater and surface drainage Standards: Applicant requests waiver from the requirement to limit peak stormwater runoff discharge to predevelopment levels which would authorize the project to minimally exceed pre-development runoff flows.

Conditions of Approval (to be included as notes on the final plan in addition to the existing notes):

- 1. No changes, erasures, modifications or revisions may be made to any Planning Board approved final plan. (Title §16.7.12.C).
- 2. Applicant/contractor will follow Maine DEP *Best Management Practices* for all work associated with site and building construction to ensure adequate erosion control and slope stabilization.
- 3. Prior to the commencement of grading and/or construction within a building envelope, as shown on the Plan, the owner and/or developer must stake all corners of the envelope. These markers must remain in place until the Code Enforcement Officer determines construction is completed and there is no danger of damage to areas that are, per Planning Board approval, to remain undisturbed.
- 4. All Notices to Applicant contained in the Findings of Fact (dated: 4/27/2023).

<u>Conditions of Approval (Not to be included as notes on the final plan):</u>

1. <u>Incorporate any plan revisions on the site plan as recommended by Staff, Planning Board, or Peer Review Engineer, and submit for Staff review prior to endorsement and recording of the plan.</u>

Notices to Applicant:

- 1. Prior to the release of the signed plans, the applicant must pay all outstanding fees associated with review, including, but not limited to, Town Attorney fees, peer review, newspaper advertisements and abutter notification.
- 2. State law requires all subdivision and shoreland development plans, and any plans receiving waivers or variances, be recorded at the York County Registry of Deeds within 90 days of the final approval.
- 3. Three (3) paper copies of the final recorded plan and any and all related state/federal permits or legal documents that may be required, must be submitted to the Town Planning Department. Date of Planning Board approval shall be included on the final plan in the Signature Block.
- 4. This approval by the Town Planning Board constitutes an agreement between the Town and the Developer, incorporating the Plan and supporting documentation, the Findings of Fact, and any Conditions of Approval.

The Planning Board authorizes the Planning Board Chair, or Vice Chair, to sign the Final Plan and the Findings of Fact upon confirmation of compliance with any conditions of approval.

Appeal:

Per Title 16.2.12.B(1) - An aggrieved party with legal standing may appeal a final decision of the Planning Board to the York County Superior Court in accordance with Maine Rules of Civil Procedures Section 80B, within forty-five (45) days from the date the decision by the Planning Board was rendered.



TOWN OF KITTERY ~ MAINE PLANNING OFFICE

200 Rogers Road, Kittery, Maine 03904 PHONE: (207) 475-1323 Fax: (207) 439-6806 www.kittery.org

APPLICATION: REQUEST FOR WAIVER

THIS REVIEW PROCESS REQUIRES APPROVAL FROM BOTH THE TOWN PLANNER AND THE CODE ENFORCEMENT OFFICER

11113	REVIEWTRO	OLOO KEC	COINCE	AI I KO	17121	KOM DOI	II IIIE IOWIN	PLANNER AND IH	L CODE ENTORC	LIMILIAI OTTICER
PROPERTY DESCRIPTION		Parcel ID	Мар	15	Lot	64	Zone Base Overlay	B-L1, R-U	Total Land Area	1.9475 acres
		Physical Address	22 S	HAPLE	IGH R	ROAD	-			
		Name	FAIR	TIDE, II	VC.					
	PERTY NER'S	Phone					Mailing	15 STATE R KITTERY, M	E	
INFORMATION		Fax					Address	C	3904	
		Email								*
st		Name	GEOF	FREY	R. ALE	EVA, PE	Name of Business	CIVIL CONSULT	ANTS	
APPI AGEI	ICANT'S	Phone	(207) -	384-25	50			293 MAIN S		
	RMATION	Fax	(207) -	384-21	12		Mailing Address	SOUTH BERWICK, ME 03908		
		Email	geoff@)civcon	.com					
	Ordinance S	Section	Descr	ibe wh	y this	request is	being made.			
	EXAMPLE 16.32.560 (B)- O PARKING.	***EXAMPLE*** Requesting a waiver of this ordinance since the proposed professional offices have a written agreement with the abutting Church owned property to share parking.								
DESCRIPTION	16.3.2.9.D(1)(Minimum park requirement o spaces per dw in B-L1 zone	ing f 1.5	The propert propert previousing	oposed by manag sly revie	1 bedrogers inc ewed a ts to or	oom and studicate that the office that the office the o	idio units will n the perspective ousing zoning r	parking spaces for the ot demand 1.5 space tenants will not nece revision allowed for a e parking stall per one	s per unit. Informat ssarily have a vehic reduction in parking	ion from the cle. The g for affordable
								application is true ar	nd correct and will	not deviate from
the plans submitted without notifying the Kittery Planning D Applicant's Signature: Date: 3-15-23				L L L	ccery P		Owner's Signature: Date:			

ARTICLE IV. WAIVERS

16.28.180 Waiver authorized.

Where the planning board finds that, due to special circumstances of a particular plan, the provision of certain required improvements is not requisite in the interest of public health, safety and general welfare, or is inappropriate because of inadequacy or lack of connecting facilities adjacent or in proximity to the proposed development, <u>upon written request</u>, it may waive or modify such requirements, subject to appropriate conditions. (Land use and dev. code § 7.4.1, 1994)

16.28.190 Objectives secured.

In granting modifications or waivers, the planning board must require such conditions as will, in its judgment, secure substantially the objectives of the requirements so waived or modified. (Land use and dev. code § 7.4.2, 1994)



TOWN OF KITTERY ~ MAINE PLANNING OFFICE

200 Rogers Road, Kittery, Maine 03904 PHONE: (207) 475-1323 Fax: (207) 439-6806 www.kittery.org

APPLICATION: REQUEST FOR WAIVER

THIS DEVIEW PROCESS REQUIRES APPROVAL FROM BOTH THE TOWN PLANNER AND THE CODE ENEODICEMENT OFFICER

IIII3	KEVIEW PKC	CL33 KEC	KOIKES	AFFRO	VALI	KOM BOI	H THE TOWN	PLANNER AND IN	E CODE ENFORCI	MENI OFFICER
PROPERTY DESCRIPTION		Parcel ID	Мар	15	Lot	64	Zone Base Overlay	B-L1, R-U	Total Land Area	1.9475 acres
		Physical Address	22 S	HAPLE	IGH R	OAD				
PROPERTY OWNER'S INFORMATION		Name	FAIR	TIDE, I	NC.					
		Phone					Mailing	15 STATE R KITTERY, M	E	
		Fax					Address	C	3904	
		Email								
		Name	GEOF	FREY	R. ALE	EVA, PE	Name of Business	CIVIL CONSULT	ANTS	
APP	LICANT'S NT	Phone	(207) -	-384-25	550			293 MAIN S		
INFORMATION		Fax	(207) -	384-21	12		Mailing Address	SOUTH BERWICK, ME 03908		
		Email	geoff@	civcon	.com					
	Ordinance S	Descr	ibe wh	y this	request is	being made.				
	EXAMPLE 16.32.560 (B)- OFFSTREET PARKING.		***EXAMPLE*** Requesting a waiver of this ordinance since the proposed professional offices have a written agreement with the abutting Church owned property to share parking.							
DESCRIPTION	16.8.10 (4) (a peak discharg development 2-yr and 25-yr	je to pre- levels for	stormw use of Implen	ater flow minimal	ws are footpri additior	very similar nt detentior nal stormwa	· with no increa n areas, as wel	o pre-development levales over 0.1 cfs. The lase over 0.1 cfs. The las reducing existing rices will create unned	e runoff will be mitiga impervious area wh	ated through the ere possible.
<u> </u>										
								application is true ar	nd correct and will i	not deviate from
the plans submitted without notifying the Kittery Planning D Applicant's Signature: Date:				Dartment of a Owner's Signature: Date:	iny crianges.					

ARTICLE IV. WAIVERS

16.28.180 Waiver authorized.

Where the planning board finds that, due to special circumstances of a particular plan, the provision of certain required improvements is not requisite in the interest of public health, safety and general welfare, or is inappropriate because of inadequacy or lack of connecting facilities adjacent or in proximity to the proposed development, <u>upon written request</u>, it may waive or modify such requirements, subject to appropriate conditions. (Land use and dev. code § 7.4.1, 1994)

16.28.190 Objectives secured.

In granting modifications or waivers, the planning board must require such conditions as will, in its judgment, secure substantially the objectives of the requirements so waived or modified. (Land use and dev. code § 7.4.2, 1994)



CMA ENGINEERS, INC. CIVIL | ENVIRONMENTAL | STRUCTURAL

35 Bow Street Portsmouth, New Hampshire 03801-3819

> P: 603|431|6196 www.cmaengineers.com

March 28, 2023

Jason Garnham, Director of Planning and Development Town of Kittery 200 Rogers Road Kittery, Maine 03904

RE: Town of Kittery, Planning Board Services Fair Tide, Inc. Development Review #2 Tax Map 15, Lot 64 CMA #591.152

Dear Jason:

CMA Engineers has received the following information for Assignment #152, review #2 of the Fair Tide preliminary plan for the proposed project at 22 Shapleigh Road (Tax Map 15, Lot 64).

- 1) Review of the Fair Tide Preliminary Plan Memorandum by Civil Consultants, Inc. dated March 15, 2023.
- 2) Stormwater waiver request.

We have reviewed the information submitted for conformance with the Kittery Land Use and Development Code (LUDC) and general engineering practices and offer the comments below that correspond directly to the Town's Ordinances.

16.7 General Development Requirements

16.7.11 Performance Standards and Approval Criteria

16.7.11.C. Stormwater and Surface Drainage

16.7.11.C.(4)(a). There are increased flows for the 2-year storm event at both outfall locations and at outfall 1 for the 25-year storm. We note that these increases are small (0.1 cfs) and that the proposed design has decreased the impervious area of the site and uses small detention areas for stormwater. The small increase in stormwater post construction is not likely to be a concern. The applicant has applied for a waiver of this standard. In addition, the post-construction O&M plan incorporates practices that ensure proper functioning of the on-site system in the future.

16.7.11.E. Vehicular Traffic

16.7.11.E.(5)(b). The fire lane for the northern building should be shown on the plan. We note that the fire lane for the southern (residential) building is indicated but none is shown for the northern building.

16.7.11.H. Exterior Lighting

16.7.11.H.(2)(a). The uniformity ratio for the access drive (s) should be shown on the plan. It appears that the uniformity ratio of the parking lots does not meet the standard.

General Comments

We have the following comments on the plans that remain unaddressed:

- 1. The plans should contain details of the wetland delineation (including the date) and be stamped by a wetland scientist.
- 2. The plans should contain a cover page with a sheet index.

Should you have any questions, please do not hesitate to call.

Very truly yours,

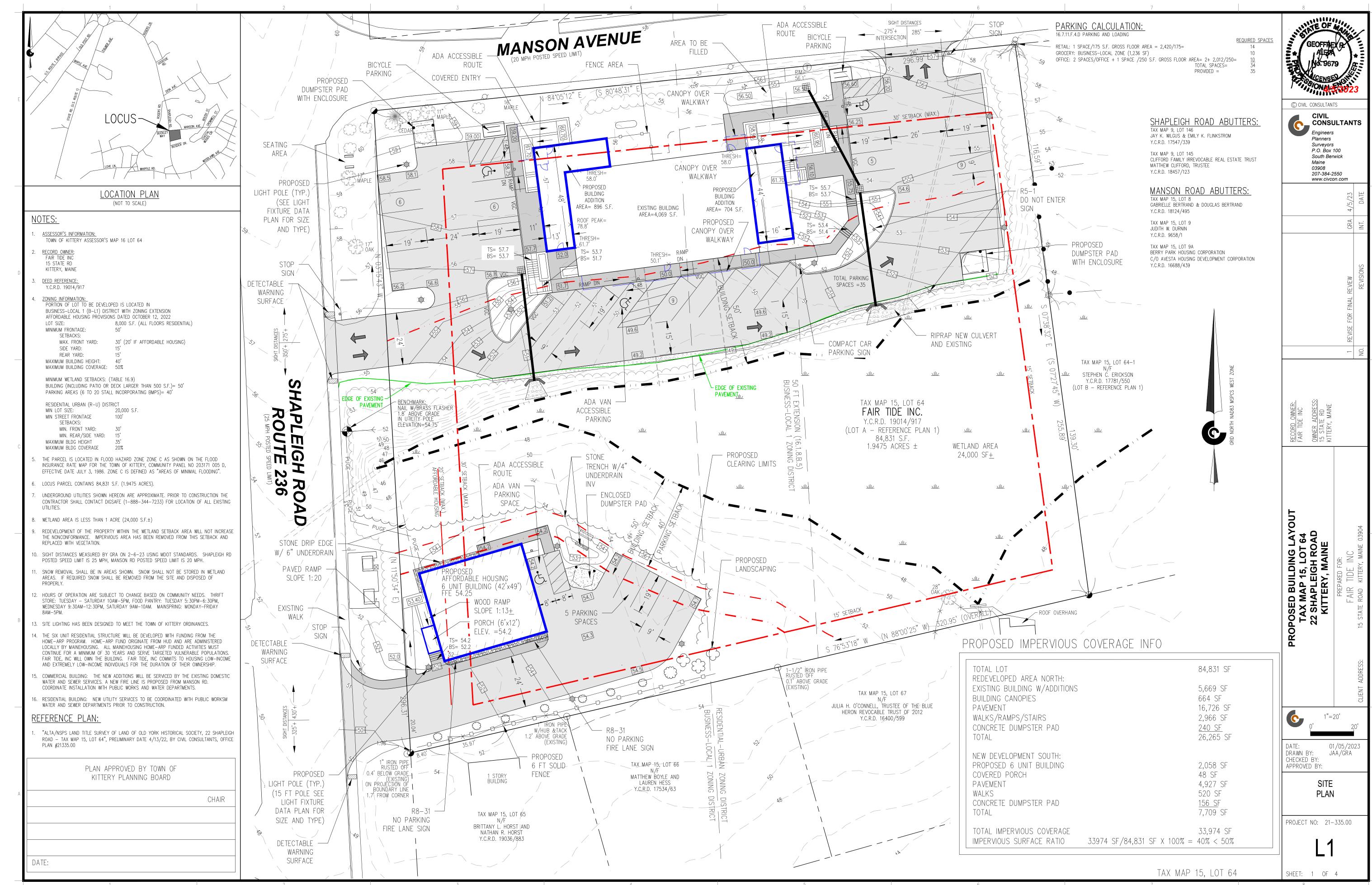
CMA ENGINEERS, INC.

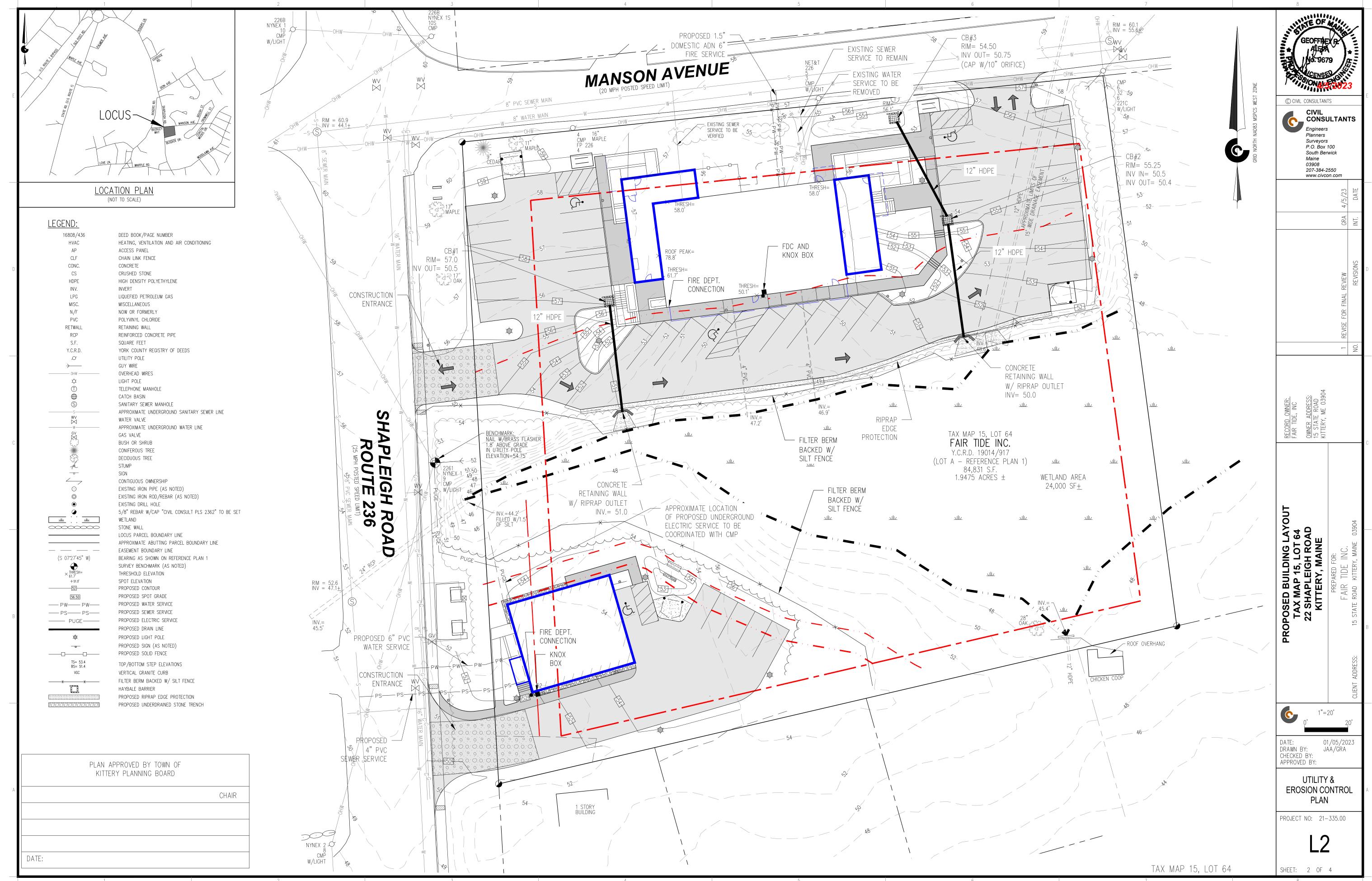
die Bray Strickland, P.E. Senior Project Engineer

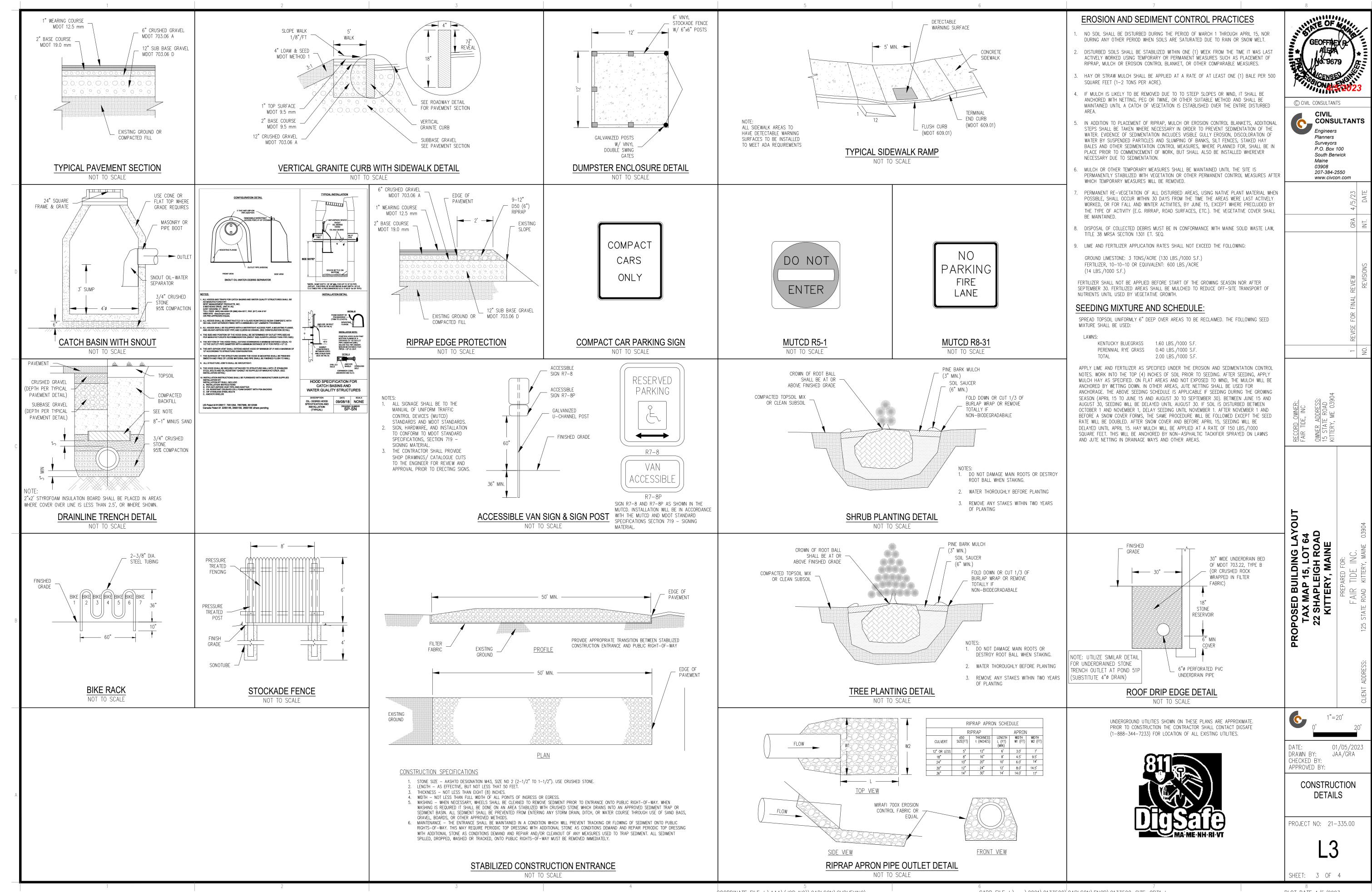
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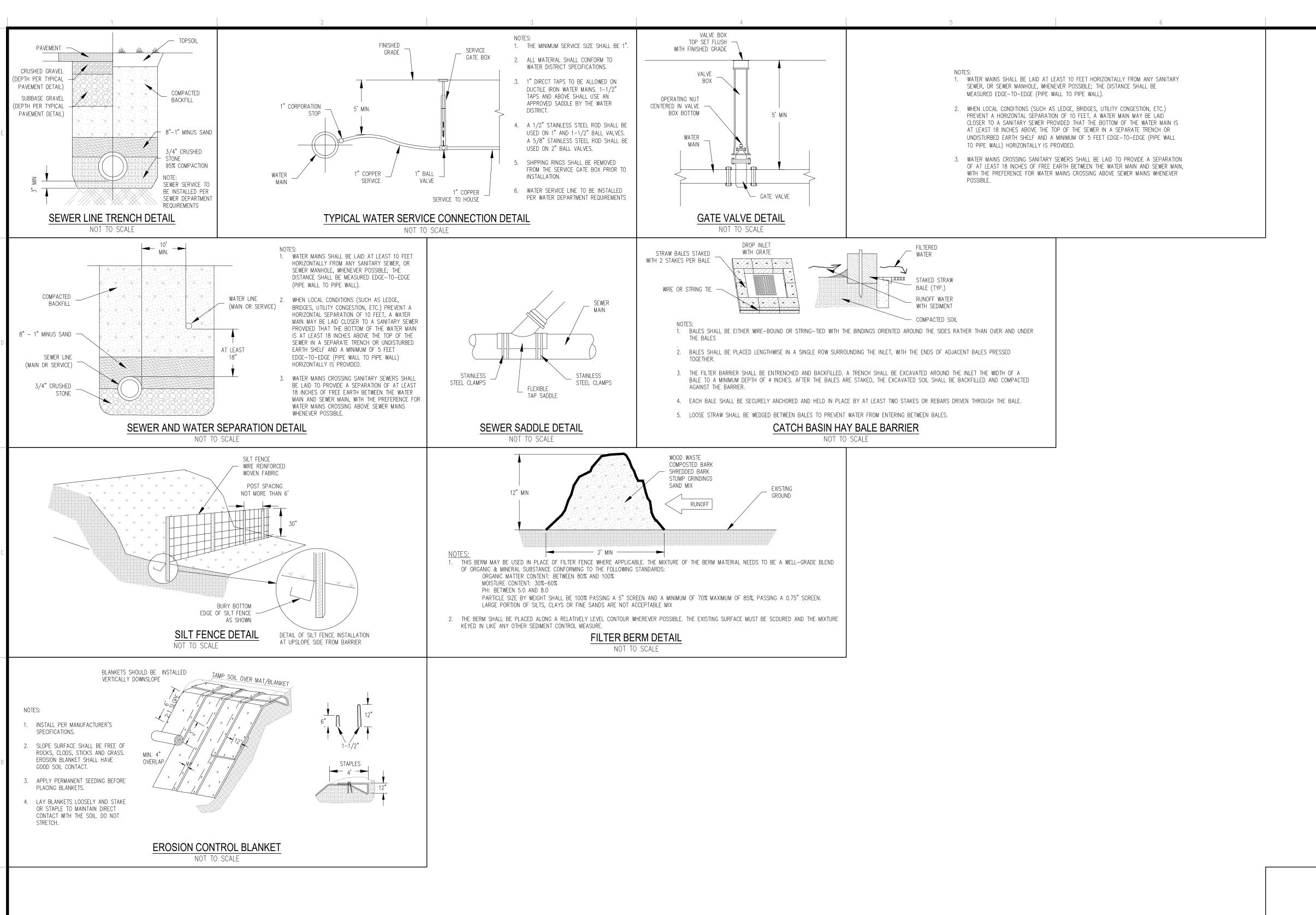
cc: Geoffrey Aleva, P.E., Civil Consultants





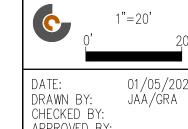






UNDERGROUND UTILITIES SHOWN ON THESE PLANS ARE APPROXIMATE. PRIOR TO CONSTRUCTION THE CONTRACTOR SHALL CONTACT DIGSAFE (1-888-344-7233) FOR LOCATION OF ALL EXISTING UTILITIES.





PROPOSED BUILDING LAYOUT TAX MAP 15, LOT 64 22 SHAPLEIGH ROAD KITTERY, MAINE

© CIVIL CONSULTANTS

Planners

Surveyors

P.O. Box 100

South Berwick

207-384-2550

www.civcon.com

CONSULTANTS

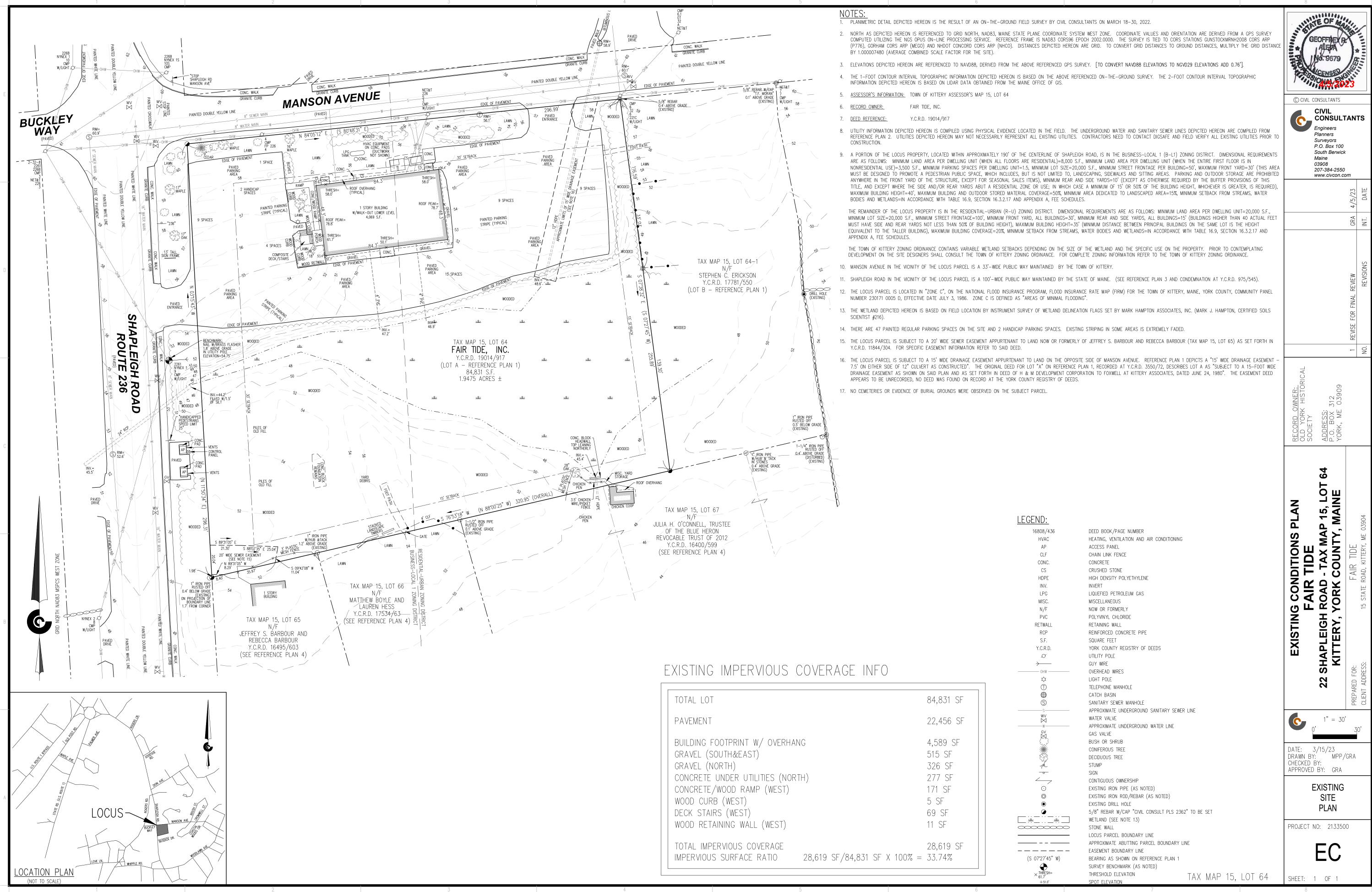
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APPROVED BY:

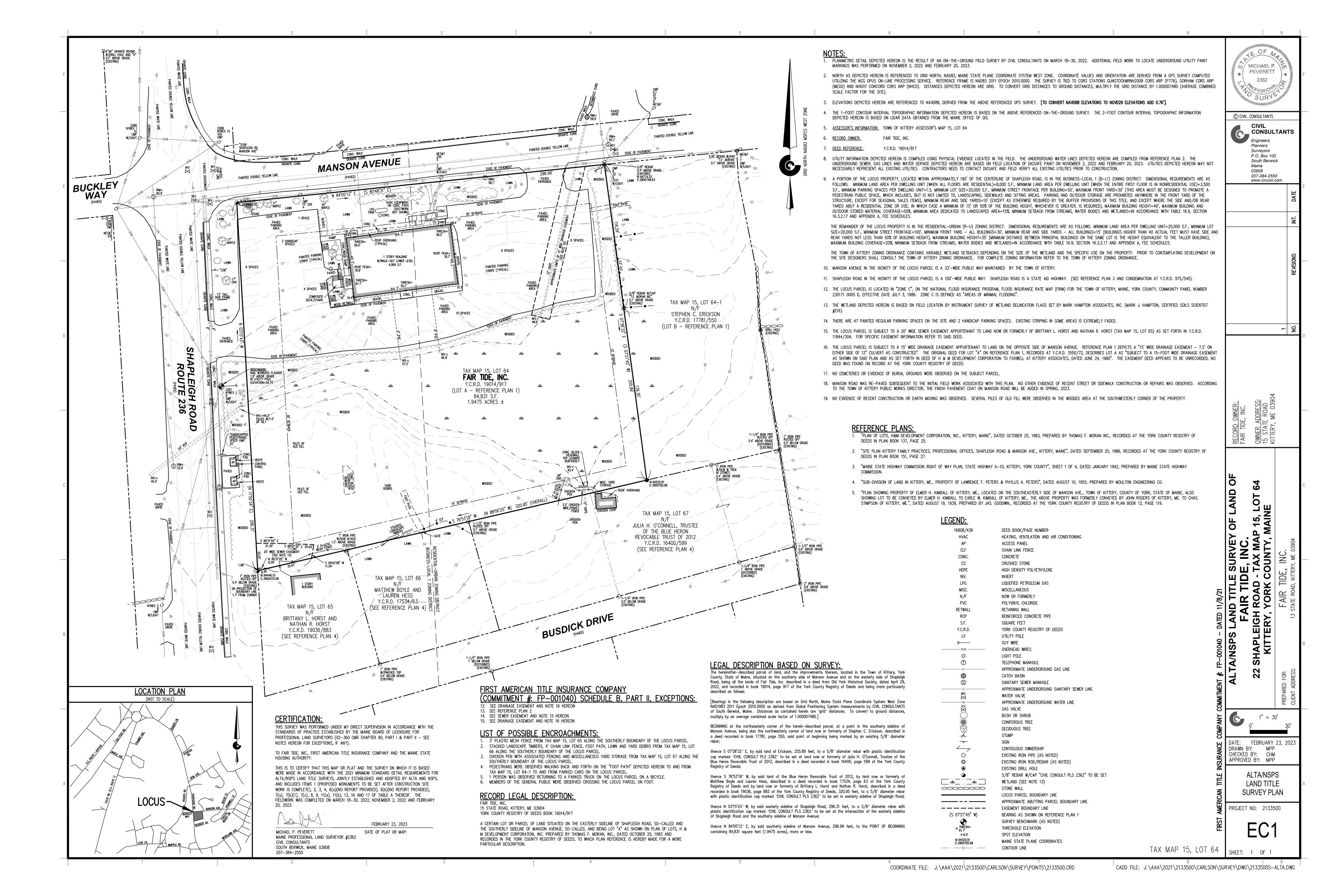
CONSTRUCTION DETAILS

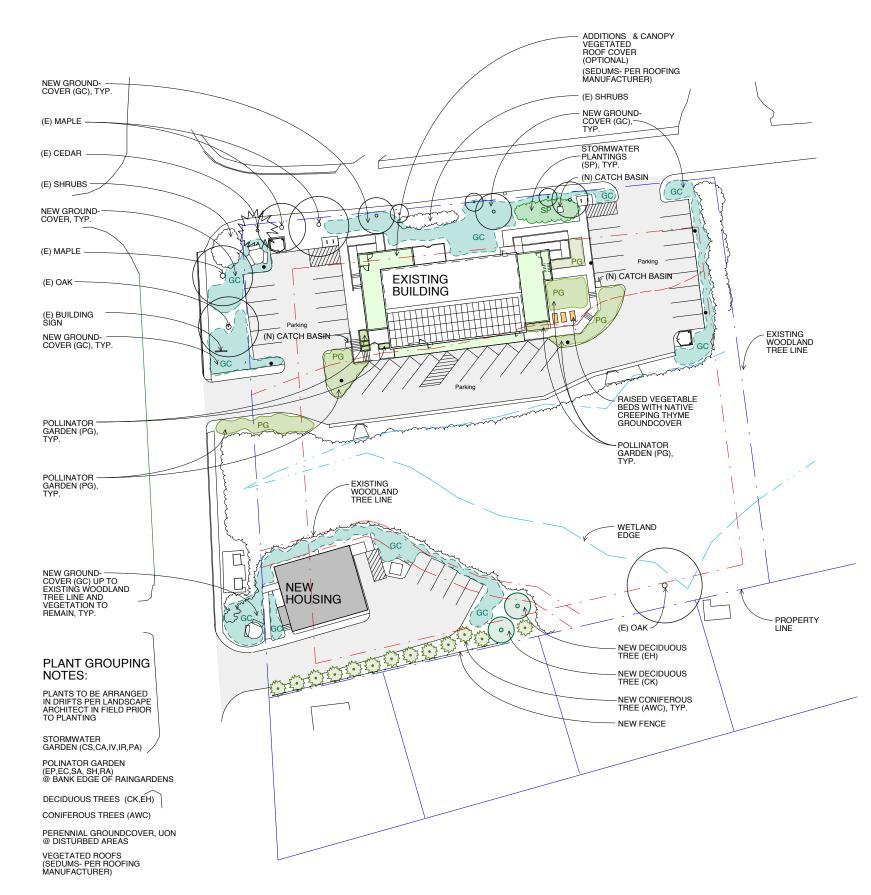
PROJECT NO: 21-335.00

L4

SHEET: 4 OF 4







PLANT SCHEDULE

ID	BOTANICAL NAME C	OMMON NAME	SIZE	
CON	NIFEROUS TREES			
AWC	CHAMAECYPARIS THYOIDES	ATLANTIC WHITE CEDAR 4' OC	4'-6'	
DEC	CIDUOUS TREES			
CK	CORNUS KOUSA	KOUSA DOGWOOD	10'-12'	
EH	CARPINUS BETULUS	EUROPEAN HORNBEAM	10'-12'	
STC	DRM-WATER GARDEN (SG)	Perennials/Grasses 24"	OC, Shrubs	4' OC
CS	CORNUS SERICEA	RED TWIGGED DOGWOOD	5 GAL.	
CA	CLETHRA ALN.	SUMMER SWEET	5 GAL.	
IV	ILEX VERTICILATTA	WINTERBERRY HOLLY	5 GAL.	
IR	IRIS VERSICOLOR	BLUE FLAG IRIS	PLUG	
PA	PANICUM	SWITCHGRASS	PLUG	
POL	LINATOR GARDEN (PG)	Perennials/Grasses 24" OC,	Shrubs 4' 0	С
EP	EUTROCHIUM PURPUREAUM	JOE PYE WEED	1 GAL.	
EC	ECHINAEA PURPUREAUM	CONE FLOWER	1 GAL.	
SA	SALVIA	MEADOW SAGE "May Night"	1 GAL.	
SH	SPOROBOLUS HETEROLEPSIS	PRAIRIE DROP SEED	PLUG	
RA		LOW GROUND SUMAC	5 GAL.	
PAC	POLYSTICHUM ACROSTICHOID	ES CHRISTMAS FERN	1 GAL.	
VEG	SETATED ROOF - SEDUM TELEF	PHIUM - AUTUMN JOY SEDUM (OP	TIONAL)	
PER	ENNIAL GROUNDCOVER (GC)			
НА	HEMEROCALLIS SPECIES	DAYLILLIES (SUN)	1 GAL.	
PAT	PEROVSKIA ATRIPLICIFOLA	RUSSIAN SAGE (SUN)	1 GAL.	
AC	ASARUM CANADENSE	WILD GINGER (SHADE)	1 GAL.	
GO	GALIUM ODORATUM	SWEET WOODRUF (SHADE)	1 GAL.	
AM	ALCHEMILLA MOLLIS	LADY'S MANTLE (SHADE)	1 GAL.	

SYMBOLS LEGEND



EXISTING DECIDUOUS TREE
EXISTING EVERGREEN



PROPOSED DECIDUOUS TREE (SHADED)

PROPOSED EVERGREEN TREE

PLANTING NOTES:

TREE

- 1. THE CONTRACTOR SHALL PREPARE PLANTING ZONES TO THE GRADES AND DEPTHS AS INDICATED ON THE DRAWINGS.
- 2. IF THE CONTRACTOR DETERMINES THE SUB-GRADE SOIL CONDITIONS ARE DELETERIOUS TO PLANT GROWTH OR WILL INHIBIT DRAINAGE, THE LANDSCAPE ARCHITECT SHALL BE NOTIFIED IMMEDIATELY AND PRIOR TO INSTALLATION OF PLANT MATERIAL.
- 3. TOPSOIL SHALL BE FREE FROM SUBSOIL, STONES LARGER THAN 1", OR ANY UNDESIRABLE MATERIAL; CONTAIN 5% ORGANIC MATTER AND HAVE A pH SUITABLE TO THE LOCAL GROWING CONDITIONS.
- 4. ALL PLANTS TO BE SELECTED AND SEALED IN THE FIELD BY THE LANDSCAPE DESIGNER OR SELECTED BY THE LANDSCAPE CONTRACTOR, AND APPROVED BY LANDSCAPE DESIGNER.
- 5. THE PLANT LIST IS PROVIDED AS A CONVENIENCE TO THE CONTRACTOR. IN THE EVENT OF A DISCREPANCY BETWEEN THE PLANT COUNT SHOWN IN THE SCHEDULE AND THE DRAWING, THE DRAWING SHALL TAKE PRECEDENCE.
- $6.\,$ ALL TRANSPLANTED SHRUBS SHALL BE "HEELED IN" OR HEAVILY MULCHED IN A SHADED AREA AND WATERED AS NECESSARY UNTIL THEY CAN BE PLANTED.
- 7. FINAL LOCATION OF ALL PLANTS TO BE DETERMINED IN THE FIELD BY THE LANDSCAPE ARCHITECTS PRIOR TO INSTALLATION OF PLANT MATERIAL.
- 8. PLANTS SHALL BEAR SAME RELATIONSHIP TO FINISHED GRADE AS THE BORE TO THE EXISTING GRADE IN THE NURSERY.
- 9. CUT AND REMOVE BURLAP FROM TOP 1/3 OF BALL. CUT AND REMOVE AT LEAST 1/3-1/2 OF WIRE BASKET. NYLON ROPE AND / OR NYLON BALLING MATERIAL IS NOT ACCEPTABLE.
- 10. LOCATE GUY WIRES AROUND MAIN TRUNK OF TREE.
- 11. PLANT PERENNIALS AND GROUNDCOVER IN 12" DEEP TOPSOIL BED CONSISTING OF 2/3 TOPSOIL AND 1/3 HUMUS.
- 12. TOPSOIL AND SEED ALL AREAS DISTURBED AS A RESULT OF ANY AND ALL DISTURBANCES, CONSTRUCTION, OR STORAGE OF EQUIPMENT WHETHER SUCH AREAS ARE SHOWN ON THE PLANS OR NOT. (SEE GRADING PLAN)
- 13. ALL PLANTS AND ENTIRE SHRUB BEDS TO RECEIVE 12" OF CASSELA'S ORGANICS OR EQUAL (40% COMPOST / 60% LOAM) AND A 3" LAYER OF DOUBLE SHREDDED HARDWOOD BARK MULCH.
- 14. UPON COMPLETION OF THE ONE (1) YEAR PLANT GUARANTEE PERIOD, THE LANDSCAPE CONTRACTOR IS RESPONSIBLE FOR ADJUSTING OR REMOVING ALL STAKES. THIS SHALL BE DONE IN CONSULTATION WITH THE LANDSCAPE ARCHITECT.
- 15. ALL TREE PLANTING AND REMOVAL TO COMPLY WITH LOCAL AND STATE TREE ORDINANCES.

PROJECT:

MAINSPRING COLLECTIVE

Fairtide + Footprints 22 Shapleigh Road, Kittery, ME

ARQ® Architects
1 Government St, Suite 2
Kittery, Maine 03904
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Summit Engineering, Structural Eng 5 Greenleaf Woods Dr #302 Portsmouth, NH 03801 603-319-1817

Sefco Solutions, Mechanical Eng 408 Main Street, South Berwick, ME 207-420-8760

Oakpoint Associates, Electrical Eng 85 Middle St., Portsmouth, NH 03801 603-431-4849

RyBak Engineering Inc Fire Protection 132 Forest Avenue Warren, MA 01083-0709 413-436-5500

Soren DeNoird, Landscape Architect 43 Wellwood Road Portland, ME 04103 207-400-2450

Civil Consultants PO BOX 100, South Berwick ME 03908 207-384-2550

NOTES:

REVISIONS :

KEVIS	REVISIONS.							
NO	DATE	REVISION						

LANDSCAPE PLAN



0 6 12 24 48

Schematic Design February 17, 2023 Revised 4-4-23



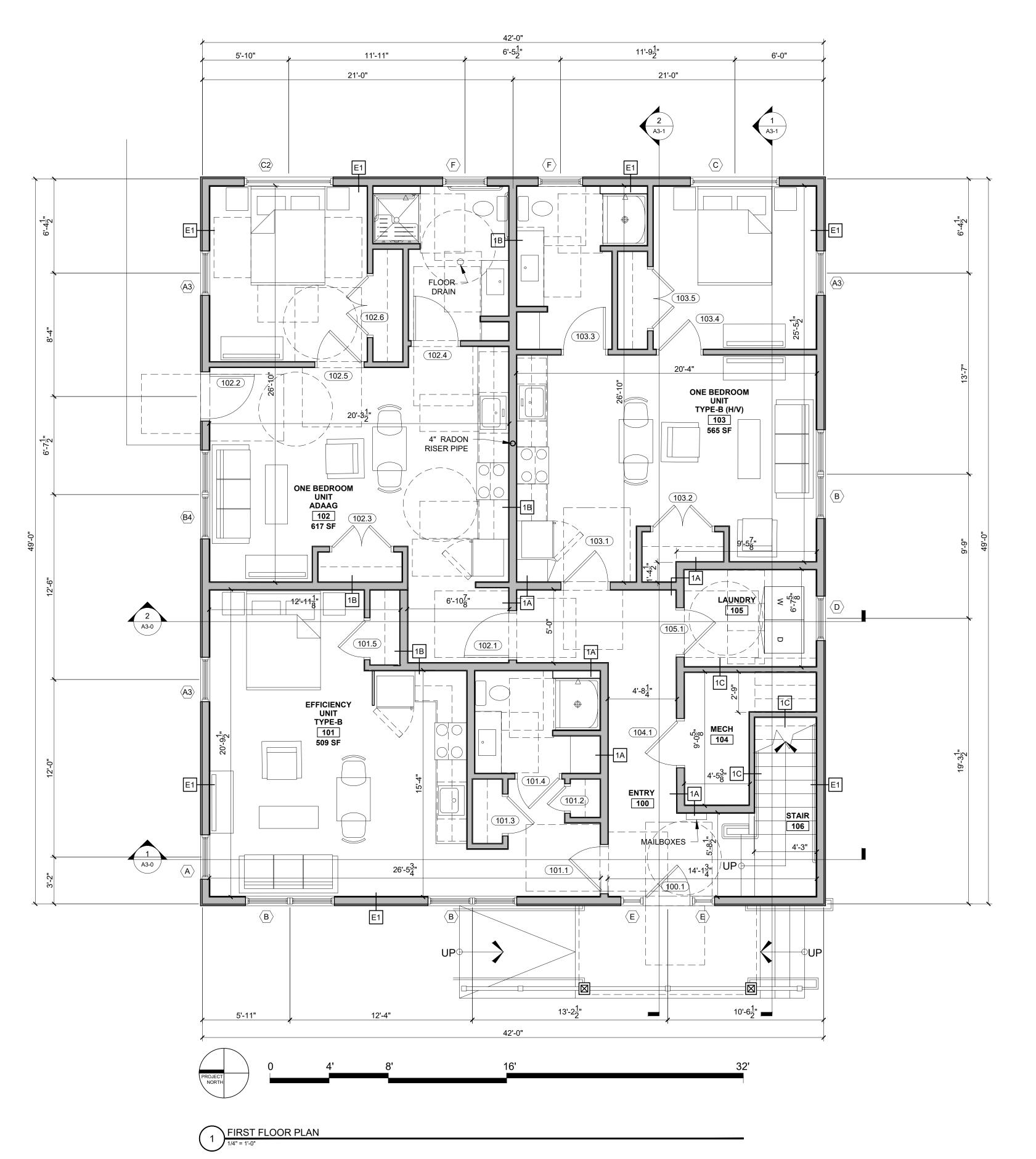
DATE: 2-17-23
PROJECT NO: 2022-10
DRAWING BY: JO
CHECK BY: LS
DWG NO:

FILE No:

GULATION: HUD 504 AND ADA, STANDARD: ADAAG 2010	PROVIDED IN PROJECT	EXCESS UNITS
SCOPING REQUIREMENT: 5% units accessible and additional 2% of units to be hearing and vision impaired		
6 units within building X 5% = 0.30 or 1 units to meet ADAAG	1 ADAAG units	0 Excess
6 units within building X 2% = 0.12 or 1 units to be hearing and vision impaired	1 Hearing and Vision Impaired Units	0 Excess
EGULATION: MAINE HUMAN RIGHTS ACT (MHRA), STANDARD: ANSI A117.1-2009		
SCOPING REQUIREMENT: 10% of Ground Floor units to be Type A		
3 Ground Floor (First Floor total) Units X 10% = 0.30 or 1 units	1 Type-A units	0 Excess
SCOPING REQUIREMENT: 10% of Upper Floor units to be Type A (NOT REQUIRED)		
(THERE IS NO REQUIREMENT FOR AN ACCESSIBLE UNIT ON THE SECOND FLOOR OF A BUILDING THAT IS NOT SERVICED BY AN ELEVATOR)	0 Type-A units	0 Excess
	1 Type-A units total (INCLUDES ADAAG)	
All the rest to be Type B	5 Type-B units (includes 1 H/V)	
MHRA requires ALL units to either be Type A or B units		

TOTALS	1 STUDIO UNITS	5 ONE BEDROOM UNITS	0 TWO BEDROOM UNITS	0 THREE BEDROOM UNITS				
SECOND FLOOR	0 STUDIO UNITS	3 ONE BEDROOM UNITS	0 TWO BEDROOM UNITS	0 THREE BEDROOM UNITS				
FIRST FLOOR	1 STUDIO UNITS	2 ONE BEDROOM UNITS	0 TWO BEDROOM UNITS	0 THREE BEDROOM UNITS				
UNIT TYPES - 6 TOTAL UNITS								

ACCESSIBLE	E UNIT ⁻	TYPES							
FLOOR	TYPE - A STUDIO	TYPE - A ONE BED		H/V IMPAIRED ONE BED	TYPE - A TWO BED	TYPE - ADDAG TWO BED	H/V IMPAIRED TWO BED	TYPE - A THREE BED	TYPE - ADDAG THREE BED
FIRST FLOOR	0	0	1	1	0	0	0	0	0
SECOND FLOOR	0	0	0	0	0	0	0	0	0
TOTALS	0	0	1	1	0	0	0	0	0



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TMENTS

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senatorearchitecture.com

CONSULTANTS:

PROGRESS PRINT ONLY
MARCH 07, 2023

DATE:
PROJECT No. 2
DRAWN BY: RRT,

CHECKED BY: RJS

SCALE: AS NOTED

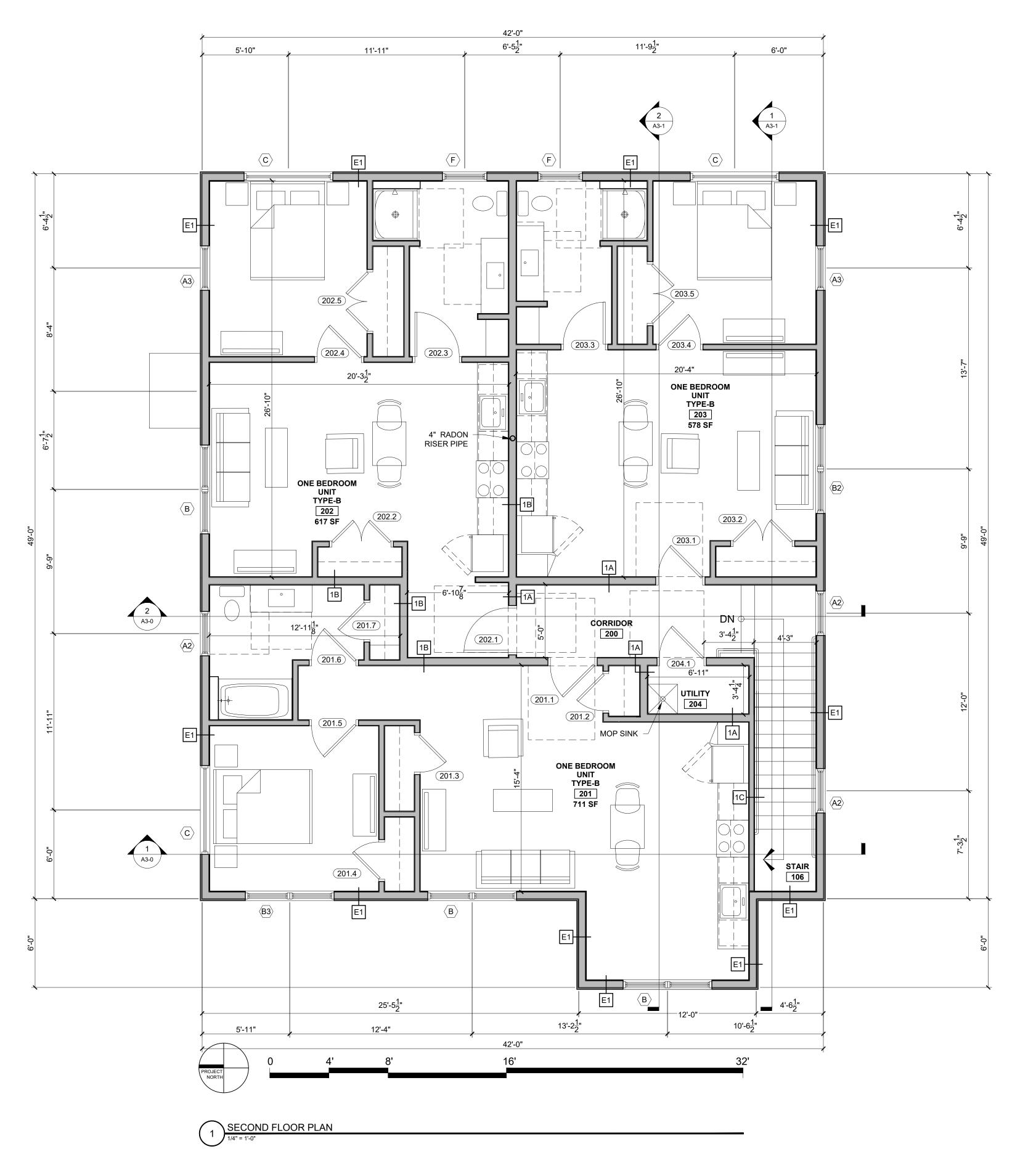
SHEET TITLE:
FIRST FLOOR
PLAN

A1-1

GULATION: HUD 504 AND ADA, STANDARD: ADAAG 2010	PROVIDED IN PROJECT	EXCESS UNITS
SCOPING REQUIREMENT: 5% units accessible and additional 2% of units to be hearing and vision impaired		
6 units within building X 5% = 0.30 or 1 units to meet ADAAG	1 ADAAG units	0 Excess
6 units within building X 2% = 0.12 or 1 units to be hearing and vision impaired	1 Hearing and Vision Impaired Units	0 Excess
EGULATION: MAINE HUMAN RIGHTS ACT (MHRA), STANDARD: ANSI A117.1-2009		
SCOPING REQUIREMENT: 10% of Ground Floor units to be Type A		
3 Ground Floor (First Floor total) Units X 10% = 0.30 or 1 units	1 Type-A units	0 Excess
SCOPING REQUIREMENT: 10% of Upper Floor units to be Type A (NOT REQUIRED)		
(THERE IS NO REQUIREMENT FOR AN ACCESSIBLE UNIT ON THE SECOND FLOOR OF A BUILDING THAT IS NOT SERVICED BY AN ELEVATOR)	0 Type-A units	0 Excess
	1 Type-A units total (INCLUDES ADAAG)	
All the rest to be Type B	5 Type-B units (includes 1 H/V)	
MHRA requires ALL units to either be Type A or B units		

TOTALS	1 STUDIO UNITS	5 ONE BEDROOM UNITS	0 TWO BEDROOM UNITS	0 THREE BEDROOM UNITS				
SECOND FLOOR	0 STUDIO UNITS	3 ONE BEDROOM UNITS	0 TWO BEDROOM UNITS	0 THREE BEDROOM UNITS				
FIRST FLOOR	1 STUDIO UNITS	2 ONE BEDROOM UNITS	0 TWO BEDROOM UNITS	0 THREE BEDROOM UNITS				
UNIT TYPES - 6 TOTAL UNITS								

ACCESSIBLE UNIT TYPES								
			H/V IMPAIRED ONE BED	TYPE - A TWO BED	TYPE - ADDAG TWO BED	H/V IMPAIRED TWO BED	TYPE - A THREE BED	TYPE - ADDAG THREE BED
0	0	1	1	0	0	0	0	0
0	0	0	0	0	0	0	0	0
0	0	1	1	0	0	0	0	0
	TYPE - A STUDIO 0	TYPE - A STUDIO ONE BED 0 0 0 0	TYPE - A STUDIO ONE BED ONE BED 0 0 1 0 0 0	TYPE - A TYPE - A TYPE - ADDAG ONE BED ONE BED 0 0 1 1 1 0 0 0 0	TYPE - A STUDIO TYPE - A ONE BED TYPE - A ONE BED H/V IMPAIRED ONE BED TYPE - A TWO BED 0 0 1 1 0 0 0 0 0 0	TYPE - A STUDIO TYPE - A ONE BED TYPE - ADDAG ONE BED H/V IMPAIRED ONE BED TYPE - A TWO BED TYPE - ADDAG TWO BED 0 0 1 1 0 0 0 0 0 0 0	TYPE - A STUDIO TYPE - A ONE BED TYPE - ADDAG ONE BED H/V IMPAIRED ONE BED TYPE - A TWO BED TYPE - ADDAG TWO BED H/V IMPAIRED TWO BED 0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0	TYPE - A STUDIO TYPE - A ONE BED TYPE - ADDAG ONE BED H/V IMPAIRED ONE BED TYPE - A TWO BED TYPE - ADDAG TWO BED H/V IMPAIRED TWO BED TYPE - A TWO BED 0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0



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ARTMENTS APLEIGH ROAD

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CONSULTANTS:

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MARCH 07, 2023

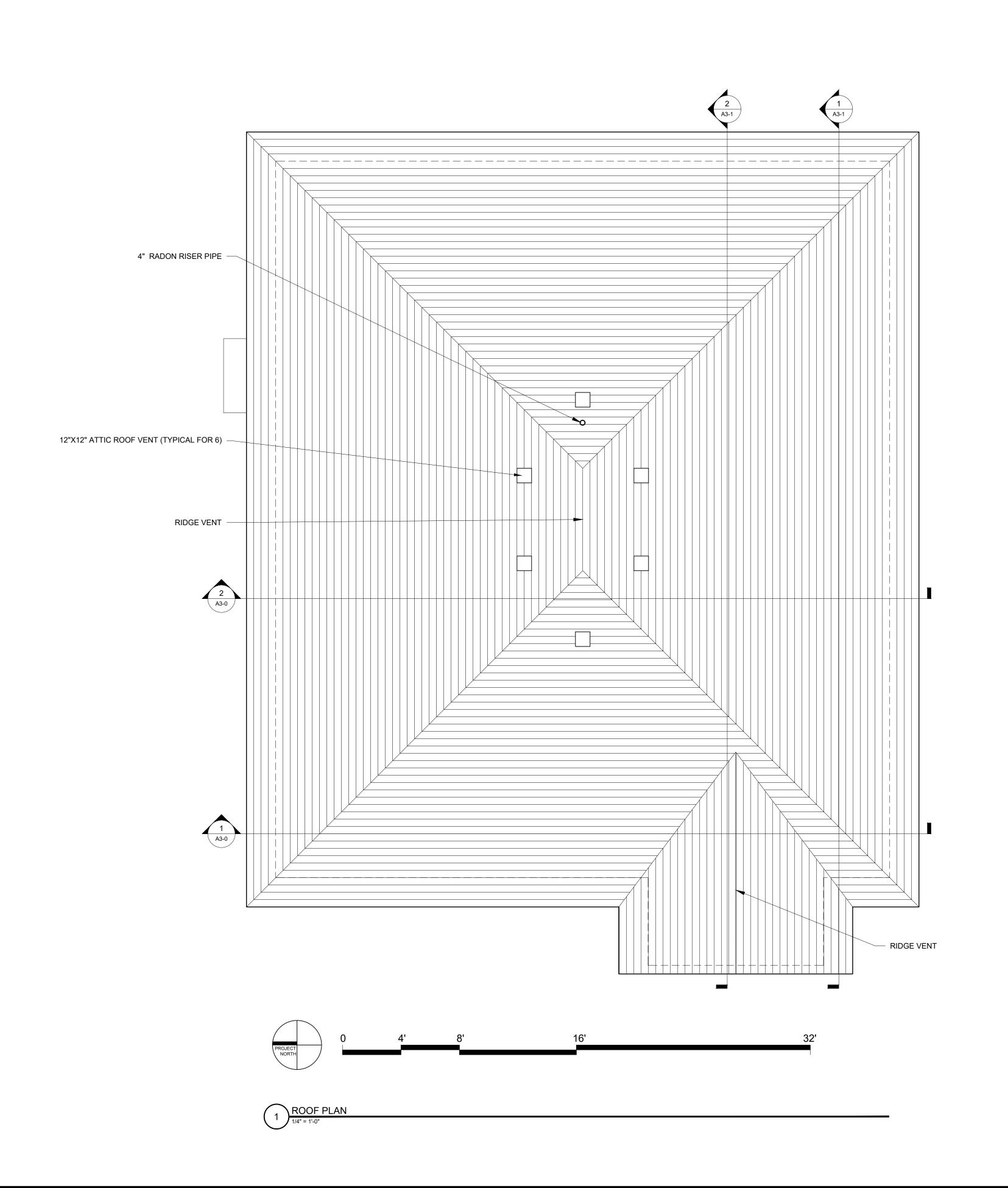
DATE:
PROJECT No. 217
DRAWN BY: RRT, RJ:

CHECKED BY: RJS

SCALE: AS NOTED

SECOND FLOOR PLAN

A1-2

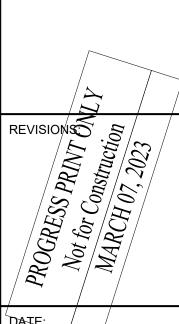


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SHAPLEIGH ROAD



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SCALE: AS NOTED

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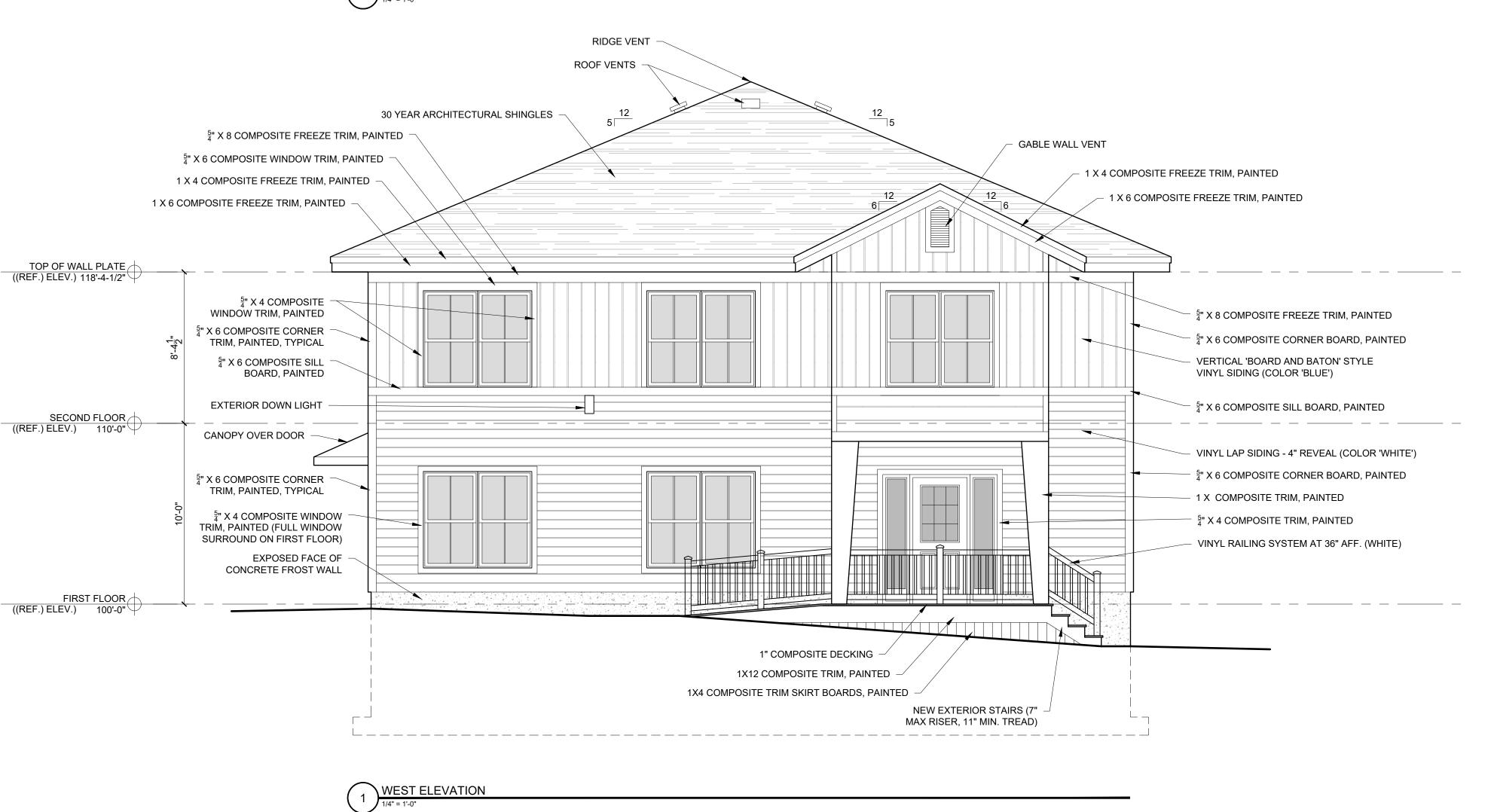
SHEET TITLE:
ROOF PLAN

A1-3



MEST ELEVATION (COLOR KEY ELEVATION)

1/4" = 1'-0"



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ARTMENTS
HAPLEIGH ROAD

AP

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PROJECT No.

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SCALE: AS NOTED

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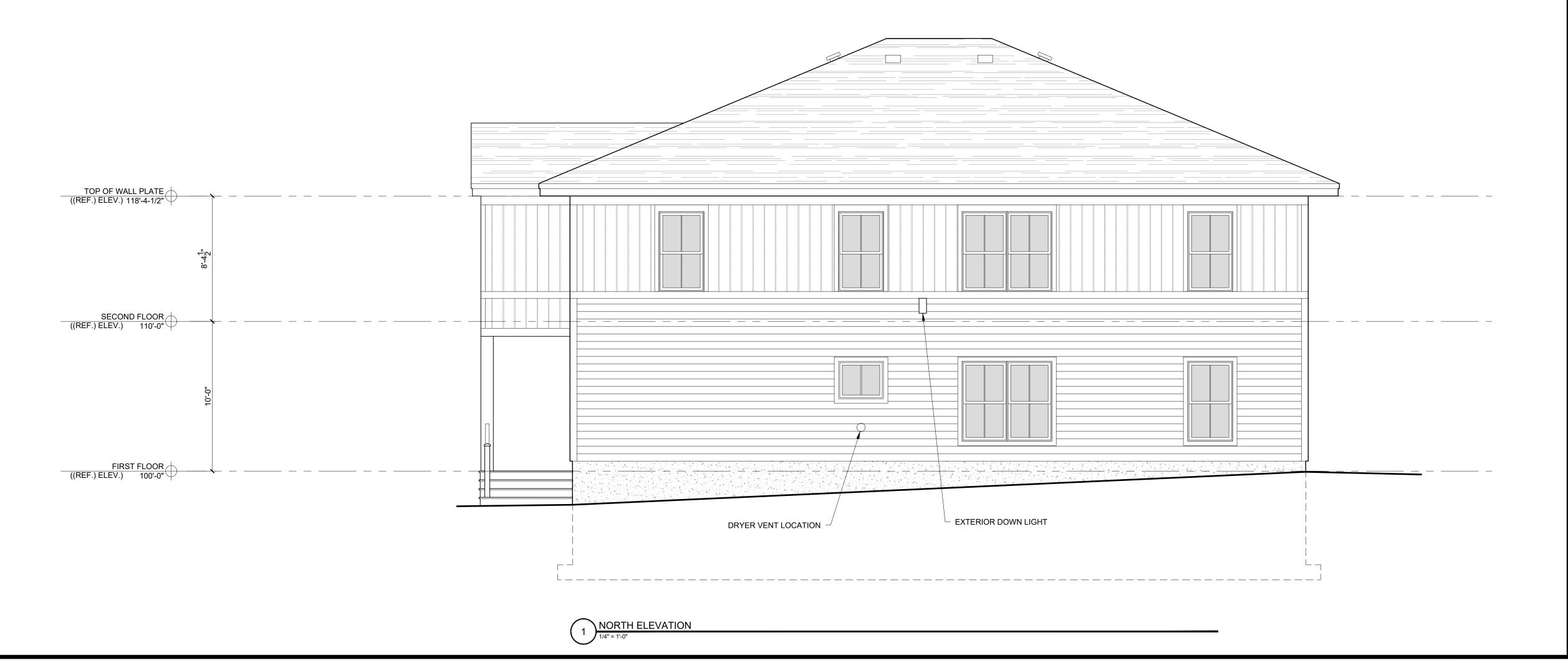
WEST ELEVATION

A2-C



NORTH ELEVATION (COLOR KEY ELEVATION)

1/4" = 1'-0"



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APARTMENTS
22 SHAPLEIGH ROAD
KITTERY, MAINE

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MARCH 07, 2023

DATE:
PROJECT No.

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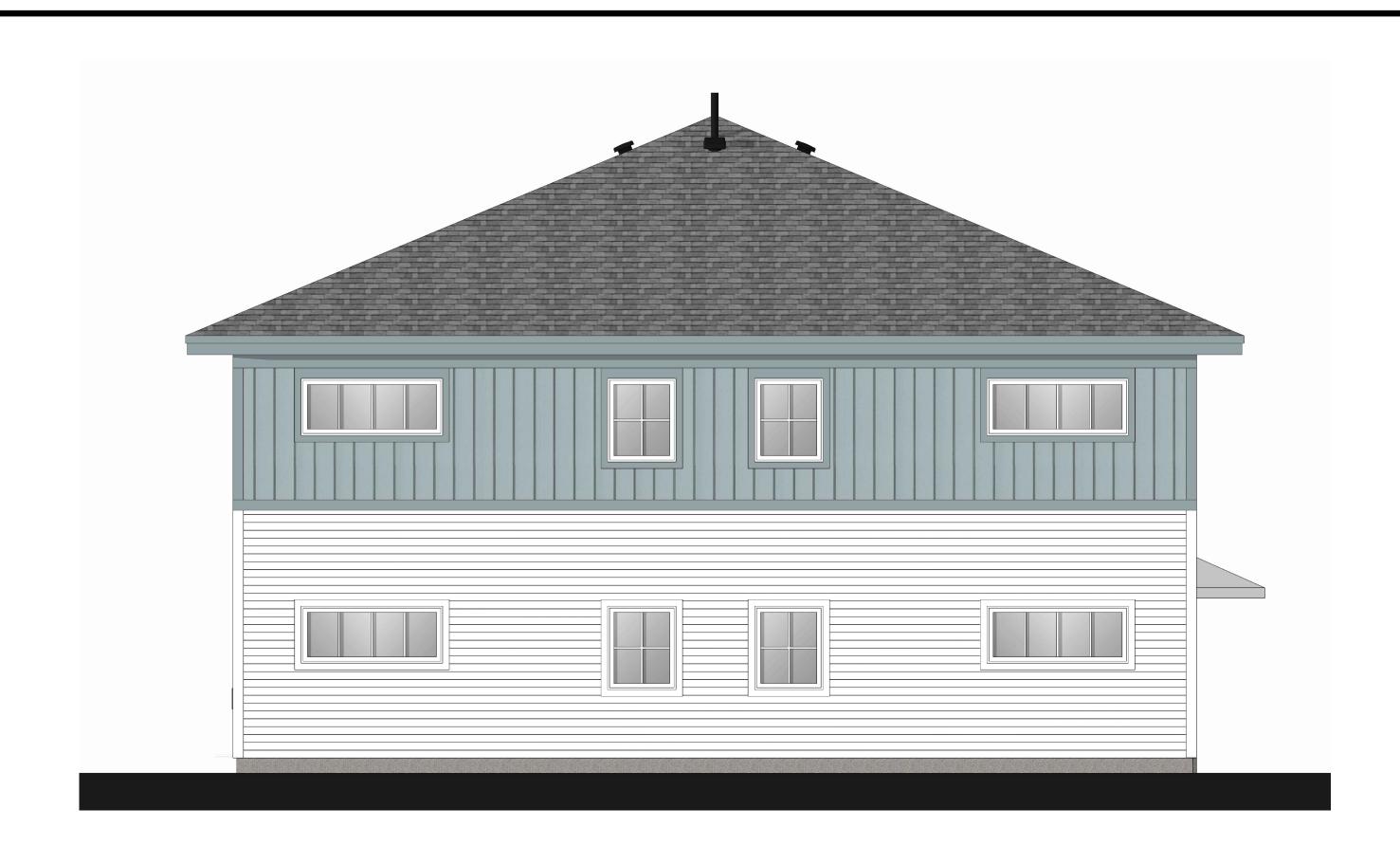
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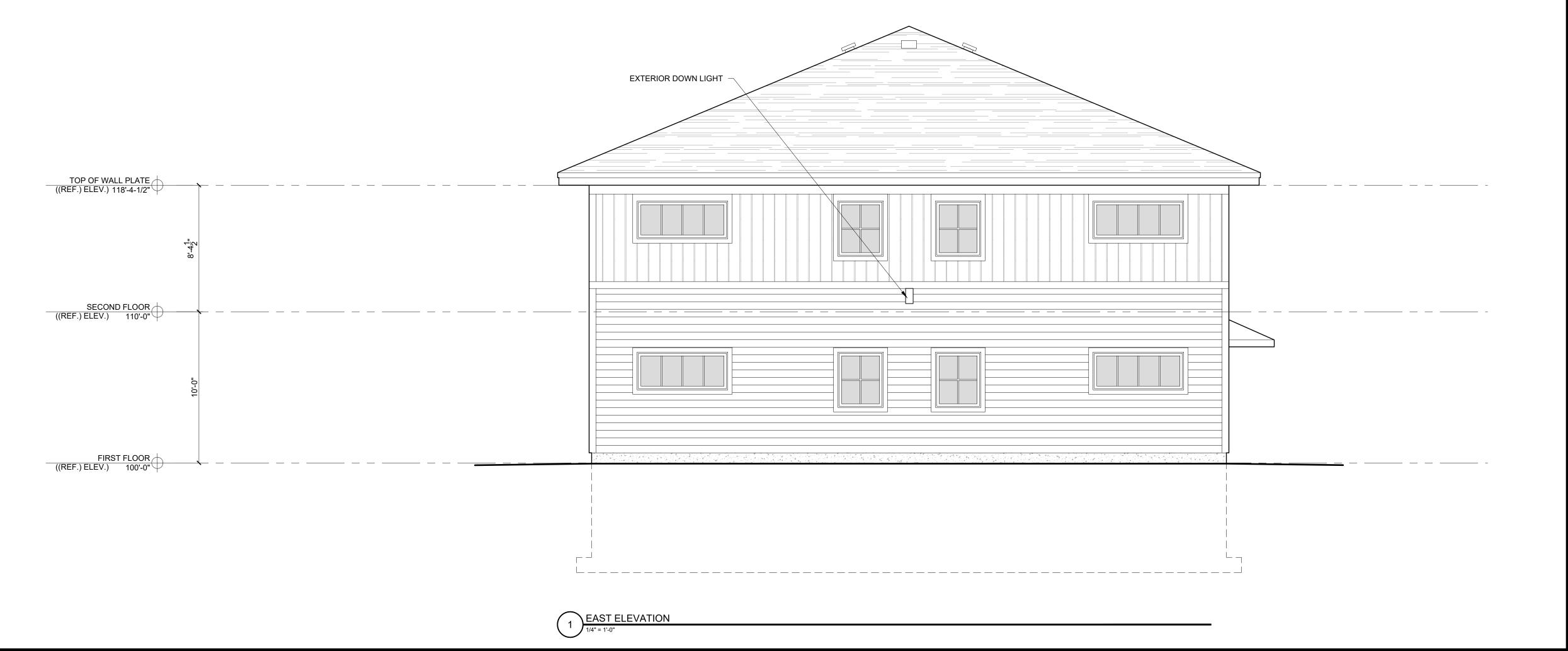
SHEET TITLE:

NORTH ELEVATION

A2-1



1B EAST ELEVATION (COLOR KEY ELEVATION)



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APARTMENTS
22 SHAPLEIGH ROAD
KITTERY, MAINE

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CONSULTANTS:

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MARCH 07, 2023

DATE:
PROJECT No. 21

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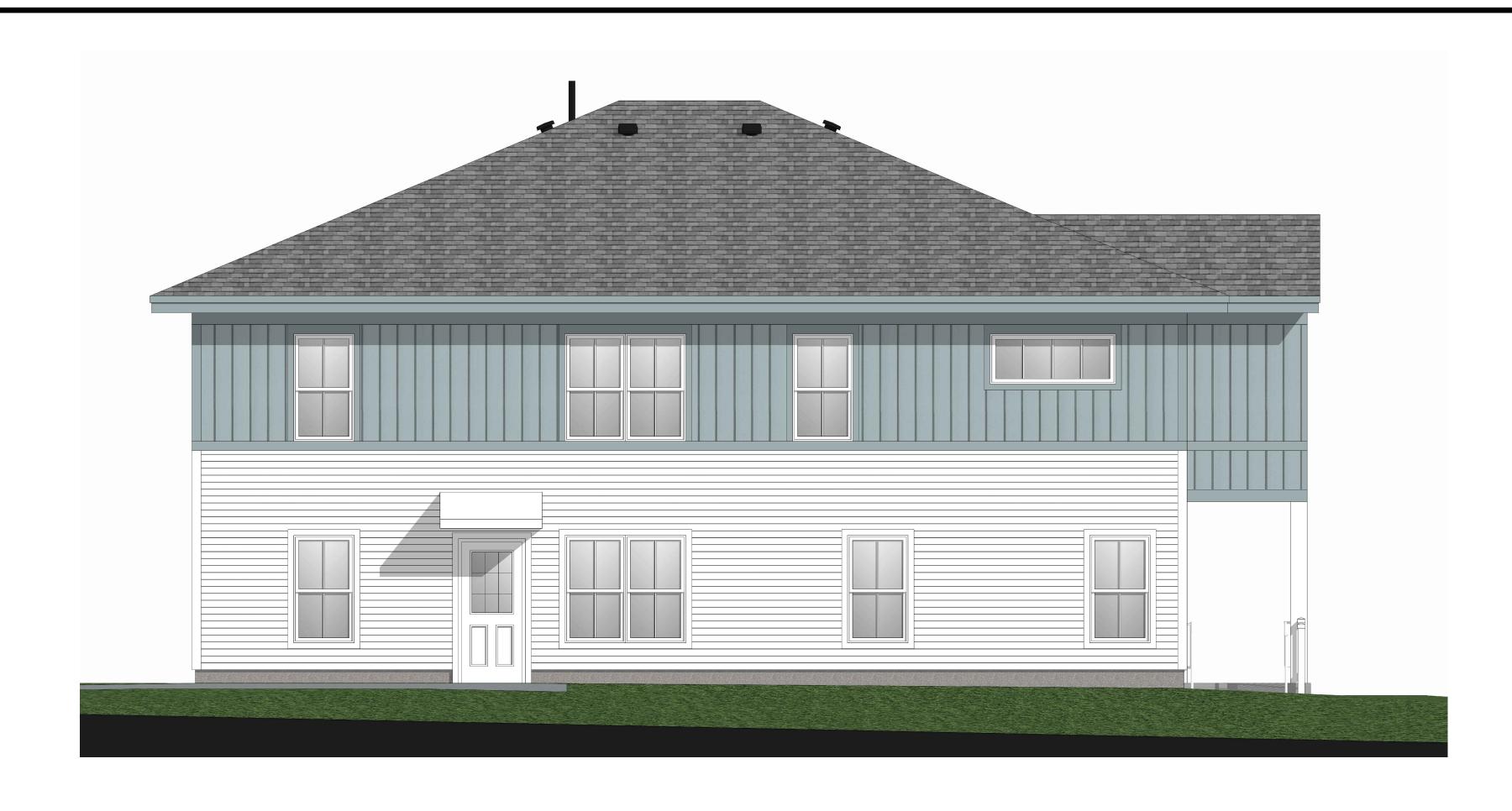
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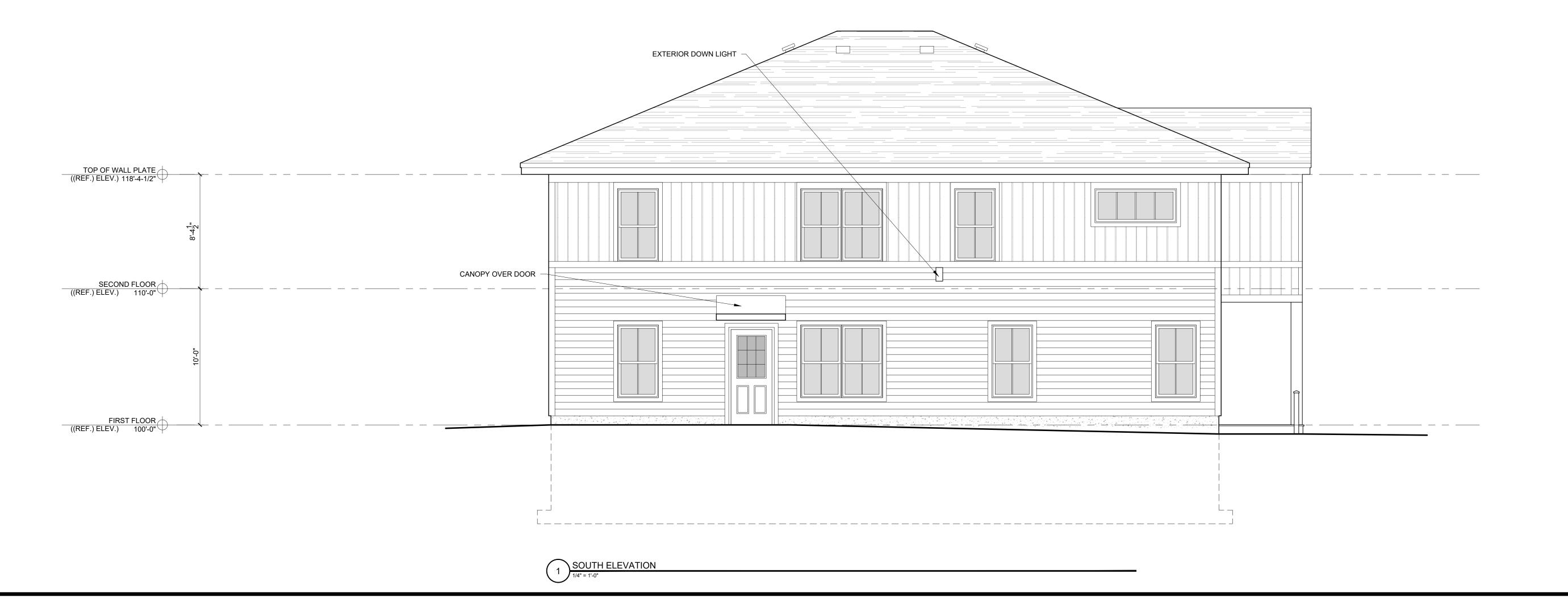
SHEET TITLE:

EAST ELEVATION

A2-2



1B SOUTH ELEVATION (COLOR KEY ELEVATION)



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APARTMENTS
2 SHAPLEIGH ROAD
KITTERY, MAINE

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CONSULTANTS:

PROGRESS PRONT CALY
Not for Construction
MARCH 07, 2023

DATE:
PROJECT No. 2

DRAWN BY: RRT, RJS

CHECKED BY: RJS

SCALE: AS NOTED

SHEET TITLE:

SOUTH ELEVATION

A2 - 3

RESIDENCES

22 SHAPLEIGH RD, KITTERY, MAINE



COLOR OPTION 1-1

RESIDENCES

22 SHAPLEIGH RD, KITTERY, MAINE



22 SHAPLEIGH RD, KITTERY, MAINE

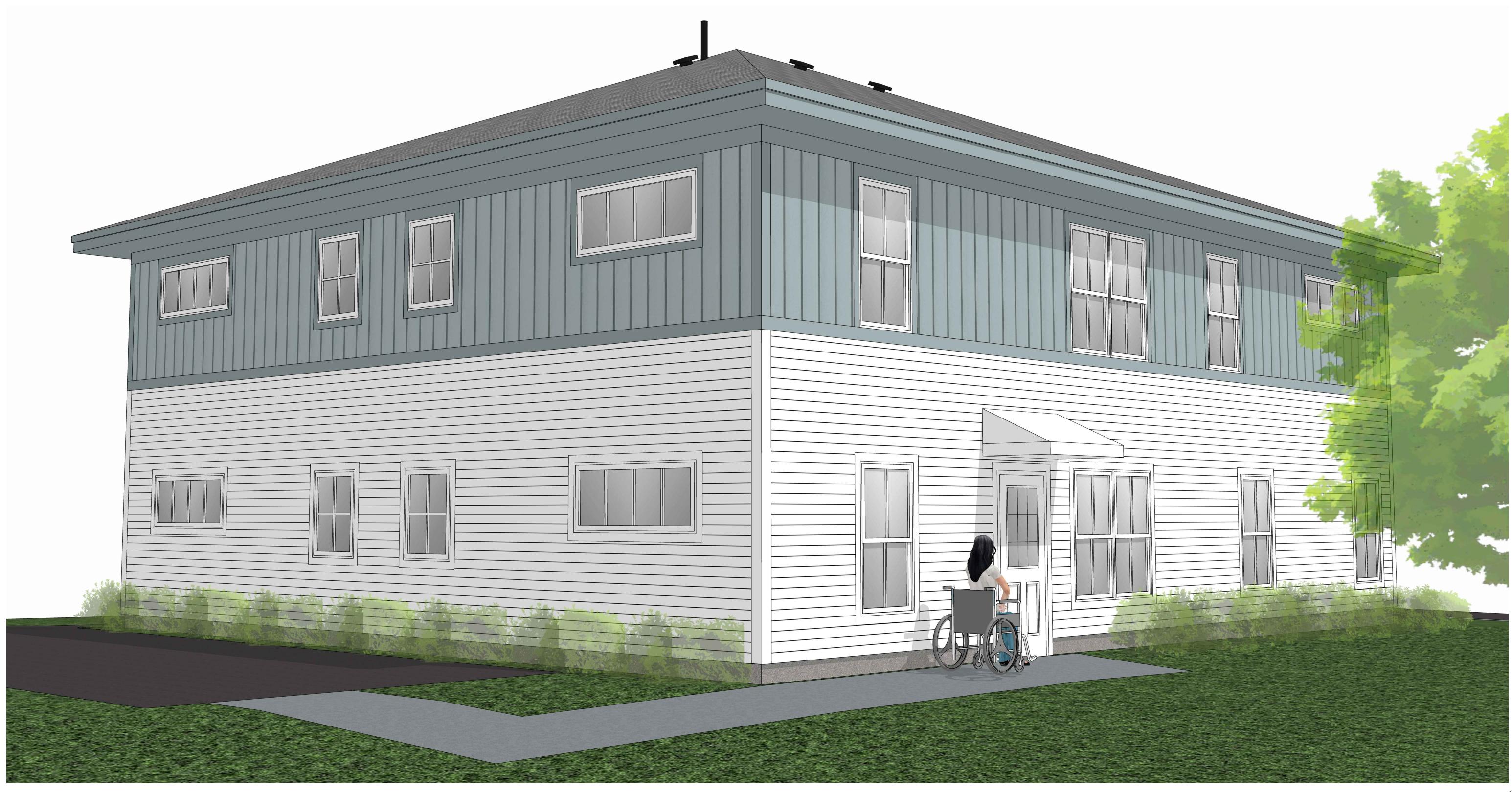


1 COLOR OPTION 1-3

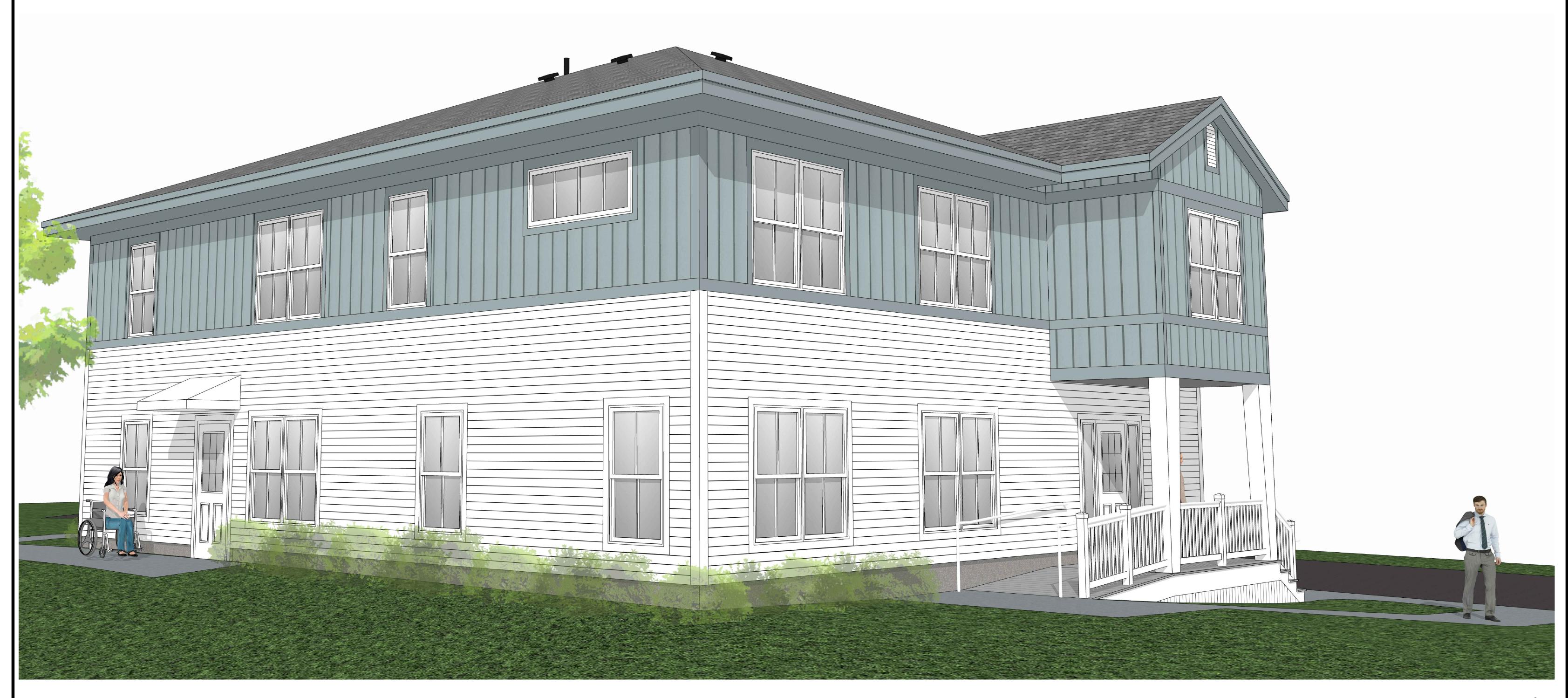
PROGRESS PRINT ONLY
Not for Construction

RESIDENCES

22 SHAPLEIGH RD, KITTERY, MAINE



22 SHAPLEIGH RD, KITTERY, MAINE



1 COLOR OPTION 1-5







MAINSPRING COLLECTIVE

Fairtide + Footprints 22 Shapleigh Road, Kittery, ME

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Kittery, Maine 03904
207.439.5286 © 2023 ARQ architects

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Sefco Solutions, Mechanical Eng 408 Main Street, South Berwick, ME 207-420-8760

Oakpoint Associates, Electrical Eng 85 Middle St., Portsmouth, NH 03801 603-431-4849

Ferguson Fire Design LLC 132 Forest Avenue Warren, MA 01083-0709 413-436-5500

Soren DeNoird, Landscape Architect 43 Wellwood Road Portland, ME 04103 207-400-2450

Civil Consultants PO BOX 100 South Berwick ME 03908 207-384-2550

NOTES:

- 1. Color Palette similar- all elevations
- 2. Vegetative Plant Cover (Optional)
- 3. Solar Array (Optional)

REVISIONS:

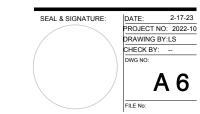
NO	DATE	REVISION

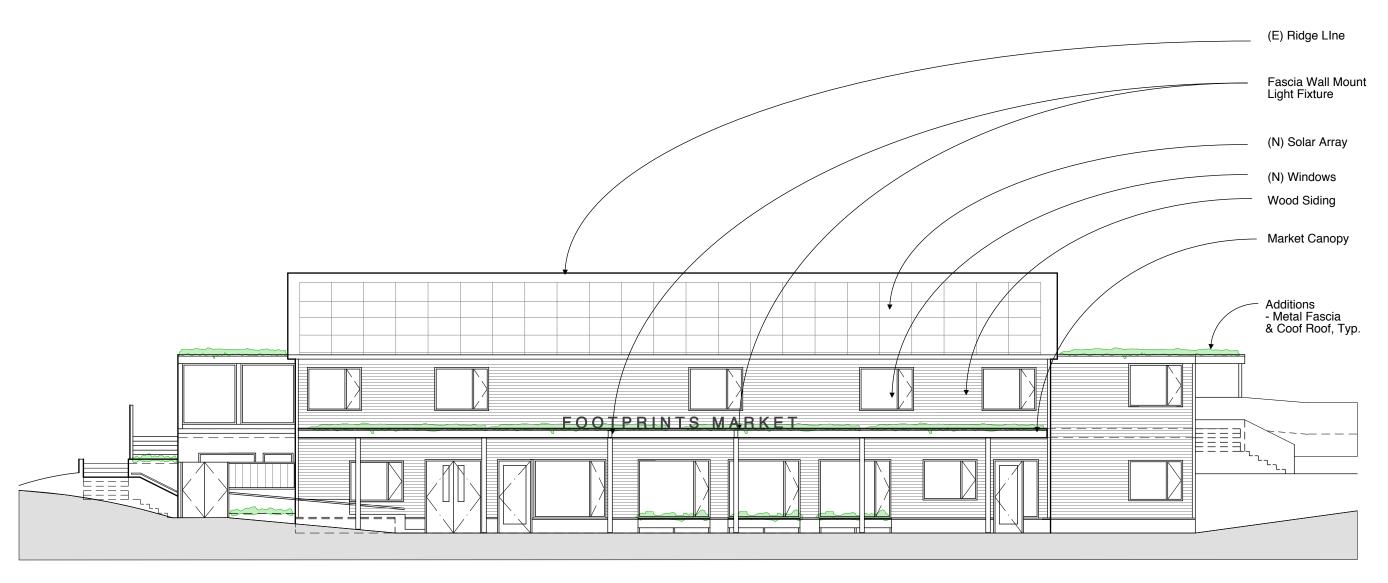
WEST ELEVATION

0 1' 2' 4'

Schematic Design February 17, 2023 Revised April 4, 2023

A 6





MAINSPRING COLLECTIVE

Fairtide + Footprints 22 Shapleigh Road, Kittery, ME

ARQ® Architects
1 Government St, Suite 2
Kittery, Maine 03904
207.439.5286
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Summit Engineering, Structural Eng 5 Greenleaf Woods Dr #302 Portsmouth, NH 03801 603-319-1817

Sefco Solutions, Mechanical Eng 408 Main Street, South Berwick, ME 207-420-8760

Oakpoint Associates, Electrical Eng 85 Middle St., Portsmouth, NH 03801 603-431-4849

Ferguson Fire Design LLC 132 Forest Avenue Warren, MA 01083-0709 413-436-5500

Soren DeNoird, Landscape Architect 43 Wellwood Road Portland, ME 04103 207-400-2450

Civil Consultants PO BOX 100 South Berwick ME 03908 207-384-2550

NOTES:

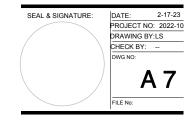
- Color Palette similar- all elevations See A6 for notes.
- 2. Vegetative Plant Cover (Optional)
- Solar Array (Optional)

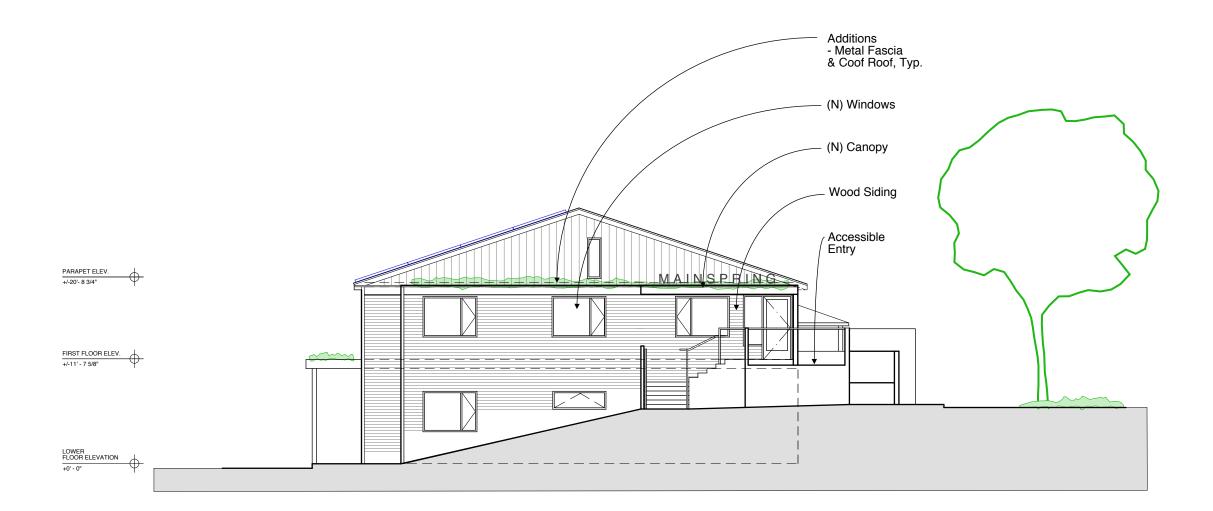
REVIS	REVISIONS:												
NO	DATE	REVISION											

SOUTH ELEVATION

0 1' 2' 4'

Schematic Design February 17, 2023 Revised April 4, 2023





MAINSPRING COLLECTIVE

Fairtide + Footprints 22 Shapleigh Road, Kittery, ME

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NOTES:

- Color Palette similar- all elevations See A6 for notes.
- 2. Vegetative Plant Cover (Optional)

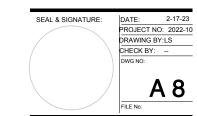
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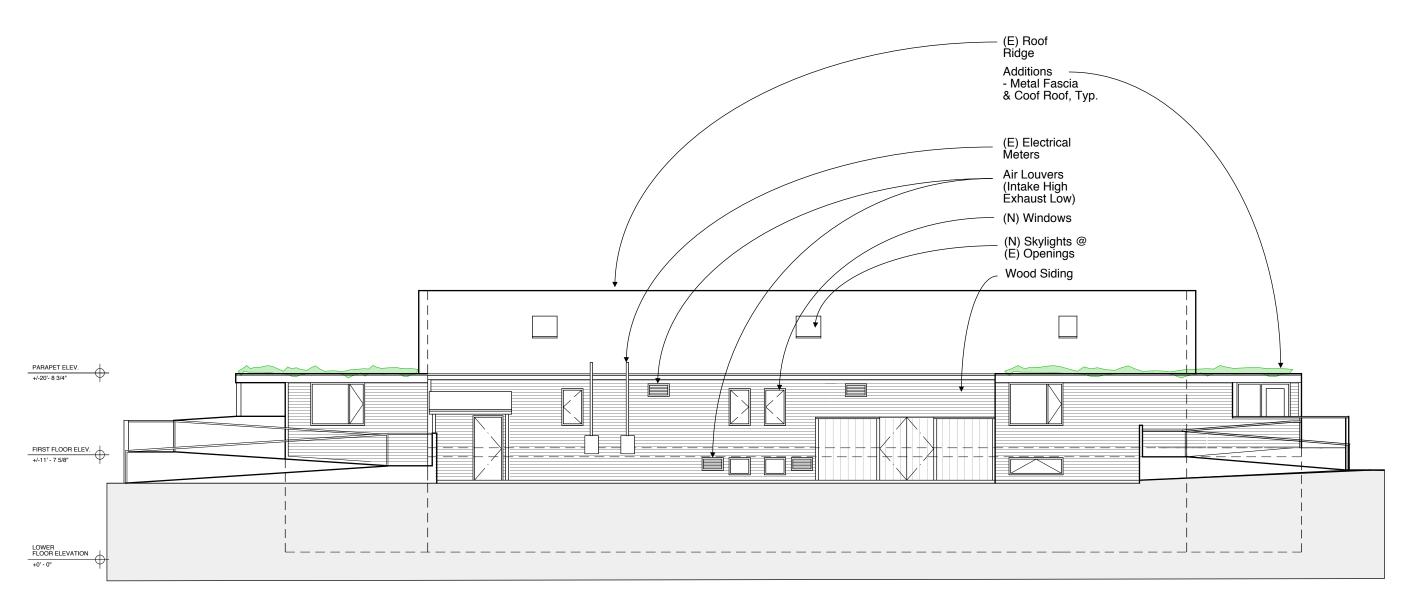
NO	DATE	REVISION

EAST ELEVATION



Schematic Design February 17, 2023 Revised April 4, 2023





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NOTES:

- Color Palette similar- all elevations See A6 for notes.
- 2. Vegetative Plant Cover (Optional)

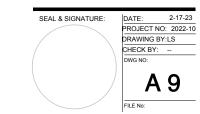
REVISIONS:

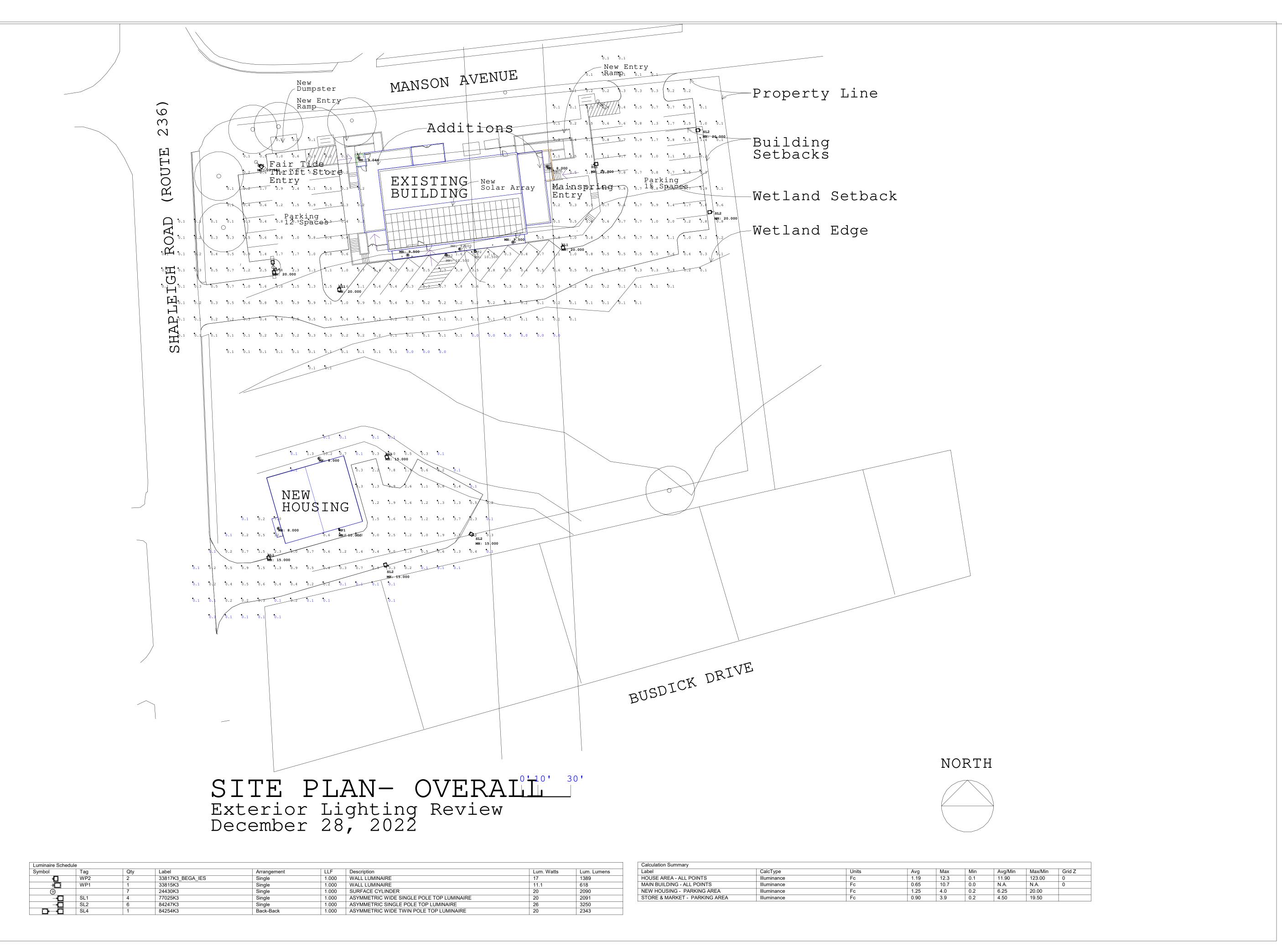
NO	DATE	REVISION

NORTH ELEVATION



Schematic Design February 17, 2023 Revised April 4, 2023

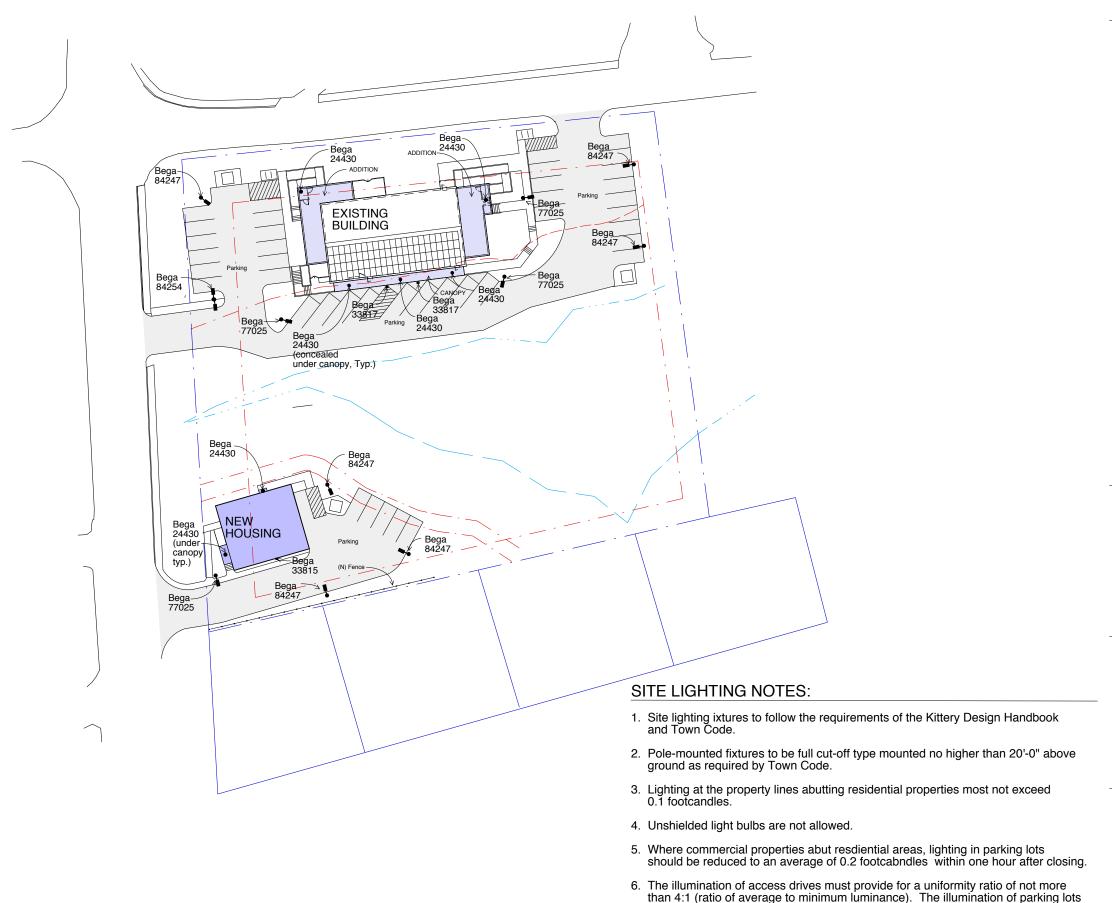




Page 1 of 1

PROPOSED

Revisions



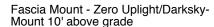
FIXTURE TYPE 1: BEGA 33817 K3

Wall Mount Tag WP2

Lamp: 17 W CCT/CRI: 3000 K 80 CRI Lumens: 1389 lumen

Finish:

: 1389 lumen Black (BLK)



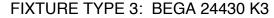
FIXTURE TYPE 2: BEGA 33815 K3

Wall Mount Tag WP1

Lamp: 11.1 W
CCT/CRI: 3000 K 80 CRI
Lumens: 618 lumen
Finish: White (WHT)

Surface Wall Mount - Zero Uplight/Darksky-

Mount 10' above grade



Single-Head

 Lamp:
 15.8 W

 CRI:
 3000 K

 Lumens:
 2,090 lumen

 Finish:
 Black

Ceiling-Mounted Under Canopy - Concealed by Fascia

FIXTURE TYPE 4: BEGA 77025 K3

Single Head Tag SL1

Lamp: 20 W
CRI: 3000 K
Lumens: 2,091 lumen
Finish: Black
BUG Rating: B1-U0-G1

Full Cut-Off, Pole-mounted Ht. as noted on Lumen Plan

FIXTURE TYPE 5: BEGA 84247 K3

Sgl Head Tag SL2

 Lamp:
 26 W

 CRI:
 3000 K

 Lumens:
 3250 lumen

 Finish:
 Black

 BUG Rating:
 B1-U0-G1

Full Cut-Off Pole-mounted Ht as Notes on Lumen Plan

FIXTURE TYPE 6: BEGA 84254 K3

Dual Head Tag SL4

and outdoor sales and service areas must provide for a uniformity ratio of not more

7. The maximum illumination level within access drives, parking lots and sales and

service areas may not exceed eight footcandles measured at the ground suface.

than 20:1 (ratio of maximum to minimum luminance).

 Lamp:
 20 W

 CRI:
 3000 K

 Lumens:
 2343 lumen

 Finish:
 Black

 BUG Rating:
 B1-U0-G1

Full Cut-Off Pole-mounted 20'-0" Above ground



Light Fixture Data







MAINSPRING

Jason Garnham

From: Jodie Bray Strickland <jstrickland@cmaengineers.com>

Sent:Wednesday, April 5, 2023 3:56 PMTo:geoff@civcon.com; Jason GarnhamSubject:RE: FAIR TIDE - WETLANDS (2133500)

Geoff-

My previous comments on the lighting plan appear to have been addressed.

Best, Jodie

Jodie Bray Strickland, P.E. Senior Project Engineer



CIVIL/ENVIRONMENTAL/STRUCTURAL

35 Bow St.

Portsmouth, NH 03801 CELL: 603-817-4716

jstrickland@cmaengineers.com

From: geoff@civcon.com <geoff@civcon.com>
Sent: Wednesday, April 5, 2023 3:47 PM

To: Jodie Bray Strickland <jstrickland@cmaengineers.com>; 'Jason Garnham' <JGarnham@kitteryme.org>

Subject: RE: FAIR TIDE - WETLANDS (2133500)

CAUTION: This email originated from outside your organization. Exercise caution when opening attachments or clicking links, especially from unknown senders.

Jodie,

That is great. Attached is the site lighting plans. Can you review this piecemeal. That was the last technical item I believe that was outstanding.

I am pushing to get the information submitted by tomorrow so we can be on the April agenda.

Thank you for your assistance with this.

Geoff

Geoff Aleva
CIVIL CONSULTANTS

From: Jodie Bray Strickland <jstrickland@cmaengineers.com>

Sent: Wednesday, April 5, 2023 3:03 PM

To: geoff@civcon.com; 'Jason Garnham' < JGarnham@kitteryme.org>

Subject: RE: FAIR TIDE - WETLANDS

Geoff-

I apologize for confusing the terminology.

This letter should be fine.

Best, Jodie

Jodie Bray Strickland, P.E. Senior Project Engineer



CIVIL/ENVIRONMENTAL/STRUCTURAL

35 Bow St.

Portsmouth, NH 03801 CELL: 603-817-4716

jstrickland@cmaengineers.com

From: geoff@civcon.com>

Sent: Saturday, April 1, 2023 9:02 AM

To: Jodie Bray Strickland < jstrickland@cmaengineers.com >; 'Jason Garnham' < JGarnham@kitteryme.org >

Subject: FAIR TIDE - WETLANDS

CAUTION: This email originated from outside your organization. Exercise caution when opening attachments or clicking links, especially from unknown senders.

Jodie,

As you know ME does not license wetland scientists. Does this letter suffice for the coordination information?

We will have the updated lighting plan for you to review on Monday. We are hoping to get a final submission package in early in the week to get on the next available planning board meeting.

Please let me know if you have any questions. Thank you for assisting us on the project review.

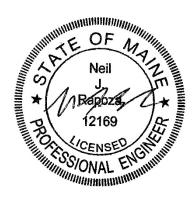
Geoff

Geoffrey R. Aleva, PE President Structural / Civil Engineer CIVIL CONSULTANTS PO Box 100 / 293 Main Street South Berwick, Maine 03908 ph: 207-384-2550

fx: 207-384-2112 mobile: 603-781-1402

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The seal affixed above applies to this report and all attachments including the HydroCAD calculations, Stormwater Plans D1, D2 $\,$

Site Plan Application Stormwater Management Plan

"FAIR TIDE, INC."
KITTERY, MAINE

Prepared for

Fair Tide, Inc. 15 State Road Kittery, ME 03904

January 2023

Site Plan Application

STORMWATER MANAGEMENT PLAN

"Fair Tide, Inc." 22 Shapleigh Road Kittery, Maine

Prepared for:

Fair Tide, Inc. 15 State Rd. Kittery, ME 03904

January 2023 Revised March 2023

INTRODUCTION:

The proposed development is located at 22 Shapleigh Road in Kittery, Maine. The lot is known as Map 15, Lot 64 on the Town of Kittery tax map system. The existing lot contains approximately 1.95 acres of land, of which 0.61 acres is impervious coverage.

There is an existing 4,070 **4,069** SF commercial building on the property. This building and the associated parking will be redeveloped for use as described in the site plan application.

The developed portion of the site contains a large parking lot and surrounding grass cover. A wetland is located in the middle of the lot that has an approximate area of 24,000 SF. Culverts convey flow into the on-site wetland across Shapleigh Road and Manson Avenue, with a single culvert outlet draining to the south.

The new development will consist of the construction of a building housing three six units with a new associated parking lot. This portion of the development will gain access to the site via a new entrance from Shapleigh Road.

The project will disturb less than an acre and will not require DEP review. The impervious area of the site will increase by approximately 0.12 acres

DESIGN REQUIREMENTS:

Section 16.7.11.C(4) of the Town of Kittery Land Use and Development Code requires post-development peak discharges be limited to pre-development levels for a 2- year and 25-year, 24 hour storm (Portsmouth, NH storm intensities).

The analysis for this report includes the 2-year and 25-year events to predict the downstream effects of the proposed site coverage changes.

EXISTING DRAINAGE CONDITIONS:

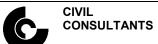
The existing lot generally slopes from the perimeter inward to an on-site wetland. The wetland outlets to the south property line through a 12" culvert, modeled as OUT 1.

A small portion drains southwest to Shapleigh Road. The flows to this area are modeled as OUT 2.

The analysis of the existing drainage has been limited in extent to the property line. This is justified by the fact that all stormwater is directed away from the property due to natural grades.

Based on the Medium Intensity Soil Survey obtained from the NRCA Web Soil Survey website, soils in the watershed were found to be entirely hydrologic soil type D soils. See sheet D1 for the predevelopment drainage conditions.

The area to be developed is not located in a flood zone. A copy of the applicable



FEMA map is included in the Town Site Plan Application.

PROPOSED DRAINAGE:

The proposed site has been designed to limit post-development flows off site to pre-development levels during 2-year and 25-year storms. This will ensure that there are minimal adverse downstream impacts as a result of the new development.

The redevelopment of the northern portion of the lot will result in a reduction of approximately 3,300 SF of impervious area, with some areas of existing pavement converted to grass and other areas of existing landscape planters becoming accessible walkways.

The portion of the development at the southwest corner will create approximately 7,700 SF of new impervious. The development as proposed will direct some of this subcatchment to the large on-site wetland, resulting in flows to Shapleigh Road that generally match those modeled in the pre-developed condition.

ANALYSIS:

The overall perimeter of the watershed remained the same for both Pre- and Post Development analyses. There were three *five* sub-catchments identified in the Pre-Development analysis and eight seven in the Post-Development analysis.

Two distinct discharge points were used to compare the pre- and postdevelopment storm water flows to ensure the town standards were met.

For further details regarding subcatchment determination, refer to the

project drawings and D1 & D2 included with this report.

METHODOLOGY:

All runoff calculations were performed using methods based on USDA–SCS Technical Release No. 20 (also known as TR-20). The 2- and 25-year events for the city of Portsmouth, NH (Type III rainfall distribution) were used for the analysis to determine the pre- and post-development peak discharge rates per Town of Kittery requirements. Rainfall data was obtained from the Extreme Precipitation in New York & New England Web Tool by Cornell University.

Runoff curve numbers (CN) and times of concentration (Tc) were determined by the methods outlined in USDA-SCS Technical Release No. 55 (better known as TR-55). On site watershed areas were determined using two-foot contour data gathered from an on the ground field survey performed by Civil Consultants, with off-site topography obtained using available LIDAR data.

The detailed analysis for this project was performed by computer utilizing "HYDROCAD" stormwater modeling software. The computer printouts are attached.

The attached Pre- and Post Development plans (D1 & D2) show subcatchment boundaries, hydraulic flow lines, existing and development, and drainage features and facilities. Land cover type boundaries used in the model for on-site areas are also shown on the plan (i.e. tree lines, gravel, etc).

FLOW RATES:

TWO-YEAR EVENT -

Discharge	Point		
Desig	Peak	Runoff(in cfs)	Change
Pre/Post	Pre	Post	(cfs)
OUT 1 OUT 2	3.48	<u>3.55</u> 0.52	+0.07 +0.05

TWENTY-FIVE-YEAR EVENT -

Discharge Desig <u>Pre/Post</u>		unoff(in cfs) Post	Change (cfs)
OUT 1	<u>4.67</u>	<u>4.73</u>	+0.06
OUT 2	1.37	1.22	-0.15

Although there are increases to individual analysis points OUT 1 and OUT 2, the proposed stormwater management design predicts essentially unchanged flows compared to the predevelopment condition. This has been achieved by reducing impervious cover from land draining to OUT 1, and by directing new pavement to now drain to that outlet and away from OUT 2.

If additional BMP's were implemented to attempt to reduce the flows further, it would likely create more disturbance than would be reasonable for a development of this size. It is our opinion that the more prudent option is to allow the smallest footprint possible with the layout as proposed.

The slope and poor soils on site make it difficult to design and implement stormwater control. This includes a gravel drip edge around the revised parking area to lessen erosion of the adjacent slope and provide additional protection for the receiving wetland.

A stormwater maintenance and inspection plan has also been included as part of this submission.

CONCLUSIONS:

It is our opinion that there will be no adverse downstream impacts as a result of this project, and the surrounding lots have been sufficiently protected by the proposed stormwater management plan.

J:\aaa\2021\2133500\DRAINAGE\20230303-2133500-DRAINAGE_NARRATIVE (Rev-1).docx

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing Yes

State New Hampshire

Location

Longitude 70.763 degrees West **Latitude** 43.072 degrees North

Elevation 0 feet

Date/Time Tue, 03 Jan 2023 14:15:46 -0500

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.50	0.65	0.81	1.04	1yr	0.70	0.98	1.21	1.56	2.03	2.66	2.92	1yr	2.35	2.81	3.22	3.94	4.55	1yr
2yr	0.32	0.50	0.62	0.81	1.02	1.30	2yr	0.88	1.18	1.52	1.94	2.49	3.21	3.57	2yr	2.84	3.43	3.94	4.68	5.33	2yr
5yr	0.37	0.58	0.73	0.98	1.25	1.61	5yr	1.08	1.47	1.89	2.43	3.14	4.07	4.58	5yr	3.60	4.40	5.04	5.94	6.70	5yr
10yr	0.41	0.65	0.82	1.12	1.45	1.89	10yr	1.25	1.73	2.23	2.89	3.75	4.87	5.53	10yr	4.31	5.32	6.09	7.11	7.98	10yr
25yr	0.48	0.76	0.97	1.34	1.77	2.34	25yr	1.53	2.14	2.78	3.63	4.74	6.17	7.10	25yr	5.46	6.83	7.80	9.03	10.05	25yr
50yr	0.54	0.86	1.10	1.54	2.07	2.76	50yr	1.79	2.53	3.29	4.32	5.66	7.39	8.58	50yr	6.54	8.25	9.42	10.81	11.98	50yr
100yr	0.60	0.97	1.25	1.77	2.42	3.26	100yr	2.09	2.98	3.90	5.16	6.77	8.85	10.38	100yr	7.83	9.98	11.38	12.96	14.27	100yr
200yr	0.67	1.10	1.43	2.05	2.82	3.83	200yr	2.44	3.52	4.62	6.13	8.08	10.61	12.55	200yr	9.39	12.07	13.76	15.55	17.02	200yr
500yr	0.80	1.31	1.71	2.48	3.48	4.76	500yr	3.00	4.38	5.76	7.70	10.22	13.48	16.14	500yr	11.93	15.52	17.67	19.78	21.49	500yr

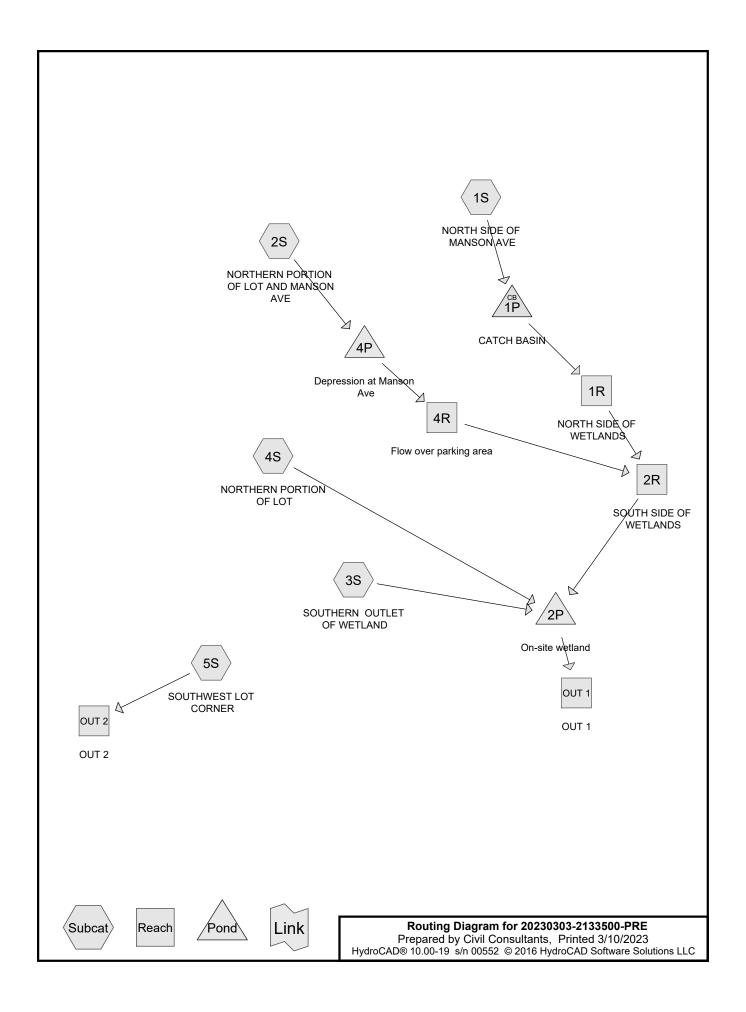
Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.23	0.36	0.44	0.59	0.72	0.88	1yr	0.63	0.86	0.92	1.33	1.68	2.24	2.49	1yr	1.98	2.40	2.87	3.18	3.90	1yr
2yr	0.31	0.49	0.60	0.81	1.00	1.19	2yr	0.86	1.16	1.37	1.82	2.34	3.06	3.45	2yr	2.71	3.32	3.82	4.55	5.08	2yr
5yr	0.35	0.54	0.67	0.92	1.17	1.40	5yr	1.01	1.37	1.61	2.12	2.73	3.79	4.19	5yr	3.35	4.03	4.72	5.53	6.24	5yr
10yr	0.39	0.59	0.73	1.03	1.33	1.60	10yr	1.14	1.56	1.80	2.39	3.06	4.37	4.86	10yr	3.87	4.67	5.44	6.41	7.20	10yr
25yr	0.44	0.67	0.83	1.19	1.56	1.90	25yr	1.35	1.86	2.10	2.75	3.53	4.72	5.89	25yr	4.18	5.66	6.65	7.79	8.68	25yr
50yr	0.48	0.73	0.91	1.31	1.76	2.17	50yr	1.52	2.12	2.35	3.07	3.93	5.33	6.80	50yr	4.72	6.54	7.72	9.04	10.02	50yr
100yr	0.54	0.81	1.01	1.47	2.01	2.47	100yr	1.73	2.41	2.63	3.41	4.35	6.00	7.85	100yr	5.31	7.55	8.98	10.51	11.56	100yr
200yr	0.59	0.89	1.13	1.63	2.28	2.81	200yr	1.96	2.75	2.93	3.78	4.79	6.72	9.06	200yr	5.95	8.71	10.42	12.22	13.37	200yr
500yr	0.68	1.02	1.31	1.90	2.71	3.36	500yr	2.34	3.29	3.41	4.31	5.45	7.82	10.94	500yr	6.92	10.52	12.69	14.96	16.19	500yr

Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.28	0.44	0.54	0.72	0.89	1.08	1yr	0.77	1.06	1.26	1.74	2.21	2.98	3.16	1yr	2.64	3.04	3.58	4.37	5.04	1yr
2yr	0.34	0.52	0.64	0.86	1.07	1.27	2yr	0.92	1.24	1.48	1.96	2.51	3.42	3.70	2yr	3.03	3.56	4.09	4.84	5.63	2yr
5yr	0.40	0.62	0.77	1.05	1.34	1.62	5yr	1.15	1.58	1.88	2.53	3.25	4.34	4.96	5yr	3.84	4.77	5.38	6.37	7.16	5yr
10yr	0.47	0.72	0.89	1.25	1.61	1.98	10yr	1.39	1.93	2.28	3.11	3.95	5.34	6.20	10yr	4.72	5.96	6.82	7.84	8.75	10yr
25yr	0.58	0.88	1.09	1.56	2.05	2.57	25yr	1.77	2.51	2.95	4.07	5.15	7.78	8.34	25yr	6.88	8.02	9.15	10.34	11.41	25yr
50yr	0.67	1.02	1.27	1.83	2.46	3.13	50yr	2.12	3.06	3.60	5.00	6.32	9.74	10.46	50yr	8.62	10.06	11.44	12.72	13.96	50yr
100yr	0.79	1.19	1.49	2.16	2.96	3.81	100yr	2.55	3.72	4.37	6.16	7.76	12.18	13.10	100yr	10.78	12.60	14.31	15.69	17.09	100yr
200yr	0.92	1.39	1.76	2.55	3.56	4.65	200yr	3.07	4.55	5.34	7.58	9.54	15.28	16.44	200yr	13.53	15.81	17.92	19.35	20.92	200yr
500yr	1.15	1.71	2.19	3.19	4.53	6.04	500yr	3.91	5.90	6.93	10.02	12.56	20.65	22.20	500yr	18.27	21.34	24.13	25.51	27.34	500yr





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Page 2

Area Listing (all nodes)

	Area	CN	Description
(a	cres)		(subcatchment-numbers)
1	1.004	87	1/4 acre lots, 38% imp, HSG D (2S, 4S)
(0.034	80	>75% Grass cover, Good, HSG D (3S, 5S)
(0.022	96	Gravel surface, HSG D (2S)
(0.855	98	Paved parking, HSG D (1S, 3S, 4S, 5S)
().524	93	Paved roads w/open ditches, 50% imp, HSG D (1S, 2S, 4S)
(0.248	98	Roofs, HSG D (1S, 2S, 4S, 5S)
1	1.085	77	Woods, Good, HSG D (3S, 4S, 5S)
().878	79	Woods/grass comb., Good, HSG D (1S, 2S, 4S)
4	4.650	86	TOTAL AREA

Prepared by Civil Consultants
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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
4.650	HSG D	1S, 2S, 3S, 4S, 5S
0.000	Other	
4.650		TOTAL AREA

Prepared by Civil Consultants
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> Subcatchi Numbers

Ground Covers (all nodes)

HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground
(acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover
0.000	0.000	0.000	1.004	0.000	1.004	1/4 acre lots, 38% imp
0.000	0.000	0.000	0.034	0.000	0.034	>75% Grass cover, Good
0.000	0.000	0.000	0.022	0.000	0.022	Gravel surface
0.000	0.000	0.000	0.855	0.000	0.855	Paved parking
0.000	0.000	0.000	0.524	0.000	0.524	Paved roads w/open ditches, 50%
						imp
0.000	0.000	0.000	0.248	0.000	0.248	Roofs
0.000	0.000	0.000	1.085	0.000	1.085	Woods, Good
0.000	0.000	0.000	0.878	0.000	0.878	Woods/grass comb., Good
0.000	0.000	0.000	4.650	0.000	4.650	TOTAL AREA

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: NORTH SIDE OF Runoff Area=1.147 ac 38.49% Impervious Runoff Depth=1.92"

Flow Length=298' Tc=8.7 min CN=87 Runoff=2.35 cfs 0.184 af

Subcatchment 2S: NORTHERN PORTION Runoff Area=52,925 sf 40.16% Impervious Runoff Depth=2.01"

Flow Length=329' Tc=7.9 min CN=88 Runoff=2.67 cfs 0.203 af

Subcatchment3S: SOUTHERN OUTLET OF Runoff Area=0.508 ac 1.77% Impervious Runoff Depth=1.22"

Flow Length=125' Tc=8.4 min CN=77 Runoff=0.65 cfs 0.052 af

Subcatchment 4S: NORTHERN PORTION Runoff Area=1.430 ac 54.90% Impervious Runoff Depth=2.18"

Flow Length=298' Tc=4.4 min CN=90 Runoff=3.83 cfs 0.260 af

Subcatchment 5S: SOUTHWEST LOT Runoff Area = 0.350 ac 6.57% Impervious Runoff Depth = 1.34"

Flow Length=138' Tc=10.0 min CN=79 Runoff=0.47 cfs 0.039 af

Reach 1R: NORTH SIDE OF WETLANDS Avg. Flow Depth=0.13' Max Vel=1.64 fps Inflow=2.35 cfs 0.184 af

n=0.030 L=51.3' S=0.0312 '/' Capacity=312.60 cfs Outflow=2.35 cfs 0.184 af

Reach 2R: SOUTH SIDE OF WETLANDS Avg. Flow Depth=0.19' Max Vel=1.73 fps Inflow=5.00 cfs 0.348 af

n=0.030 L=75.0' S=0.0213 '/' Capacity=258.53 cfs Outflow=4.98 cfs 0.348 af

Reach 4R: Flow over parking area Avg. Flow Depth=0.07' Max Vel=3.11 fps Inflow=2.66 cfs 0.164 af

n=0.016 L=95.0' S=0.0505'/' Capacity=130.20 cfs Outflow=2.65 cfs 0.164 af

Reach OUT 1: OUT 1 Inflow=3.48 cfs 0.659 af

Outflow=3.48 cfs 0.659 af

Reach OUT 2: OUT 2 Inflow=0.47 cfs 0.039 af

Outflow=0.47 cfs 0.039 af

Pond 1P: CATCH BASIN Peak Elev=56.02' Inflow=2.35 cfs 0.184 af

Primary=2.35 cfs 0.184 af Secondary=0.00 cfs 0.000 af Outflow=2.35 cfs 0.184 af

Pond 2P: On-site wetland Peak Elev=46.75' Storage=5,219 cf Inflow=8.67 cfs 0.659 af

Primary=3.48 cfs 0.659 af Secondary=0.00 cfs 0.000 af Outflow=3.48 cfs 0.659 af

Pond 4P: Depression at Manson Ave Peak Elev=55.58' Storage=1,807 cf Inflow=2.67 cfs 0.203 af

Outflow=2.66 cfs 0.164 af

Total Runoff Area = 4.650 ac Runoff Volume = 0.737 af Average Runoff Depth = 1.90" 62.44% Pervious = 2.903 ac 37.56% Impervious = 1.747 ac

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Summary for Subcatchment 1S: NORTH SIDE OF MANSON AVE

Runoff = 2.35 cfs @ 12.12 hrs, Volume= 0.184 af, Depth= 1.92"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

	Area	(ac) C	N Des	cription		
		`		-	/open ditch	ies, 50% imp, HSG D
				fs, HSG D	, opon anon	100, 00 % mp, 1100 B
				ed parking.	. HSG D	
					omb., Goo	d, HSG D
				ghted Aver		-
		705		1% Pervio		
	_	441		9% Imperv		
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	'
	7.1	50	0.0800	0.12		Sheet Flow, 1.1
						Woods: Light underbrush n= 0.400 P2= 3.17"
	0.1	17	0.3529	2.97		Shallow Concentrated Flow, 1.2
						Woodland Kv= 5.0 fps
	1.1	74	0.0541	1.16		Shallow Concentrated Flow, 1.3
						Woodland Kv= 5.0 fps
	0.2	29	0.2069	2.27		Shallow Concentrated Flow, 1.4
						Woodland Kv= 5.0 fps
	0.2	128	0.0711	13.59	62.83	Trap/Vee/Rect Channel Flow, 1.5
						Bot.W=3.00' D=0.50' Z= 10.0 & 15.0 '/' Top.W=15.50'
_						n= 0.013 Asphalt, smooth
	87	298	Total			

8.7 298 Total

Summary for Subcatchment 2S: NORTHERN PORTION OF LOT AND MANSON AVE

Runoff = 2.67 cfs @ 12.11 hrs, Volume= 0.203 af, Depth= 2.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

Area (sf)	CN	Description
42,863	87	1/4 acre lots, 38% imp, HSG D
4,269	93	Paved roads w/open ditches, 50% imp, HSG D
2,831	98	Roofs, HSG D
958	96	Gravel surface, HSG D
2,004	79	Woods/grass comb., Good, HSG D
52,925	88	Weighted Average
31,672		59.84% Pervious Area
21,253		40.16% Impervious Area

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(m		Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7	7.1	50	0.0800	0.12	, ,	Sheet Flow, 2.1
						Woods: Light underbrush n= 0.400 P2= 3.17"
().2	38	0.1800	2.97		Shallow Concentrated Flow, 2.2
						Short Grass Pasture Kv= 7.0 fps
().2	101	0.0400	11.01	112.52	
						Bot.W=5.00' D=0.75' Z= 3.0 & 20.0 '/' Top.W=22.25'
						n= 0.016 Asphalt, rough
().4	140	0.0210	5.94	18.93	Trap/Vee/Rect Channel Flow, 2.4
						Bot.W=2.00' D=0.75' Z= 3.0 '/' Top.W=6.50'
						n= 0.022 Earth, clean & straight
7	7.9	329	Total			

Summary for Subcatchment 3S: SOUTHERN OUTLET OF WETLAND

Runoff = 0.65 cfs @ 12.13 hrs, Volume= 0.052 af, Depth= 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

 Area	(ac) C	N Desc	cription		
0.	353 7	77 Woo	ds, Good,	HSG D	
0.	009	98 Pave	ed parking	, HSG D	
0.	140 7		ds, Good,		
0.	006			over, Good	, HSG D
0.	508 7	77 Weid	hted Aver	age	
0.	499		3% Pervio	•	
0.	009	1.77	% Impervi	ous Area	
			•		
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	<u> </u>
8.0	50	0.0600	0.10		Sheet Flow, 3.1
					Woods: Light underbrush n= 0.400 P2= 3.17"
0.3	30	0.1333	1.83		Shallow Concentrated Flow, 3.2
					Woodland Kv= 5.0 fps
0.1	45	0.0578	7.85	294.44	Trap/Vee/Rect Channel Flow, 3.3
					Bot.W=5.00' D=1.00' Z= 50.0 & 15.0 '/' Top.W=70.00'
					n= 0.030 Stream, clean & straight
8.4	125	Total	•		

Summary for Subcatchment 4S: NORTHERN PORTION OF LOT

Runoff = 3.83 cfs @ 12.06 hrs, Volume= 0.260 af, Depth= 2.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

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Area	(ac) C	N Desc	cription		
0.	293 7	7 Woo	ds, Good,	HSG D	
0.	238 7	'9 Woo	ds/grass d	omb., Goo	d, HSG D
0.	020 8	37 1/4 a	acre lots, 3	8% imp, H	SG D
0.	203 9	3 Pave	ed roads w	/open ditch	ies, 50% imp, HSG D
0.	628		ed parking	, HSG D	
0.	048 9	8 Root	fs, HSG D		
1.	430	00 Weig	ghted Aver	age	
0.	645	_	0% Pervio		
0.	785	54.9	0% Imper	/ious Area	
_				_	
Tc	Length	Slope		Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
3.6	25	0.0400	0.12		Sheet Flow, 4.1
					Grass: Dense n= 0.240 P2= 3.17"
0.1	25	0.3200	2.83		Shallow Concentrated Flow, 4.2
0.4			0.07		Woodland Kv= 5.0 fps
0.4	73	0.0200	2.87		Shallow Concentrated Flow, 4.3
0.0	405	0.0000	0.00	00.00	Paved Kv= 20.3 fps
0.2	105	0.0600	9.80	22.06	
					Bot.W=1.50' D=0.75' Z= 1.0 & 3.0 '/' Top.W=4.50'
0.4	70	0.0570	12.00	220 54	n= 0.022 Earth, clean & straight
0.1	70	0.0570	12.00	229.54	Trap/Vee/Rect Channel Flow, 4.5
					Bot.W=3.00' D=0.75' Z= 30.0 '/' Top.W=48.00'
4.4	000	T.4.1			n= 0.016 Asphalt, rough
4.4	298	Total			

Summary for Subcatchment 5S: SOUTHWEST LOT CORNER

Runoff = 0.47 cfs @ 12.14 hrs, Volume= 0.039 af, Depth= 1.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

Area (ac)	CN	Description
0.005	98	Roofs, HSG D
0.299	77	Woods, Good, HSG D
0.018	98	Paved parking, HSG D
0.028	80	>75% Grass cover, Good, HSG D
0.350	79	Weighted Average
0.327		93.43% Pervious Area
0.023		6.57% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.6	50	0.0500	0.10		Sheet Flow, 5.1
					Woods: Light underbrush n= 0.400 P2= 3.17"
1.4	76	0.0350	0.94		Shallow Concentrated Flow, 5.2
					Woodland Kv= 5.0 fps
0.0	12	0.0208	7.49	29.98	Trap/Vee/Rect Channel Flow, 5.3
					Bot.W=3.00' D=0.50' Z= 10.0 '/' Top.W=13.00'
					n= 0.013 Asphalt, smooth
10.0	138	Total			

Summary for Reach 1R: NORTH SIDE OF WETLANDS

Inflow Area = 1.147 ac, 38.49% Impervious, Inflow Depth = 1.92" for 2 yr event

Inflow = 2.35 cfs @ 12.12 hrs, Volume= 0.184 af

Outflow = 2.35 cfs @ 12.13 hrs, Volume= 0.184 af, Atten= 0%, Lag= 0.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Max. Velocity= 1.64 fps, Min. Travel Time= 0.5 min Avg. Velocity = 0.60 fps, Avg. Travel Time= 1.4 min

Peak Storage= 73 cf @ 12.13 hrs Average Depth at Peak Storage= 0.13'

Bank-Full Depth= 1.00' Flow Area= 55.0 sf, Capacity= 312.60 cfs

5.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value = 50.0 '/' Top Width = 105.00'

Length= 51.3' Slope= 0.0312 '/'

Inlet Invert= 48.60', Outlet Invert= 47.00'



Summary for Reach 2R: SOUTH SIDE OF WETLANDS

[62] Hint: Exceeded Reach 1R OUTLET depth by 0.07' @ 12.15 hrs

Inflow Area = 2.362 ac, 39.35% Impervious, Inflow Depth = 1.77" for 2 yr event

Inflow = 5.00 cfs @ 12.13 hrs, Volume= 0.348 af

Outflow = 4.98 cfs @ 12.14 hrs, Volume= 0.348 af, Atten= 0%, Lag= 0.5 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Max. Velocity= 1.73 fps, Min. Travel Time= 0.7 min

Avg. Velocity = 0.61 fps, Avg. Travel Time= 2.0 min

Peak Storage= 215 cf @ 12.14 hrs Average Depth at Peak Storage= 0.19'

Bank-Full Depth= 1.00' Flow Area= 55.0 sf, Capacity= 258.53 cfs

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 $5.00' \times 1.00'$ deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 50.0 '/' Top Width= 105.00'

Length= 75.0' Slope= 0.0213 '/'

Inlet Invert= 47.00', Outlet Invert= 45.40'



Summary for Reach 4R: Flow over parking area

Inflow Area = 1.215 ac, 40.16% Impervious, Inflow Depth = 1.62" for 2 yr event

Inflow = 2.66 cfs @ 12.12 hrs, Volume= 0.164 af

Outflow = 2.65 cfs @ 12.13 hrs, Volume= 0.164 af, Atten= 0%, Lag= 0.3 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Max. Velocity= 3.11 fps, Min. Travel Time= 0.5 min Avg. Velocity = 0.94 fps, Avg. Travel Time= 1.7 min

Peak Storage= 81 cf @ 12.13 hrs Average Depth at Peak Storage= 0.07'

Bank-Full Depth= 0.50' Flow Area= 13.8 sf, Capacity= 130.20 cfs

10.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 35.0 '/' Top Width= 45.00'

Length= 95.0' Slope= 0.0505 '/'

Inlet Invert= 55.30', Outlet Invert= 50.50'



Summary for Reach OUT 1: OUT 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 4.300 ac, 40.08% Impervious, Inflow Depth = 1.84" for 2 yr event

Inflow = 3.48 cfs @ 12.40 hrs, Volume= 0.659 af

Outflow = 3.48 cfs @ 12.40 hrs, Volume= 0.659 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

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Summary for Reach OUT 2: OUT 2

[40] Hint: Not Described (Outflow=Inflow)

0.350 ac, 6.57% Impervious, Inflow Depth = 1.34" for 2 yr event 0.47 cfs @ 12.14 hrs, Volume= 0.039 af Inflow Area =

Inflow

0.47 cfs @ 12.14 hrs, Volume= Outflow 0.039 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Summary for Pond 1P: CATCH BASIN

Inflow Area =	1.147 ac, 38.49% Impervious, Inflow De	epth = 1.92" for 2 yr event
Inflow =	2.35 cfs @ 12.12 hrs, Volume=	0.184 af
Outflow =	2.35 cfs @ 12.12 hrs, Volume=	0.184 af, Atten= 0%, Lag= 0.0 min
Primary =	2.35 cfs @ 12.12 hrs, Volume=	0.184 af
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Peak Elev= 56.02' @ 12.12 hrs

Flood Elev= 60.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	54.90'	12.0" Round Culvert
	•		L= 163.3' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 54.90' / 48.60' S= 0.0386 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Secondary	59.50'	10.0' long x 30.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=2.35 cfs @ 12.12 hrs HW=56.02' TW=48.73' (Dynamic Tailwater) 1=Culvert (Inlet Controls 2.35 cfs @ 2.99 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=54.90' TW=48.60' (Dynamic Tailwater) -2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 2P: On-site wetland

[62] Hint: Exceeded Reach 2R OUTLET depth by 1.22' @ 12.48 hrs

Inflow Area =	4.300 ac, 40.08% Impervious, Inflow Do	epth = 1.84" for 2 yr event
Inflow =	8.67 cfs @ 12.10 hrs, Volume=	0.659 af
Outflow =	3.48 cfs @ 12.40 hrs, Volume=	0.659 af, Atten= 60%, Lag= 17.8 min
Primary =	3.48 cfs @ 12.40 hrs, Volume=	0.659 af
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 46.75' @ 12.40 hrs Surf.Area= 15,115 sf Storage= 5,219 cf

Plug-Flow detention time= 12.9 min calculated for 0.659 af (100% of inflow)

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Center-of-Mass det. time= 13.0 min (840.2 - 827.2)

Volume	Inve	rt Avail.Sto	rage Storage	Description			
#1	45.40	0' 65,8	11 cf Custom	Stage Data (Coni	c) Listed below (Recalc)		
Elevation	on S	Surf.Area	Inc.Store	Cum.Store	Wet.Area		
(fee		(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)		
45.4	40	500	0	0	500		
46.0	00	800	386	386	805		
47.0	00	24,000	9,727	10,114	24,007		
48.0		28,151	26,048	36,162	28,197		
49.0	00	31,173	29,649	65,811	31,280		
Device	Routing	Invert	Outlet Devices	3			
#1	Primary	45.40'	12.0" Round	Culvert			
	•		L= 90.0' CPP	, square edge hea	dwall, Ke= 0.500		
			Inlet / Outlet In	vert= 45.40' / 44.0	0' S= 0.0156 '/' Cc= 0.900)	
				•	h interior, Flow Area= 0.79		
#2	Secondar	y 48.50'	•		ıd-Crested Rectangular We	əir	
					0 1.00 1.20 1.40 1.60		
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63				

Primary OutFlow Max=3.48 cfs @ 12.40 hrs HW=46.75' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 3.48 cfs @ 4.43 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=45.40' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 4P: Depression at Manson Ave

Inflow Area = 1.215 ac, 40.16% Impervious, Inflow Depth = 2.01" for 2 yr event

Inflow = 2.67 cfs @ 12.11 hrs, Volume= 0.203 af

Outflow = 2.66 cfs @ 12.12 hrs, Volume= 0.164 af, Atten= 0%, Lag= 0.5 min

Primary = 2.66 cfs @ 12.12 hrs, Volume= 0.164 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 55.58' @ 12.12 hrs Surf.Area= 1,451 sf Storage= 1,807 cf

Plug-Flow detention time= 112.7 min calculated for 0.164 af (81% of inflow)

Center-of-Mass det. time= 38.0 min (854.7 - 816.7)

<u>Volume</u>	Invert	Avai	il.Storage	Storage	e Description	
#1	53.00'		2,506 cf	Custor	n Stage Data (Conic	c) Listed below (R
Elevation (feet)		.Area (sq-ft)		:.Store c-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
53.00		256		0	0	256
54.00		554		396	396	562
55.00		917		728	1,123	937
56.00		1,909		1,383	2,506	1,938

Type III 24-hr 2 yr Rainfall=3.21" Printed 3/10/2023

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Device	Routing	Invert	Outlet Devices
#1	Primary	55.50'	45.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=2.66 cfs @ 12.12 hrs HW=55.58' TW=55.37' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 2.66 cfs @ 0.72 fps)

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: NORTH SIDE OF Runoff Area=1.147 ac 38.49% Impervious Runoff Depth=4.68"

Flow Length=298' Tc=8.7 min CN=87 Runoff=5.57 cfs 0.447 af

Subcatchment 2S: NORTHERN PORTION Runoff Area=52,925 sf 40.16% Impervious Runoff Depth=4.79"

Flow Length=329' Tc=7.9 min CN=88 Runoff=6.17 cfs 0.485 af

Subcatchment3S: SOUTHERN OUTLET OF Runoff Area=0.508 ac 1.77% Impervious Runoff Depth=3.63"

Flow Length=125' Tc=8.4 min CN=77 Runoff=1.99 cfs 0.154 af

Subcatchment 4S: NORTHERN PORTION Runoff Area=1.430 ac 54.90% Impervious Runoff Depth=5.01"

Flow Length=298' Tc=4.4 min CN=90 Runoff=8.46 cfs 0.597 af

Subcatchment 5S: SOUTHWEST LOT Runoff Area = 0.350 ac 6.57% Impervious Runoff Depth = 3.83"

Flow Length=138' Tc=10.0 min CN=79 Runoff=1.37 cfs 0.112 af

Reach 1R: NORTH SIDE OF WETLANDS Avg. Flow Depth=0.19' Max Vel=2.05 fps Inflow=5.57 cfs 0.447 af

 $n = 0.030 \quad L = 51.3' \quad S = 0.0312 \; \text{$^{\prime}$}' \quad \text{Capacity} = 312.60 \; \text{cfs} \quad \text{Outflow} = 5.56 \; \text{cfs} \quad 0.447 \; \text{af} \quad \text{$^{\prime}$} = 1.000 \; \text{$^{\prime}$}' = 1.000 \; \text{$^{\prime}$

Reach 2R: SOUTH SIDE OF WETLANDS Avg. Flow Depth=0.28' Max Vel=2.16 fps Inflow=11.71 cfs 0.893 af

n=0.030 L=75.0' S=0.0213 '/' Capacity=258.53 cfs Outflow=11.67 cfs 0.893 af

Reach 4R: Flow over parking area Avg. Flow Depth=0.11' Max Vel=4.06 fps Inflow=6.15 cfs 0.446 af

n=0.016 L=95.0' S=0.0505 '/' Capacity=130.20 cfs Outflow=6.14 cfs 0.446 af

Reach OUT 1: OUT 1 Inflow=4.67 cfs 1.644 af

Outflow=4.67 cfs 1.644 af

Reach OUT 2: OUT 2 Inflow=1.37 cfs 0.112 af

Outflow=1.37 cfs 0.112 af

Pond 1P: CATCH BASIN Peak Elev=58.88' Inflow=5.57 cfs 0.447 af

Primary=5.57 cfs 0.447 af Secondary=0.00 cfs 0.000 af Outflow=5.57 cfs 0.447 af

Pond 2P: On-site wetland Peak Elev=47.43' Storage=20,761 cf Inflow=20.56 cfs 1.644 af

Primary=4.67 cfs 1.644 af Secondary=0.00 cfs 0.000 af Outflow=4.67 cfs 1.644 af

Pond 4P: Depression at Manson Ave Peak Elev=55.64' Storage=1,899 cf Inflow=6.17 cfs 0.485 af

Outflow=6.15 cfs 0.446 af

Total Runoff Area = 4.650 ac Runoff Volume = 1.795 af Average Runoff Depth = 4.63" 62.44% Pervious = 2.903 ac 37.56% Impervious = 1.747 ac

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Summary for Subcatchment 1S: NORTH SIDE OF MANSON AVE

Runoff = 5.57 cfs @ 12.12 hrs, Volume= 0.447 af, Depth= 4.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

	Area	(ac) C	N Des	cription		
			-	/open ditch	ies, 50% imp, HSG D	
				fs, HSG D	, opon anon	100, 00 % mp, 1100 B
				ed parking.	. HSG D	
					omb., Goo	d, HSG D
				ghted Aver		-
		705		1% Pervio		
	_	441		9% Imperv		
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	'
	7.1	50	0.0800	0.12		Sheet Flow, 1.1
						Woods: Light underbrush n= 0.400 P2= 3.17"
	0.1	17	0.3529	2.97		Shallow Concentrated Flow, 1.2
						Woodland Kv= 5.0 fps
	1.1	74	0.0541	1.16		Shallow Concentrated Flow, 1.3
						Woodland Kv= 5.0 fps
	0.2	29	0.2069	2.27		Shallow Concentrated Flow, 1.4
						Woodland Kv= 5.0 fps
	0.2	128	0.0711	13.59	62.83	Trap/Vee/Rect Channel Flow, 1.5
						Bot.W=3.00' D=0.50' Z= 10.0 & 15.0 '/' Top.W=15.50'
_						n= 0.013 Asphalt, smooth
	87	298	Total			

8.7 298 Total

Summary for Subcatchment 2S: NORTHERN PORTION OF LOT AND MANSON AVE

Runoff = 6.17 cfs @ 12.11 hrs, Volume= 0.485 af, Depth= 4.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

Area ((sf) CN	Description
42,8	863 87	1/4 acre lots, 38% imp, HSG D
4,2	269 93	Paved roads w/open ditches, 50% imp, HSG D
2,8	31 98	Roofs, HSG D
9	96	Gravel surface, HSG D
2,0	004 79	Woods/grass comb., Good, HSG D
52,9	25 88	Weighted Average
31,6	672	59.84% Pervious Area
21,2	253	40.16% Impervious Area

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T (mir		Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.		50	0.0800	0.12	()	Sheet Flow, 2.1
						Woods: Light underbrush n= 0.400 P2= 3.17"
0.	.2	38	0.1800	2.97		Shallow Concentrated Flow, 2.2
_	_					Short Grass Pasture Kv= 7.0 fps
0.	.2	101	0.0400	11.01	112.52	Trap/Vee/Rect Channel Flow, 2.3
						Bot.W=5.00' D=0.75' Z= 3.0 & 20.0 '/' Top.W=22.25'
						n= 0.016 Asphalt, rough
0.	.4	140	0.0210	5.94	18.93	Trap/Vee/Rect Channel Flow, 2.4
						Bot.W=2.00' D=0.75' Z= 3.0 '/' Top.W=6.50'
						n= 0.022 Earth, clean & straight
7.	.9	329	Total			

Summary for Subcatchment 3S: SOUTHERN OUTLET OF WETLAND

Runoff = 1.99 cfs @ 12.12 hrs, Volume= 0.154 af, Depth= 3.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

Area	(ac) C	N Des	cription		
0.353 77 Woods, Good, HSG D					
0.	009	98 Pave	ed parking	, HSG D	
0.	140	77 Woo	ds, Good,	HSG D	
0.	006	30 >75°	% Grass co	over, Good	, HSG D
0.	508		ghted Aver		
0.	499	98.2	3% Pervio	us Area	
0.	009	1.77	% Impervi	ous Area	
_					
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.0	50	0.0600	0.10		Sheet Flow, 3.1
					Woods: Light underbrush n= 0.400 P2= 3.17"
0.3	30	0.1333	1.83		Shallow Concentrated Flow, 3.2
					Woodland Kv= 5.0 fps
0.1	45	0.0578	7.85	294.44	Trap/Vee/Rect Channel Flow, 3.3
					Bot.W=5.00' D=1.00' Z= 50.0 & 15.0 '/' Top.W=70.00'
					n= 0.030 Stream, clean & straight
8.4	125	Total			

Summary for Subcatchment 4S: NORTHERN PORTION OF LOT

Runoff = 8.46 cfs @ 12.06 hrs, Volume= 0.597 af, Depth= 5.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

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Area	(ac) C	N Des	cription					
0.293 77 Woods, Good, HSG D			ds, Good,	HSG D				
0.	.238 7	79 Woo	Woods/grass comb., Good, HSG D					
0.	.020	37 1/4 a	1/4 acre lots, 38% imp, HSG D					
0.	.203	3 Pave	ed roads w	/open ditch	ies, 50% imp, HSG D			
0.	.628	98 Pave	ed parking	, HSG D				
0	.048 9	98 Root	fs, HSG D					
1.	.430	90 Weig	ghted Aver	age				
0.	.645	45.1	0% Pervio	us Area				
0.	.785	54.9	0% Imperv	/ious Area				
_					—			
Tc	Length	Slope	Velocity		Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
3.6	25	0.0400	0.12		Sheet Flow, 4.1			
					Grass: Dense n= 0.240 P2= 3.17"			
0.1	25	0.3200	2.83		Shallow Concentrated Flow, 4.2			
0.4	70	0.0000	0.07		Woodland Kv= 5.0 fps			
0.4	73	0.0200	2.87		Shallow Concentrated Flow, 4.3			
0.0	105	0.0000	0.00	22.06	Paved Kv= 20.3 fps			
0.2	105	0.0600	9.80	22.06	Trap/Vee/Rect Channel Flow, 4.4 Bot.W=1.50' D=0.75' Z= 1.0 & 3.0 '/' Top.W=4.50'			
					n= 0.022 Earth, clean & straight			
0.1	70	0.0570	12.00	229.54	Trap/Vee/Rect Channel Flow, 4.5			
0.1	70	0.0070	12.00	223.54	Bot.W=3.00' D=0.75' Z= 30.0 '/' Top.W=48.00'			
					n= 0.016 Asphalt, rough			
4.4	298	Total			ii olo io repliali, roagii			
7.7	230	iolai						

Summary for Subcatchment 5S: SOUTHWEST LOT CORNER

Runoff = 1.37 cfs @ 12.14 hrs, Volume= 0.112 af, Depth= 3.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

Area (ac)	CN	Description
0.005	98	Roofs, HSG D
0.299	77	Woods, Good, HSG D
0.018	98	Paved parking, HSG D
0.028	80	>75% Grass cover, Good, HSG D
0.350	79	Weighted Average
0.327		93.43% Pervious Area
0.023		6.57% Impervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	8.6	50	0.0500	0.10		Sheet Flow, 5.1
	1.4	76	0.0350	0.94		Woods: Light underbrush n= 0.400 P2= 3.17" Shallow Concentrated Flow, 5.2 Woodland Kv= 5.0 fps
	0.0	12	0.0208	7.49	29.98	Trap/Vee/Rect Channel Flow, 5.3 Bot.W=3.00' D=0.50' Z= 10.0 '/' Top.W=13.00'
_						n= 0.013 Asphalt, smooth
_	10.0	138	Total			

Summary for Reach 1R: NORTH SIDE OF WETLANDS

Inflow Area = 1.147 ac, 38.49% Impervious, Inflow Depth = 4.68" for 25 yr event

Inflow = 5.57 cfs @ 12.12 hrs, Volume= 0.447 af

Outflow = 5.56 cfs @ 12.12 hrs, Volume= 0.447 af, Atten= 0%, Lag= 0.3 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Max. Velocity= 2.05 fps, Min. Travel Time= 0.4 min Avg. Velocity = 0.74 fps, Avg. Travel Time= 1.2 min

Peak Storage= 139 cf @ 12.12 hrs Average Depth at Peak Storage= 0.19'

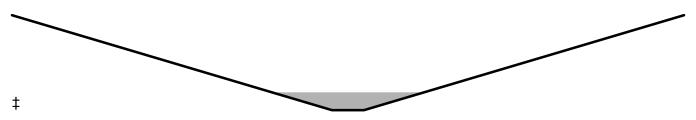
Bank-Full Depth= 1.00' Flow Area= 55.0 sf, Capacity= 312.60 cfs

5.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 50.0 '/' Top Width= 105.00'

Length= 51.3' Slope= 0.0312 '/'

Inlet Invert= 48.60', Outlet Invert= 47.00'



Summary for Reach 2R: SOUTH SIDE OF WETLANDS

[62] Hint: Exceeded Reach 1R OUTLET depth by 0.10' @ 12.14 hrs

Inflow Area = 2.362 ac, 39.35% Impervious, Inflow Depth = 4.54" for 25 yr event

Inflow = 11.71 cfs @ 12.12 hrs, Volume= 0.893 af

Outflow = 11.67 cfs @ 12.13 hrs, Volume= 0.893 af, Atten= 0%, Lag= 0.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Max. Velocity= 2.16 fps, Min. Travel Time= 0.6 min

Avg. Velocity = 0.75 fps, Avg. Travel Time= 1.7 min

Peak Storage= 406 cf @ 12.13 hrs Average Depth at Peak Storage= 0.28'

Average Depth at Feak Storage - 0.20

Bank-Full Depth= 1.00' Flow Area= 55.0 sf, Capacity= 258.53 cfs

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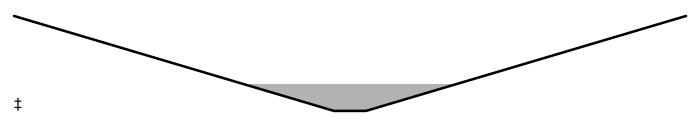
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5.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 50.0 '/' Top Width= 105.00'

Length= 75.0' Slope= 0.0213 '/'

Inlet Invert= 47.00', Outlet Invert= 45.40'



Summary for Reach 4R: Flow over parking area

Inflow Area = 1.215 ac, 40.16% Impervious, Inflow Depth = 4.41" for 25 yr event

Inflow = 6.15 cfs @ 12.12 hrs, Volume= 0.446 af

Outflow = 6.14 cfs @ 12.12 hrs, Volume= 0.446 af, Atten= 0%, Lag= 0.3 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Max. Velocity= 4.06 fps, Min. Travel Time= 0.4 min Avg. Velocity = 1.28 fps, Avg. Travel Time= 1.2 min

Peak Storage= 144 cf @ 12.12 hrs Average Depth at Peak Storage= 0.11'

Bank-Full Depth= 0.50' Flow Area= 13.8 sf, Capacity= 130.20 cfs

10.00' x 0.50' deep channel, n= 0.016 Asphalt, rough

Side Slope Z-value= 35.0 '/' Top Width= 45.00'

Length= 95.0' Slope= 0.0505 '/'

Inlet Invert= 55.30', Outlet Invert= 50.50'



Summary for Reach OUT 1: OUT 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 4.300 ac, 40.08% Impervious, Inflow Depth = 4.59" for 25 yr event

Inflow = 4.67 cfs @ 12.54 hrs, Volume= 1.644 af

Outflow = 4.67 cfs @ 12.54 hrs, Volume= 1.644 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

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Summary for Reach OUT 2: OUT 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.350 ac, 6.57% Impervious, Inflow Depth = 3.83" for 25 yr event

Inflow = 1.37 cfs @ 12.14 hrs, Volume= 0.112 af

Outflow = 1.37 cfs @ 12.14 hrs, Volume= 0.112 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Summary for Pond 1P: CATCH BASIN

Inflow Area =	1.147 ac, 38.49% Impervious, Inflow De	epth = 4.68" for 25 yr event
Inflow =	5.57 cfs @ 12.12 hrs, Volume=	0.447 af
Outflow =	5.57 cfs @ 12.12 hrs, Volume=	0.447 af, Atten= 0%, Lag= 0.0 min
Primary =	5.57 cfs @ 12.12 hrs, Volume=	0.447 af
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Peak Elev= 58.88' @ 12.12 hrs

Flood Elev= 60.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	54.90'	12.0" Round Culvert
	_		L= 163.3' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 54.90' / 48.60' S= 0.0386 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Secondary	59.50'	10.0' long x 30.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=5.57 cfs @ 12.12 hrs HW=58.88' TW=48.79' (Dynamic Tailwater) 1=Culvert (Inlet Controls 5.57 cfs @ 7.09 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=54.90' TW=48.60' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 2P: On-site wetland

[63] Warning: Exceeded Reach 2R INLET depth by 0.29' @ 12.64 hrs

Inflow Area =	4.300 ac, 40.08% Impervious, Inflow	v Depth = 4.59" for 25 yr event
Inflow =	20.56 cfs @ 12.10 hrs, Volume=	1.644 af
Outflow =	4.67 cfs @ 12.54 hrs, Volume=	1.644 af, Atten= 77%, Lag= 26.4 min
Primary =	4.67 cfs @ 12.54 hrs, Volume=	1.644 af
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 47.43' @ 12.54 hrs Surf.Area= 25,737 sf Storage= 20,761 cf

Plug-Flow detention time= 32.8 min calculated for 1.644 af (100% of inflow)

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Center-of-Mass det. time= 32.8 min (833.0 - 800.2)

Volume	Inve	rt Avail.Sto	rage Storage	Description				
#1	45.4	0' 65,8	11 cf Custom	Stage Data (Coni	c) Listed below (Rec	alc)		
Elevation	an .	Surf.Area	Inc.Store	Cum.Store	Wet.Area			
(fee		(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)			
45.4	40	500	0	0	500			
46.0	00	800	386	386	805			
47.0	00	24,000	9,727	10,114	24,007			
48.0		28,151	26,048	36,162	28,197			
49.0	00	31,173	29,649	65,811	31,280			
Device	Routing	Invert	Outlet Devices	S				
#1	Primary	45.40'	12.0" Round	Culvert				
	-		L= 90.0' CPF	L= 90.0' CPP, square edge headwall, Ke= 0.500				
				Inlet / Outlet Invert= 45.40' / 44.00' S= 0.0156 '/' Cc= 0.900				
				n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf				
#2	Seconda	ry 48.50'	•	15.0' long x 40.0' breadth Broad-Crested Rectangular Weir				
					0 1.00 1.20 1.40			
			Coet. (English	1) 2.68 2.70 2.70	2.64 2.63 2.64 2.6	04 2.63		

Primary OutFlow Max=4.67 cfs @ 12.54 hrs HW=47.43' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 4.67 cfs @ 5.95 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=45.40' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 4P: Depression at Manson Ave

1.215 ac, 40.16% Impervious, Inflow Depth = 4.79" for 25 yr event Inflow Area = Inflow 0.485 af

6.17 cfs @ 12.11 hrs, Volume=

6.15 cfs @ 12.12 hrs, Volume= Outflow 0.446 af, Atten= 0%, Lag= 0.4 min

Primary 6.15 cfs @ 12.12 hrs, Volume= 0.446 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 55.64' @ 12.12 hrs Surf.Area= 1,515 sf Storage= 1,899 cf

Plug-Flow detention time= 65.7 min calculated for 0.446 af (92% of inflow)

Center-of-Mass det. time= 24.5 min (816.8 - 792.3)

<u>Volume</u>	Invert	Avail	.Storage	Storage	e Description	
#1	53.00'		2,506 cf	Custor	n Stage Data (Con	ic)Listed below
Elevation (feet)	Surf./	Area sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
53.00	•	256	·	0	0	256
54.00		554		396	396	562
55.00		917		728	1,123	937
56.00	1	1,909		1,383	2,506	1,938

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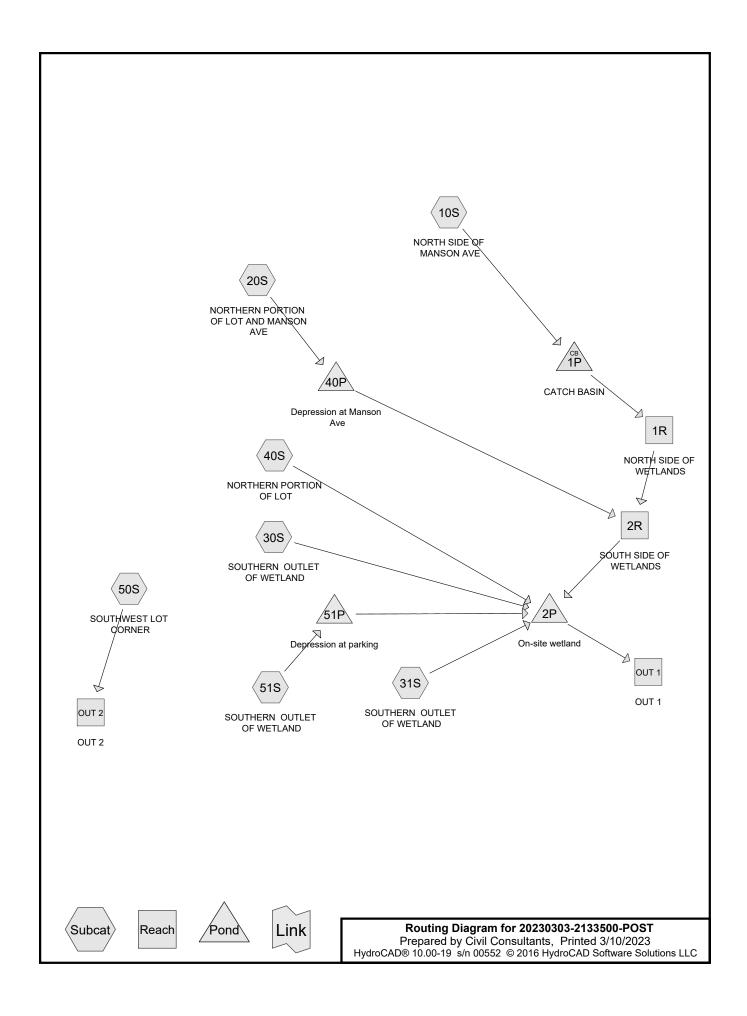
Type III 24-hr 25 yr Rainfall=6.17" Printed 3/10/2023

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Device	Routing	Invert	Outlet Devices
#1	Primary	55.50'	45.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=6.14 cfs @ 12.12 hrs HW=55.64' TW=55.41' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 6.14 cfs @ 0.95 fps)



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Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
1.004	87	1/4 acre lots, 38% imp, HSG D (20S, 40S)
0.118	80	>75% Grass cover, Good, HSG D (30S, 40S, 50S, 51S)
0.005	96	Gravel surface, HSG D (20S)
0.976	98	Paved parking, HSG D (10S, 20S, 30S, 40S, 50S, 51S)
0.524	93	Paved roads w/open ditches, 50% imp, HSG D (10S, 20S, 40S)
0.295	98	Roofs, HSG D (10S, 20S, 30S, 40S, 50S, 51S)
0.757	77	Woods, Good, HSG D (30S, 31S, 40S)
0.972	79	Woods/grass comb., Good, HSG D (10S, 20S, 40S, 50S)
4.651	87	TOTAL AREA

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
4.651	HSG D	10S, 20S, 30S, 31S, 40S, 50S, 51S
0.000	Other	
4.651		TOTAL AREA

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> Subcatchi Numbers

Ground Covers (all nodes)

HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground
(acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover
0.000	0.000	0.000	1.004	0.000	1.004	1/4 acre lots, 38% imp
0.000	0.000	0.000	0.118	0.000	0.118	>75% Grass cover, Good
0.000	0.000	0.000	0.005	0.000	0.005	Gravel surface
0.000	0.000	0.000	0.976	0.000	0.976	Paved parking
0.000	0.000	0.000	0.524	0.000	0.524	Paved roads w/open ditches, 50%
						imp
0.000	0.000	0.000	0.295	0.000	0.295	Roofs
0.000	0.000	0.000	0.757	0.000	0.757	Woods, Good
0.000	0.000	0.000	0.972	0.000	0.972	Woods/grass comb., Good
0.000	0.000	0.000	4.651	0.000	4.651	TOTAL AREA

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points x 5
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 10S: NORTH SIDE OF Runoff Area=1.147 ac 38.49% Impervious Runoff Depth=1.92"

Flow Length=298' Tc=8.7 min CN=87 Runoff=2.35 cfs 0.184 af

Subcatchment 20S: NORTHERN PORTION Runoff Area=1.220 ac 41.80% Impervious Runoff Depth=2.01"

Flow Length=329' Tc=7.9 min CN=88 Runoff=2.68 cfs 0.204 af

Subcatchment 30S: SOUTHERN OUTLET Runoff Area=0.335 ac 13.43% Impervious Runoff Depth=1.41" Flow Length=60' Tc=8.3 min CN=80 Runoff=0.51 cfs 0.039 af

Subcatchment 31S: SOUTHERN OUTLET Runoff Area=0.203 ac 0.00% Impervious Runoff Depth=1.22" Flow Length=125' Tc=8.4 min CN=77 Runoff=0.26 cfs 0.021 af

Subcatchment 40S: NORTHERN PORTION Runoff Area=1.426 ac 53.09% Impervious Runoff Depth=2.09" Flow Length=298' Tc=4.4 min CN=89 Runoff=3.68 cfs 0.248 af

Subcatchment 50S: SOUTHWEST LOT

Runoff Area=0.232 ac 42.24% Impervious Runoff Depth=1.92"
Flow Length=98' Tc=6.3 min CN=87 Runoff=0.52 cfs 0.037 af

Subcatchment 51S: SOUTHERN OUTLET Runoff Area=0.088 ac 71.59% Impervious Runoff Depth=2.46"

Tc=6.0 min CN=93 Runoff=0.25 cfs 0.018 af

Reach 1R: NORTH SIDE OF WETLANDS Avg. Flow Depth=0.13' Max Vel=1.64 fps Inflow=2.35 cfs 0.184 af n=0.030 L=51.3' S=0.0312'/ Capacity=312.60 cfs Outflow=2.35 cfs 0.184 af

Reach 2R: SOUTH SIDE OF WETLANDS Avg. Flow Depth=0.19' Max Vel=1.74 fps Inflow=5.01 cfs 0.388 af n=0.030 L=75.0' S=0.0213'/' Capacity=258.53 cfs Outflow=4.99 cfs 0.388 af

Reach OUT 1: OUT 1 Inflow=3.55 cfs 0.714 af Outflow=3.55 cfs 0.714 af

Reach OUT 2: OUT 2 Inflow=0.52 cfs 0.037 af

Outflow=0.52 cfs 0.037 af

Pond 1P: CATCH BASIN Peak Elev=56.02' Inflow=2.35 cfs 0.184 af

Primary=2.35 cfs 0.184 af Secondary=0.00 cfs 0.000 af Outflow=2.35 cfs 0.184 af

Pond 2P: On-site wetland Peak Elev=46.78' Storage=5,726 cf Inflow=9.03 cfs 0.714 af Primary=3.55 cfs 0.714 af Secondary=0.00 cfs 0.000 af Outflow=3.55 cfs 0.714 af

Pond 40P: Depression at Manson Ave
Peak Elev=52.21' Storage=19 cf Inflow=2.68 cfs 0.204 af
Primary=2.68 cfs 0.204 af Secondary=0.00 cfs 0.000 af Outflow=2.68 cfs 0.204 af

Pond 51P: Depression at parking Peak Elev=53.00' Storage=0 cf Inflow=0.25 cfs 0.018 af

Primary=0.25 cfs 0.018 af Secondary=0.00 cfs 0.000 af Outflow=0.25 cfs 0.018 af

Total Runoff Area = 4.651 ac Runoff Volume = 0.751 af Average Runoff Depth = 1.94" 58.84% Pervious = 2.736 ac 41.16% Impervious = 1.915 ac

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Summary for Subcatchment 10S: NORTH SIDE OF MANSON AVE

Runoff = 2.35 cfs @ 12.12 hrs, Volume= 0.184 af, Depth= 1.92"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

Are	ea (ac)	С	N Desc	cription					
0.223 93 Paved roads w/open ditche						nes, 50% imp, HSG D			
	0.130	Ç	8 Roof	fs, HSG D	•	·			
	0.200	Ç	8 Pave	Paved parking, HSG D					
	0.594	7	79 Woo	ds/grass c	omb., Goo	d, HSG D			
	1.147	8	37 Weid	hted Aver	age				
	0.705			1% Pervio					
	0.441		38.4	9% Imperv	ious Area				
				•					
Т	c Len	gth	Slope	Velocity	Capacity	Description			
(min	n) (fe	et)	(ft/ft)	(ft/sec)	(cfs)	·			
7.	1	50	0.0800	0.12		Sheet Flow, 10.1			
						Woods: Light underbrush n= 0.400 P2= 3.17"			
0.	1	17	0.3529	2.97		Shallow Concentrated Flow, 10.2			
						Woodland Kv= 5.0 fps			
1.	1	74	0.0541	1.16		Shallow Concentrated Flow, 10.3			
						Woodland Kv= 5.0 fps			
0.:	2	29	0.2069	2.27		Shallow Concentrated Flow, 10.4			
						Woodland Kv= 5.0 fps			
0.:	2 1	28	0.0711	13.59	62.83	Trap/Vee/Rect Channel Flow, 10.5			
						Bot.W=3.00' D=0.50' Z= 10.0 & 15.0 '/' Top.W=15.50'			
						n= 0.013 Asphalt, smooth			
8	7 2	98	Total						

8.7 298 Total

Summary for Subcatchment 20S: NORTHERN PORTION OF LOT AND MANSON AVE

Runoff = 2.68 cfs @ 12.11 hrs, Volume= 0.204 af, Depth= 2.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

Area (ac) CN	Description
0.984	87	1/4 acre lots, 38% imp, HSG D
0.098	3 93	Paved roads w/open ditches, 50% imp, HSG D
0.065	98	Roofs, HSG D
0.005	96	Gravel surface, HSG D
0.046	79	Woods/grass comb., Good, HSG D
0.022	98	Paved parking, HSG D
1.220	88 (Weighted Average
0.710)	58.20% Pervious Area
0.510)	41.80% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.1	50	0.0800	0.12		Sheet Flow, 2.1
0.0	20	0.4000	2.07		Woods: Light underbrush n= 0.400 P2= 3.17"
0.2	38	0.1800	2.97		Shallow Concentrated Flow, 2.2 Short Grass Pasture Kv= 7.0 fps
0.2	101	0.0400	11.01	112.52	Trap/Vee/Rect Channel Flow, 2.3
					Bot.W=5.00' D=0.75' Z= 3.0 & 20.0 '/' Top.W=22.25'
					n= 0.016 Asphalt, rough
0.4	140	0.0210	5.94	18.93	Trap/Vee/Rect Channel Flow, 2.4
					Bot.W=2.00' D=0.75' Z= 3.0 '/' Top.W=6.50'
					n= 0.022 Earth, clean & straight
7.9	329	Total			

Summary for Subcatchment 30S: SOUTHERN OUTLET OF WETLAND

Runoff = 0.51 cfs @ 12.12 hrs, Volume= 0.039 af, Depth= 1.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

	Area	(ac)	CN [Desc	ription		
	0.	261	77 \	Woo	ds, Good,	HSG D	
	0.	009	98 F	Pave	ed parking,	, HSG D	
	0.	036	98 F	Roof	s, HSG D		
	0.	029	80 >	>75%	√ Grass co	over, Good,	, HSG D
	0.	335	ا 80	Weig	hted Aver	age	
	0.	290	3	86.5	7% Pervio	us Area	
	0.	045	•	13.43	3% Imperv	∕ious Area	
	_						
	Tc	Length		ре	Velocity	Capacity	Description
_	(min)	(feet) (f1	t/ft)	(ft/sec)	(cfs)	
	8.0	25	0.01	150	0.05		Sheet Flow, 30.1
							Woods: Light underbrush n= 0.400 P2= 3.17"
	0.3	35	0.15	500	1.94		Shallow Concentrated Flow, 30.2
							Woodland Kv= 5.0 fps
	8.3	60) Tota	al			

Summary for Subcatchment 31S: SOUTHERN OUTLET OF WETLAND

Runoff = 0.26 cfs @ 12.13 hrs, Volume= 0.021 af, Depth= 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

Area (ac)	CN	Description
0.203	77	Woods, Good, HSG D
0.203	•	100.00% Pervious Area

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_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	8.0	50	0.0600	0.10		Sheet Flow, 31.1
						Woods: Light underbrush n= 0.400 P2= 3.17"
	0.3	30	0.1333	1.83		Shallow Concentrated Flow, 31.2
						Woodland Kv= 5.0 fps
	0.1	45	0.0578	7.85	294.44	Trap/Vee/Rect Channel Flow, 31.3
						Bot.W=5.00' D=1.00' Z= 50.0 & 15.0 '/' Top.W=70.00'
						n= 0.030 Stream, clean & straight
	8 4	125	Total	•		

Summary for Subcatchment 40S: NORTHERN PORTION OF LOT

Runoff 3.68 cfs @ 12.06 hrs, Volume= 0.248 af, Depth= 2.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

Area	(ac) C	N Des	cription						
0.	0.293 77 Woods, Good, HSG D								
0.	0.236 79 Woods/grass comb., Good, HSG D								
0.	0.020 87 1/4 acre lots, 38% imp, HSG D								
0.	203	93 Pave	ed roads w	/open ditch	nes, 50% imp, HSG D				
0.	601 9	98 Pave	ed parking	, HSG D					
0.	047	98 Roo	fs, HSG D						
0.	026 8	30 >75°	% Grass co	over, Good,	, HSG D				
1.	426 8	39 Weig	ghted Aver	age					
0.	669	46.9	1% Pervio	us Area					
0.	757	53.0	9% Imperv	/ious Area					
Tc	Length	Slope	•	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
3.6	25	0.0400	0.12		Sheet Flow, 4.1				
					Grass: Dense n= 0.240 P2= 3.17"				
0.1	25	0.3200	2.83		Shallow Concentrated Flow, 4.2				
					Woodland Kv= 5.0 fps				
0.4	73	0.0200	2.87		Shallow Concentrated Flow, 4.3				
					Paved Kv= 20.3 fps				
0.2	105	0.0600	9.80	22.06					
					Bot.W=1.50' D=0.75' Z= 1.0 & 3.0 '/' Top.W=4.50'				
					n= 0.022 Earth, clean & straight				
0.1	70	0.0570	12.00	229.54					
					Bot.W=3.00' D=0.75' Z= 30.0 '/' Top.W=48.00'				
					n= 0.016 Asphalt, rough				
4.4	298	Total							

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Summary for Subcatchment 50S: SOUTHWEST LOT CORNER

Runoff = 0.52 cfs @ 12.09 hrs, Volume= 0.037 af, Depth= 1.92"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

 Area	(ac)	CN	Desc	ription		
0.005 98 Roofs, HSG D						
0.	024	79	Woo	ds/grass d	omb., Goo	d, HSG D
0.	093	98		ed parking		
0.	072	79		_	omb., Goo	•
0.	038	80	>75%	⁶ Grass co	over, Good,	, HSG D
0.	232	87		hted Aver		
0.	134		57.70	6% Pervio	us Area	
0.	098		42.2	4% Imperv	ious Area	
_		_				
Tc	Length		lope	Velocity	Capacity	Description
 (min)	(feet) ((ft/ft)	(ft/sec)	(cfs)	
6.2	50	0.0	0400	0.13		Sheet Flow, 60.1
						Grass: Dense n= 0.240 P2= 3.17"
0.1	48	0.0	0310	8.84	46.41	Trap/Vee/Rect Channel Flow, 60.2
						Bot.W=3.00' D=0.50' Z= 10.0 & 20.0 '/' Top.W=18.00'
						n= 0.013 Asphalt, smooth
6.3	98	То	tal			

Summary for Subcatchment 51S: SOUTHERN OUTLET OF WETLAND

Runoff = 0.25 cfs @ 12.09 hrs, Volume= 0.018 af, Depth= 2.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2 yr Rainfall=3.21"

	Area	(ac)	CN	Desc	Description				
	0.	051	98	Pave	ed parking	, HSG D			
	0.	025	80	>75%	75% Grass cover, Good, HSG D				
_	0.	012	98	Roof	Roofs, HSG D				
	0.	088	93	Weig	Weighted Average				
	0.	0.025 28.41% Pervious Area							
	0.063 71.59% lm			9% Imperv	/ious Area				
	Tc	Leng	th :	Slope	Velocity	Capacity	Description		
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)			
	~ ~						B: (E (E4418 T		

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Summary for Reach 1R: NORTH SIDE OF WETLANDS

Inflow Area = 1.147 ac, 38.49% Impervious, Inflow Depth = 1.92" for 2 yr event

Inflow = 2.35 cfs @ 12.12 hrs, Volume= 0.184 af

Outflow = 2.35 cfs @ 12.13 hrs, Volume= 0.184 af, Atten= 0%, Lag= 0.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Max. Velocity= 1.64 fps, Min. Travel Time= 0.5 min Avg. Velocity = 0.60 fps, Avg. Travel Time= 1.4 min

Peak Storage= 73 cf @ 12.13 hrs Average Depth at Peak Storage= 0.13'

Bank-Full Depth= 1.00' Flow Area= 55.0 sf, Capacity= 312.60 cfs

5.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 50.0 '/' Top Width= 105.00'

Length= 51.3' Slope= 0.0312 '/'

Inlet Invert= 48.60', Outlet Invert= 47.00'



Summary for Reach 2R: SOUTH SIDE OF WETLANDS

[62] Hint: Exceeded Reach 1R OUTLET depth by 0.07' @ 12.13 hrs

Inflow Area = 2.367 ac, 40.20% Impervious, Inflow Depth = 1.97" for 2 yr event

Inflow = 5.01 cfs @ 12.12 hrs, Volume= 0.388 af

Outflow = 4.99 cfs @ 12.13 hrs, Volume= 0.388 af, Atten= 0%, Lag= 0.5 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Max. Velocity= 1.74 fps, Min. Travel Time= 0.7 min Avg. Velocity = 0.64 fps, Avg. Travel Time= 1.9 min

Peak Storage= 216 cf @ 12.13 hrs Average Depth at Peak Storage= 0.19'

Bank-Full Depth= 1.00' Flow Area= 55.0 sf, Capacity= 258.53 cfs

5.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 50.0 '/' Top Width= 105.00'

Length= 75.0' Slope= 0.0213 '/'

Inlet Invert= 47.00', Outlet Invert= 45.40'

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Summary for Reach OUT 1: OUT 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 4.419 ac, 41.11% Impervious, Inflow Depth = 1.94" for 2 yr event

Inflow = 3.55 cfs @ 12.40 hrs, Volume= 0.714 af

Outflow = 3.55 cfs @ 12.40 hrs, Volume= 0.714 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Summary for Reach OUT 2: OUT 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.232 ac, 42.24% Impervious, Inflow Depth = 1.92" for 2 yr event

Inflow = 0.52 cfs @ 12.09 hrs, Volume= 0.037 af

Outflow = 0.52 cfs @ 12.09 hrs, Volume= 0.037 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Summary for Pond 1P: CATCH BASIN

Inflow Area = 1.147 ac, 38.49% Impervious, Inflow Depth = 1.92" for 2 yr event

Inflow = 2.35 cfs @ 12.12 hrs, Volume= 0.184 af

Outflow = 2.35 cfs @ 12.12 hrs, Volume= 0.184 af, Atten= 0%, Lag= 0.0 min

Primary = 2.35 cfs @ 12.12 hrs, Volume= 0.184 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Peak Elev= 56.02' @ 12.12 hrs

Flood Elev= 60.10'

Routing	Invert	Outlet Devices
Primary	54.90'	12.0" Round Culvert
-		L= 163.3' CPP, projecting, no headwall, Ke= 0.900
		Inlet / Outlet Invert= 54.90' / 48.60' S= 0.0386 '/' Cc= 0.900
		n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
Secondary	59.50'	10.0' long x 30.0' breadth Broad-Crested Rectangular Weir
•		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
		Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63
	Primary	Primary 54.90'

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Primary OutFlow Max=2.35 cfs @ 12.12 hrs HW=56.02' TW=48.73' (Dynamic Tailwater) T-1=Culvert (Inlet Controls 2.35 cfs @ 2.99 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=54.90' TW=48.60' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 2P: On-site wetland

[62] Hint: Exceeded Reach 2R OUTLET depth by 1.26' @ 12.48 hrs

Inflow Area = 4.419 ac, 41.11% Impervious, Inflow Depth = 1.94" for 2 yr event Inflow 9.03 cfs @ 12.10 hrs, Volume= 0.714 af Outflow 3.55 cfs @ 12.40 hrs, Volume= 0.714 af, Atten= 61%, Lag= 17.8 min 3.55 cfs @ 12.40 hrs, Volume= Primary 0.714 af 0.00 cfs @ 0.00 hrs, Volume= Secondary = 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5 Peak Elev= 46.78' @ 12.40 hrs Surf.Area= 16,144 sf Storage= 5,726 cf

Plug-Flow detention time= 13.5 min calculated for 0.714 af (100% of inflow)

Center-of-Mass det. time= 13.4 min (831.8 - 818.4)

Volume	Inve	rt Avail.Sto	rage Storage	Description				
#1	45.40	0' 65,8	11 cf Custom	Stage Data (Coni	c)Listed below (Rec	alc)		
Elevation Sur		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)			
45.4	40	500	0	0	500			
46.0	00	800	386	386	805			
47.0	00	24,000	9,727	10,114	24,007			
48.0	00	28,151	26,048	36,162	28,197			
49.0	00	31,173	29,649	65,811	31,280			
Device	Routing	Invert	Outlet Devices	S				
#1	Primary	45.40'	12.0" Round	Culvert				
	•		L= 90.0' CPF	P, square edge hea	dwall, Ke= 0.500			
			Inlet / Outlet Ir	nvert= 45.40' / 44.0	0' S= 0.0156 '/' C	c= 0.900		
			n= 0.013 Cor	rugated PE, smoot	h interior, Flow Area	a= 0.79 sf		
#2	Secondar	y 48.50'		15.0' long x 40.0' breadth Broad-Crested Rectangular Weir				
			` ,		0 1.00 1.20 1.40			
			Coef. (English	i) 2.68 2.70 2.70	2.64 2.63 2.64 2.6	34 2.63		

Primary OutFlow Max=3.55 cfs @ 12.40 hrs HW=46.78' TW=0.00' (Dynamic Tailwater) -1=Culvert (Inlet Controls 3.55 cfs @ 4.52 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=45.40' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 40P: Depression at Manson Ave

Inflow Area = 1.220 ac, 41.80% Impervious, Inflow Depth = 2.01" for 2 yr event

Inflow = 2.68 cfs @ 12.11 hrs, Volume= 0.204 af

Outflow = 2.68 cfs @ 12.11 hrs, Volume= 0.204 af, Atten= 0%, Lag= 0.2 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Peak Elev= 52.21' @ 12.11 hrs Surf.Area= 13 sf Storage= 19 cf

Plug-Flow detention time= 0.4 min calculated for 0.204 af (100% of inflow)

Center-of-Mass det. time= 0.3 min (817.0 - 816.7)

Volume	Invert	Avail.Storage	Storage Description
#1	50.75'	1,156 cf	Custom Stage Data (Conic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store	Wet.Area
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)
50.75	13	0	0	13
53.00	13	29	29	42
54.50	13	20	49	61
54.55	172	4	53	220
55.00	310	107	160	360
56.00	1,909	996	1,156	1,963

Device	Routing	Invert	Outlet Devices
#1	Secondary	55.50'	45.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
"0	Б.	50.751	Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64
#2	Primary	50.75	12.0" Round Culvert L= 101.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 50.75' / 50.00' S= 0.0074 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#3	Device 2	50.75'	10.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=2.67 cfs @ 12.11 hrs HW=52.20' TW=47.19' (Dynamic Tailwater) 2=Culvert (Passes 2.67 cfs of 2.91 cfs potential flow)

1—3=Orifice/Grate (Orifice Controls 2.67 cfs @ 4.90 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=50.75' TW=47.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 51P: Depression at parking

Inflow Area =	0.088 ac, 71.59% Impervious, Inflow De	epth = 2.46" for 2 yr event
Inflow =	0.25 cfs @ 12.09 hrs, Volume=	0.018 af
Outflow =	0.25 cfs @ 12.09 hrs, Volume=	0.018 af, Atten= 0%, Lag= 0.0 min
Primary =	0.25 cfs @ 12.09 hrs, Volume=	0.018 af
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

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Peak Elev= 53.00' @ 12.09 hrs Surf.Area= 106 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 0.0 min (792.6 - 792.6)

<u>Volume</u>	Invert	Avail.Sto	rage Storage l	Description			
#1	53.00' 27		8 cf Custom Stage Data (Conic)Listed below (Recalc)			c)	
Elevatio		urf.Area	Inc.Store	Cum.Store (cubic-feet)	Wet.Area		
(fee		(sq-ft)	(cubic-feet)	(cubic-leet)	<u>(sq-ft)</u>		
53.0	00	106	0	0	106		
54.0	00	305	197	197	311		
54.2	54.25 340		81	278	349		
Device	Routing	Invert	Outlet Devices	;			
#1	Secondary	54.00'	10.0' long x 1	0.0' breadth Broa	d-Crested Rectangul	lar Weir	
,, .		000	•		0 1.00 1.20 1.40 1.6		
			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64				
#2	Primary	51.50'	4.0" Round Culvert				
	•		L= 35.0' CPP	, projectina, no he	adwall, Ke= 0.900		
				, , , ,	5' S= 0.0071 '/' Cc=	0.900	
					Flow Area= 0.09 sf	0.000	
			11- 0.010 FVC	, эпосит писпог,	1 10W AIGA- 0.03 SI		

Primary OutFlow Max=0.38 cfs @ 12.09 hrs HW=53.00' TW=46.55' (Dynamic Tailwater) 2=Culvert (Inlet Controls 0.38 cfs @ 4.39 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=53.00' TW=45.40' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points x 5
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 10S: NORTH SIDE OF Runoff Area=1.147 ac 38.49% Impervious Runoff Depth=4.68"

Flow Length=298' Tc=8.7 min CN=87 Runoff=5.57 cfs 0.447 af

Subcatchment 20S: NORTHERN PORTION Runoff Area=1.220 ac 41.80% Impervious Runoff Depth=4.79" Flow Length=329' Tc=7.9 min CN=88 Runoff=6.19 cfs 0.487 af

Subcatchment 30S: SOUTHERN OUTLET Runoff Area=0.335 ac 13.43% Impervious Runoff Depth=3.93" Flow Length=60' Tc=8.3 min CN=80 Runoff=1.42 cfs 0.110 af

Subcatchment 31S: SOUTHERN OUTLET Runoff Area=0.203 ac 0.00% Impervious Runoff Depth=3.63" Flow Length=125' Tc=8.4 min CN=77 Runoff=0.79 cfs 0.061 af

Subcatchment 40S: NORTHERN PORTION Runoff Area=1.426 ac 53.09% Impervious Runoff Depth=4.90" Flow Length=298' Tc=4.4 min CN=89 Runoff=8.31 cfs 0.582 af

Subcatchment 50S: SOUTHWESTLOT

Runoff Area=0.232 ac 42.24% Impervious Runoff Depth=4.68"
Flow Length=98' Tc=6.3 min CN=87 Runoff=1.22 cfs 0.090 af

Subcatchment 51S: SOUTHERN OUTLET Runoff Area=0.088 ac 71.59% Impervious Runoff Depth=5.35" Tc=6.0 min CN=93 Runoff=0.51 cfs 0.039 af

Reach 1R: NORTH SIDE OF WETLANDS Avg. Flow Depth=0.19' Max Vel=2.05 fps Inflow=5.57 cfs 0.447 af n=0.030 L=51.3' S=0.0312 '/' Capacity=312.60 cfs Outflow=5.56 cfs 0.447 af

Reach 2R: SOUTH SIDE OF WETLANDSAvg. Flow Depth=0.27' Max Vel=2.12 fps Inflow=10.87 cfs 0.934 af n=0.030 L=75.0' S=0.0213 '/' Capacity=258.53 cfs Outflow=10.85 cfs 0.934 af

Reach OUT 1: OUT 1 Inflow=4.73 cfs 1.727 af Outflow=4.73 cfs 1.727 af

Reach OUT 2: OUT 2 Inflow=1.22 cfs 0.090 af
Outflow=1.22 cfs 0.090 af

Pond 1P: CATCH BASIN Peak Elev=58.88' Inflow=5.57 cfs 0.447 af

Primary=5.57 cfs 0.447 af Secondary=0.00 cfs 0.000 af Outflow=5.57 cfs 0.447 af

Pond 2P: On-site wetlandPeak Elev=47.46' Storage=21,610 cf Inflow=20.38 cfs 1.727 af Primary=4.73 cfs 1.727 af Secondary=0.00 cfs 0.000 af Outflow=4.73 cfs 1.727 af

Pond 40P: Depression at Manson Ave Peak Elev=55.33' Storage=318 cf Inflow=6.19 cfs 0.487 af Primary=5.36 cfs 0.487 af Secondary=0.00 cfs 0.000 af Outflow=5.36 cfs 0.487 af

Pond 51P: Depression at parking Peak Elev=53.24' Storage=30 cf Inflow=0.51 cfs 0.039 af

Primary=0.42 cfs 0.039 af Secondary=0.00 cfs 0.000 af Outflow=0.42 cfs 0.039 af

Total Runoff Area = 4.651 ac Runoff Volume = 1.818 af Average Runoff Depth = 4.69" 58.84% Pervious = 2.736 ac 41.16% Impervious = 1.915 ac

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Summary for Subcatchment 10S: NORTH SIDE OF MANSON AVE

5.57 cfs @ 12.12 hrs, Volume= 0.447 af, Depth= 4.68" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

Aroo	(ac) C	N Doc	orintion				
	`						
				/open ditch	ies, 50% imp, HSG D		
			,				
0.	<u>594 7</u>	<u> 79 Woo</u>	ds/grass c	omb., Goo	d, HSG D		
1.	147 8	37 Weig	ghted Aver	age			
0.	705	61.5	1% Pervio	us Area			
0.	441	38.4	9% Imperv	ious Area			
			•				
Tc	Lenath	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	•		
7.1	50	0.0800	0.12	` ,	Sheet Flow, 10.1		
					Woods: Light underbrush n= 0.400 P2= 3.17"		
0.1	17	0.3529	2.97		Shallow Concentrated Flow, 10.2		
					Woodland Kv= 5.0 fps		
1.1	74	0.0541	1.16		Shallow Concentrated Flow, 10.3		
		0.00			Woodland Kv= 5.0 fps		
0.2	29	0.2069	2 27		Shallow Concentrated Flow, 10.4		
0.2		0.2000	2.21		Woodland Kv= 5.0 fps		
0.2	128	0 0711	13 50	62.83	Trap/Vee/Rect Channel Flow, 10.5		
0.2	120	0.07 11	10.00	02.00	Bot.W=3.00' D=0.50' Z= 10.0 & 15.0 '/' Top.W=15.50'		
					n= 0.013 Asphalt, smooth		
8.7	298	Total			11- 0.0 to Aophail, Sillooth		
	0. 0. 0. 1. 0. Tc (min) 7.1 0.1 1.1 0.2	0.223	0.223 93 Pave 0.130 98 Roof 0.200 98 Pave 0.594 79 Woo 1.147 87 Weig 0.705 61.5 0.441 38.4 Tc Length Slope (min) (feet) (ft/ft) 7.1 50 0.0800 0.1 17 0.3529 1.1 74 0.0541 0.2 29 0.2069 0.2 128 0.0711	0.223 93 Paved roads word not only the content of the	0.223 93 Paved roads w/open ditch 0.130 98 Roofs, HSG D 0.200 98 Paved parking, HSG D 0.594 79 Woods/grass comb., Good 1.147 87 Weighted Average 0.705 61.51% Pervious Area 0.441 38.49% Impervious Area Tc Length (ft/ft) (ft/sec) (cfs) Capacity (min) (feet) (ft/ft) (ft/sec) (cfs) 7.1 50 0.0800 0.12 0.1 17 0.3529 2.97 1.1 74 0.0541 1.16 0.2 29 0.2069 2.27 0.2 128 0.0711 13.59 62.83		

8.7 298 Total

Summary for Subcatchment 20S: NORTHERN PORTION OF LOT AND MANSON AVE

Runoff 6.19 cfs @ 12.11 hrs, Volume= 0.487 af, Depth= 4.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

Ar	ea (ac)	CN	Description
	0.984	87	1/4 acre lots, 38% imp, HSG D
	0.098	93	Paved roads w/open ditches, 50% imp, HSG D
	0.065	98	Roofs, HSG D
	0.005	96	Gravel surface, HSG D
	0.046	79	Woods/grass comb., Good, HSG D
	0.022	98	Paved parking, HSG D
	1.220	88	Weighted Average
	0.710		58.20% Pervious Area
	0.510		41.80% Impervious Area

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٦ mi)		Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	.1	50	0.0800	0.12		Sheet Flow, 2.1
	_					Woods: Light underbrush n= 0.400 P2= 3.17"
0	.2	38	0.1800	2.97		Shallow Concentrated Flow, 2.2
						Short Grass Pasture Kv= 7.0 fps
0	.2	101	0.0400	11.01	112.52	
						Bot.W=5.00' D=0.75' Z= 3.0 & 20.0 '/' Top.W=22.25'
						n= 0.016 Asphalt, rough
0	.4	140	0.0210	5.94	18.93	Trap/Vee/Rect Channel Flow, 2.4
						Bot.W=2.00' D=0.75' Z= 3.0 '/' Top.W=6.50'
						n= 0.022 Earth, clean & straight
7	.9	329	Total			

Summary for Subcatchment 30S: SOUTHERN OUTLET OF WETLAND

Runoff = 1.42 cfs @ 12.12 hrs, Volume= 0.110 af, Depth= 3.93"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

	Area	(ac) C	N Des	cription		
	0.	261	77 Woo	ds, Good,	HSG D	
	0.	009	98 Pav	ed parking	, HSG D	
	0.	036	98 Roo	fs, HSG D		
	0.	029	30 >75°	% Grass co	over, Good	, HSG D
	0.	335	30 Wei	ghted Aver	age	
	0.	290	86.5	7% Pervio	us Area	
	0.	045	13.4	3% Imperv	/ious Area	
	То	Longth	Slope	Volocity	Canacity	Description
	Tc (min)	Length	Slope	Velocity (ft/sec)	Capacity (cfs)	Description
	(min)	(feet)	(ft/ft)		(CIS)	
	8.0	25	0.0150	0.05		Sheet Flow, 30.1
						Woods: Light underbrush n= 0.400 P2= 3.17"
	0.3	35	0.1500	1.94		Shallow Concentrated Flow, 30.2
_						Woodland Kv= 5.0 fps
	8.3	60	Total			

Summary for Subcatchment 31S: SOUTHERN OUTLET OF WETLAND

Runoff = 0.79 cfs @ 12.12 hrs, Volume= 0.061 af, Depth= 3.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

Area (ac)	CN	Description
0.203	77	Woods, Good, HSG D
0.203		100.00% Pervious Area

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 Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.0	50	0.0600	0.10		Sheet Flow, 31.1
					Woods: Light underbrush n= 0.400 P2= 3.17"
0.3	30	0.1333	1.83		Shallow Concentrated Flow, 31.2
					Woodland Kv= 5.0 fps
0.1	45	0.0578	7.85	294.44	Trap/Vee/Rect Channel Flow, 31.3
					Bot.W=5.00' D=1.00' Z= 50.0 & 15.0 '/' Top.W=70.00'
					n= 0.030 Stream, clean & straight
8.4	125	Total			

Summary for Subcatchment 40S: NORTHERN PORTION OF LOT

Runoff = 8.31 cfs @ 12.06 hrs, Volume= 0.582 af, Depth= 4.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

Area	(ac) C	N Des	cription			
0.293 77 Woods, Good, HSG D						
0.	236 7			omb., Goo	d, HSG D	
0.	020 8	37 1/4 a	acre lots, 3	8% imp, H	SG D	
0.	203	93 Pave	ed roads w	/open ditch	nes, 50% imp, HSG D	
0.	601 9	98 Pave	ed parking	, HSG D		
0.	047	98 Roo	fs, HSG D			
0.	026 8	30 >75°	% Grass co	over, Good,	, HSG D	
1.	426 8	39 Weig	ghted Aver	age		
0.	669	46.9	1% Pervio	us Area		
0.	757	53.0	9% Imperv	/ious Area		
Tc	Length	Slope	•	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
3.6	25	0.0400	0.12		Sheet Flow, 4.1	
					Grass: Dense n= 0.240 P2= 3.17"	
0.1	25	0.3200	2.83		Shallow Concentrated Flow, 4.2	
					Woodland Kv= 5.0 fps	
0.4	73	0.0200	2.87		Shallow Concentrated Flow, 4.3	
					Paved Kv= 20.3 fps	
0.2	105	0.0600	9.80	22.06		
					Bot.W=1.50' D=0.75' Z= 1.0 & 3.0 '/' Top.W=4.50'	
					n= 0.022 Earth, clean & straight	
0.1	70	0.0570	12.00	229.54		
					Bot.W=3.00' D=0.75' Z= 30.0 '/' Top.W=48.00'	
					n= 0.016 Asphalt, rough	
4.4	298	Total				

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Summary for Subcatchment 50S: SOUTHWEST LOT CORNER

Runoff 1.22 cfs @ 12.09 hrs, Volume= 0.090 af, Depth= 4.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

	Area	(ac)	CN	Desc	ription		
	0.	005	98	Roof	s, HSG D		
	0.	024	79	Woo	ds/grass d	omb., Goo	d, HSG D
	0.	093	98	Pave	ed parking,	, HSG D	
	0.	072	79	Woo	ds/grass c	omb., Goo	d, HSG D
_	0.	038	80	>75%	⁶ Grass co	over, Good,	, HSG D
	0.	232	87	Weig	hted Aver	age	
	0.	134		57.7	6% Pervio	us Area	
	0.	098		42.2	4% Imperv	ious Area	
	_		_				
	Tc	Length		Slope	Velocity	Capacity	Description
_	(min)	(feet)		(ft/ft)	(ft/sec)	(cfs)	
	6.2	50	0.0	0400	0.13		Sheet Flow, 60.1
							Grass: Dense n= 0.240 P2= 3.17"
	0.1	48	0.0	0310	8.84	46.41	Trap/Vee/Rect Channel Flow, 60.2
							Bot.W=3.00' D=0.50' Z= 10.0 & 20.0 '/' Top.W=18.00'
							n= 0.013 Asphalt, smooth
	6.3	98	To	otal			

Summary for Subcatchment 51S: SOUTHERN OUTLET OF WETLAND

Runoff 0.51 cfs @ 12.08 hrs, Volume= 0.039 af, Depth= 5.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25 yr Rainfall=6.17"

	Area	(ac)	CN	Desc	ription		
	0.	051	98	Pave	ed parking,	HSG D	
	0.	025	80	>75%	√ Grass co	over, Good,	d, HSG D
_	0.	012	98	Roof	s, HSG D		
	0.	.088 93 Weighted Average					
	0.025 28.41% Pervious Area				1% Pervio	us Area	
	0.	063		71.5	9% Imperv	ious Area	
	_					• "	-
	Tc	Lengt		Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	
	6.0						Direct Entry, 51.1 Min Tc

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Summary for Reach 1R: NORTH SIDE OF WETLANDS

Inflow Area = 1.147 ac, 38.49% Impervious, Inflow Depth = 4.68" for 25 yr event

Inflow = 5.57 cfs @ 12.12 hrs, Volume= 0.447 af

Outflow = 5.56 cfs @ 12.12 hrs, Volume= 0.447 af, Atten= 0%, Lag= 0.3 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Max. Velocity= 2.05 fps, Min. Travel Time= 0.4 min Avg. Velocity = 0.74 fps, Avg. Travel Time= 1.2 min

Peak Storage= 139 cf @ 12.12 hrs Average Depth at Peak Storage= 0.19'

Bank-Full Depth= 1.00' Flow Area= 55.0 sf, Capacity= 312.60 cfs

5.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 50.0 '/' Top Width= 105.00'

Length= 51.3' Slope= 0.0312 '/'

Inlet Invert= 48.60', Outlet Invert= 47.00'



Summary for Reach 2R: SOUTH SIDE OF WETLANDS

[62] Hint: Exceeded Reach 1R OUTLET depth by 0.10' @ 12.23 hrs

Inflow Area = 2.367 ac, 40.20% Impervious, Inflow Depth = 4.74" for 25 yr event

Inflow = 10.87 cfs @ 12.13 hrs, Volume= 0.934 af

Outflow = 10.85 cfs @ 12.14 hrs, Volume= 0.934 af, Atten= 0%, Lag= 0.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Max. Velocity= 2.12 fps, Min. Travel Time= 0.6 min Avg. Velocity = 0.79 fps, Avg. Travel Time= 1.6 min

Peak Storage= 384 cf @ 12.14 hrs Average Depth at Peak Storage= 0.27'

Bank-Full Depth= 1.00' Flow Area= 55.0 sf, Capacity= 258.53 cfs

5.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 50.0 '/' Top Width= 105.00'

Length= 75.0' Slope= 0.0213 '/'

Inlet Invert= 47.00', Outlet Invert= 45.40'

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Summary for Reach OUT 1: OUT 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 4.419 ac, 41.11% Impervious, Inflow Depth = 4.69" for 25 yr event

Inflow = 4.73 cfs @ 12.54 hrs, Volume= 1.727 af

Outflow = 4.73 cfs @ 12.54 hrs, Volume= 1.727 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Summary for Reach OUT 2: OUT 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.232 ac, 42.24% Impervious, Inflow Depth = 4.68" for 25 yr event

Inflow = 1.22 cfs @ 12.09 hrs, Volume= 0.090 af

Outflow = 1.22 cfs @ 12.09 hrs, Volume= 0.090 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Summary for Pond 1P: CATCH BASIN

Inflow Area = 1.147 ac, 38.49% Impervious, Inflow Depth = 4.68" for 25 yr event

Inflow = 5.57 cfs @ 12.12 hrs, Volume= 0.447 af

Outflow = 5.57 cfs (a) 12.12 hrs, Volume= 0.447 af, Atten= 0%, Lag= 0.0 min

Primary = 5.57 cfs @ 12.12 hrs, Volume= 0.447 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Peak Elev= 58.88' @ 12.12 hrs

Flood Elev= 60.10'

<u>Device</u>	Routing	Invert	Outlet Devices
#1	Primary	54.90'	12.0" Round Culvert
	-		L= 163.3' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 54.90' / 48.60' S= 0.0386 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Secondary	59.50'	10.0' long x 30.0' breadth Broad-Crested Rectangular Weir
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

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Primary OutFlow Max=5.57 cfs @ 12.12 hrs HW=58.88' TW=48.79' (Dynamic Tailwater) T-1=Culvert (Inlet Controls 5.57 cfs @ 7.09 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=54.90' TW=48.60' (Dynamic Tailwater) -2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 2P: On-site wetland

[63] Warning: Exceeded Reach 2R INLET depth by 0.32' @ 12.64 hrs

Inflow Area = 4.419 ac, 41.11% Impervious, Inflow Depth = 4.69" for 25 yr event

Inflow 20.38 cfs @ 12.09 hrs, Volume= 1.727 af

Outflow 4.73 cfs @ 12.54 hrs, Volume= 1.727 af, Atten= 77%, Lag= 26.8 min

4.73 cfs @ 12.54 hrs, Volume= Primary 1.727 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5 Peak Elev= 47.46' @ 12.54 hrs Surf.Area= 25,873 sf Storage= 21,610 cf

Plug-Flow detention time= 33.4 min calculated for 1.727 af (100% of inflow)

Center-of-Mass det. time= 33.3 min (827.3 - 794.1)

Volume	Inve	rt Avail.Sto	rage Storage	Description		
#1	45.40	0' 65,8	11 cf Custom	Stage Data (Coni	c) Listed below (Recal	c)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
45.4	40	500	0	0	500	
46.0	00	800	386	386	805	
47.0	00	24,000	9,727	10,114	24,007	
48.0	00	28,151	26,048	36,162	28,197	
49.0	00	31,173	29,649	65,811	31,280	
Device	Routing	Invert	Outlet Devices	6		
#1	Primary	45.40'	12.0" Round	Culvert		
	•		L= 90.0' CPF	P, square edge hea	dwall, Ke= 0.500	
					0' S= 0.0156 '/' Cc=	
					h interior, Flow Area=	
#2	Secondar	y 48.50'			d-Crested Rectangu	
					0 1.00 1.20 1.40 1.6	
			Coef. (English) 2.68 2.70 2.70	2.64 2.63 2.64 2.64	2.63

Primary OutFlow Max=4.72 cfs @ 12.54 hrs HW=47.46' TW=0.00' (Dynamic Tailwater) -1=Culvert (Inlet Controls 4.72 cfs @ 6.02 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=45.40' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 40P: Depression at Manson Ave

Inflow Area = 1.220 ac, 41.80% Impervious, Inflow Depth = 4.79" for 25 yr event

Inflow = 6.19 cfs @ 12.11 hrs, Volume= 0.487 af

Outflow = 5.36 cfs @ 12.16 hrs, Volume= 0.487 af, Atten= 14%, Lag= 3.2 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5

Peak Elev= 55.33' @ 12.16 hrs Surf.Area= 682 sf Storage= 318 cf

Plug-Flow detention time= 0.4 min calculated for 0.487 af (100% of inflow)

Center-of-Mass det. time= 0.3 min (792.6 - 792.3)

Volume	Invert	Avail.Storage	Storage Description
#1	50.75'	1,156 cf	Custom Stage Data (Conic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store	Wet.Area
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)
50.75	13	0	0	13
53.00	13	29	29	42
54.50	13	20	49	61
54.55	172	4	53	220
55.00	310	107	160	360
56.00	1,909	996	1,156	1,963

Device	Routing	Invert	Outlet Devices
#1	Secondary	55.50'	45.0' long x 10.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64
#2	Primary	50.75'	12.0" Round Culvert
	•		L= 101.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 50.75' / 50.00' S= 0.0074 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#3	Device 2	50.75'	10.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=5.36 cfs @ 12.16 hrs HW=55.33' TW=47.27' (Dynamic Tailwater) 2=Culvert (Passes 5.36 cfs of 5.82 cfs potential flow)

3=Orifice/Grate (Orifice Controls 5.36 cfs @ 9.82 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=50.75' TW=47.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 51P: Depression at parking

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=592)

Inflow Area =	0.088 ac, 71.59% Impervious, Inflow D	epth = 5.35" for 25 yr event
Inflow =	0.51 cfs @ 12.08 hrs, Volume=	0.039 af
Outflow =	0.42 cfs @ 12.14 hrs, Volume=	0.039 af, Atten= 19%, Lag= 3.4 min
Primary =	0.42 cfs @ 12.14 hrs, Volume=	0.039 af
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 5 Peak Elev= 53.24' @ 12.14 hrs Surf.Area= 144 sf Storage= 30 cf

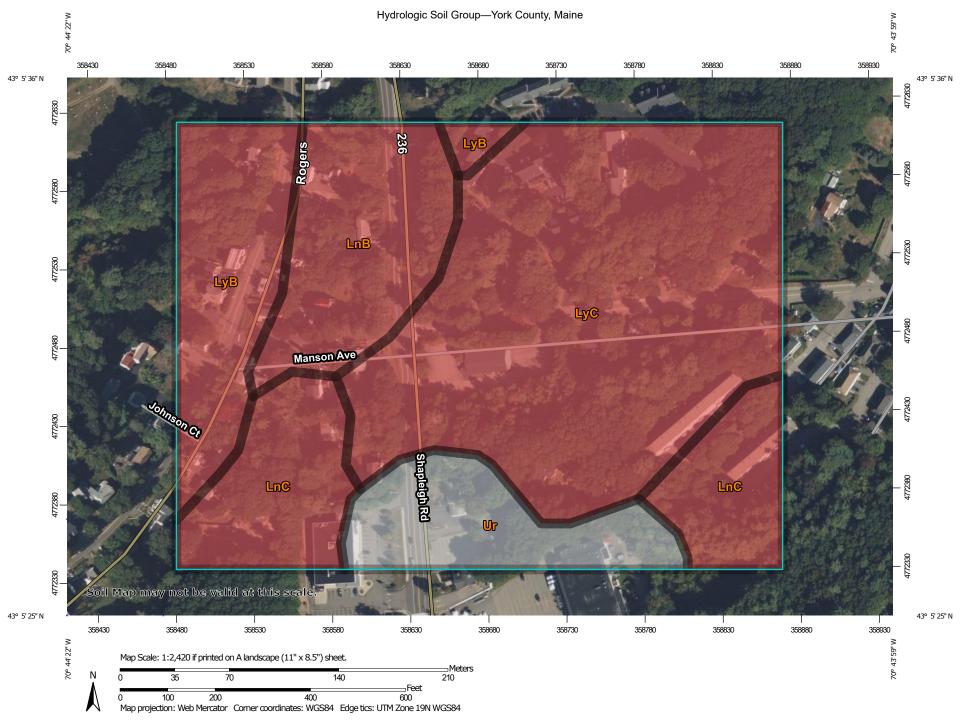
Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 0.2 min (772.4 - 772.2)

Volume	Invert	Avail.Sto	rage Storage l	Description		
#1	53.00'	27	78 cf Custom	Stage Data (Coni	c)Listed below (Recal	c)
Elevation (fee		ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
53.0	00	106	0	0	106	
54.0	00	305	197	197	311	
54.2	25	340	81	278	349	
Device	Routing	Invert	Outlet Devices			
#1	Secondary	54.00'	10.0' long x 1	0.0' breadth Broa	d-Crested Rectangu	lar Weir
#2	Primary	51.50'	Head (feet) 0. Coef. (English) 4.0" Round C	20 0.40 0.60 0.8) 2.49 2.56 2.70 Sulvert	0 1.00 1.20 1.40 1. 2.69 2.68 2.69 2.67 adwall, Ke= 0.900	60
			Inlet / Outlet In	vert= 51.50' / 51.2	25' S= 0.0071 '/' Cc= Flow Area= 0.09 sf	= 0.900

Primary OutFlow Max=0.42 cfs @ 12.14 hrs HW=53.24' TW=47.13' (Dynamic Tailwater) 2=Culvert (Barrel Controls 0.42 cfs @ 4.76 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=53.00' TW=45.40' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:20.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: York County, Maine Survey Area Data: Version 21, Aug 30, 2022 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Jun 19, 2020—Sep 20. 2020 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI		
LnB	Lyman loam, 3 to 8 percent slopes, rocky	D	3.8	13.7%		
LnC	Lyman loam, 8 to 15 percent slopes, rocky	D	4.4	16.0%		
LyB	Lyman-Rock outcrop complex, 3 to 8 percent slopes	D	3.8	13.7%		
LyC	Lyman-Rock outcrop complex, 8 to 15 percent slopes	D	12.8	46.6%		
Ur	Urban land		2.7	9.9%		
Totals for Area of Interest			27.5	100.0%		

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

Stormwater Maintenance/Inspection Plan

During the construction of parking and drainage facilities, maintenance of all erosion, sedimentation, and stormwater flow control structures and devices will be the responsibility of the contractor performing the site work. The contractor will be notified of this prior to the start of work by Fair Tide, Inc.

Fair Tide, Inc. will be responsible for the continued maintenance of the stormwater systems after final stabilization.

During construction, all erosion control devices and structures shall be checked weekly and after each "significant rainfall"**. Necessary repairs will be made to correct undermining or deterioration of the devices and/or structures.

After construction, all stormwater BMPs shall be checked annually and after major storm events. Sediment in the catch basins will be removed annually or as needed to maintain functionality of the facility.

Fair Tide, Inc shall maintain inspection logs (attached) of all stormwater and erosion control measures. The log shall reflect the dates of the inspections and describe actions taken. The log shall be kept on file for a minimum of 5 years and be made available to the Town upon request.

If invasive species are observed in any of the stormwater facilities, they shall be removed immediately. Any damage to the surface of slope adjacent to wetlands shall be repaired and stabilized as soon as possible after disturbance.

The activities listed in the inspection log will be accomplished in early spring and in late fall.

A major storm event is classified as a rainfall exceeding 2.0 inches in a 24-hr storm event.

The inspections should be completed by a qualified stormwater inspector, and maintenance logs must be provided to the Kittery CEO annually by July 1st.

** Significant rainfall is 0.5" in 24 hr

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During Construction

During construction, maintenance shall be performed routinely on all erosion and sediment control BMPs. Refer to the following list of erosion and sediment control procedures.

Dust Control

Stabilize all laydown areas and all unpaved surfaces with a base gravel or coarse gravel as soon as possible. Use traffic control to restrict speed and route.

Water Application with frequent reapplication during warm sunny days will mitigate dust. The distribution of water should not cause turbid runoff.

Sweep and Vacuum paved road surface when dry. Sweep from the centerline to the edge of the travel way. Do not sweep into a waterbody or wetland. The public roadway may also require sweeping.

Construction Entrance

The entrance/exit pad should have a length of 50 feet or more and a 12-foot minimum width (or as appropriate to contain the wheel base of construction vehicles plus 3 feet on either side). The pad should be 6 inches or more thick with angular aggregate (2-3 inch diameter). Appropriate reclaimed concrete material may be used. The aggregate should be placed over a geotextile filter to prevent the stones from pushing into the native soil. At the bottom of slopes, a diversion ridge should be provided to intercept runoff. Berms may be necessary to divert water around any exposed soil, and runoff should be directed to a sediment trap. The pad should be inspected weekly, and before and after each storm. The pad may have to be replaced if the voids become filled with sediment. Street sweeping may be necessary.

<u>Sediment Controls</u> – All sediment controls shall be checked weekly and after significant rainfalls.

Silt Fence - The fence should be anchored to resist pull-out, and be stretched tightly between stakes to prevent sagging. A 6-inch wide and 6-inch deep trench should be excavated upgradient of the fence line to key the "flap" of the fabric. The trench is backfilled and compacted. When joints are necessary, filter cloth should be spliced by wrapping end stakes together. In areas where the flap cannot be keyed properly (due to frozen ground, bedrock, stony soil, roots, near a protected natural resource, etc.), the silt fence should be anchored with aggregate, crushed stone, erosion control mix, or other material.

Erosion Control Mix Berm - It may be necessary to cut, pack down or remove tall grasses, brush or woody vegetation to avoid voids and bridges that allow the washing away of fine soil particles. The ECM berm should be a minimum of 12" high and a minimum of two feet wide. On longer or steeper slopes, the berm will need to be wider and higher. Berms composed of ECM can be reshaped when necessary.

Storm Drain Inlet Protection - An inlet protection (storm drain drop inlet or curb inlet) captures sediment before runoff enters a catch basin. It is not effective for silts and clays. Various types of off-the-shelf devices are acceptable if installed, used, and maintained as specified by the manufacturer.

Overwinter Construction – The winter construction period runs from November 1st through April 15th; however no vegetation growth should be anticipated past October 15th in southern Maine. Additional stabilization measures should be provided by November 1st for winter and spring snowmelt if a construction site is not permanently stabilized with pavement, a gravel road base, 90% mature vegetation cover, erosion control mulch, or riprap. Ideally, permanent seeding should occur 45 days before the first killing frost (different dates for different Maine locations); otherwise, overwinter mulching is necessary.



<u>Mulching</u> – Mulching is the application of an organic cover over exposed soil to protect its structure from the impact of raindrops, to reduce the potential for erosion, and to maintain soil permeability and moisture for vegetation uptake. Erosion will occur where the soil does not have firm and continuous contact with an erosion control cover. Mulch must remain until the site is permanently stabilized or revegetated. Mulching shall be performed per weather prediction, soil erodibility, season, extent of disturbance, etc. within 7 days in sensitive areas (within 100 feet of a natural resource) or within 14 to 30 days in other areas.

Hay/Straw Mulch - Hay (straw will not import weeds) mulch prevents rain drop erosion, protects new seeding from sun exposure, and maintains moisture during germination. Loose mulch is not effective in windy areas, in areas of groundwater seepage or in channels with concentrated flows. Temporary mulch should be applied to areas that will not be actively worked for more than 14 days (7 days in sensitive areas). Application rate should be 2 bales (70-90 pounds) per 1000 square feet or 1.5 to 2 tons (90-100 bales) per acre and must be evenly distributed. Provide a mulch cover to soil stockpiles. Anchoring should be provided in areas with strong wind or on slopes greater than 5%. Hay mulch should be limited to slopes flatter than 2:1 unless short (less than 10 feet), and in non-seepage areas. Another measure should be used on steeper slopes with a high runoff potential. Anchoring can be accomplished by punching, crimping the mulch into the soil or tracking with a punch-roller or a knife blade roller. Walking and punching with a spade or shovel may be practicable on very small sites. Peg and twine or netting should be installed per the manufacturer's recommendations. Non-biodegradable plastic netting should be removed after the site is revegetated. Apply additional mulch if not revegetated with 90% grass uptake.

Erosion Control Blankets - An erosion control blanket could be used in the following conditions:

- Vegetated waterways and ditches; but not in areas of groundwater seepage
- Steep slopes (15% or greater and up to 2:1)
- In protected natural resource areas
- On areas that may be slow to revegetate
- For overwinter stabilization (November 1st April 15th)

The soil surface should be finely graded and smooth for the blanket to have direct contact with the soil and to prevent undermining. Erosion control blankets perform best on loamy soils and should not be used on rocky sites or shallow soils. Seed should be sown before installing the erosion control blanket. Always unroll the blanket downhill without stretching and anchor the upslope edge in a 12 inch deep trench that is backfilled and tamped. Overlap shingle style a minimum of 12 inches at the top of each row and 4 inches at the edges of parallel rows. Anchor along the overlap with a maximum spacing of 3 feet or as required by the manufacturer.

Erosion Control Mix - Erosion control mix can be used on frozen ground, forested areas, on cut and fill slopes, and on roadside embankments. Apply a thickness of 2 inches on 3:1 slopes or less and add an additional 1/2 inch per 20 feet of slope or up to 4 inches for a 100 foot slope. On slopes greater than 3:1, 4 inches or more of material is recommended; and if slopes are greater than 60 feet long, 5 inches are needed. Erosion control mix is not recommended for slopes steeper than 1:1. The mix must be distributed evenly with a hydraulic bucket, pneumatic blower, or by hand. Other reinforcement BMPs (i.e. riprap) should be used on slopes with groundwater seepage, within drainage channels and their outlets, or in gullies.



<u>Slopes</u> – To be effective, slope stabilization and reinforcement should be adapted to the soil type, angle and length of the slope, presence of surface or groundwater, depth to bedrock, etc. Consultation with a civil engineer is advised for slopes that are over six feet, steeper than 1.5:1 grade, on unstable soils, with groundwater seeps, or where a structure is located near the top of the bank. A proper permit and design may be required for an embankment repair near a waterbody.

Cuts and Fills - Erosion potentials on fill slopes depend upon the depth of the fill, steepness, watershed size and presence of water. Fill slopes are more unstable than cut slopes from being disturbed or if lacking fines for proper compaction. In a wet area, gravel fill is preferred; but is at risk of being unstable. Terracing prevents surface runoff and promotes vegetation establishment by retaining moisture. The time between initial exposure and final stabilization should be minimized to prevent soil loss. Divert clean water away from the area and disperse to an undisturbed buffer or swale. For a fill slope, the native area should be cleared, grubbed, and scarified to a 3-inch depth. When working in below freezing temperatures, the ground should be scarified immediately before adding fill. The fill should be free of brush, rocks, or roots, and should not include frozen, soft or mucky material. The fill should be placed and compacted in 8-inch lifts to reduce lenses of loose soil. When filling or cutting a long slope (greater than 20 feet), benches (or terraces) should be provided to direct runoff away from the slope. The number of benches should be based upon the erodibility of the soil, steepness of the slope, and groundwater seeps. Mulch any soil exposed for longer than 7 days and with seed if ready for revegetation. Rill or gully erosion should be repaired immediately. Use winter stabilization practices if the construction is stopped for the winter months.

Geotextiles - Geotextiles should be placed with 12 inch overlaps and keyed 6 to 12 inches at the top and bottom of the area. Avoid using damaged cloth. Woven Geotextiles are mostly used for soil reinforcement beneath sharp, angular aggregates if dropped more than 5 feet; and where the cover will be more than 10 feet thick. It may be used for seepage management if the fabric's openings are smaller than the soil gradation. A woven filter fabric is usually used in a road base to provide bearing capacity and linear strength over soft subsoil. Nonwoven Geotextiles will retain more fine particles than woven geotextiles; and may allow water seepage without clogging. Nonwoven geotextiles have a rough surface that will bond soil layers and resists sliding along the planes of contact.

Riprap Protection - Riprap is used for structural support when a slope cannot be vegetated due to length or steepness of the slope, groundwater or surface water seepage, poor soil conditions, flowing water, etc. On a long slope, larger stones are used and placed at the bottom of the embankment and gradually grading down to smaller stones toward the top. A riprap stabilization project is composed of three sections:

- The surface armor layer of rough, angular rocks.
- The filter layer (a sand and gravel layer and/or a geotextile fabric) that supports the stones against settlement, allows groundwater to drain through the structure, and prevents the soil beneath from being washed through the riprap layer.
- The toe protection that reinforce the slope and prevents movement of the riprap. It is usually anchored in a trench at the toe of the slope.

<u>Pipe Outlet Protection</u> – Pipe outlet protection is the armor and/or plunge pool at the outlet of a culvert that prevents scour or turbulence, and will dissipate the flow energy from the pipe to the channel. For channels with a continuous flow, the culvert should be imbedded one quarter (1/4) its diameter to prevent a 'hanging' condition (drop from the pipe outlet to channel).



Post Construction

Sweeping

Paved surfaces shall be swept or vacuumed at least annually in the Spring to remove all Winter sand, and periodically during the year on an as-needed basis to minimize transportation of sediment during rainfall events. Applicable to: All parking lots and travel ways on site.

Roadways and Parking Surfaces				
		Fall	After a	Every
	Spring	or	Major	2-5
		Yearly	Storm	Years
Clear accumulated winter sand in parking lots and along roadways	X			
Sweep pavement to remove sediment	X			
Ensure that stormwater is not impeded by accumulations of material or				
false ditches in the shoulder	Λ			

Vegetated Areas

All areas of maintained lawn are to be inspected regularly for signs of erosions and channelization. Areas where erosion is occurring or areas of sparse growth shall be replanted and stabilized. Channelized flows from the eroded land shall be diverted to buffers or other areas able to withstand the high sediment load in the erosive runoff. Applicable to: Lawn areas receiving/conveying flows in any storm event.

Vegetated Areas				
		Fall	After a	Every
	Spring	or	Major	2-5
		Yearly	Storm	Years
Inspect all slopes and embankments	X		X	
Replant bare areas or areas with sparse growth	X		X	
Armor areas with fill erosions with an appropriate lining or divert the erosive flows to on-site areas able to withstand concentrated flows, such as areas of well-established vegetation or previously installed armoring materials	X		X	

Ditches, Swales and Culverts

Open swales and ditches need to be inspected on a monthly basis or after a major rainfall event to assure that debris or sediments do not reduce the effectiveness of the system. Debris needs to be removed at that time. Any sign of erosion or blockage shall be immediately repaired to assure a vigorous growth of vegetation for the stability of the structure and proper functioning.

Vegetated ditches should be mowed at least monthly during the growing season. Larger brush or trees must not be allowed to become established in the channel. Any areas where the vegetation fails will be subject to erosion and should be repaired and revegetated.

If sediment in culverts or piped drainage systems exceeds 20% of the diameter of the pipe, it should be removed. This may be accomplished by hydraulic flushing or any mechanical means; however, care should be taken to not flush the sediments into the retention/detention pond as it will reduce the pond's capacity and hasten the time when it must be cleaned. All pipes should be inspected on an annual basis.

Stormwater Channels					
		Fall	After a	Every	
	Spring	or	Major	2-5	
		Yearly	Storm	Years	
Inspect ditches, swales and other open stormwater channels	X	X	X		
Remove any obstructions and accumulated sediments or debris	X	X			
Control vegetated growth and woody vegetation		X			
Repair any erosion of the ditch lining		X			
Mow vegetated ditches		X			
Remove woody vegetation growing through riprap		X			
Repair any slumping side slopes	X	X			
Replace riprap where underlying filter fabric or underdrain gravel is showing or where stones have dislodge	X			X	

Catch Basins/Manholes

All catch basins, and any other field inlets throughout the collection system, need to be inspected on a monthly basis to assure that the inlet entry point is clear of debris and will allow the intended water entry. These will be cleared, if necessary on a yearly basis or when sediment reaches two thirds of total volume. Catch basins and manholes need to be vacuumed and cleaned of all accumulated sediment. This work must be done by a vacuum truck. The removed material must be disposed of in accordance with the Maine Solid Waste Disposal Rules.

Catch Basin/Manhole Systems				
		Fall	After a	Every
	Spring	or	Major	2-5
		Yearly	Storm	Years
Remove and legally dispose of accumulated sediments and debris from the				
bottom of the basin, inlet grates, inflow channels to the basin, and pipes	X	X		
between basins.				
Remove floating debris and floating oils (using oil absorptive pads) from	v	v		
any trap designed for such	Λ	Λ		



Stormwater Maintenance

Fair Tide, Inc.

Post Construction Maintenance Checklist

This log is intended to accompany the Stormwater Management Facilities Maintenance Plan for Fair Tide, Inc's Site Plan. The following items shall be checked, cleaned and maintained on regular basis as specified in the Maintenance Plan and as described in the table below. This log shall be kept on file for a minimum of five years and shall be available for review by the Town upon request. Qualified personnel familiar with drainage systems and soils shall perform all inspections.

Item	Maintenance Required & Frequency	Date Completed	Maintenance Personnel	Comments
Sweeping of Paved areas	Sweep annually in the Spring.			
Ditches, Swales and Culverts	Inspect after major rainfall event. Repair erosion or drainage immediately. Remove sediment if filtration times become greater than 12 hours. Clean culverts when sediment occupies more than 20% of pipe diameter.			
Vegetated Areas	Inspected regularly for signs of erosions and channelization. Areas where erosion is occurring or areas of sparse growth shall be replanted and stabilized.			
Catch Basins/ Manhole	Clean sumps with vacuum pump annually or when sediment occupies more than two thirds of the sump capacity.			

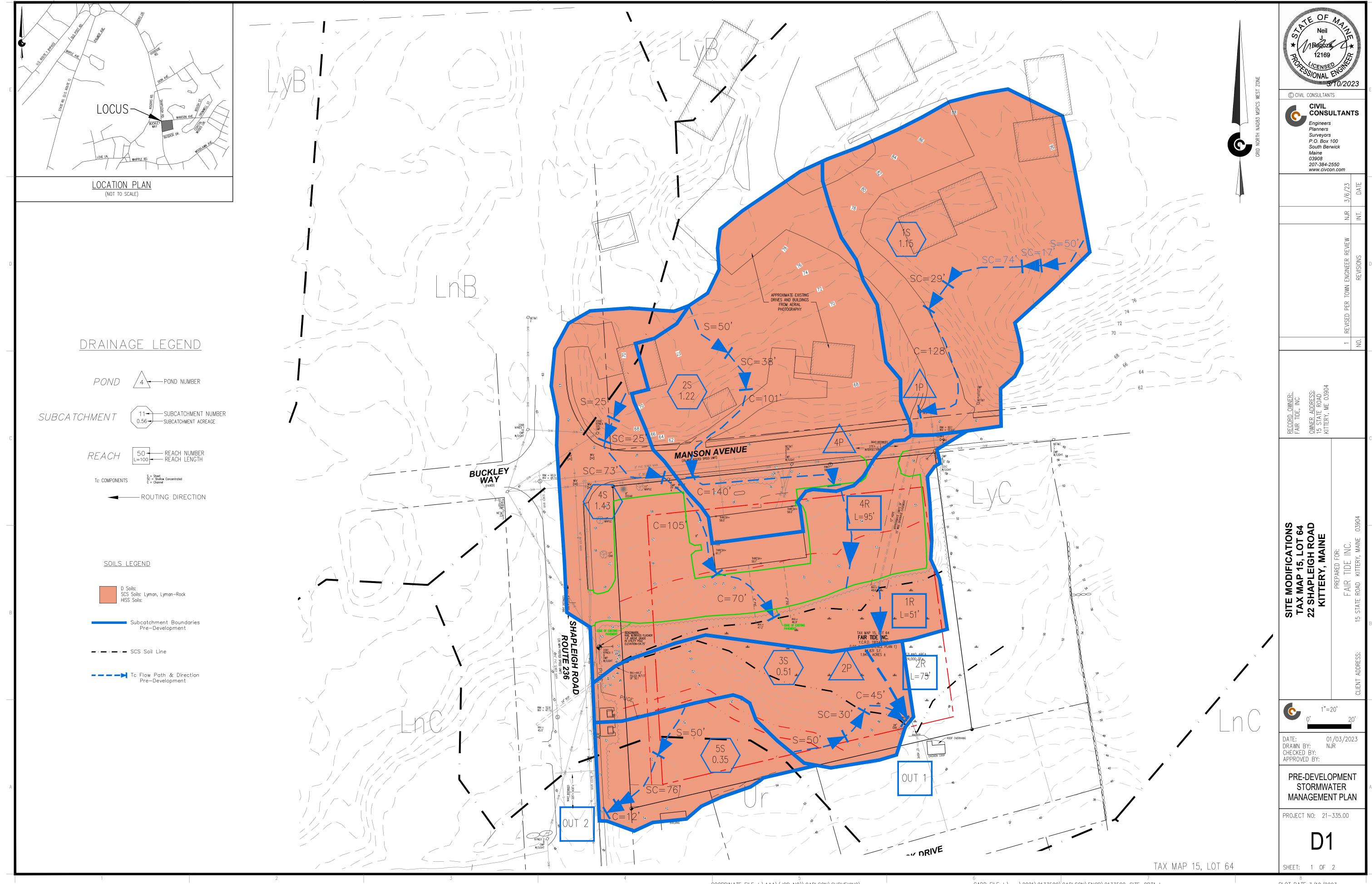
Stormwater Management System

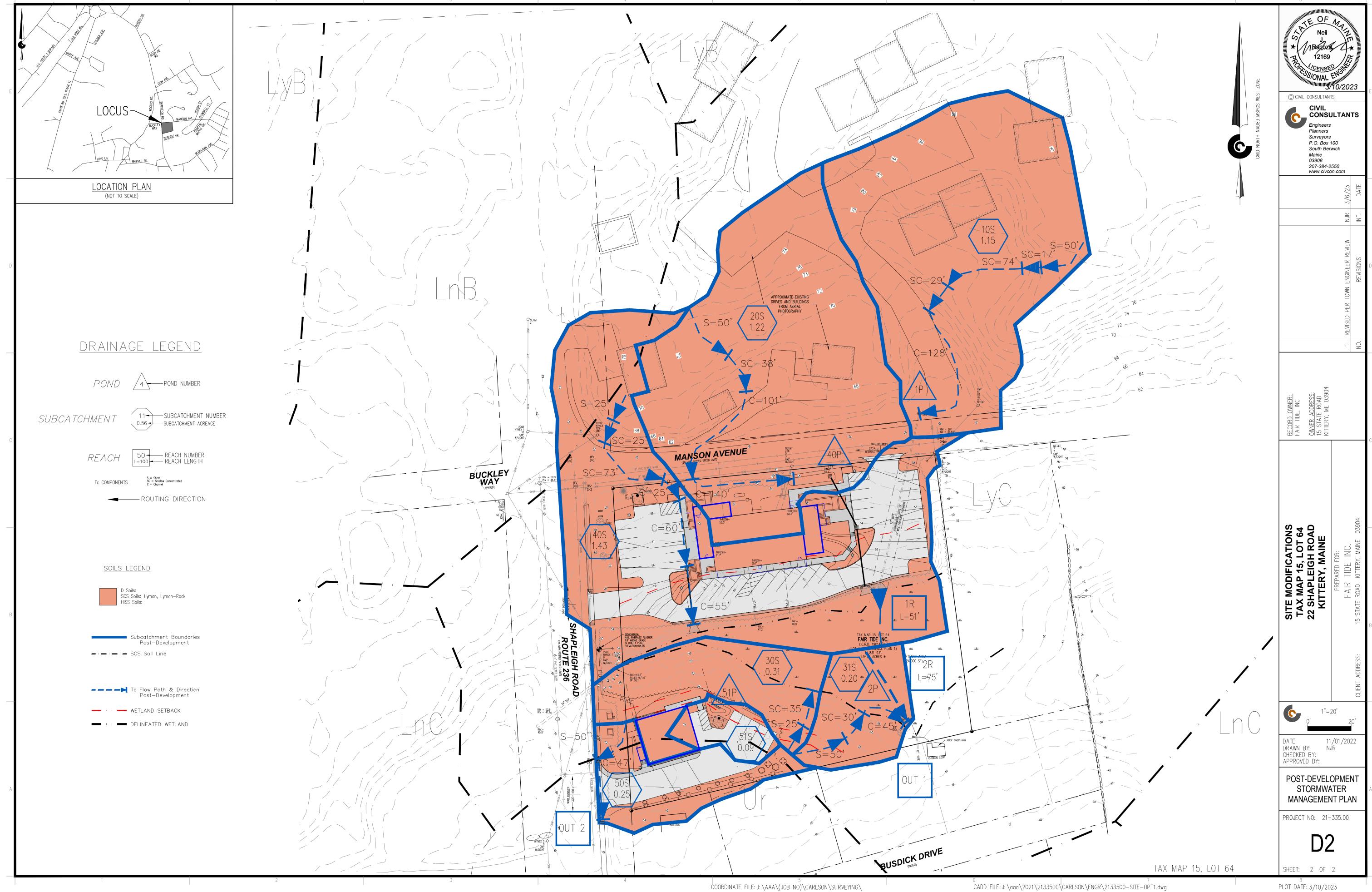
Fair Tide, Inc.

Inspection & Maintenance Log

BMP/System Component	Date Inspected	Inspector	Cleaning/Repair Needed (List Items/Comments)	Date of Cleaning/Repair	Performed By

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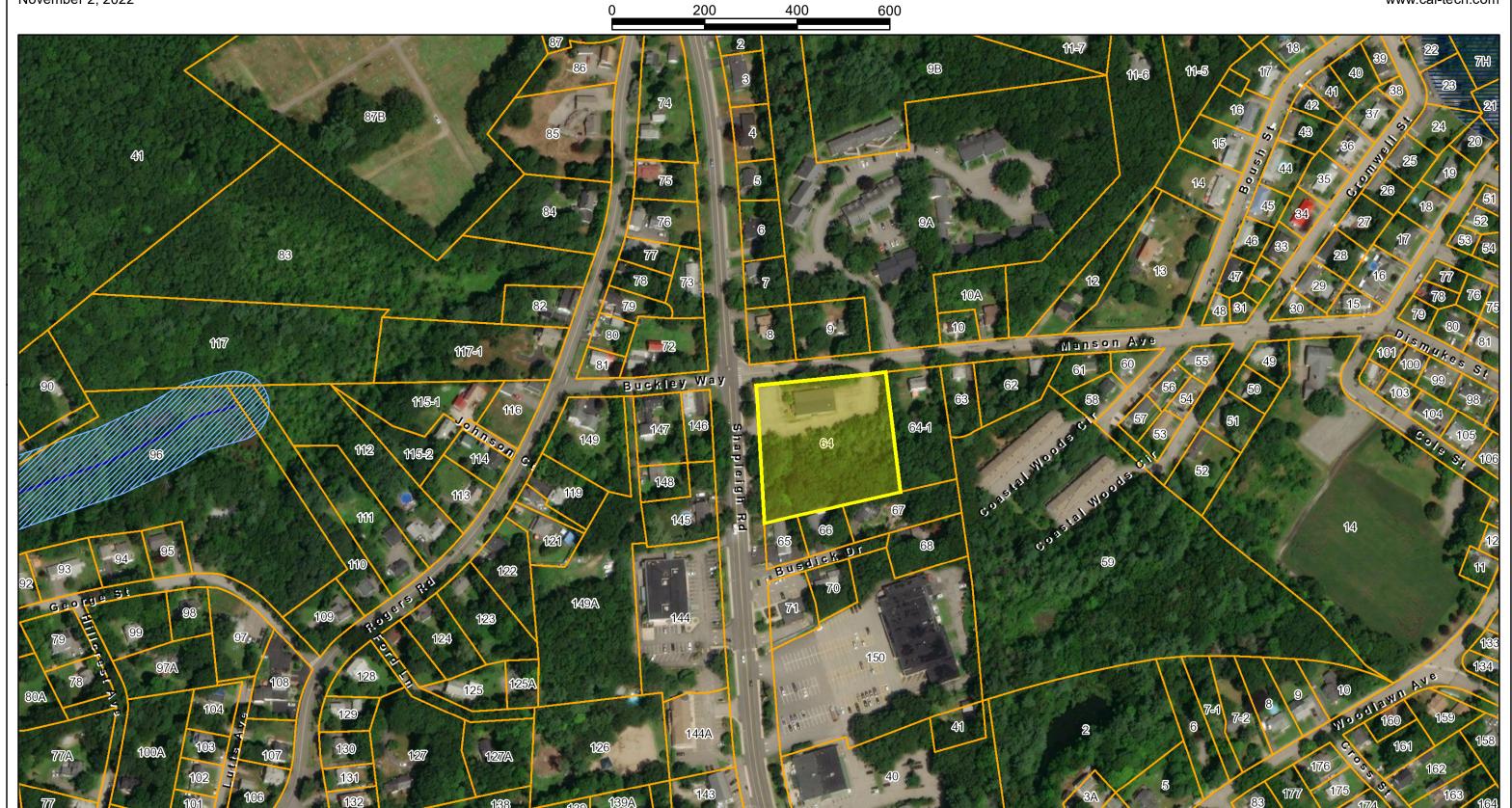
22 Shapleigh Road - Vicinity Map

Kittery, ME

CAI Technologies

1 inch = 200 Feet November 2, 2022 200

www.cai-tech.com



RE: Final Site Plan Review Notification 22 Shapleigh Road Kittery, ME 03904

This letter is to inform you that a Final Site plan Review application will be filed with the Planning Department for a redevelopment project at 22 Shapleigh Road (Tax Map 15, Lot 64). Work is being done for Fair Tide Inc located at 15 State Road, Kittery, ME. Which proposes work abutting your property. This project was granted preliminary approval on February 28, 2023.

The project consists of the redevelopment of the existing site and building to create a community service space called Mainspring. You can find more information at the following website on the services to be provided. (https://www.mainspringcollective.org/). The project will also construct a residential building that will house 6 units of affordable housing.

The project will require a Major Site Plan review to redevelop the existing building, parking areas and new residential construction into what is proposed for the property.

Detailed information will be presented at the Planning Board meeting that indicates use and how this project will benefit the community. Information is available to review at the Town Hall or at Civil Consultants.

Should you have any questions or comments, please call at your convenience.

Respectfully yours, CIVIL CONSULTANTS

Anden

Geoffrey R. Aleva, P.E.,

President

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LIST OF ABUTTERS

22 Shapleigh Road Kittery, ME Map 15 Lot 64 April 2023

MAP	LOT	NAME & MAILING ADDRESS
15	64 (locus)	Fair Tide Inc 15 State Road Kittery Me 03904
15	65	Brittany Horst Nathan Horst 16 Shapleigh Road Kittery ME 03904
15	66	Matthew Boyle 5 Busdick Drive Kittery ME 03904
15	67	Julia O'Connell Trustee The Blue Heron Rev. Trust of 2012 9 Busdick Drive Kittery ME 03904
15	64-1	Stephen Erickson 616 E Devonhurst Lane Ponte Vedre, FL 32081
15	8	Gabrielle Bertrand Douglas Bertrand 24 Shapleigh Road Kittery ME 03904
15	9	Judith Durnin PO Box 833 Kittery ME 03904
15	9A	Berry Park Housing Corp C/O Avesta Housing Development Corp 307 Cumberland Avenue Portland, ME 04101
9	146	Jay Wilgus Emily Flinkstrom 12 Buckley Way Kittery ME 03904
9	145	Clifford Family IRR R.E. Trust Matthew Clifford TR 79 York Woods Road South Berwick, ME 03908